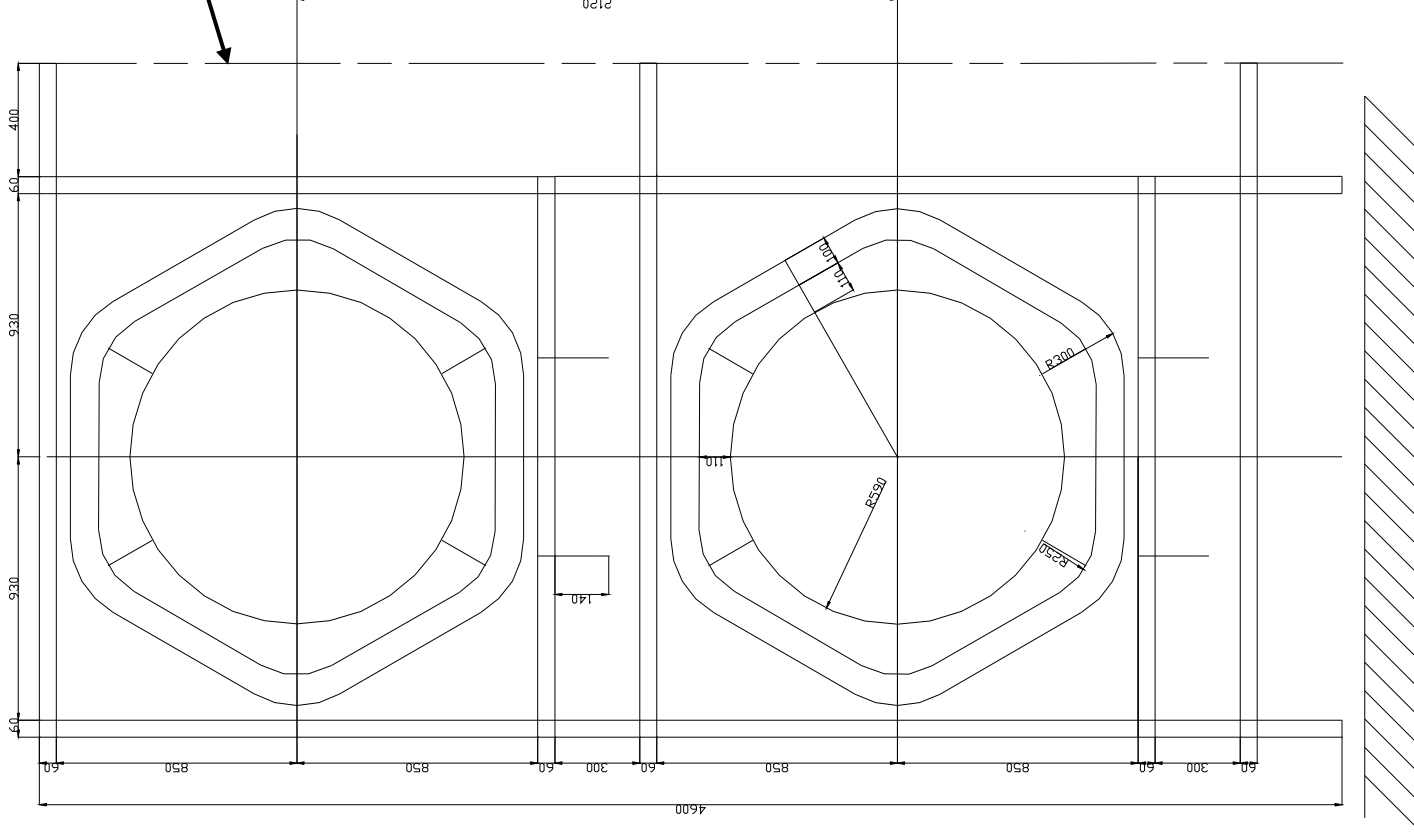


Four horns support system – static analysis, new results

B.Szybiński, Cracow University of Technology

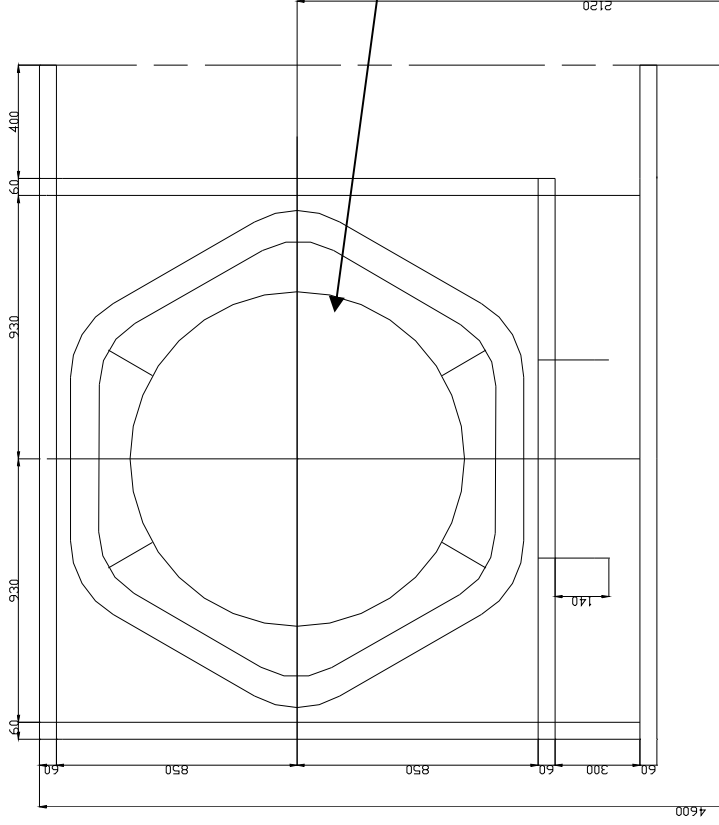


Axe of symmetry

1. Total height: $H = 4600$ [mm]
2. Distance between horn centres: $L = 2120$
3. Distance between frames: $B = 2 \times 400$ [mm]
4. Width of the cell for single horn: $C = 2 \times 930$ [mm]
5. Height of the cell for single horn: $J = 2 \times 850$ [mm]

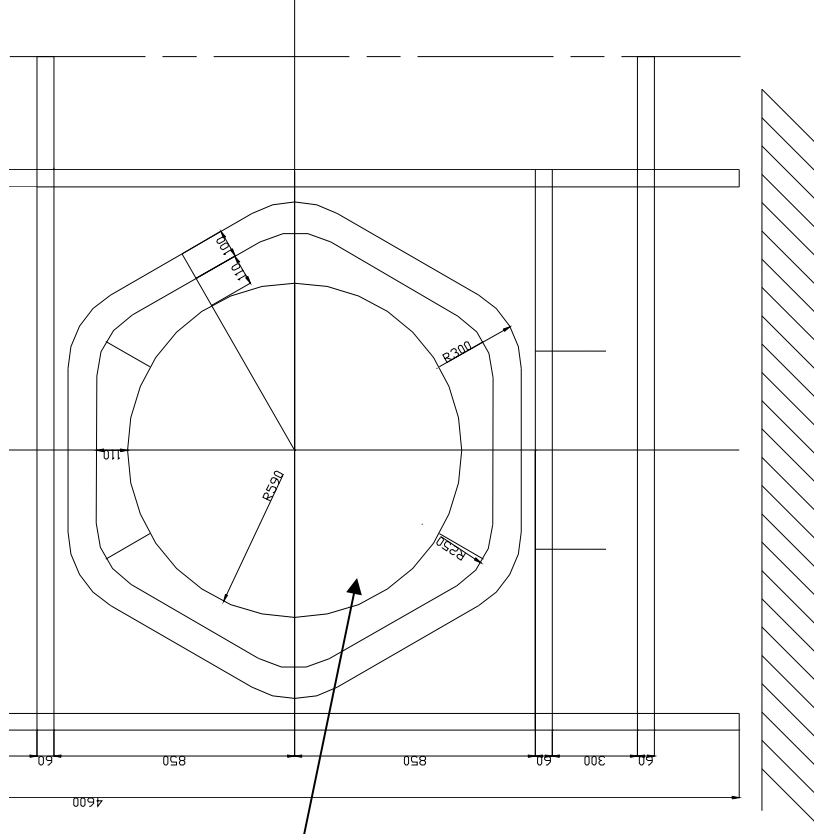
Symmetric $\frac{1}{2}$ of four
horns supporting
system –front view

Symmetric $\frac{1}{2}$ of four
horns supporting
system –front view



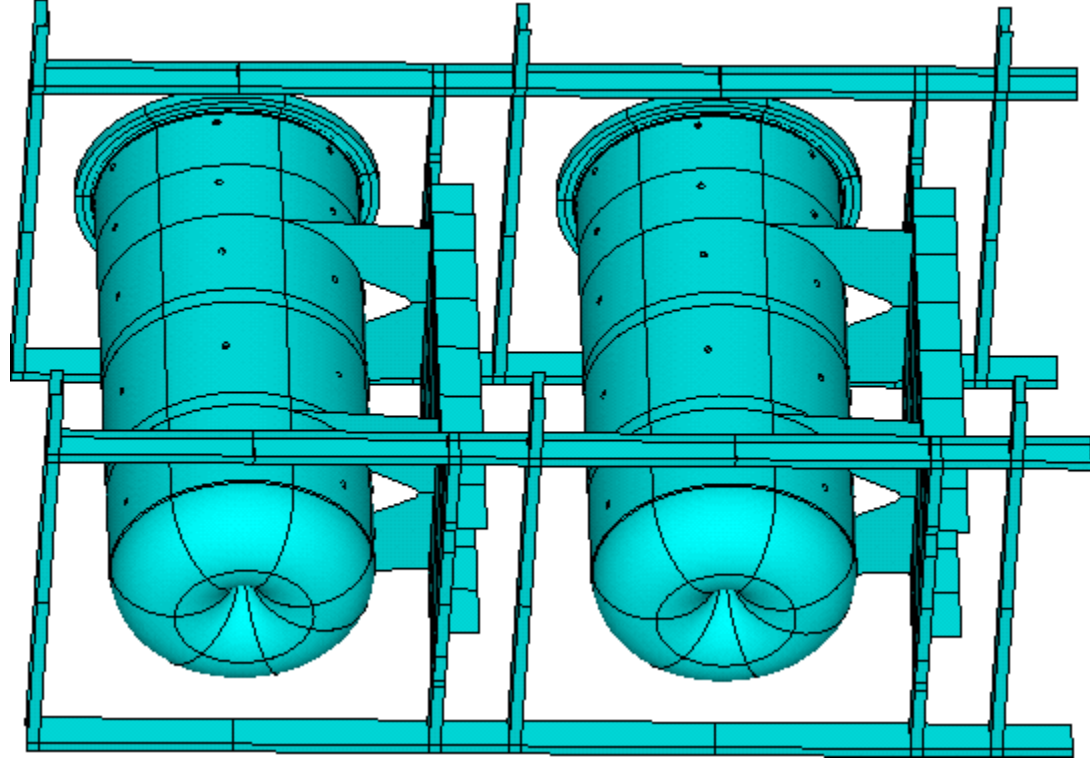
Upper left horn

Bottom left horn

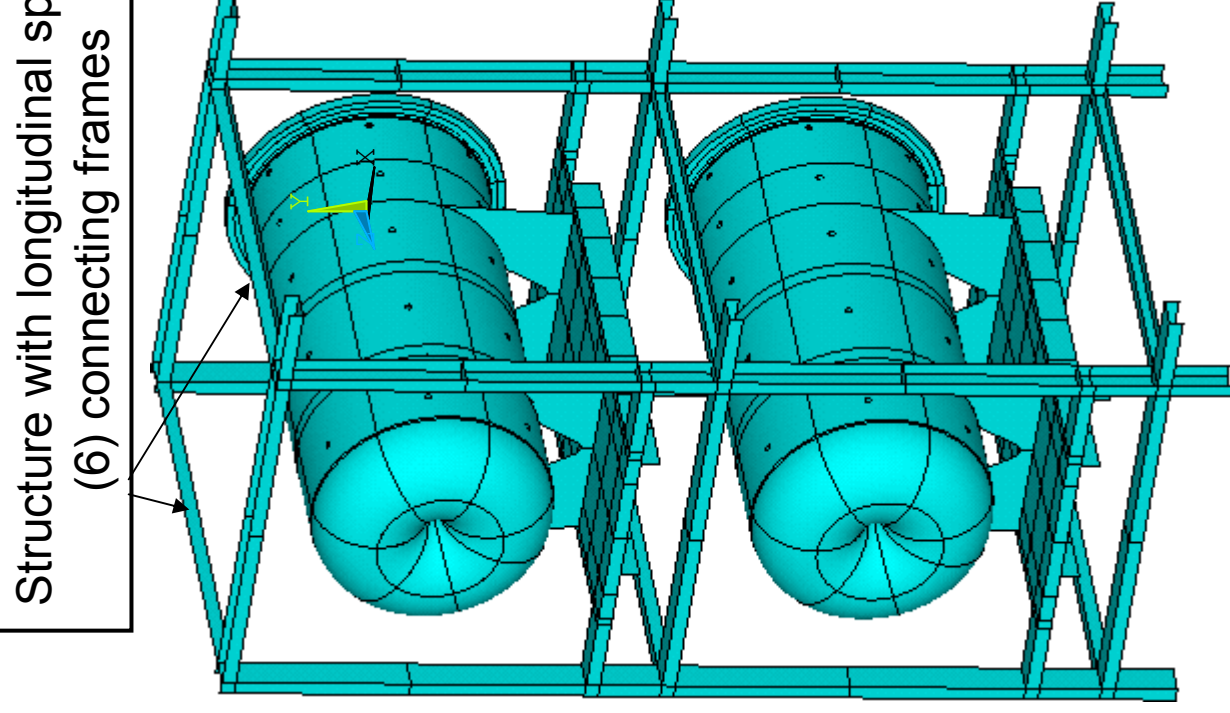


1. Distance between the bottom line of channel section for upper horn and top surface of channel section for lower horn : $D = 300 \text{ [mm]}$
2. Width of the channel section $H1 = 65 \text{ [mm]}$

Symmetric half with ribs under horizontal horn supporting plates

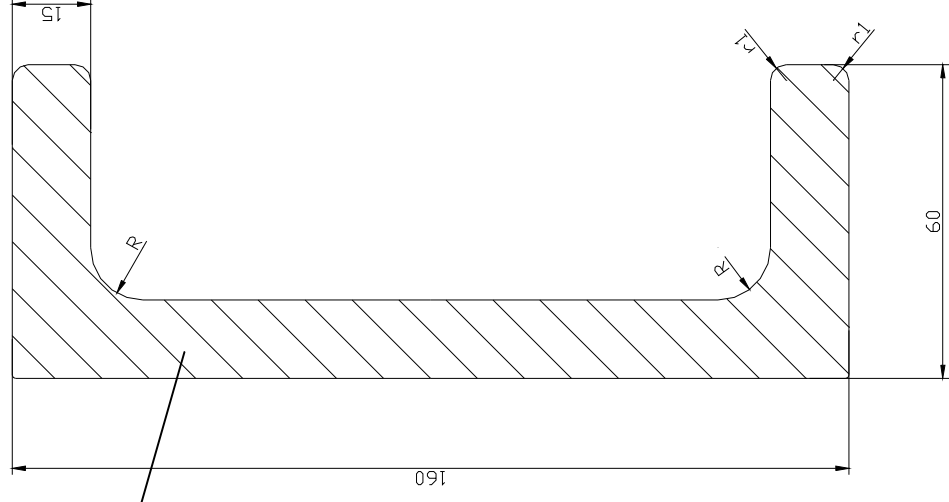
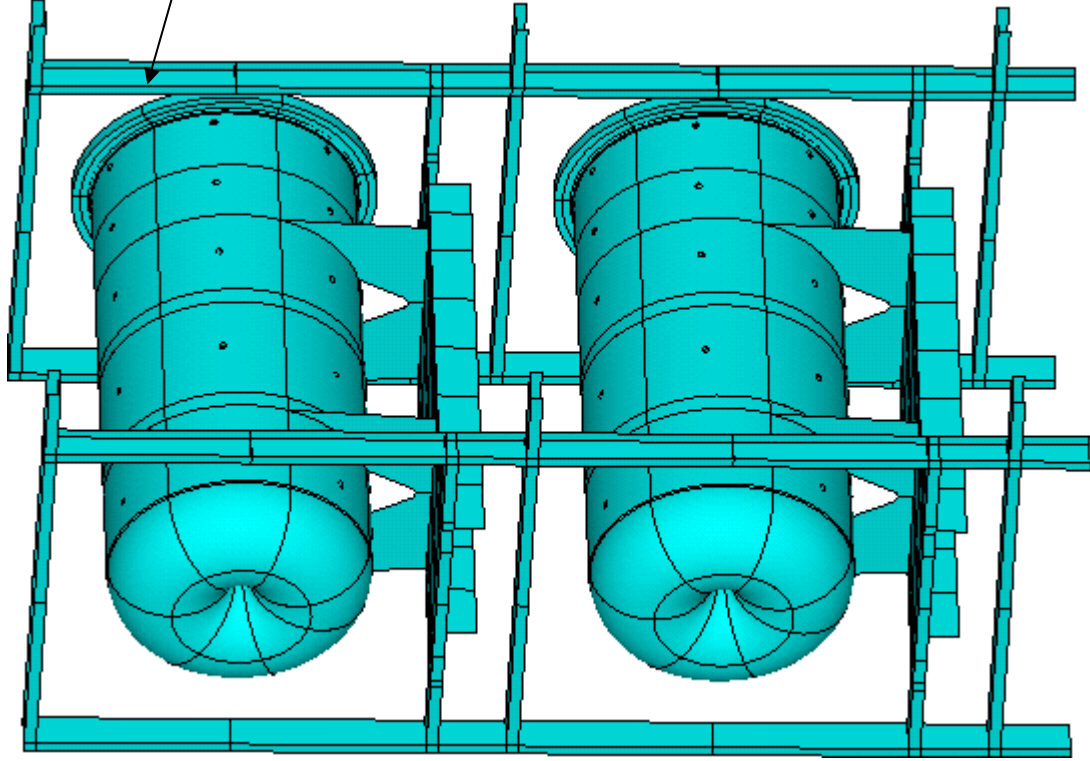


Structure without longitudinal spans
connecting frames



Structure with longitudinal spans
(6) connecting frames

Standard aluminium channel
section for frame structure



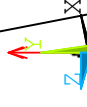
Top isometric
view

Horizontal supporting plate
with $t_h = 20$ [mm]

Vertical saddle supports with
 $t_s = 12$ [mm]

Ribs with thickness $t_r = 15$ [mm]

Bottom isom.
view

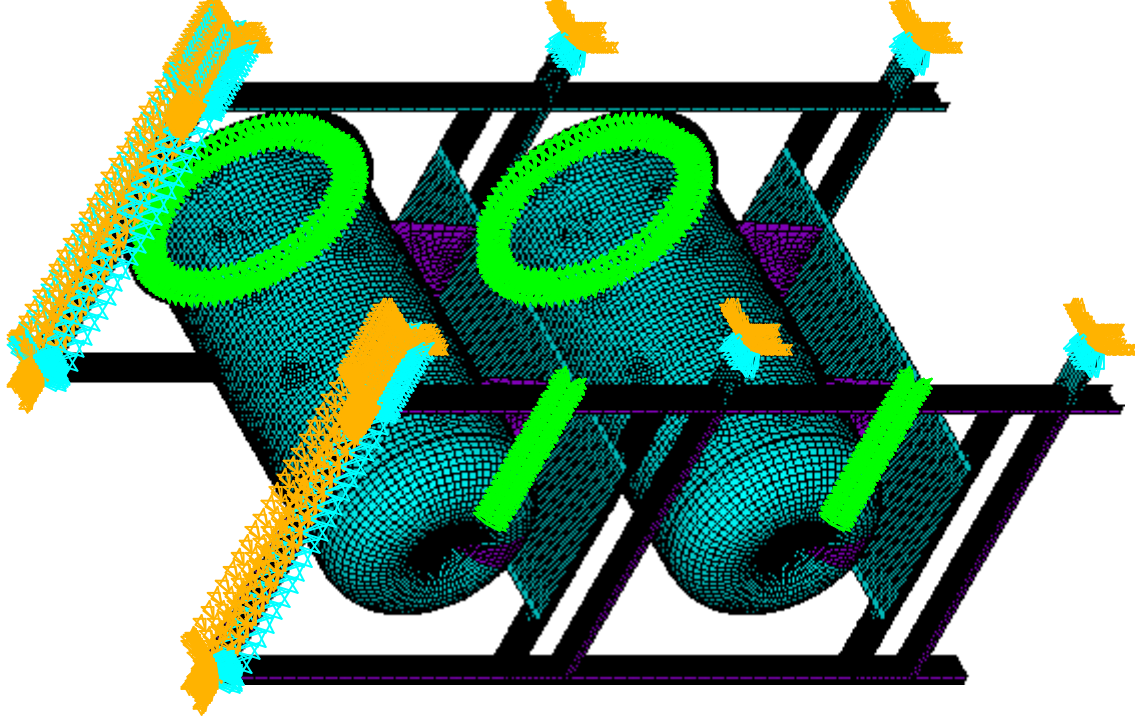
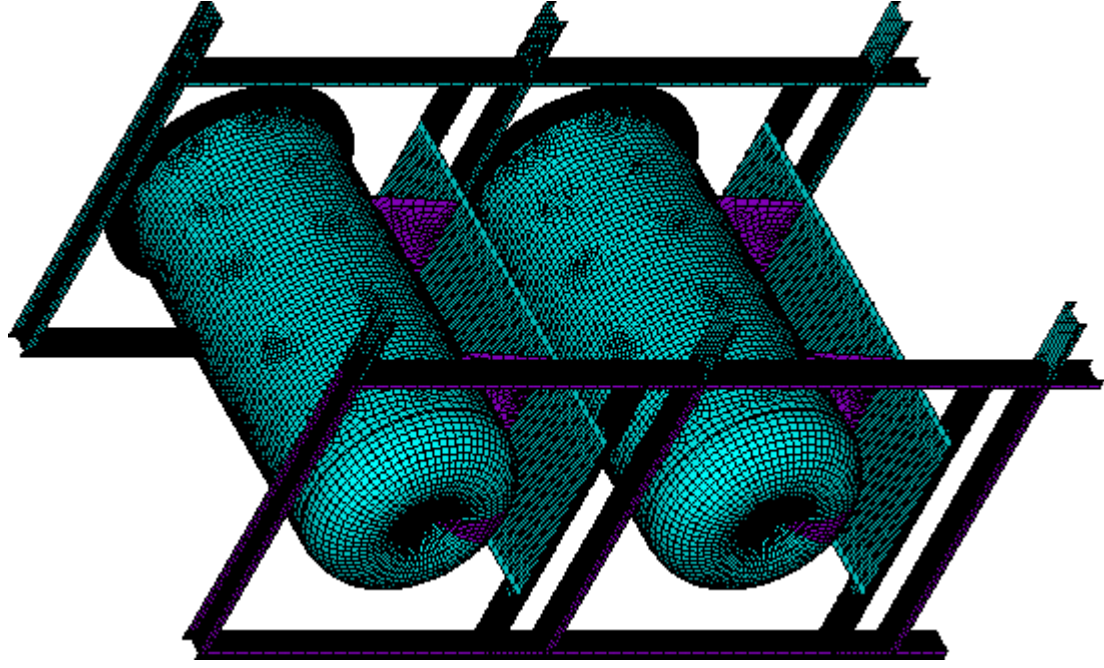


Symmetric $\frac{1}{2}$ of structure with
ribs, without longitudinal spans,
supported on the top,

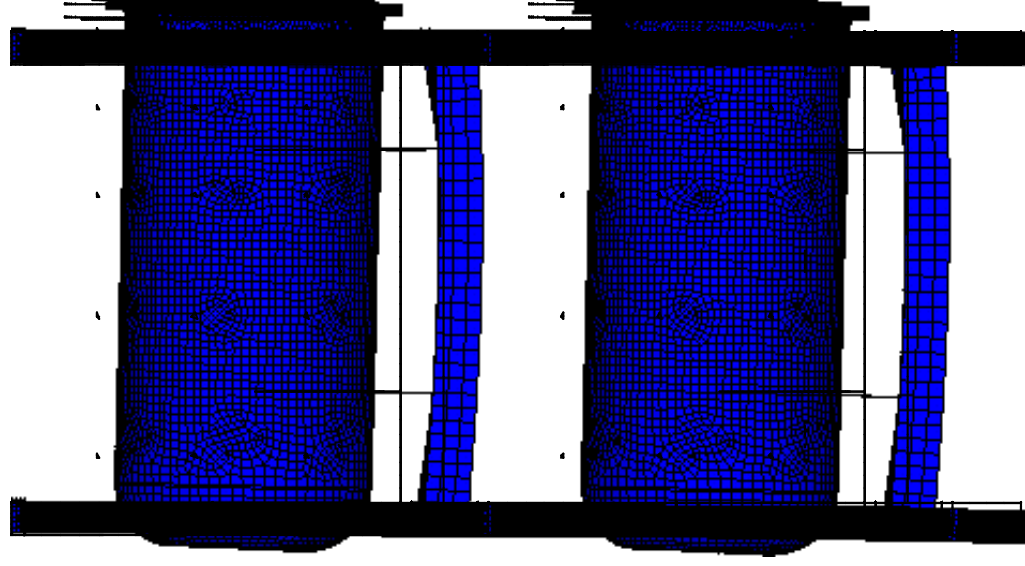
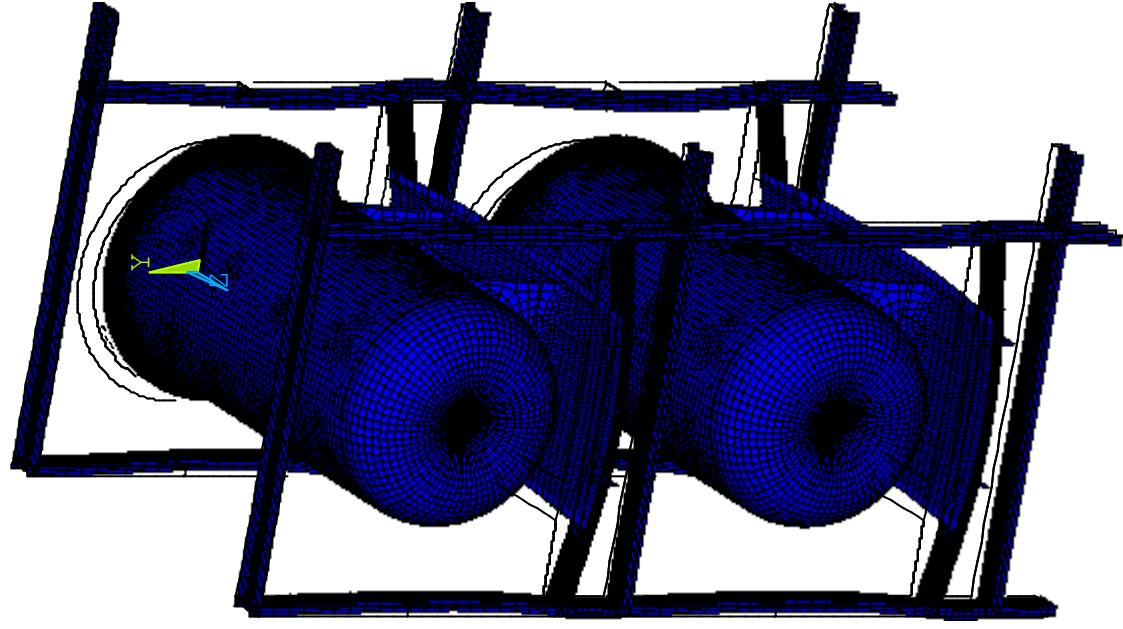
Slides: 8 – 18 (load: deadweight)

Slides: 8 – 26 (load: deadweight
+ hydrostatic pressure)

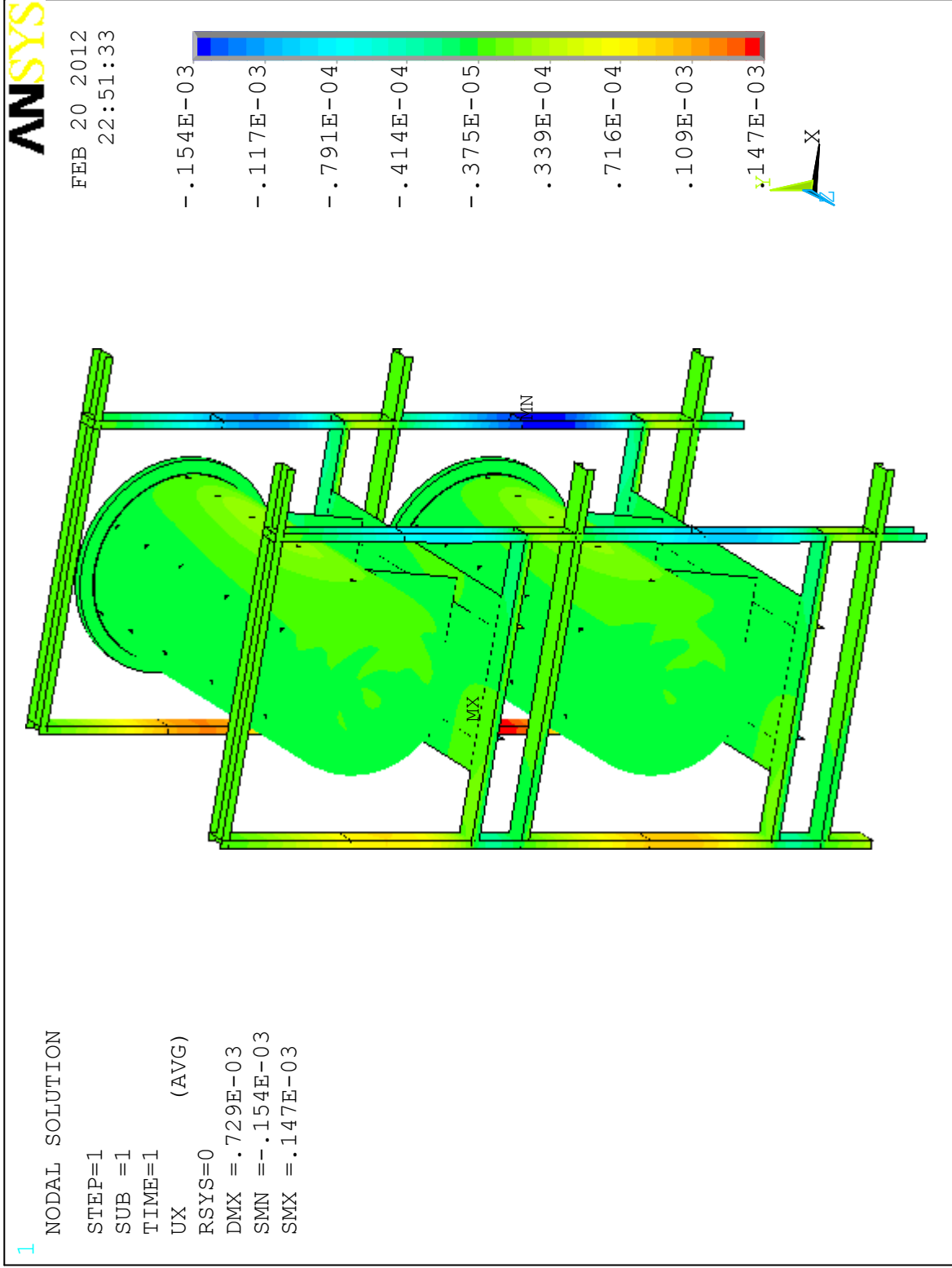
Slides: 27 – 30 results for str. without ribs under supporting plate, only
deadweight introduced



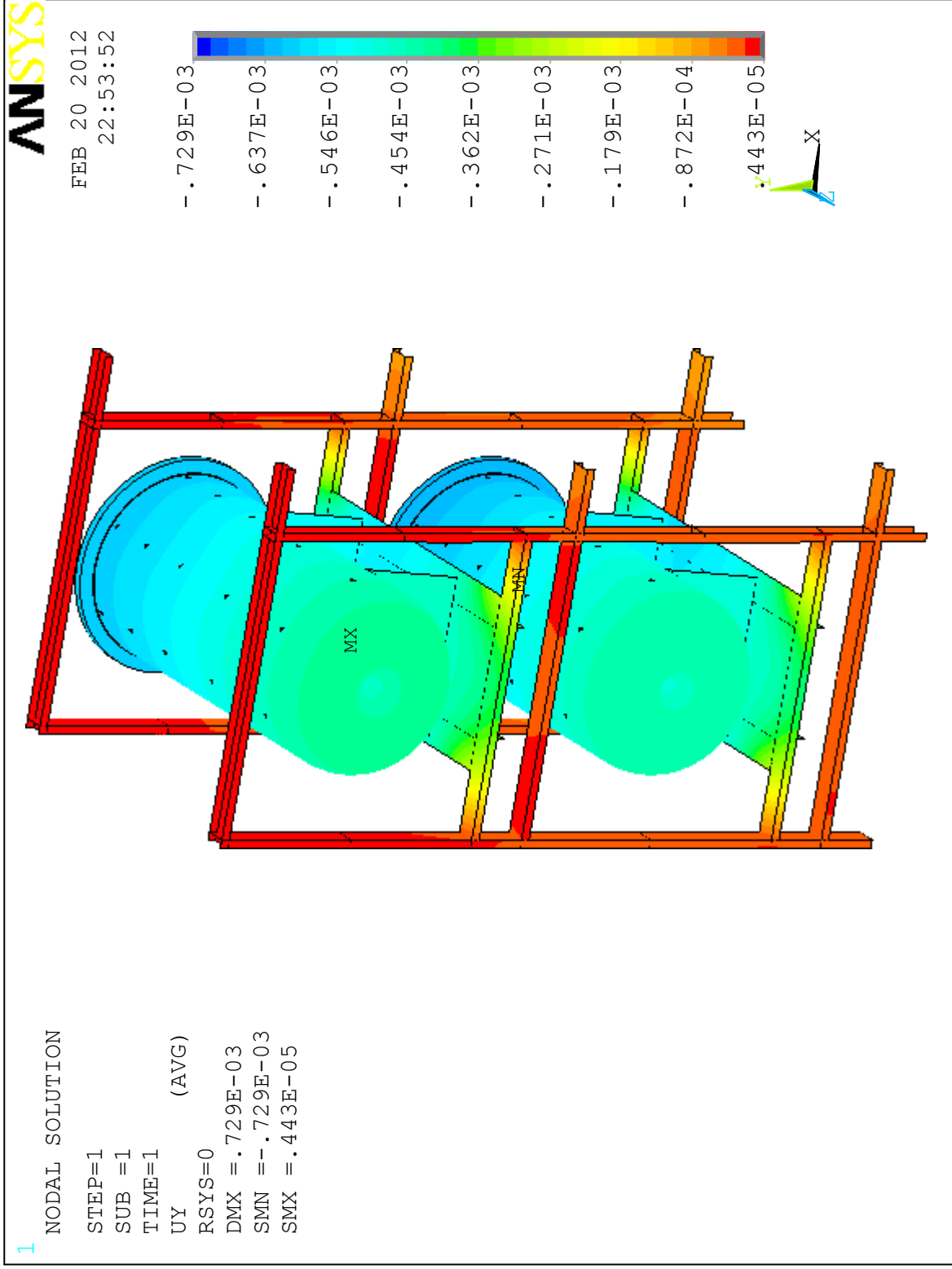
Isometric view of mesh and mesh with boundary conditions introduced



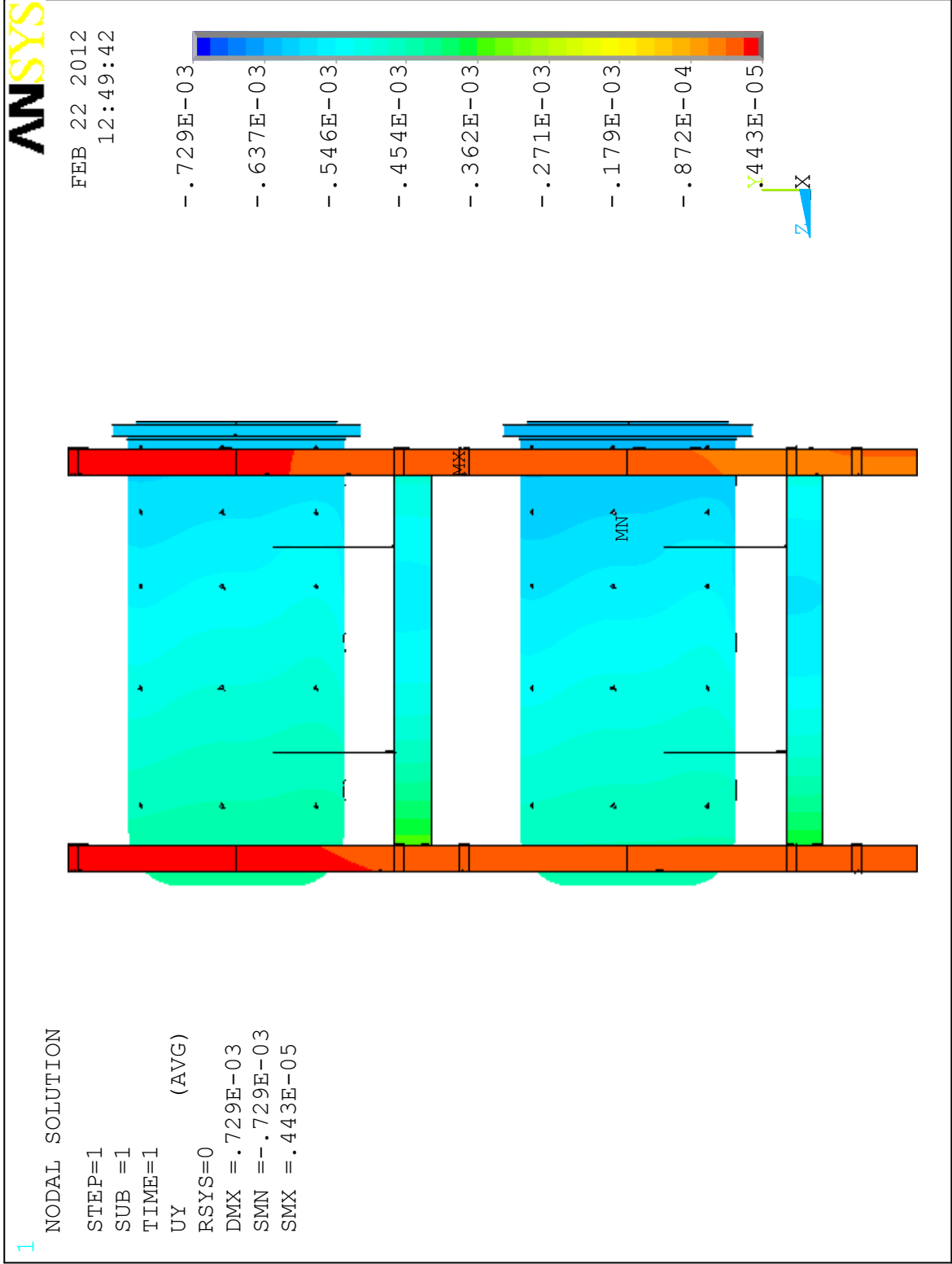
Deformation of structure under deadweight – not to scale drawing



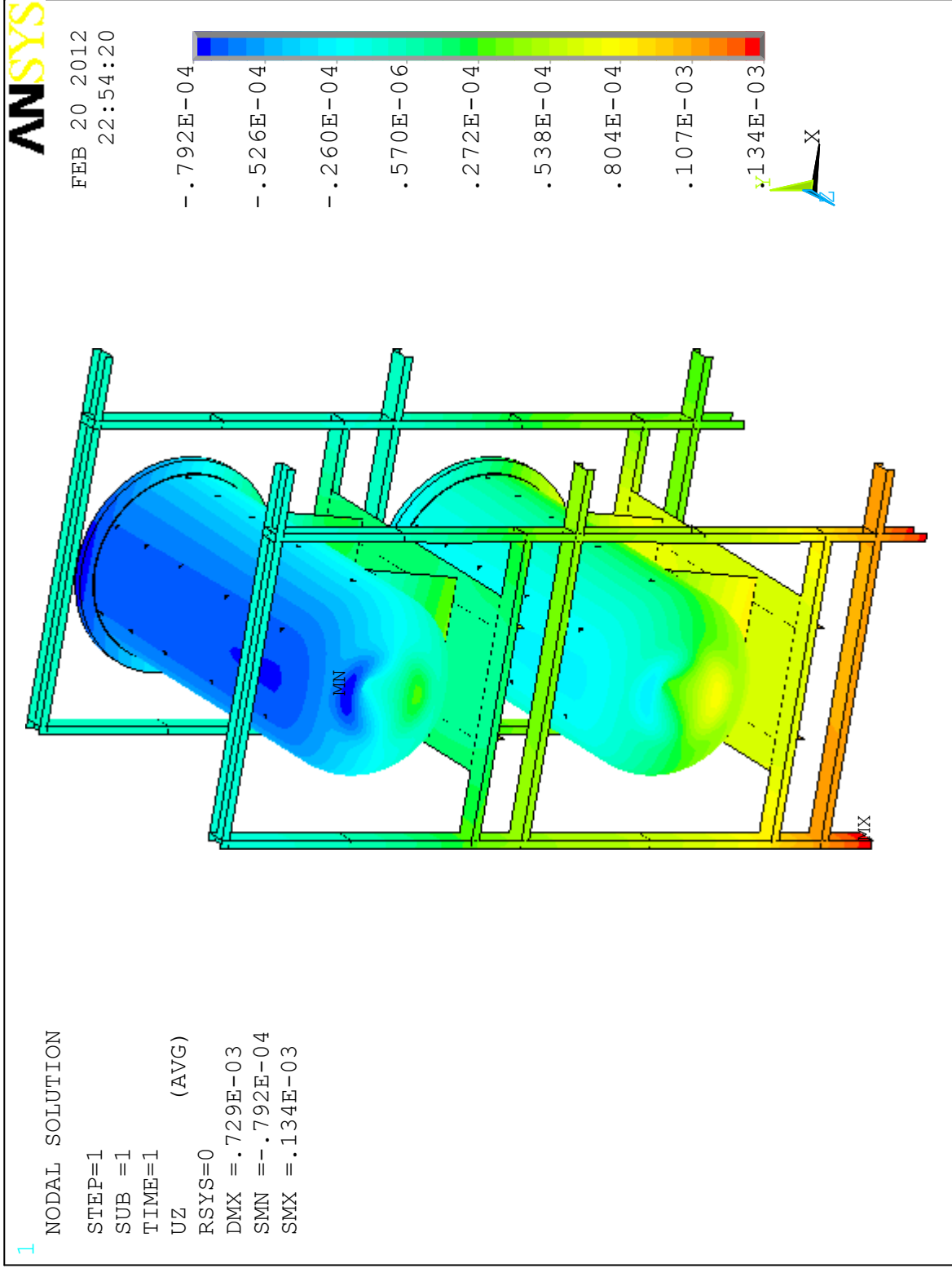
U_x displacement in [m]



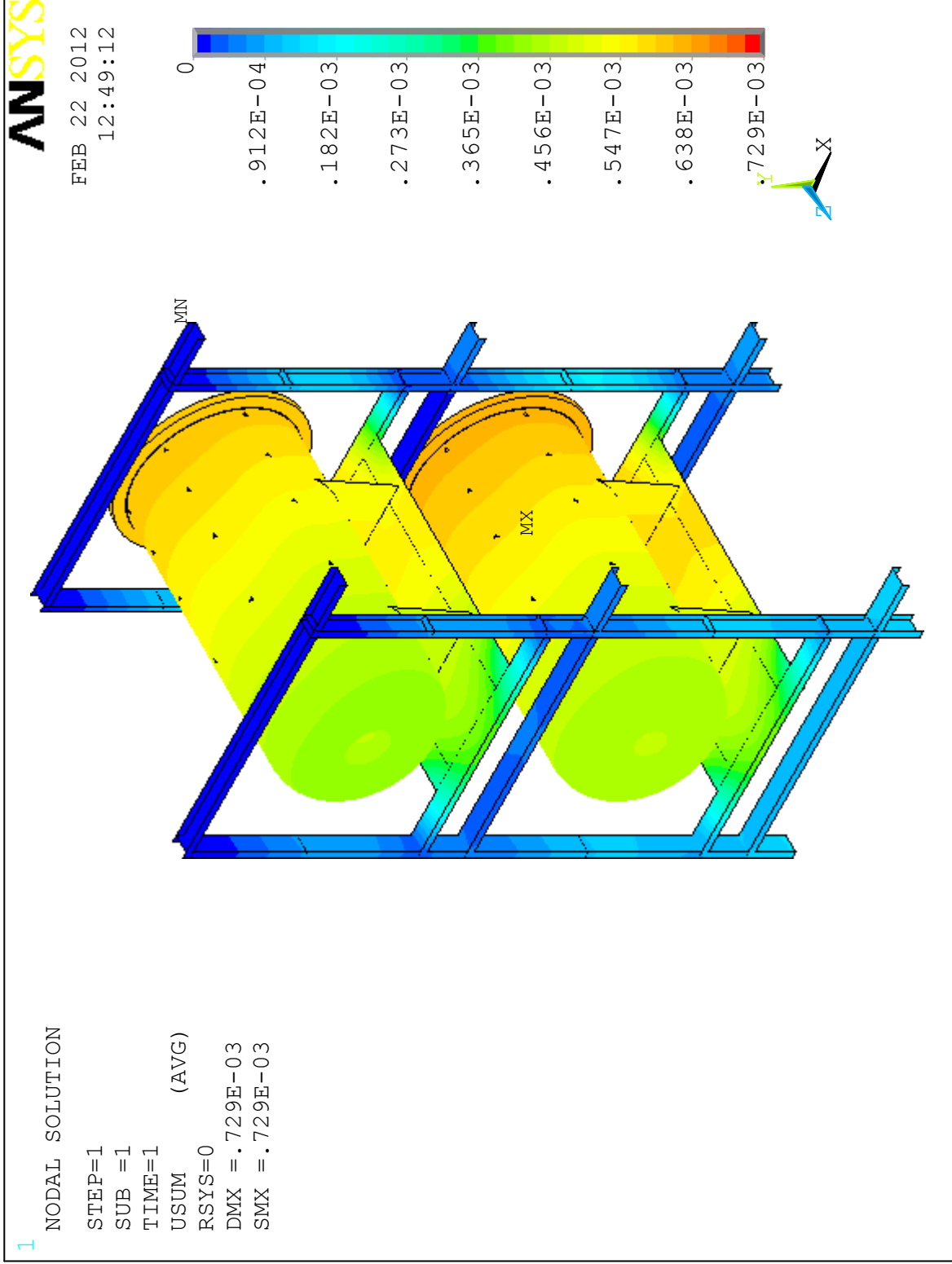
U_y displacement in [m]



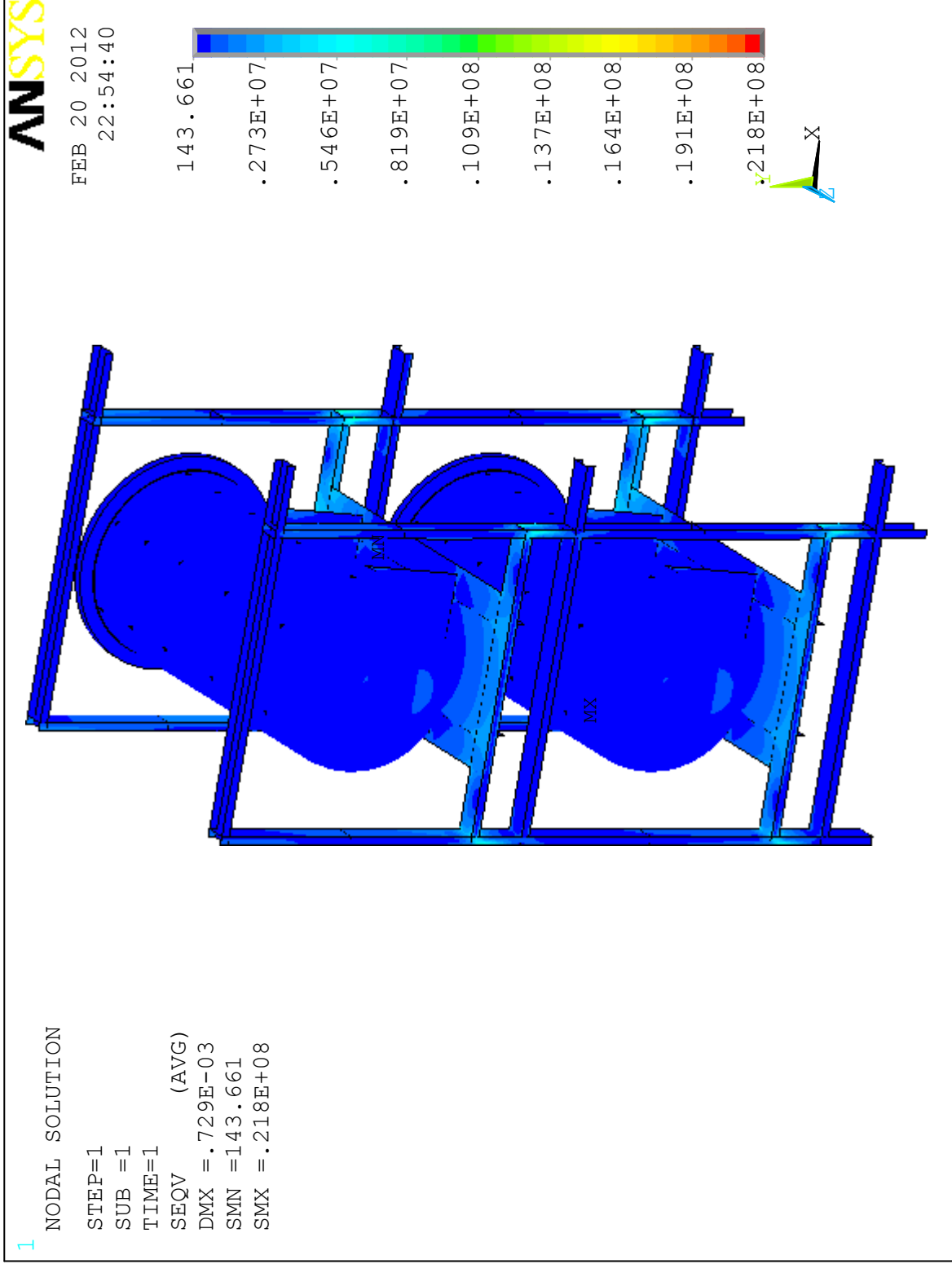
UY displacement in [m]



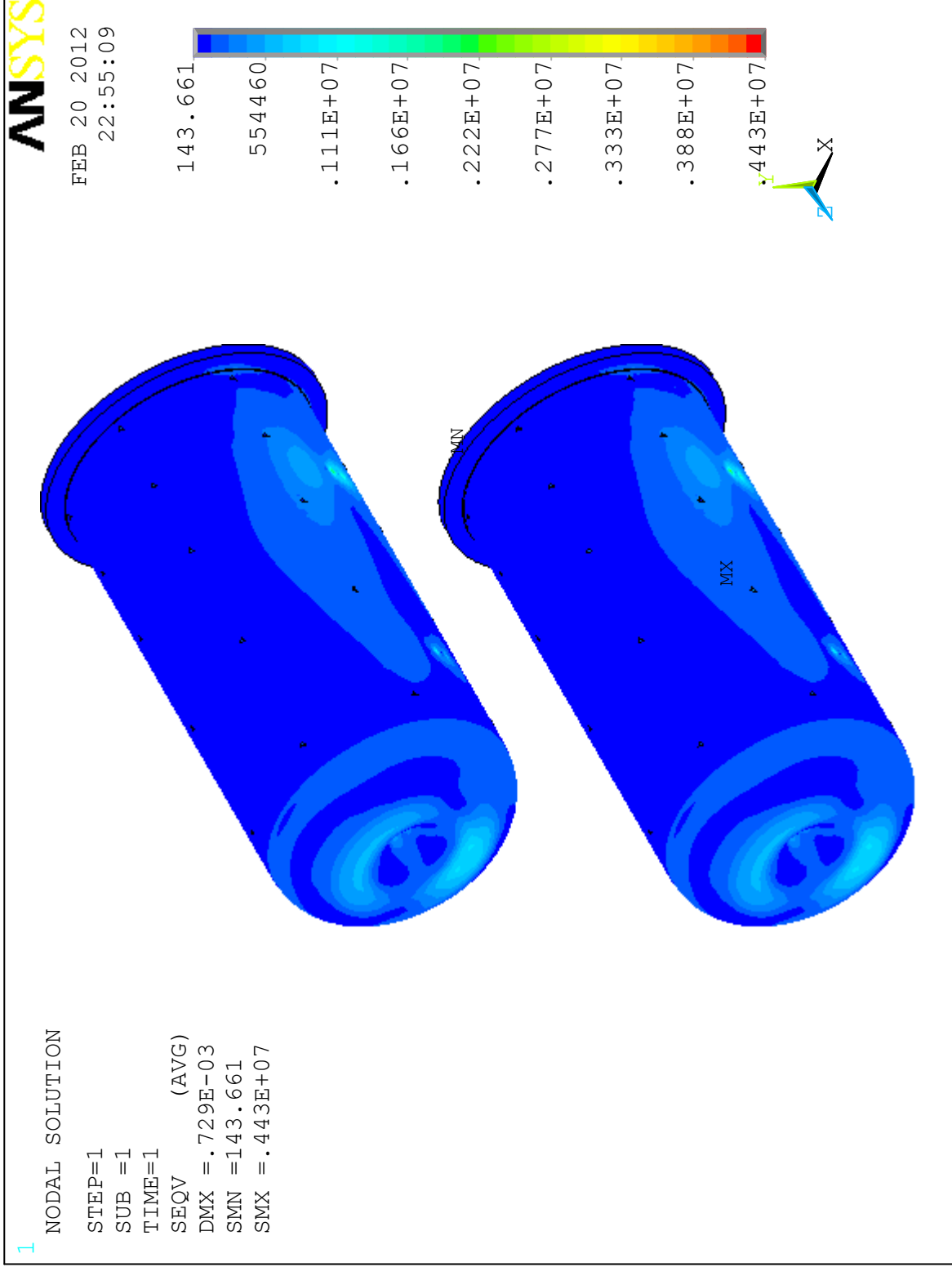
Uz displacement in [m]



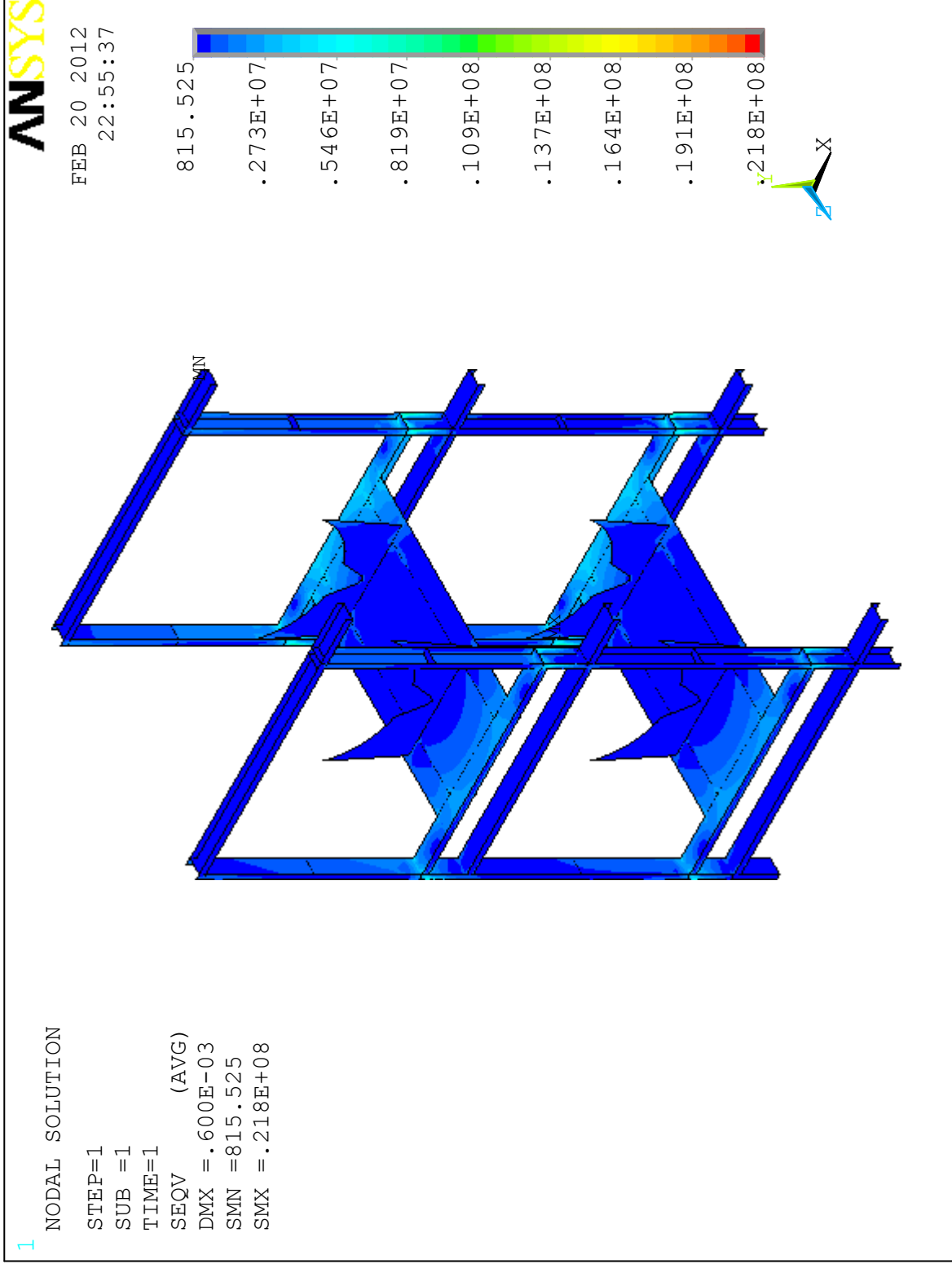
Distribution of displacement vector displacement in [m]



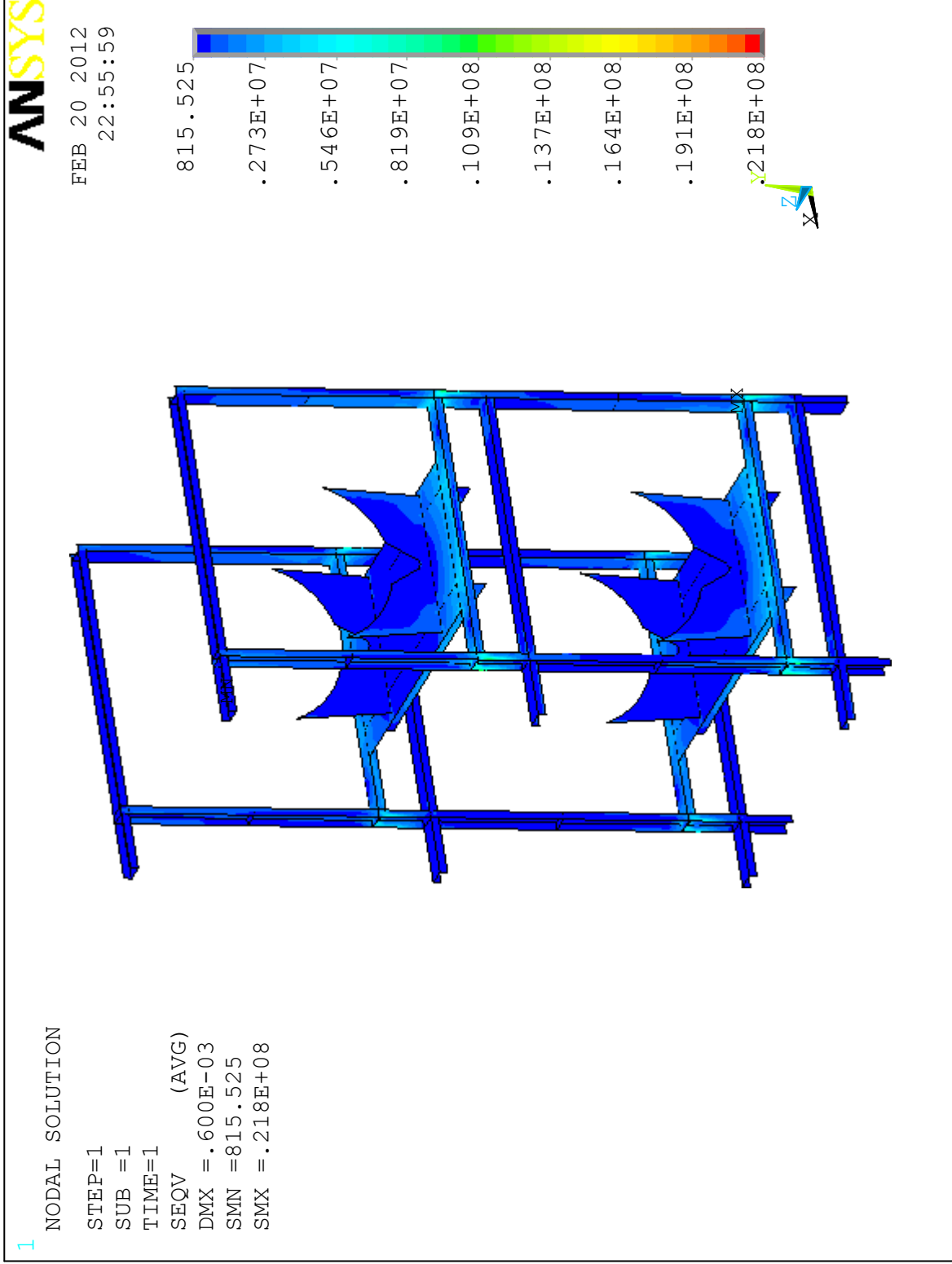
Distribution of equivalent stress in [Pa]



Distribution of equivalent stress in [Pa] – only horns are shown

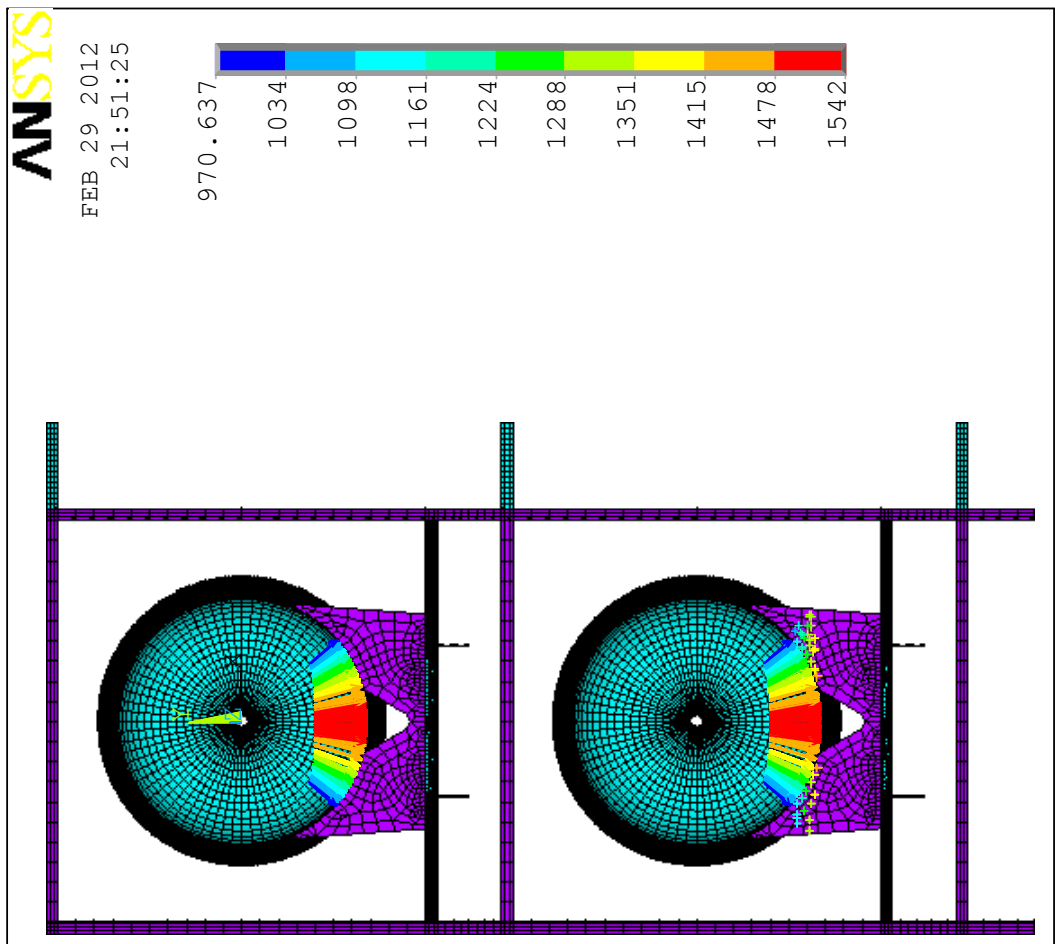
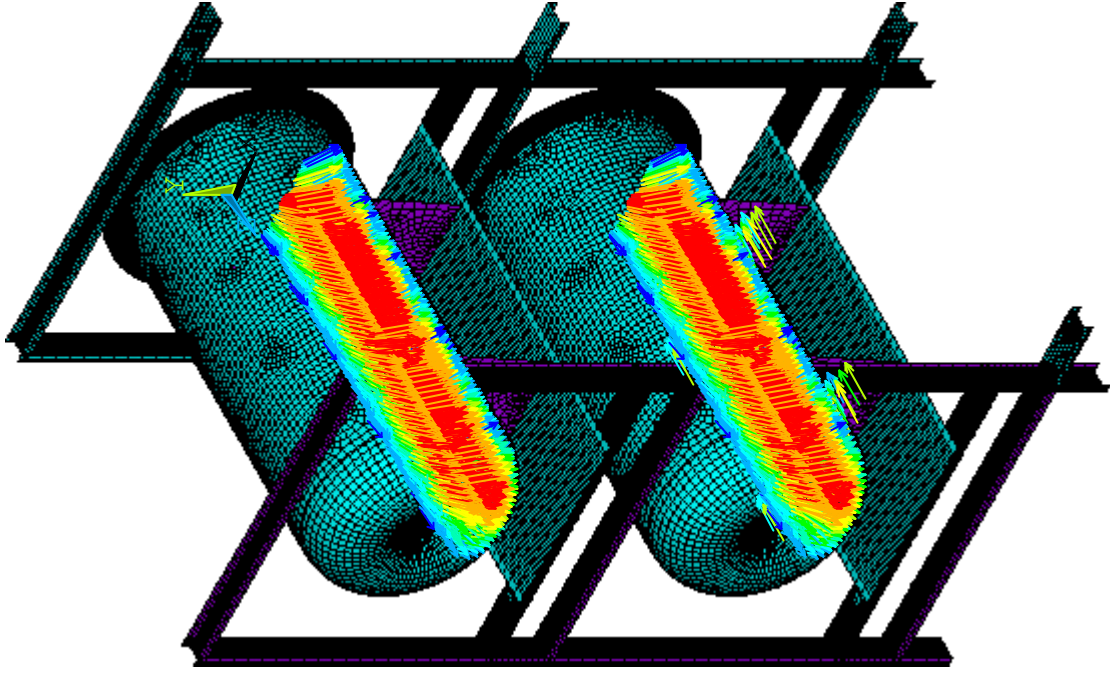


Distribution of equivalent stress in [Pa] – only frames are shown

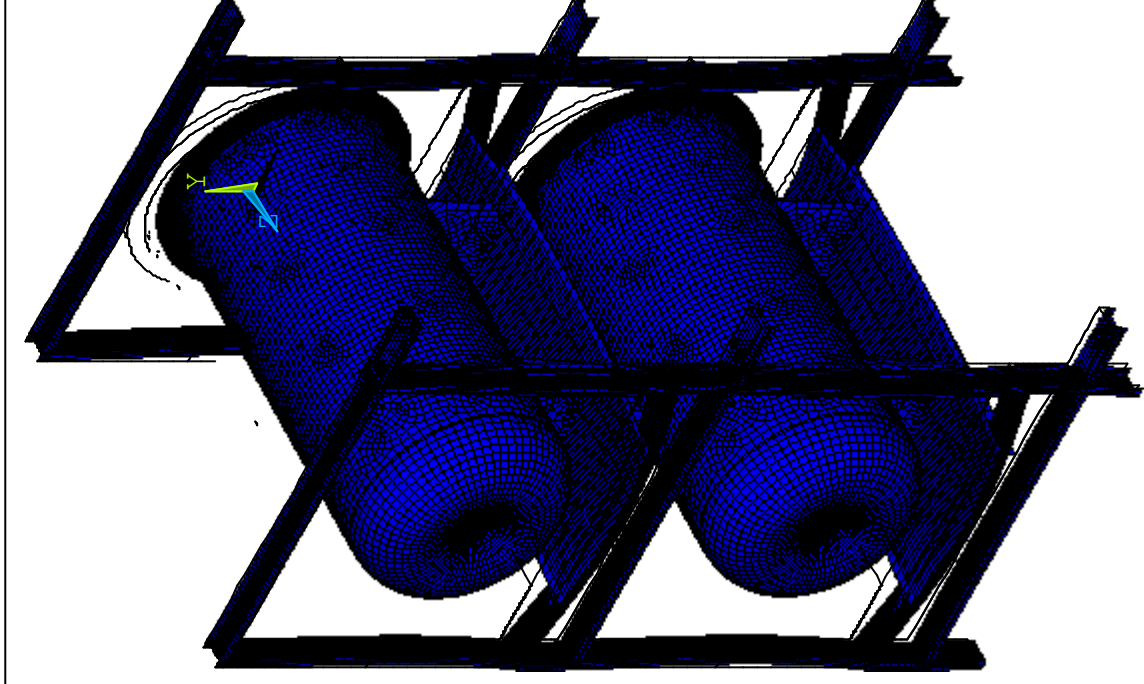


Distribution of equivalent stress in [Pa] – only frames are shown (opposite view)

Pressure of water inside
horns added



1 DISPLACEMENT
STEP=1
SUB =1
TIME=1
DMX =.962E-03

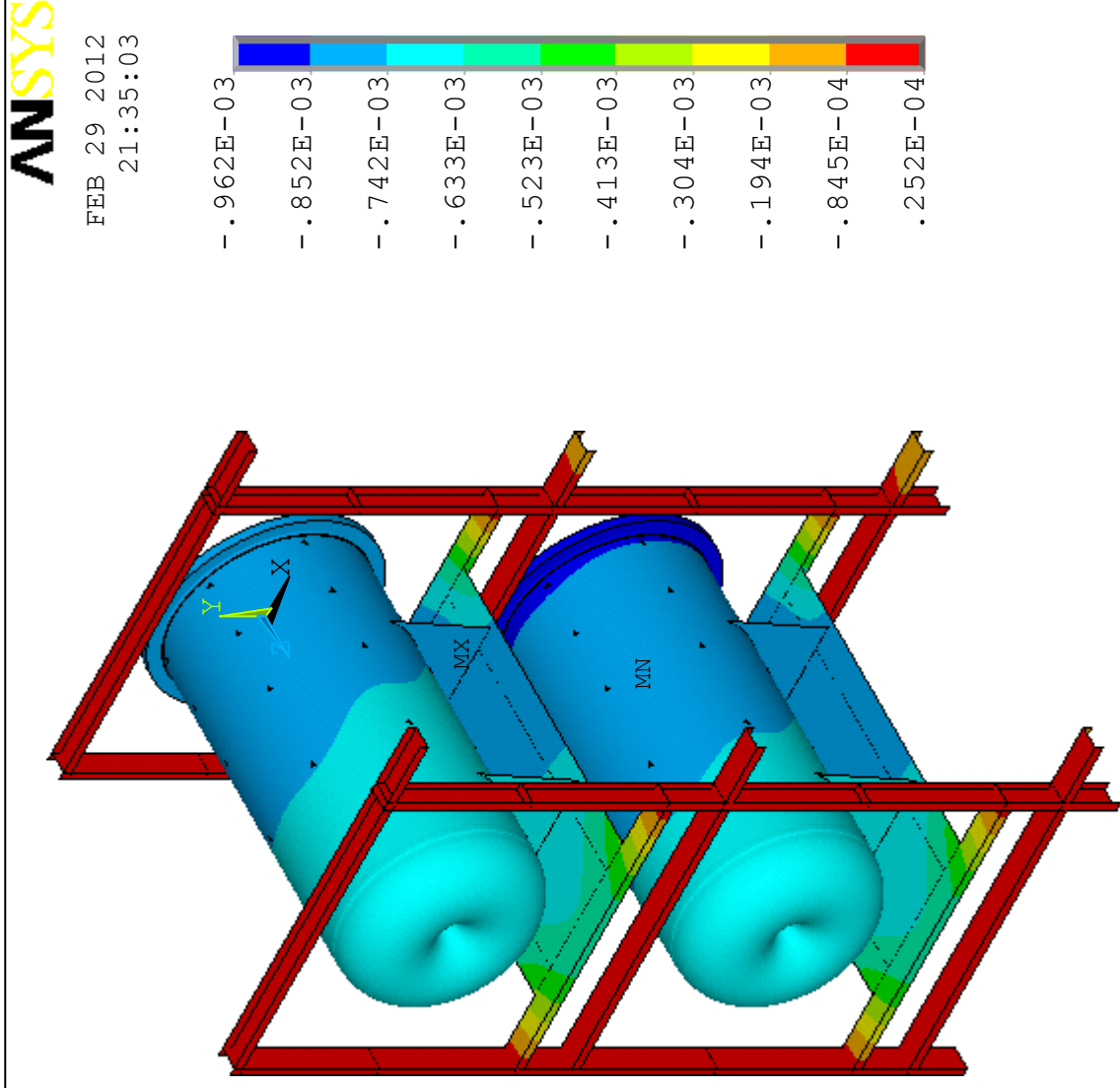


A
FEB 2
21

Loads:
deadweight +
hydrostatic
pressure of
water

Loads:
deadweight +
hydrostatic
pressure of
water

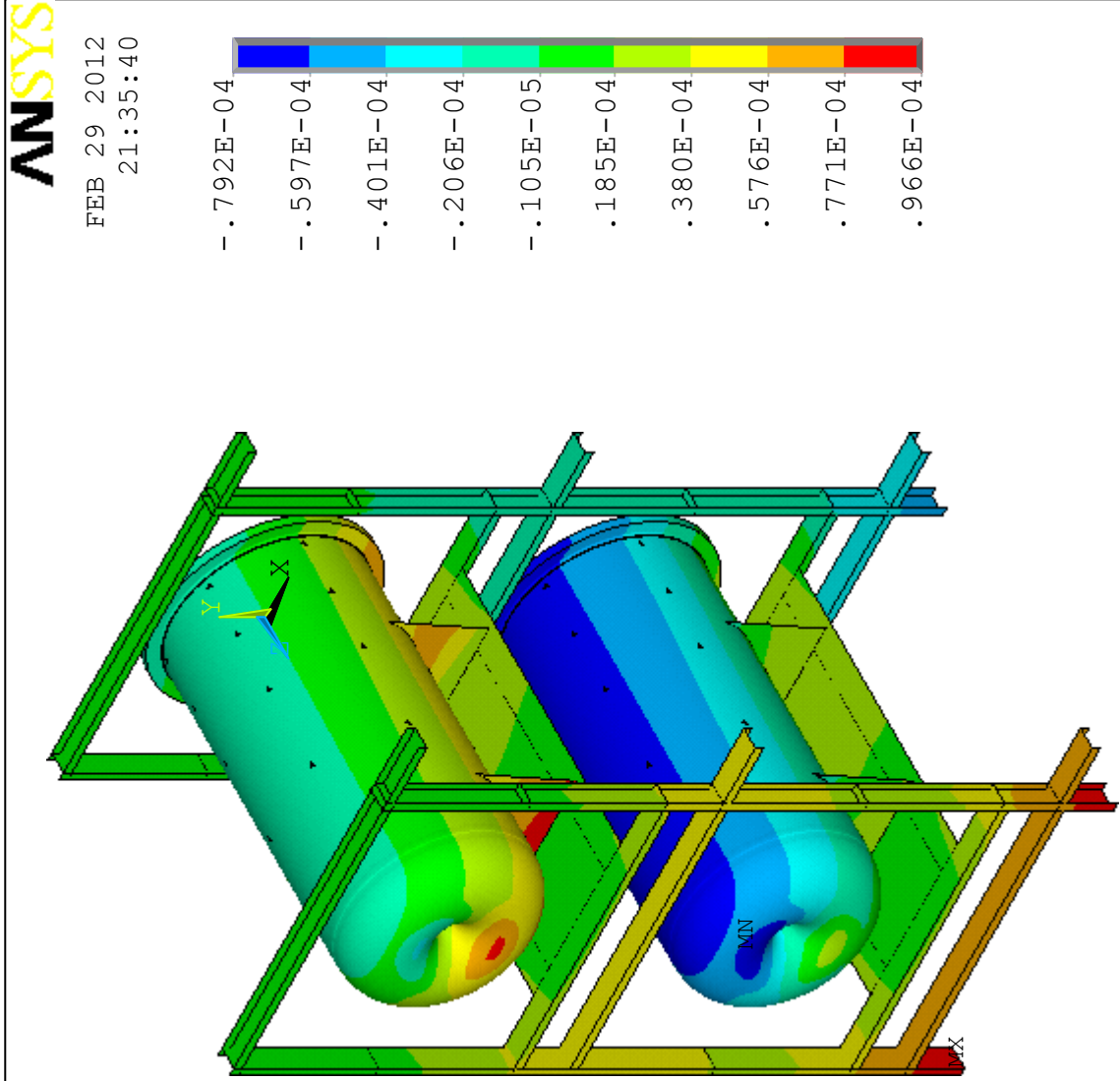
RSYS=0
DMX =.962E-03
SMN =-.962E-03
SMX =.252E-04



U_y displacement in [m]

Loads:
deadweight +
hydrostatic
pressure of
water

Uz (AVG)
RSYS=0
DMX =.962E-03
SMN =-.792E-04
SMX =.966E-04



Uz displacement in [m]

Loads:
deadweight +
hydrostatic
pressure of
water

USUM (AVG)

RSYS=0

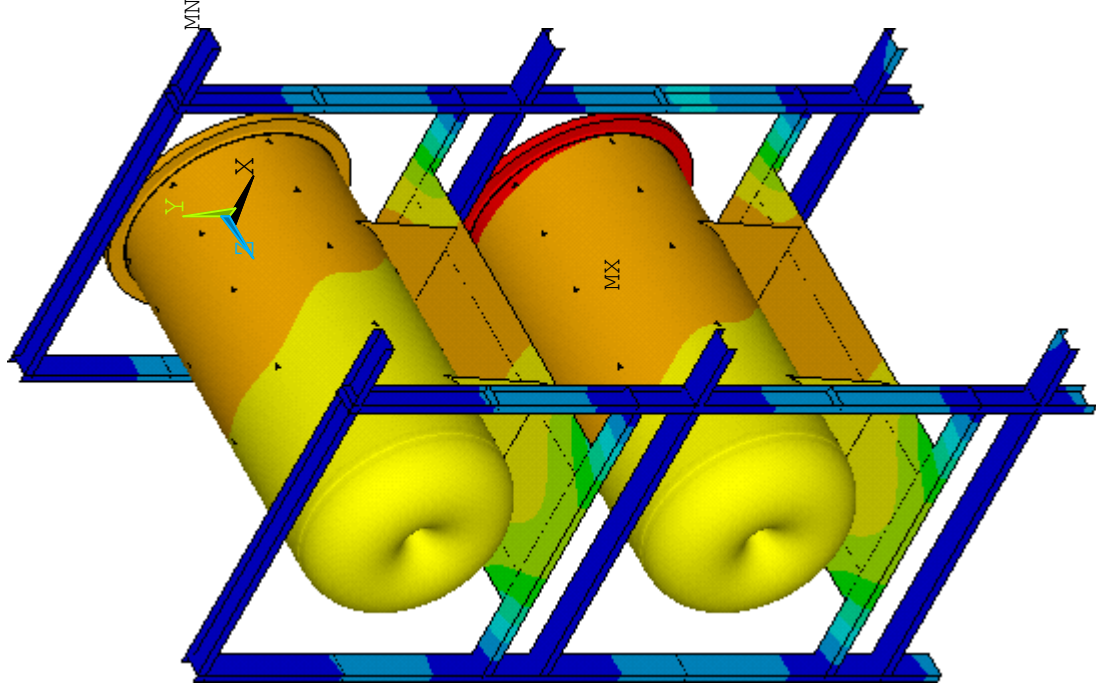
DMX = .962E-03

SMX = .962E-03

ANSYS

FEB 29 2012

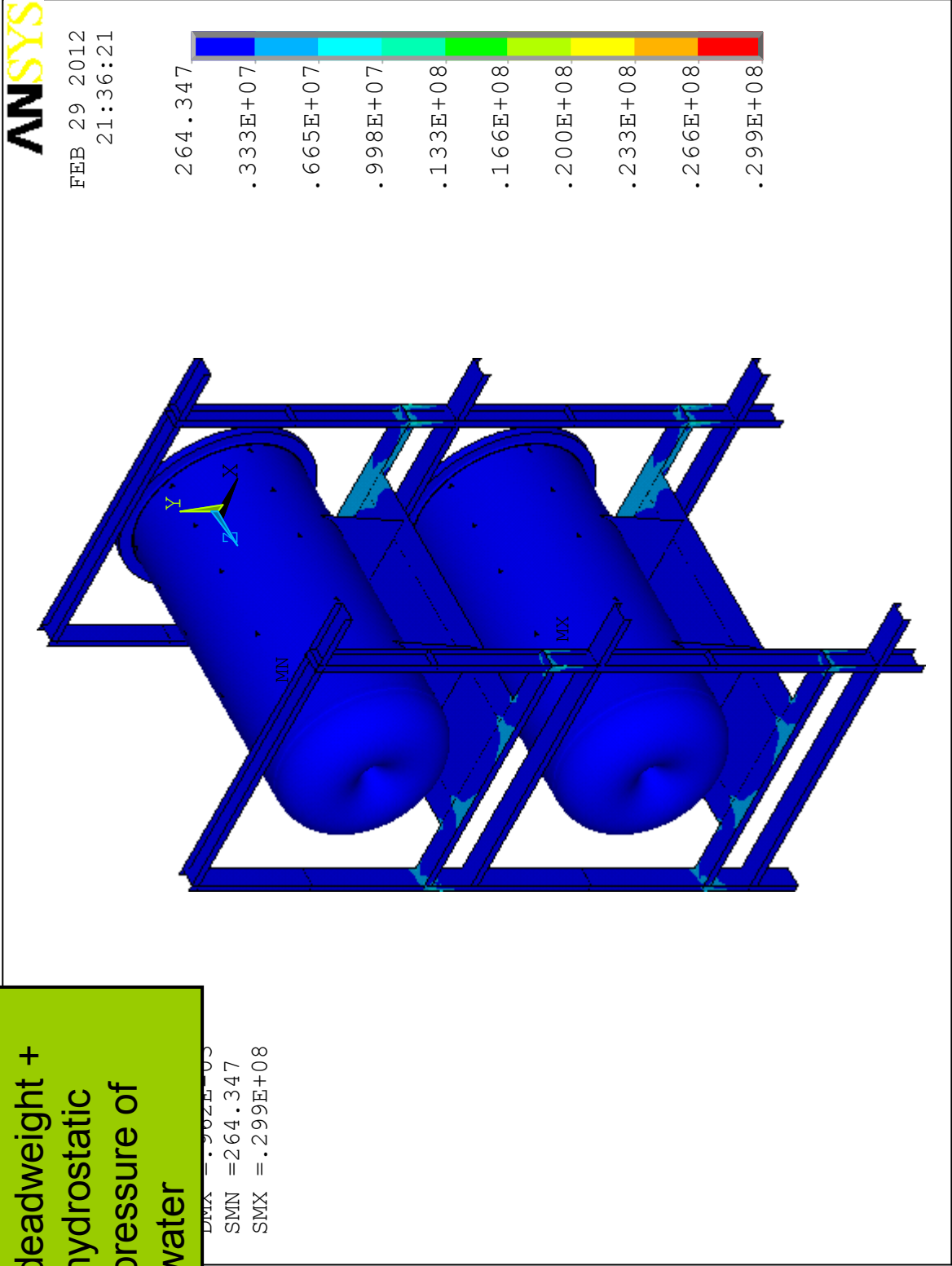
21:35:59



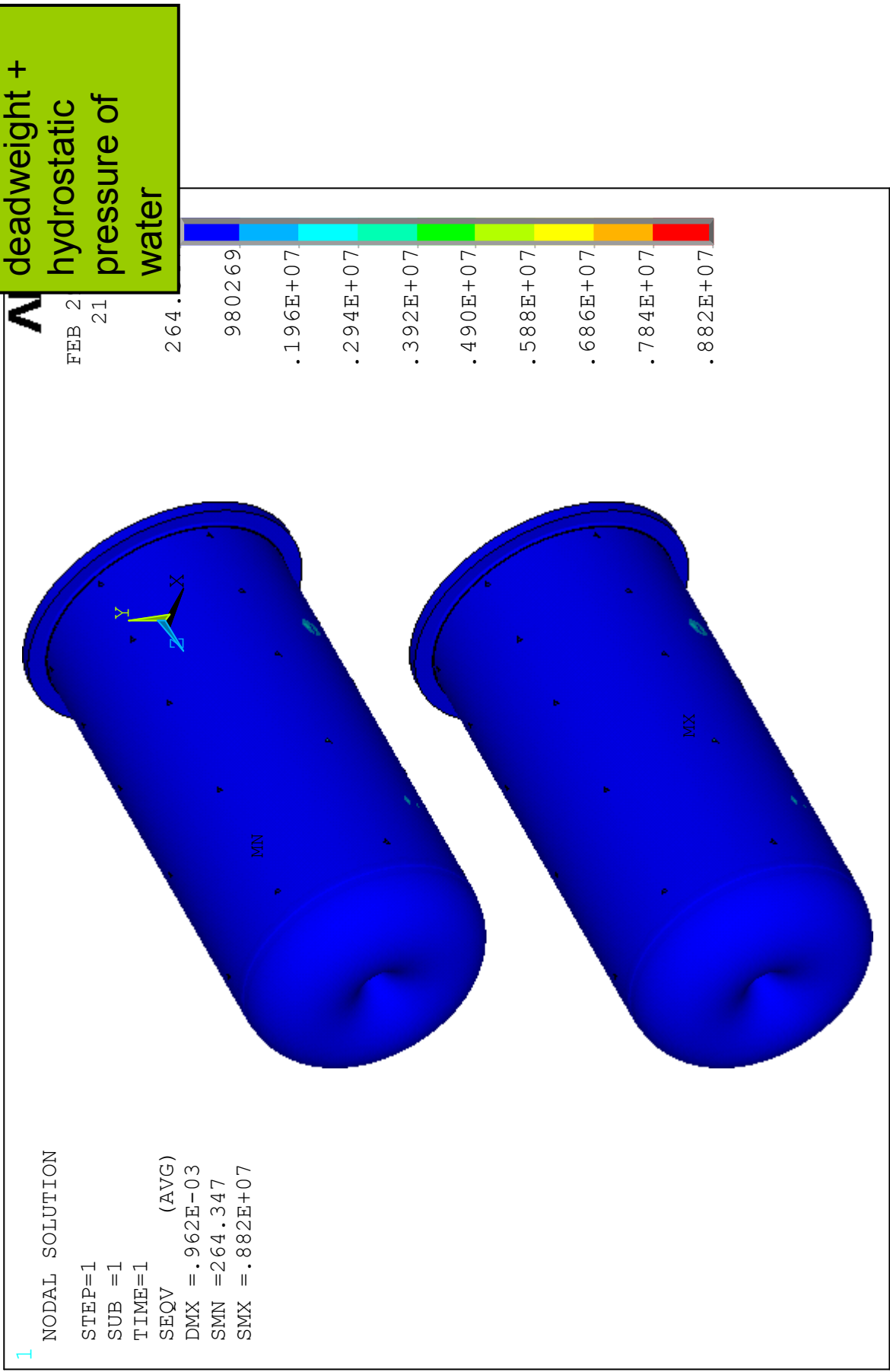
Distribution of displacement vector displacement in [m]

Loads:
deadweight +
hydrostatic
pressure of
water

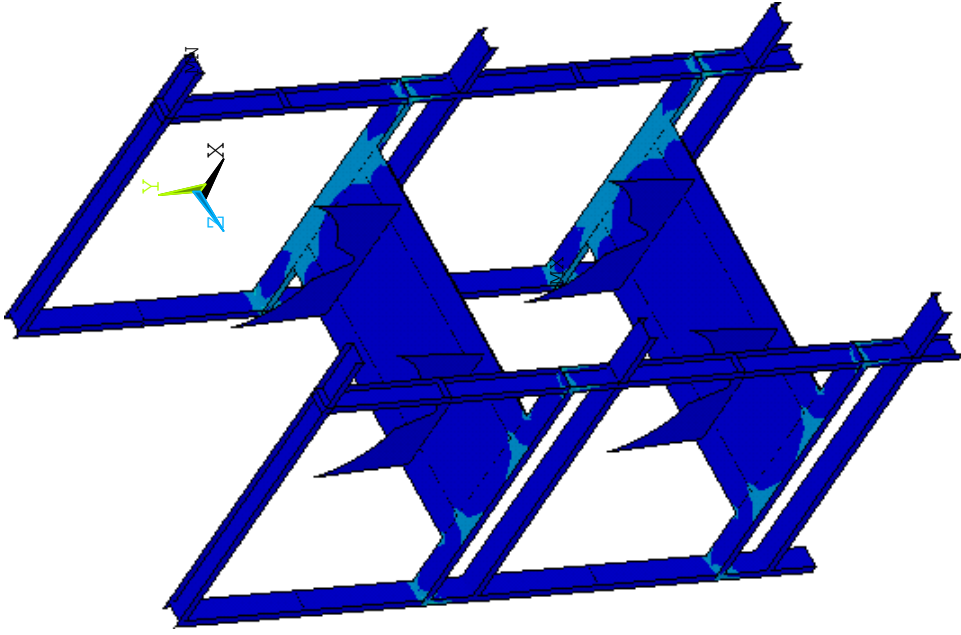
DMX =.902E+03
SMN =264.347
SMX =.299E+08



Distribution of equivalent stress in [Pa]



Distribution of equivalent stress in [Pa] – only horns are shown

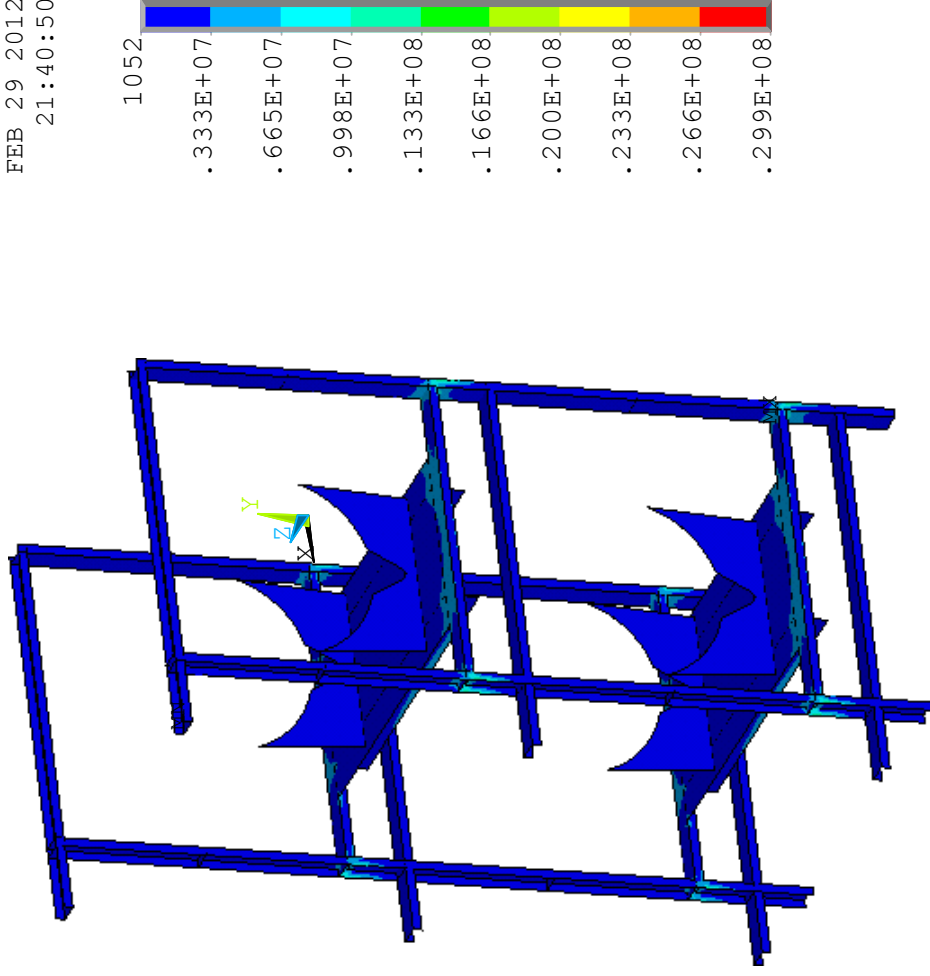


Distribution of equivalent stress in [Pa]
 – only frames are shown

Loads:
 deadweight +
 hydrostatic
 pressure of
 water

ANSYS

FEB 29 2012
 21:40:50



1

NODAL SOLUTION

STEP=1

SUB =1

TIME=1

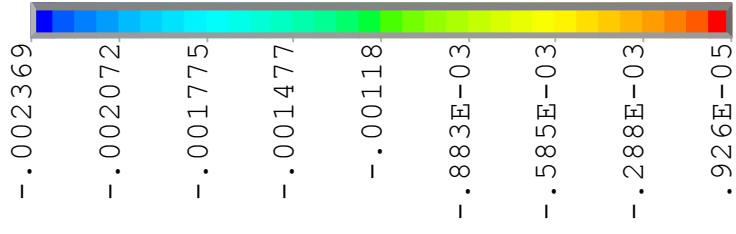
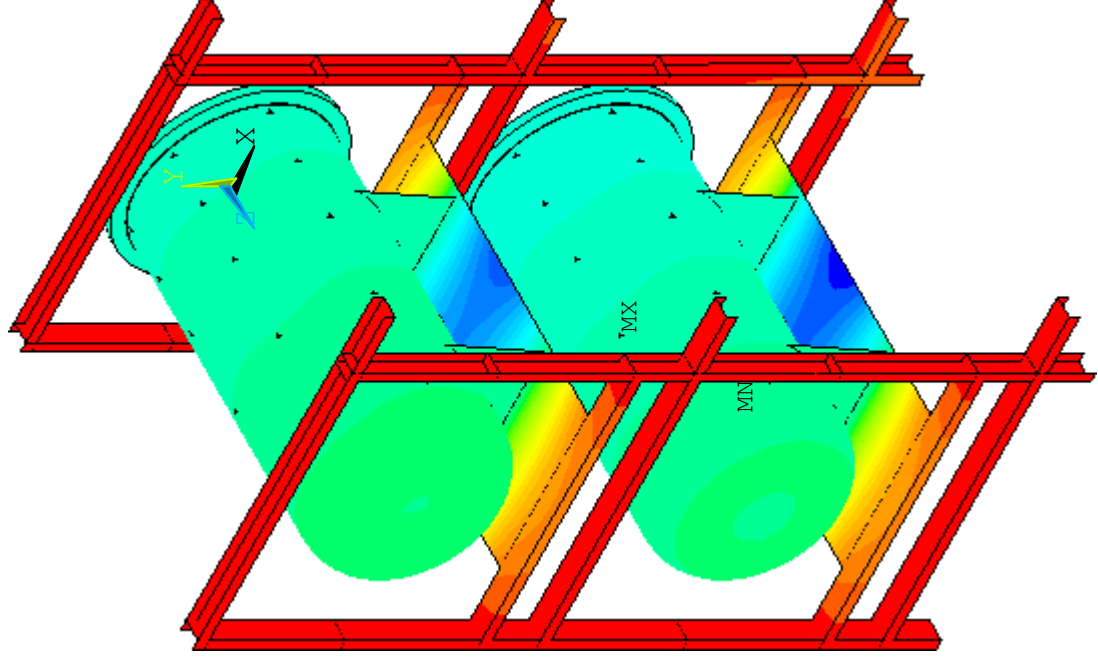
UY (AVG)

RSYS=0

DMX =.002496

SMN =-.002369

SMX =.926E-05



Loads:
deadweight no
ribs under
hor.supp. plate

1

NODAL SOLUTION

STEP=1

SUB =1

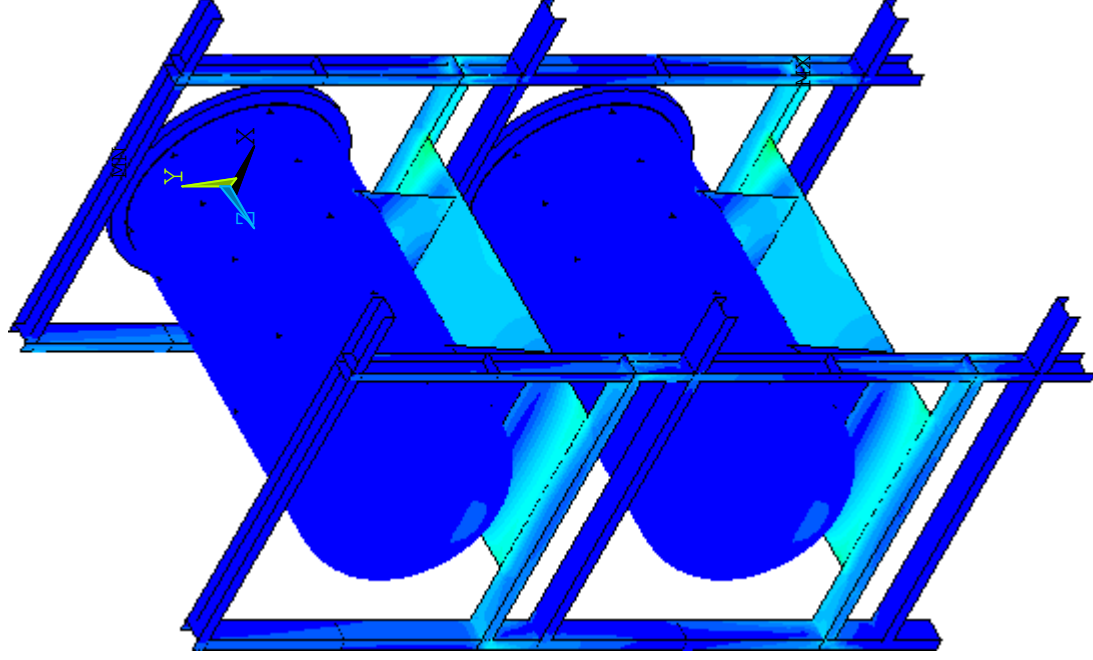
TIME=1

SEQV (AVG)

DMX =.002496

SMN =159.816

SMX =.216E+08



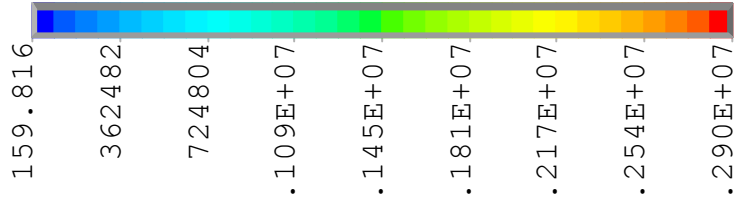
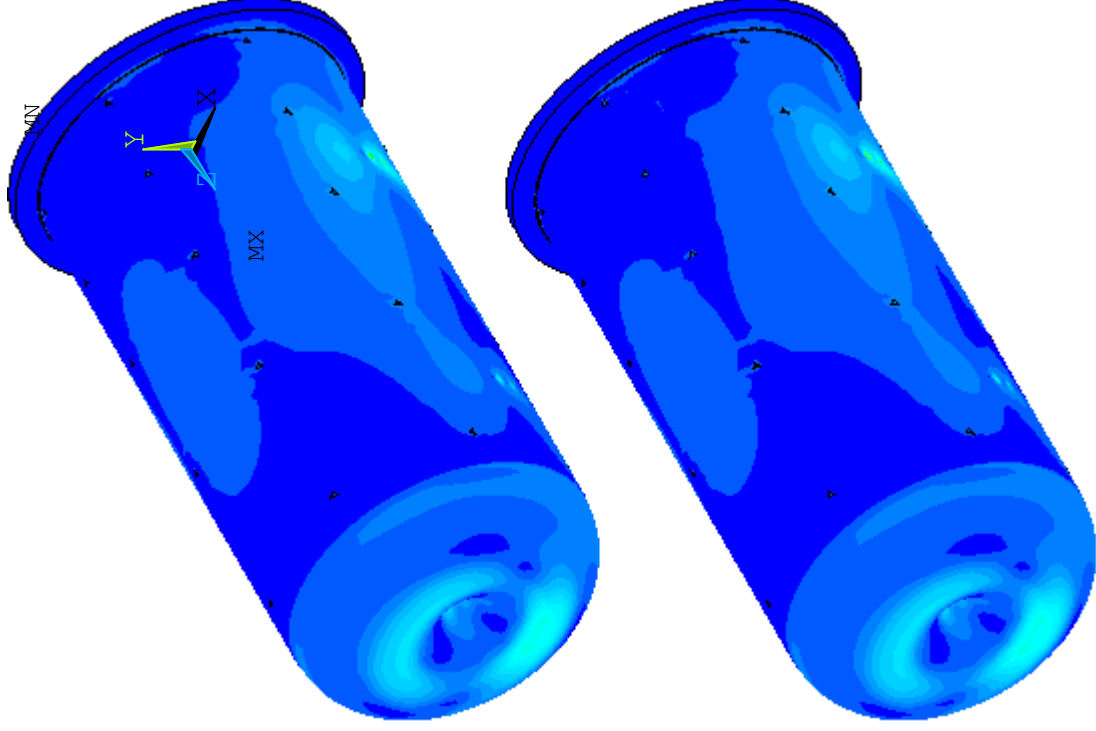
Loads:
deadweight no
ribs under
hor.supp. plate

AN

FEB 2
23

1

NODAL SOLUTION
STEP=1
SUB =1
TIME=1
SEQV (AVG)
DMX =.001725
SMN =159.816
SMX =.290E+07



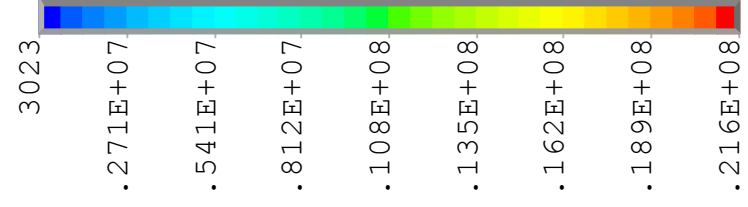
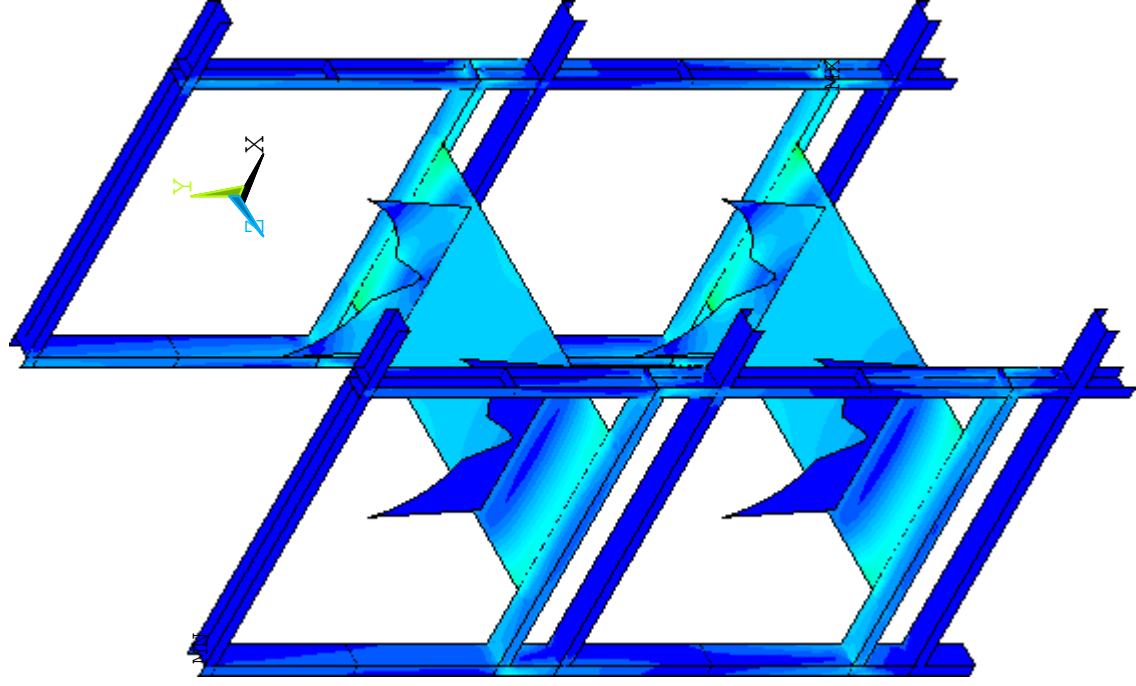
Loads:
deadweight no
ribs under
hor.supp. plate

1

NODAL SOLUTION
STEP=1
SUB =1
TIME=1
SEQV (AVG)
DMX =.002496
SMN =3023
SMX =.216E+08



FEB 23



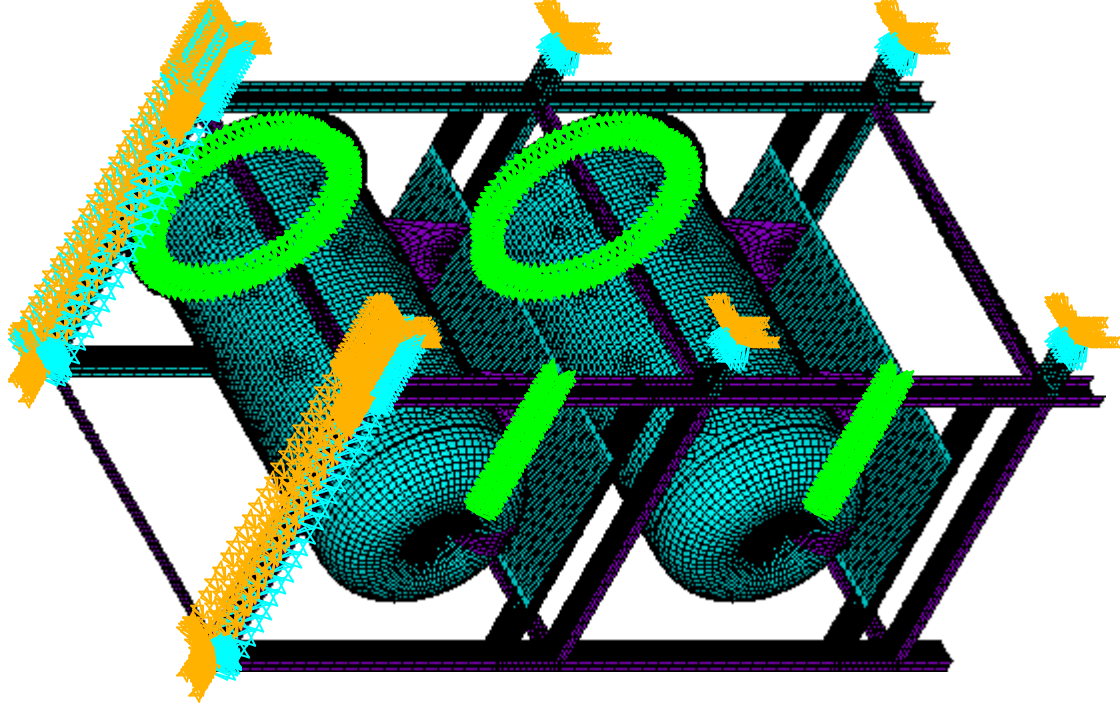
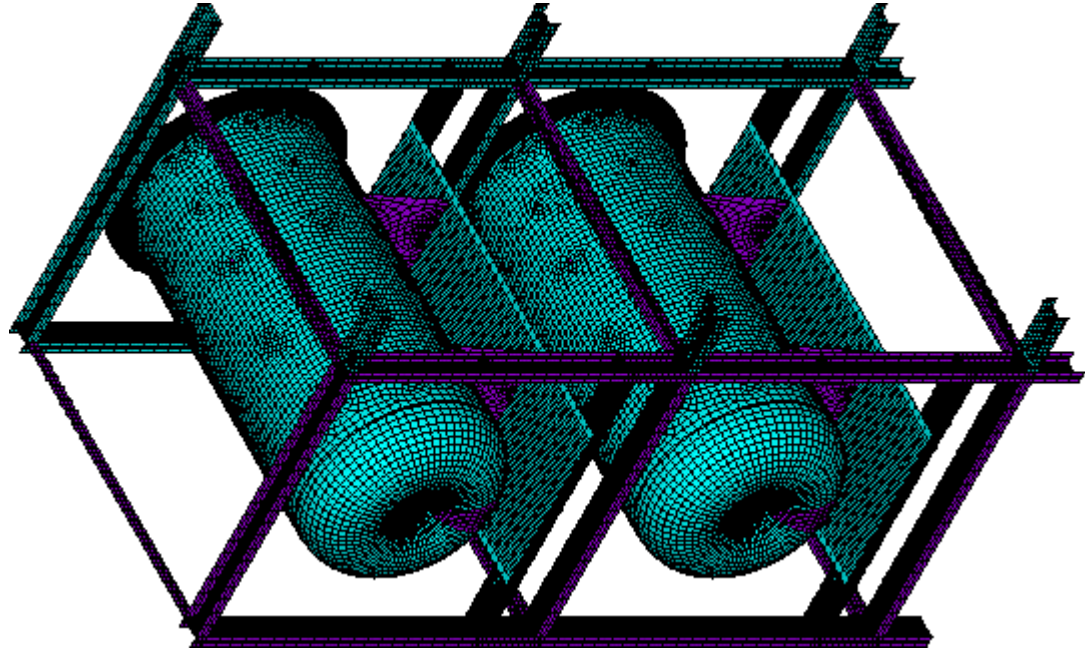
Loads:
deadweight no
ribs under
hor.supp. plate

Summary of results for structure without longitudinal spans

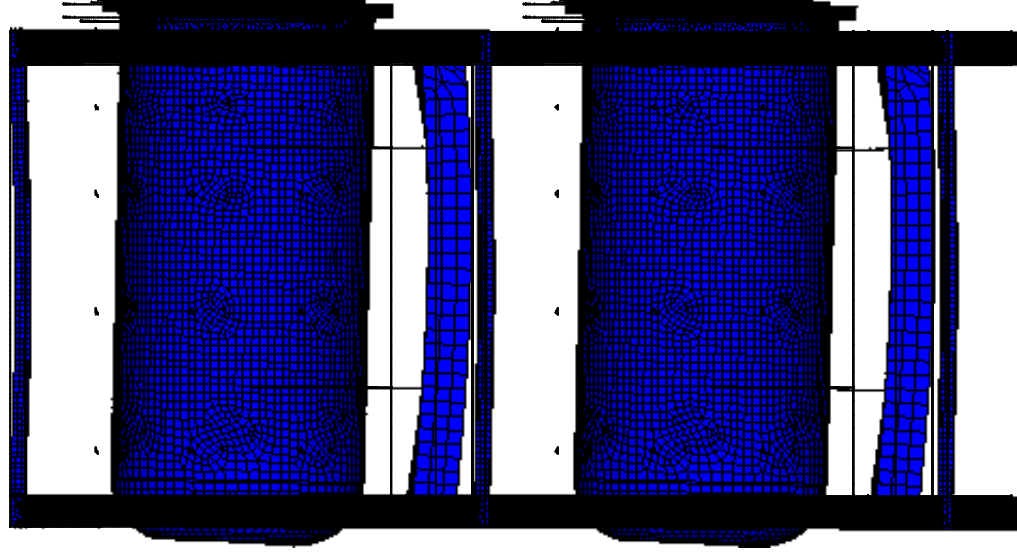
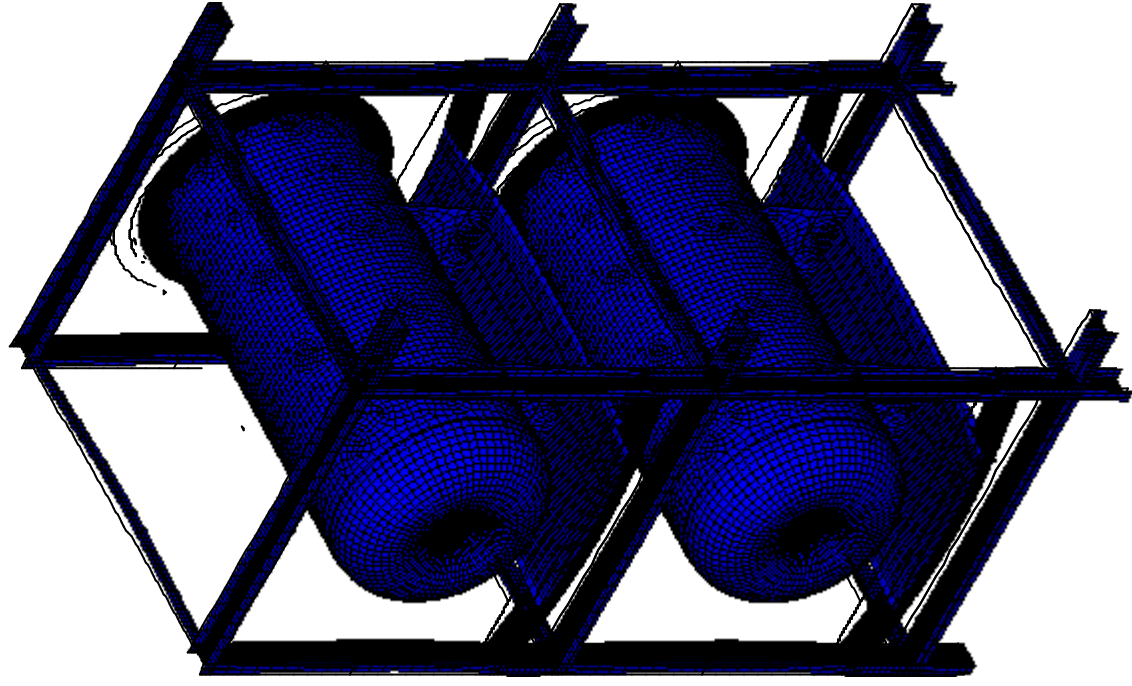
Strucutre, loads	$ u_y _{\max}$ <i>mm</i>	$\sigma_{\text{eqv}, \max}$ <i>MPa (horn)</i>	$\sigma_{\text{eqv}, \max}$ <i>MPa (frame)</i>
(plate with ribs), deadweight	0.73	4.4	21.8
(plate with ribs), deadweight + hydrostatic pressure	0.96	8.8	29.9
(plate without ribs), deadweight	2.37	2.9	21.6

Symmetric $\frac{1}{2}$ of structure with ribs,
with longitudinal spans, supported
on the top,

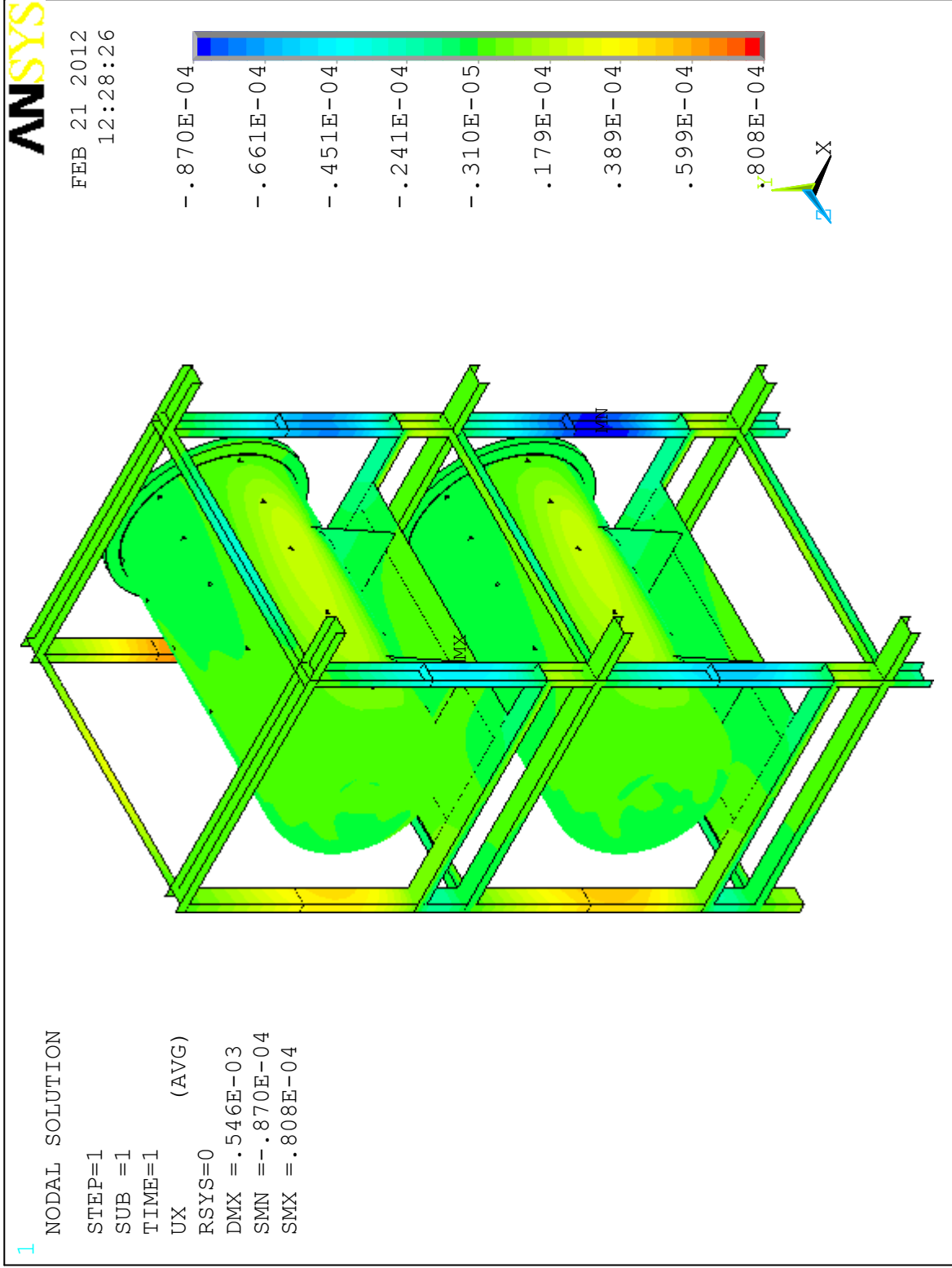
Slides: 33 – 43 (load: deadweight)



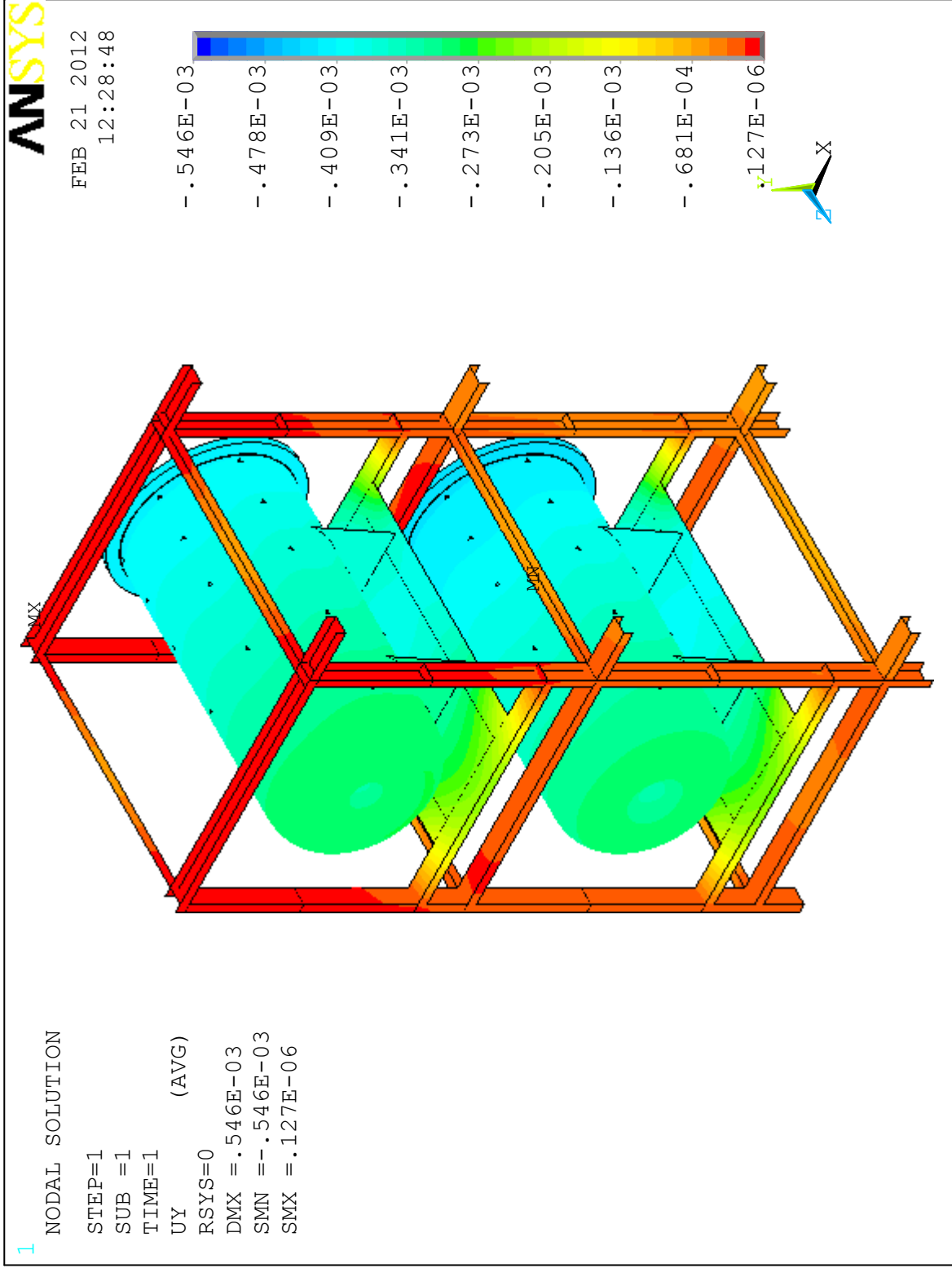
Isometric view of mesh and mesh with boundary conditions introduced



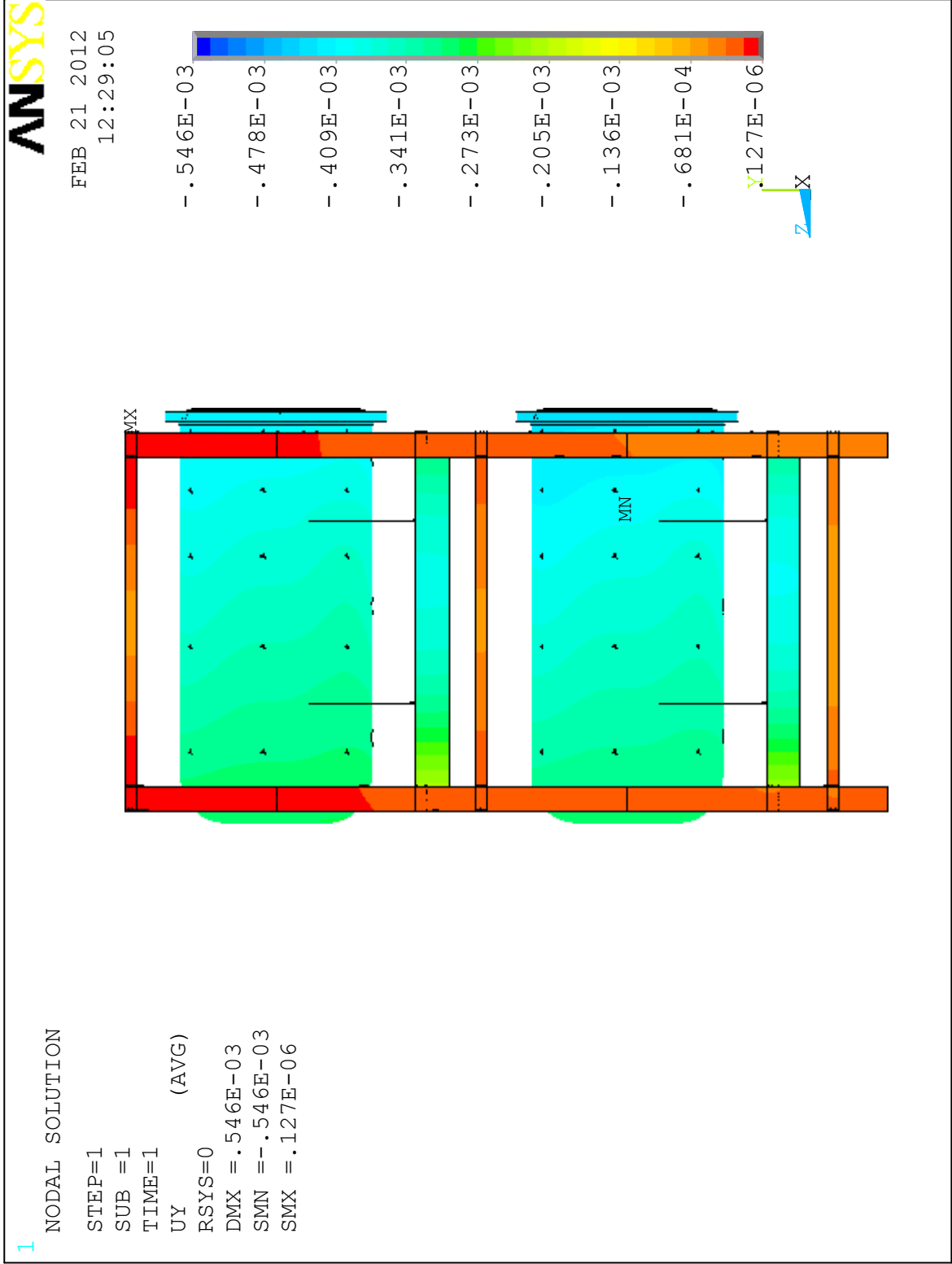
Deformation of structure under deadweight – not to scale drawing



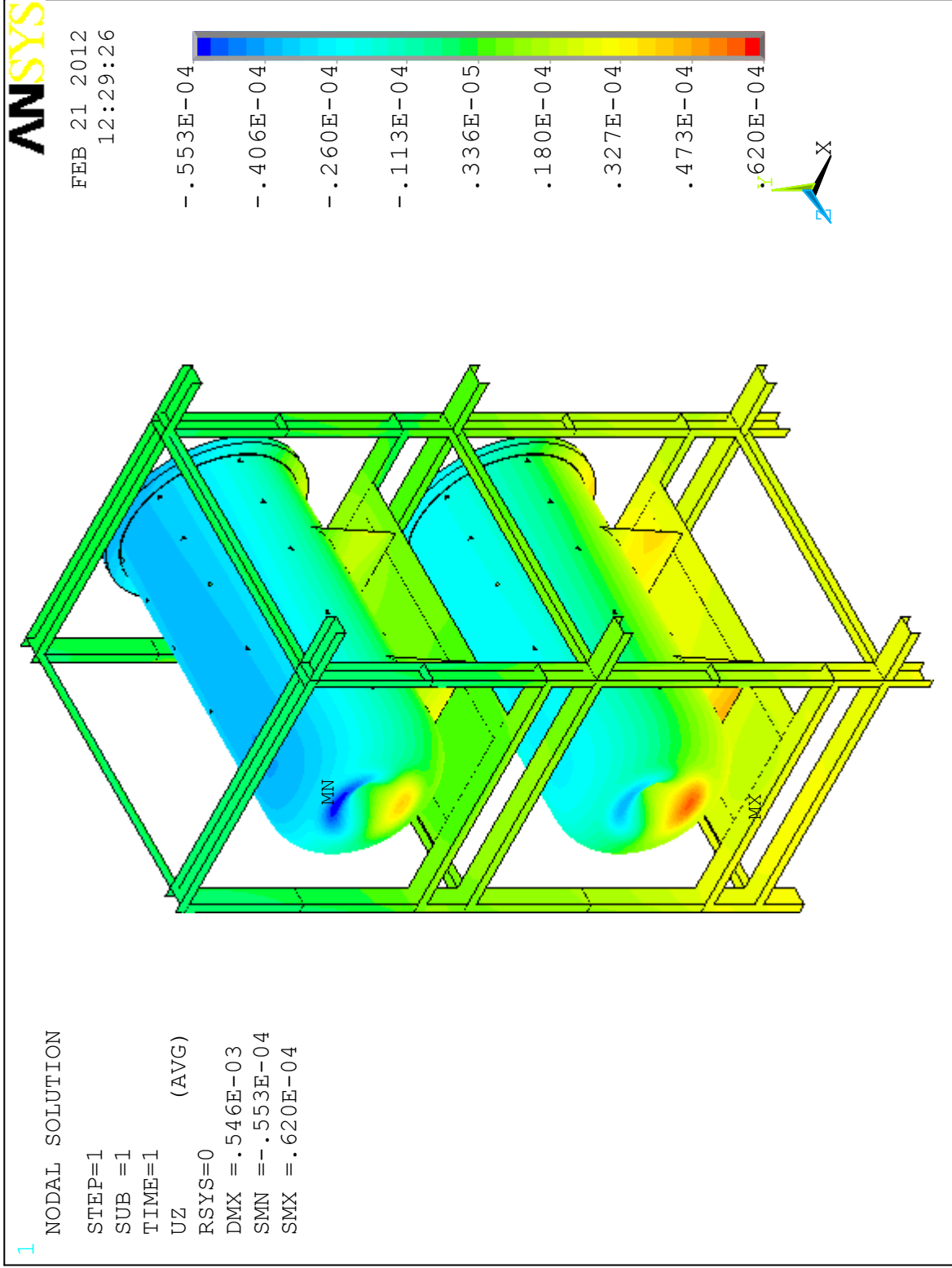
U_x displacement in [m]



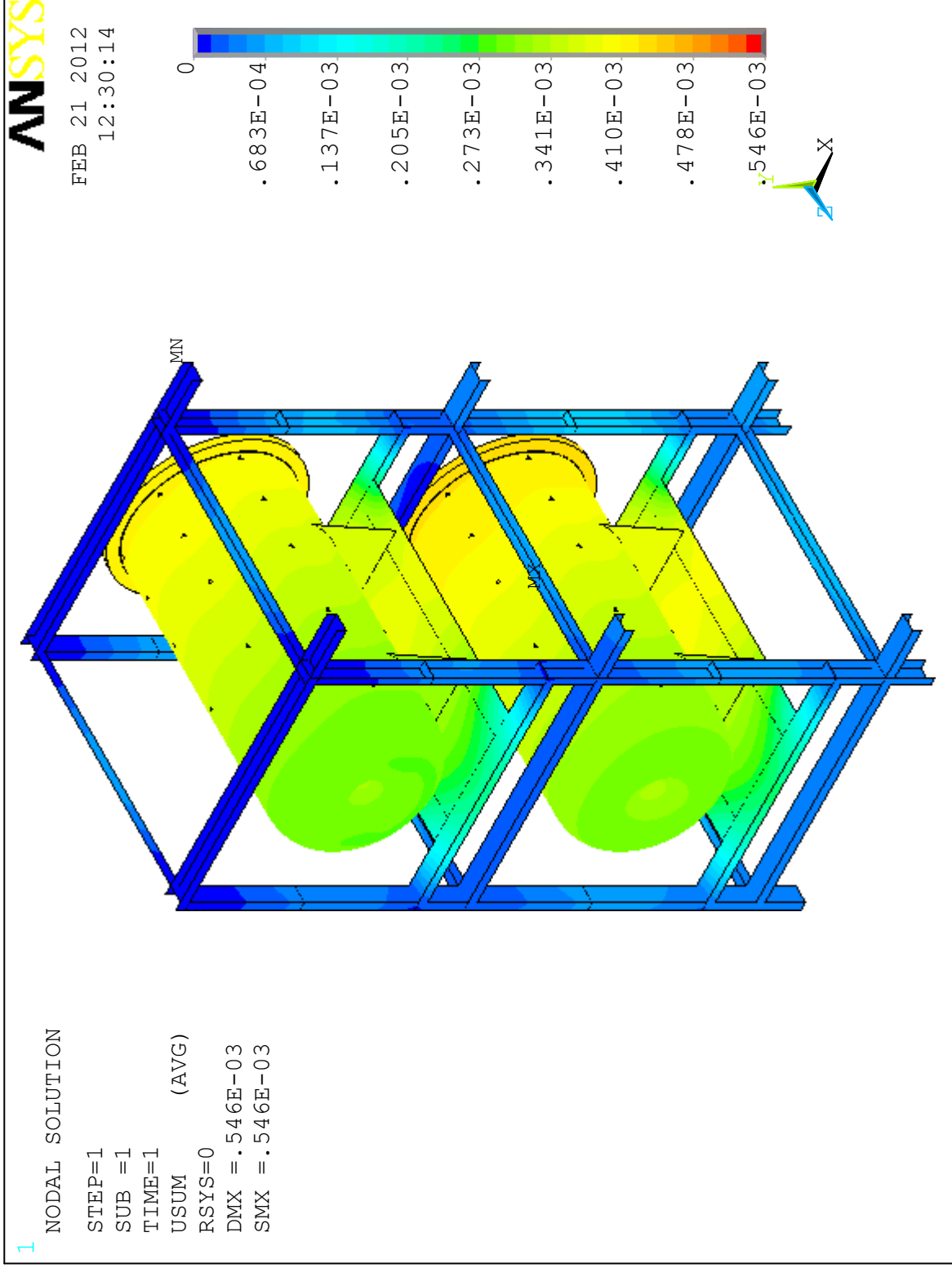
U_y displacement in [m]



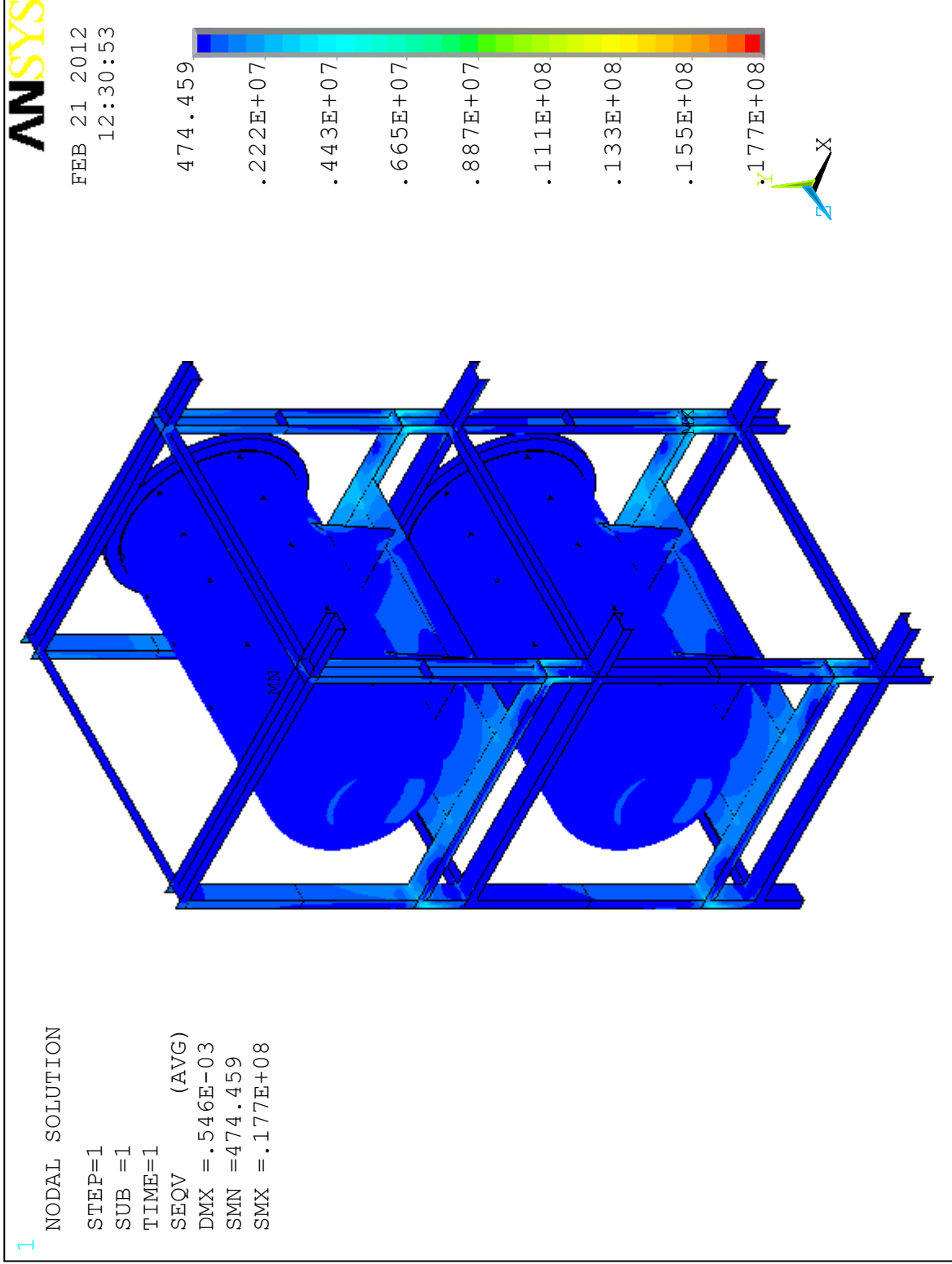
Uy displacement in [m]



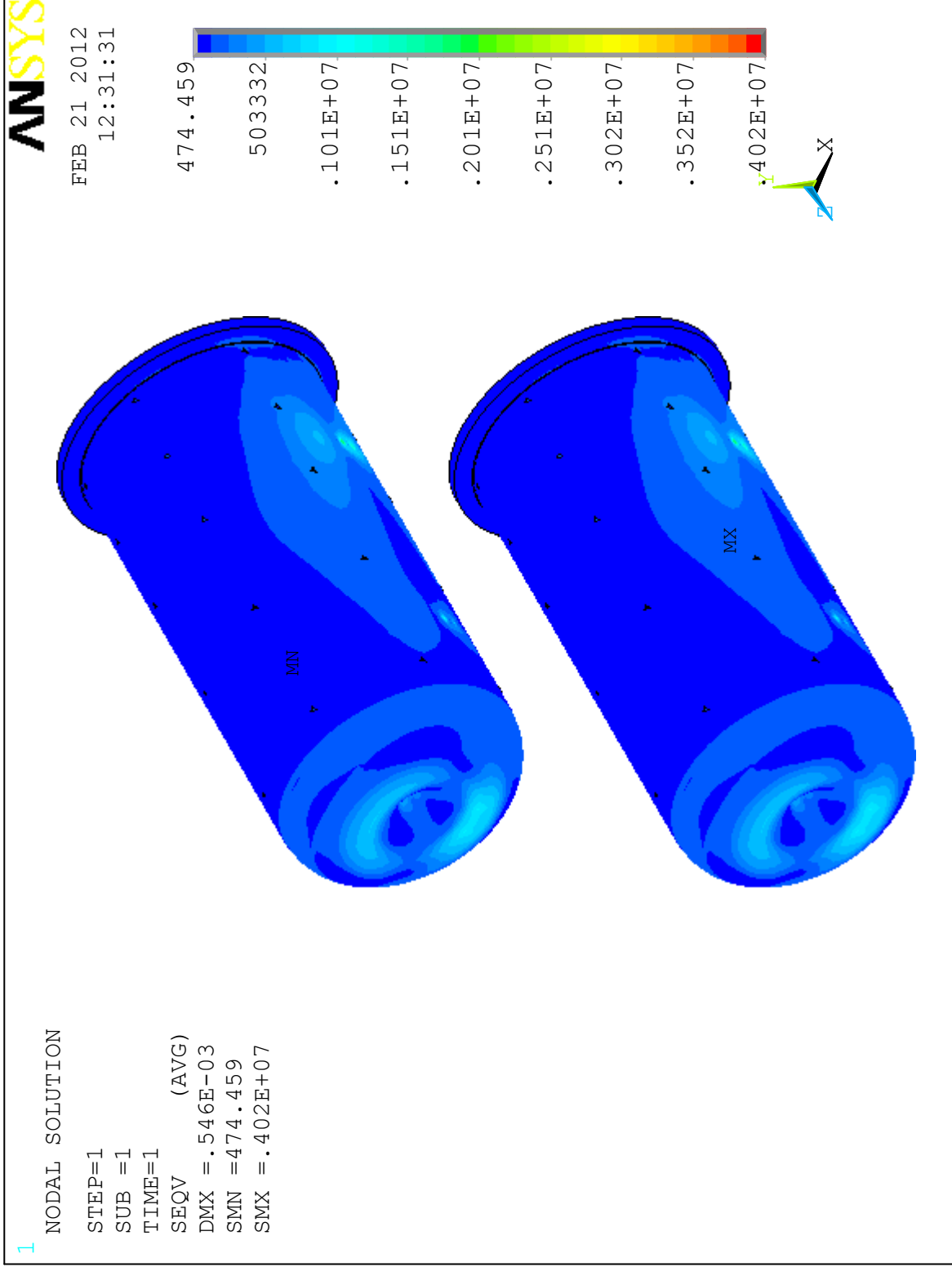
Uz displacement in [m]



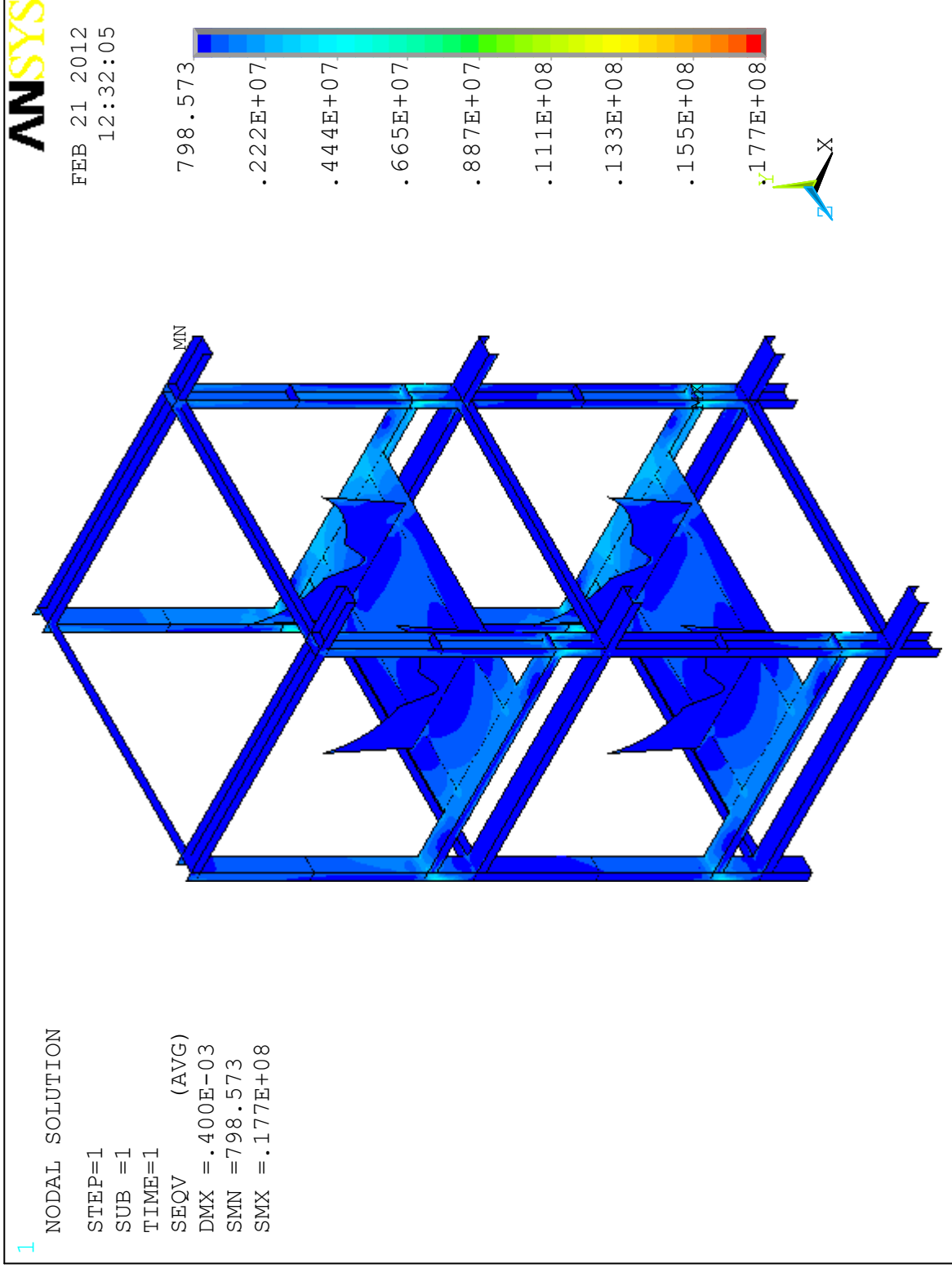
Distribution of displacement vector displacement in [m]



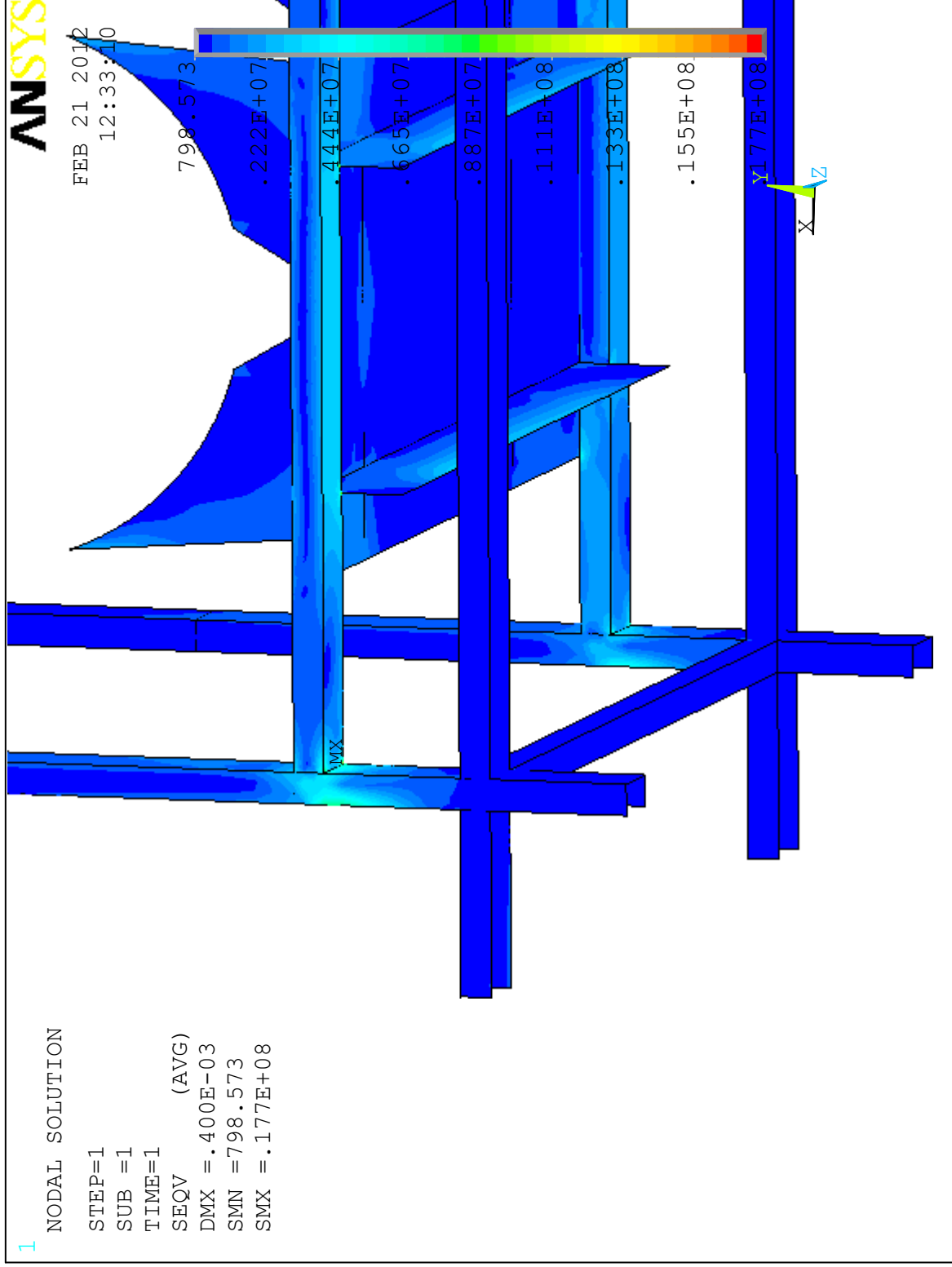
Distribution of equivalent stress in [Pa]



Distribution of equivalent stress in [Pa] – only horns are shown



Distribution of equivalent stress in [Pa] – only frames are shown



Distribution of equivalent stress in [Pa] – only frames are shown (opposite view, magnification)

Further steps to make:

1. Optimization of thickness for supporting plates and shape optimization for ribs (?)
2. Calculations of natural frequencies for the whole structure (not only symmetric half)
3. Introduction of water frame
4. Introduction of strip line plates

Thank you for your attention