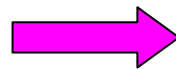


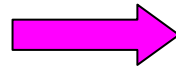
SPECIFICATIONS



PULSER: 350kA maxi, $\frac{1}{2}$ sinusoid, 100 μ s large, 50 pulses per second



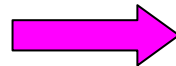
critical lifetime $13 \cdot 10^9$ pulses



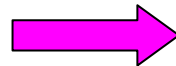
modularity



STUDY 2 SOLUTIONS :



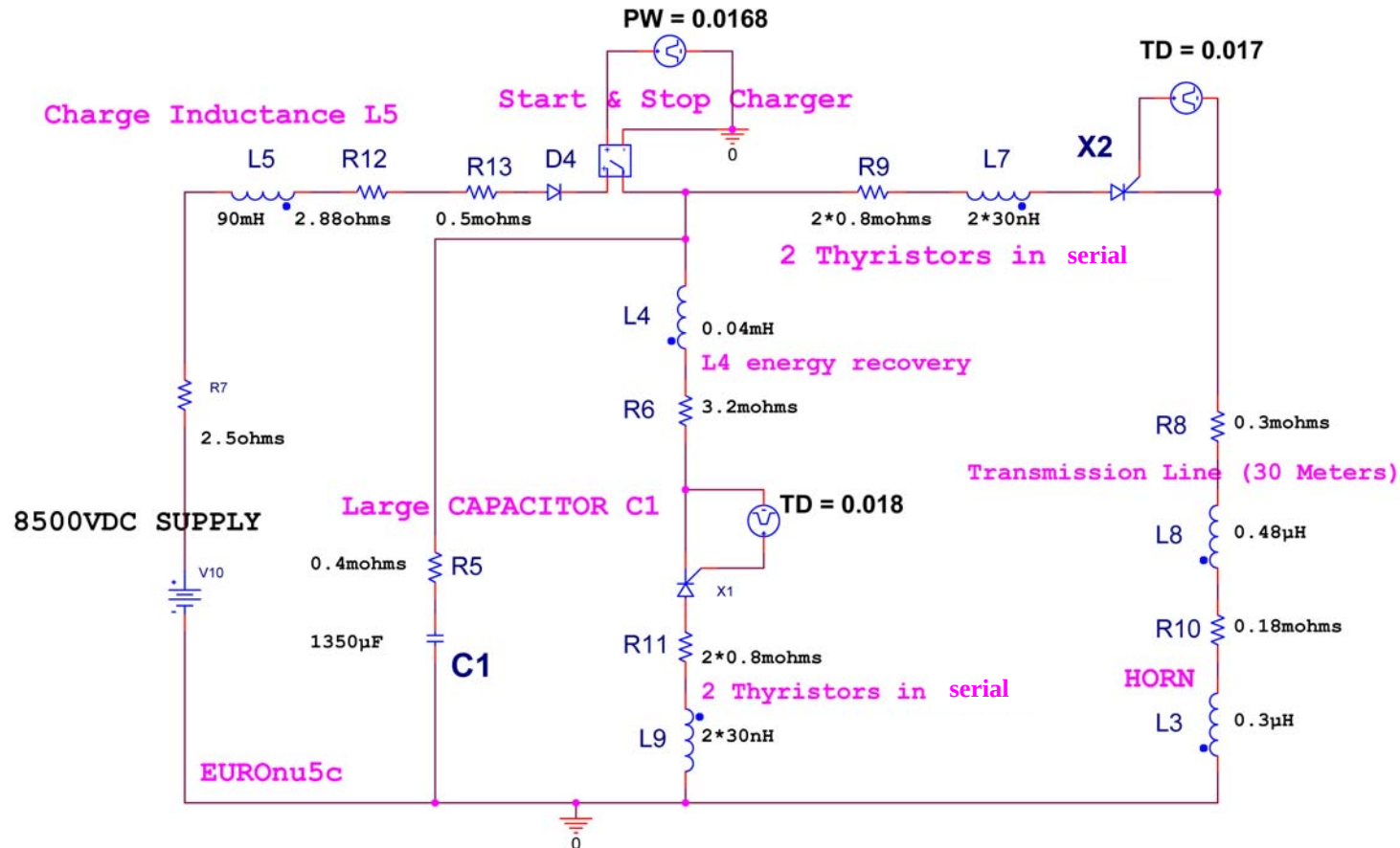
Energy recovery with a self



Energy recovery with diode and resistor

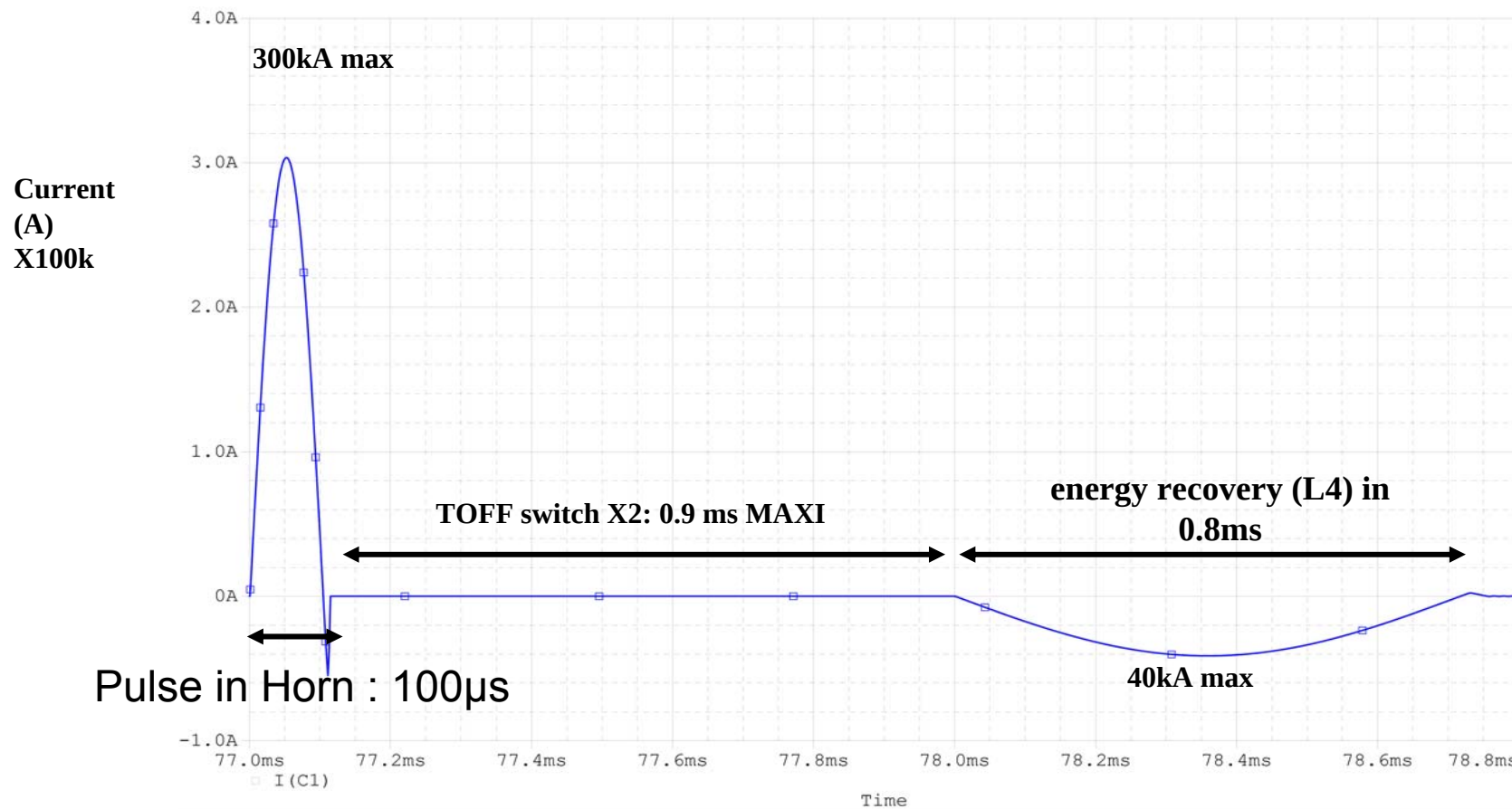
High current pulse power supply design

energy recovery with self (L4)



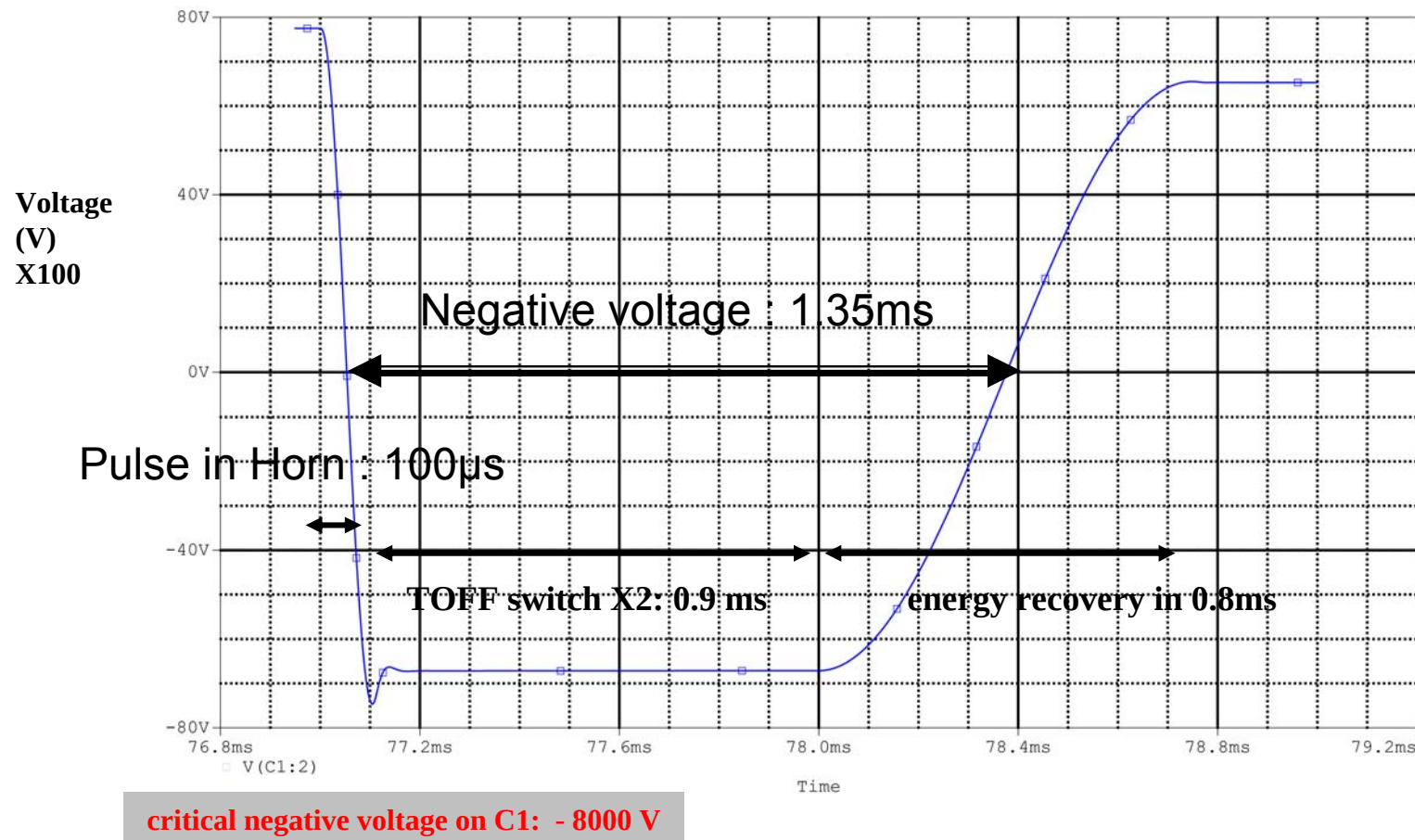
High current pulse power supply design

energy recovery with self : current in capacitor C1



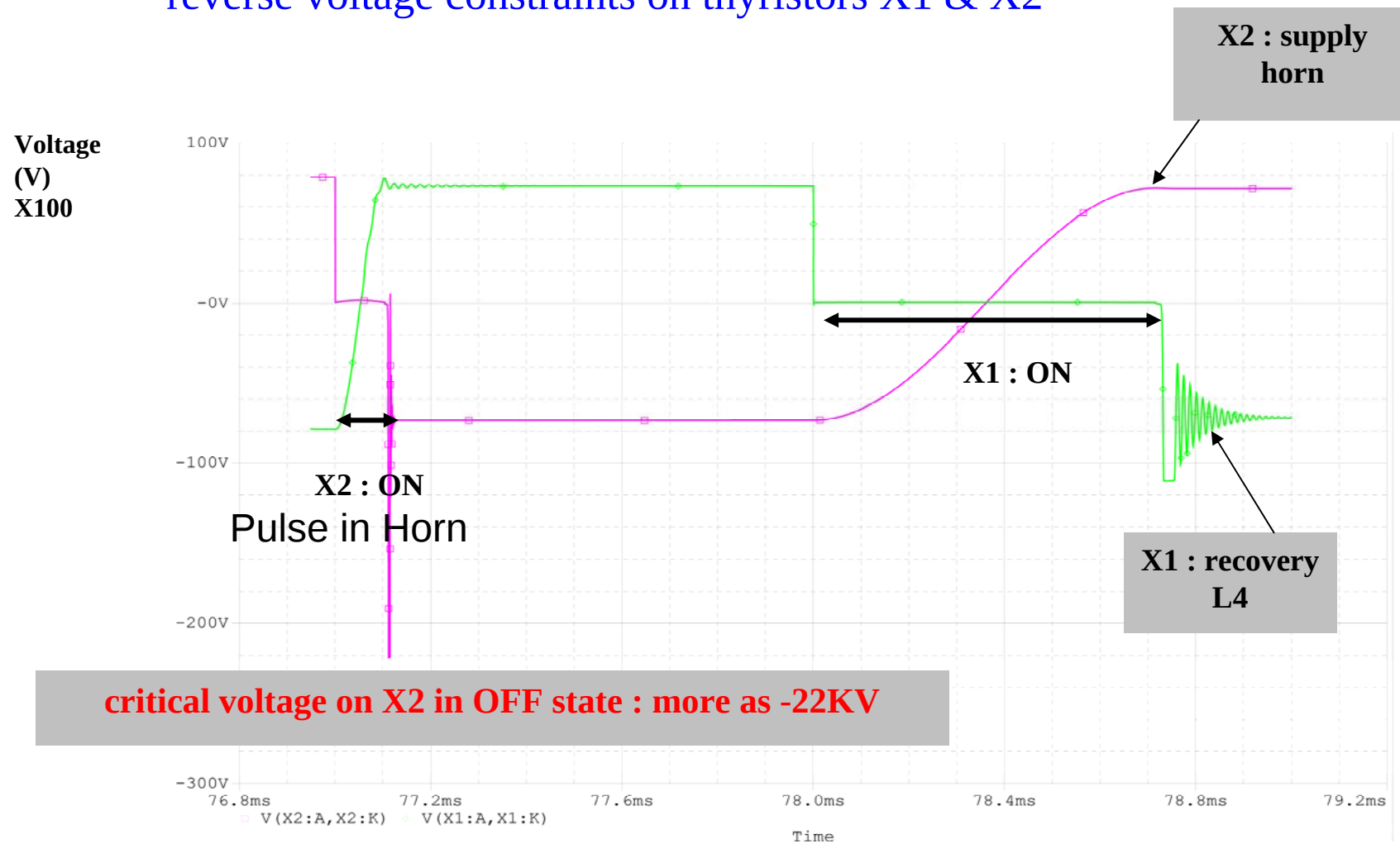
High current pulse power supply design

energy recovery with self :
critical constraints on capacitor C1



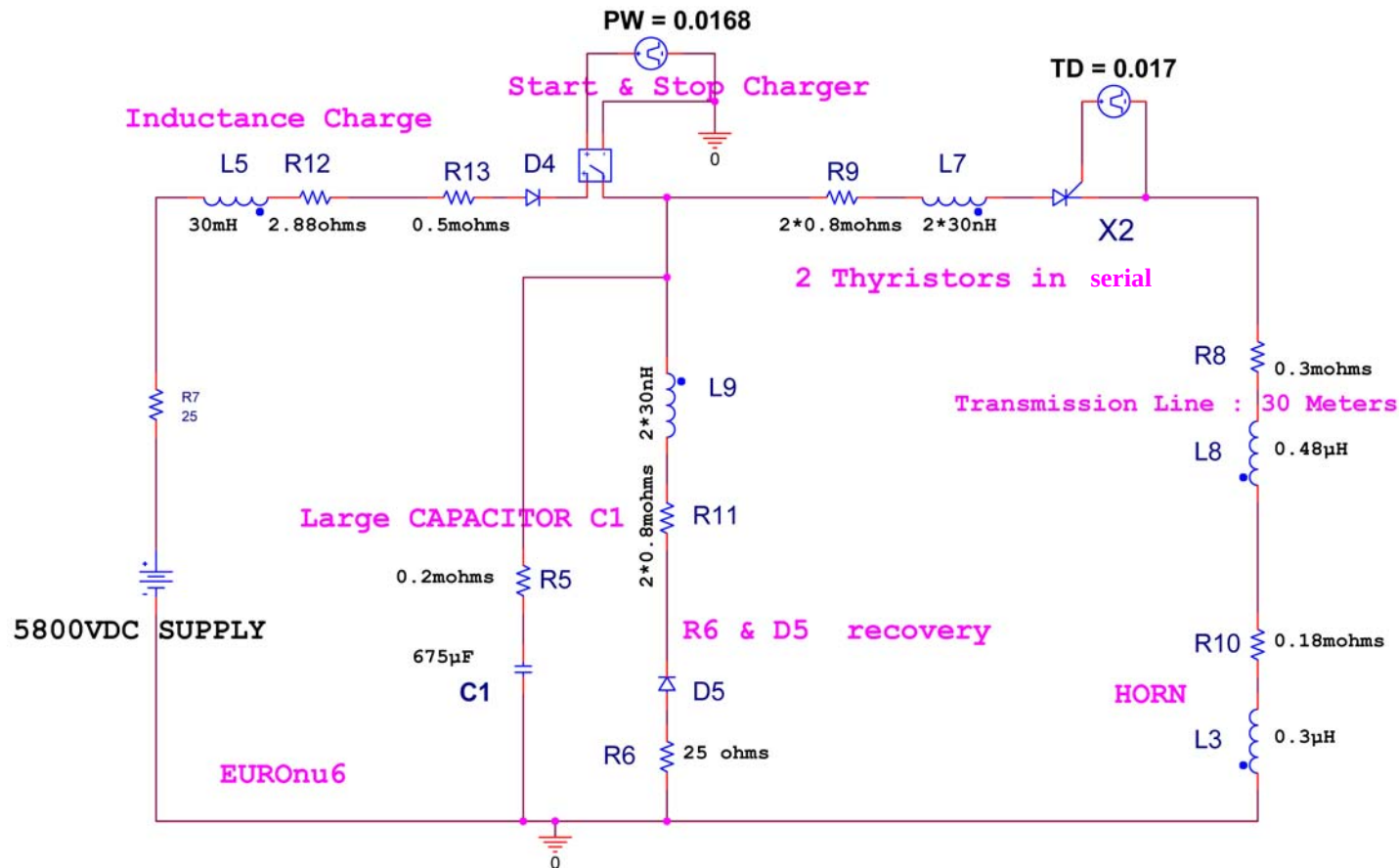
High current pulse power supply design

energy recovery with self :
reverse voltage constraints on thyristors X1 & X2



High current pulse power supply design

energy recovery with diode D5 and resistor R6

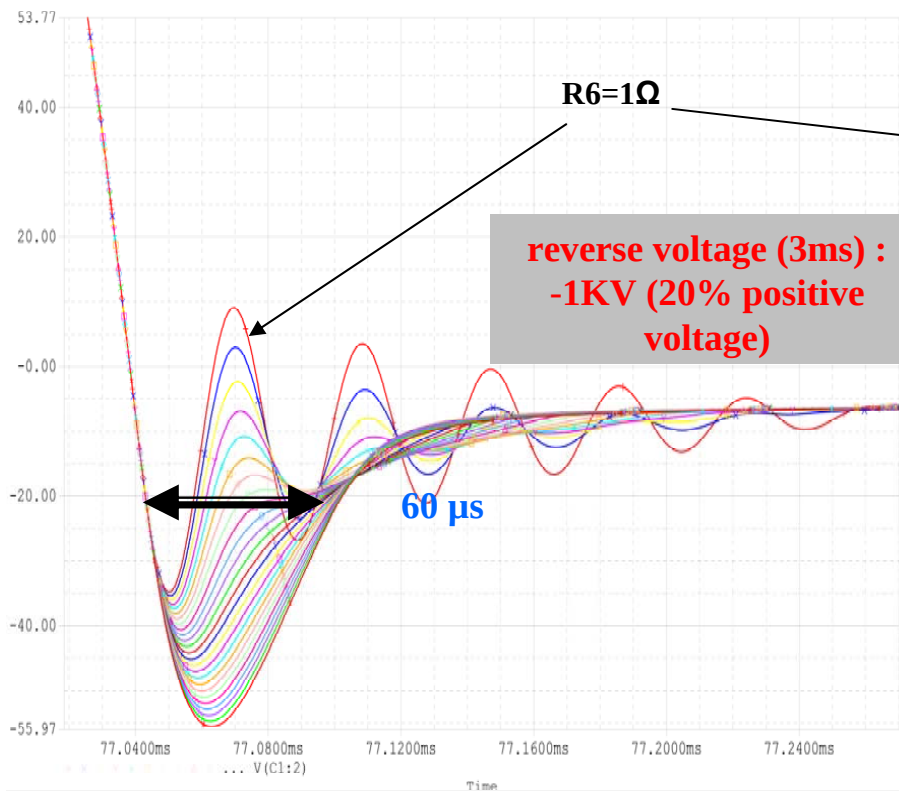


High current pulse power supply design

energy recovery with diode and resistor
(vs $R6 = 1$ to $25\ \Omega$)

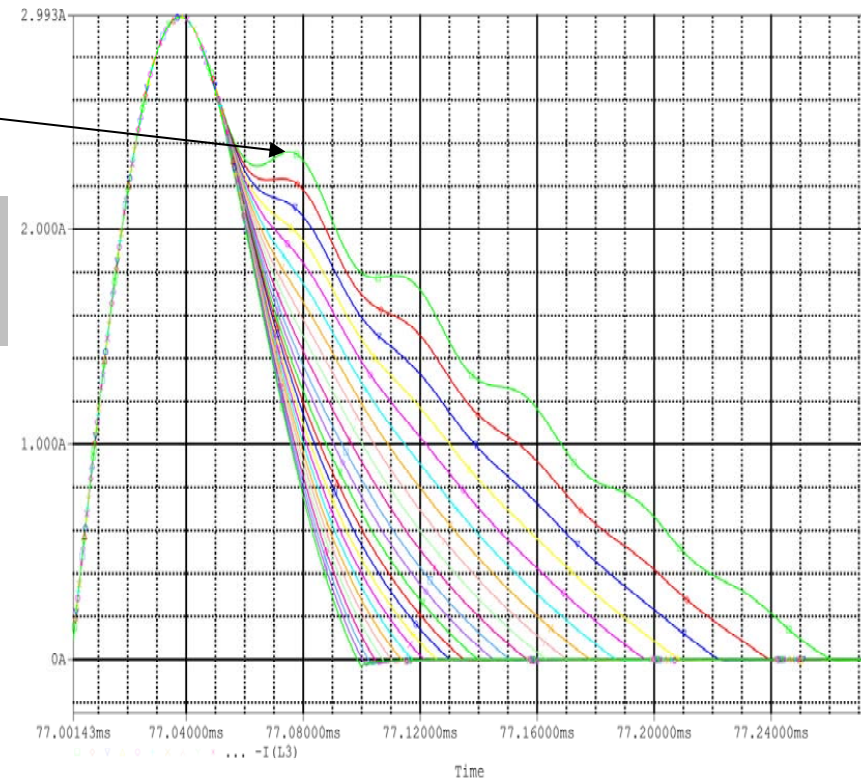
Voltage (V)
X100

Reverse voltage on capacitor C1



Current (A)
X100k

Current in horn



maxi reverse voltage (60μs) : -2KV to -5.5kV

High current pulse power supply design

energy recovery with diode and resistor

Critical reverse voltage
on switch X2 (supply horn)



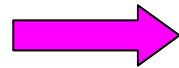
critical reverse voltage : - 3000 V

WORK PLANNING

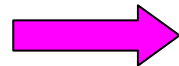
Comparison between 2 methods (recovery on L4 OR D5&R6)



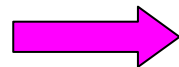
DEFINE LIMIT MODULE (ex 1000V-15kA)



respect critical limits characteristics of X2 and capacitor C1 (vs lifetime of $13 \cdot 10^9$ pulses)



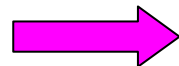
effect of SNUBBER on limitation of reverse voltage on X2 (and dV/dt)



thermal dissipation to evacuate



DEFINE POWER SUPPLY



electric consumption and thermal dissipation



COST of the 2 SOLUTIONS