



Superbeam target work at RAL

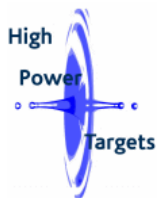
Work by:

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and Patrick Hurr (Fermilab)

Presented by Ottone Caretta

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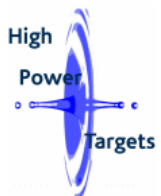
LBNE vs EUROnu

LBNE:

- 120Gev (or 60Gev)
- 0.7MW or 2.3MW (of which less than 10kW on target)
- rep rate ~1s
- beam sigma? $r/3$ seems roughly best for pion yield
- Target diameter 9 to 21 mm (~1m long)
- Materials: Be, Al, AlBeMet

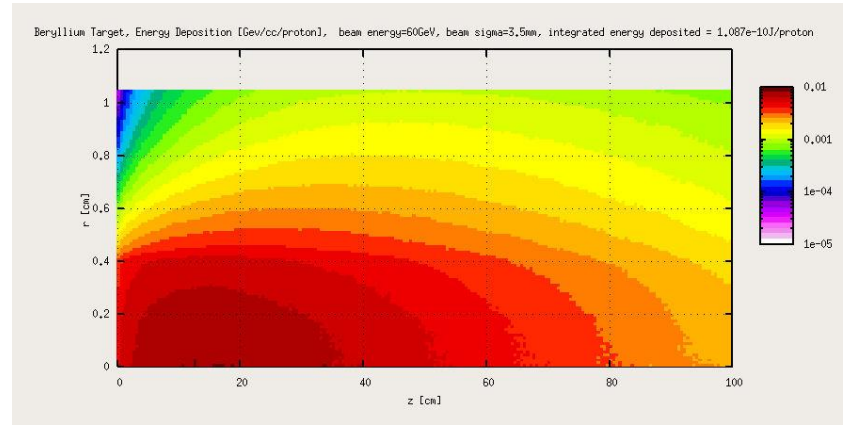
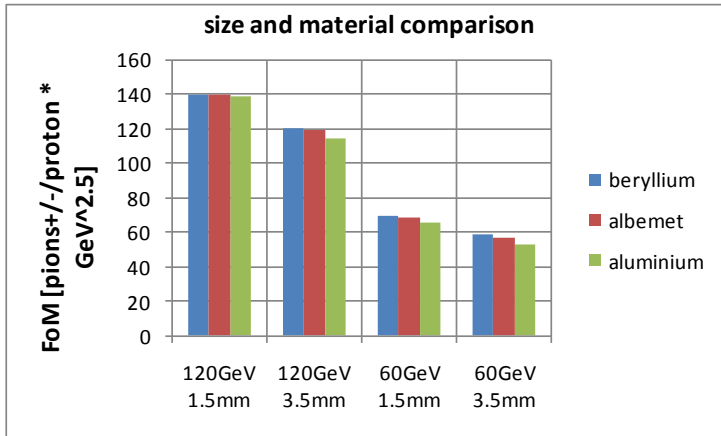
EUROnu SPL:

- 4.5GeV
- 1MW (of which 50kW on target)
- rep rate 12.5Hz
- beam sigma 4mm
- Target diameter 30mm (around 780mm long)
- Material: graphite

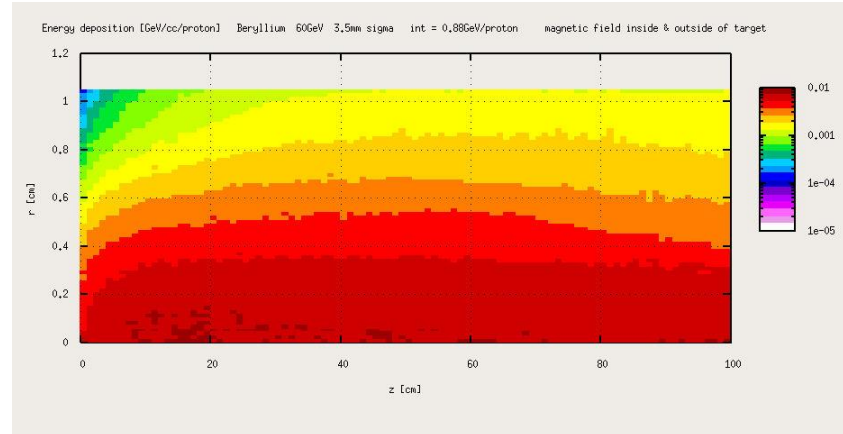
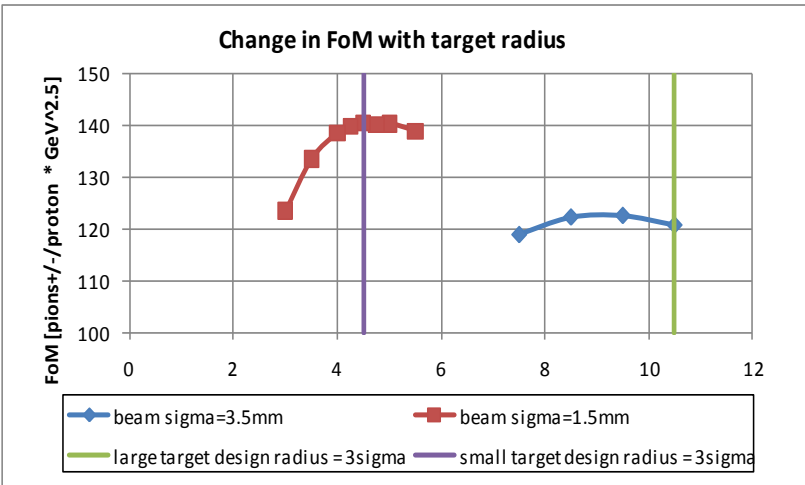


LBNE targets comparison: physics

$$FoM = \sum_{n=1}^{21} (Ecen_n)^{2.5} \int_{E_{min_n}}^{E_{max_n}} \int_0^{\Delta p} \frac{\partial^2 N}{\partial E \partial p} dp dE$$



Energy deposition in beryllium target with 60GeV 3.5mm sigma beam, Integrated energy deposition=16.9kJ/spill



Energy deposition in Beryllium target with 60GeV 3.5mm beam sigma with magnetic field, Integrated energy deposition=22.6kJ/spill



LBNE targets comparison: engineering

Table 3.5.1, beam heating parameter study results

Beryllium

Beam Energy (GeV)	Beam Power (MW)	Beam Sigma (mm)	Deposited Energy (kJ/spill)	Time Averaged Power (kW)	Peak Energy Density (J/cc/spill)	Max. ΔT per spill (K)	Max. Von-Mises Stress (MPa)
120	0.7	1.5	4.2	3.2	254	76	100
		3.5	9.2	6.9	74	22	27
60	0.7	1.5	2.9	3.8	243	73	99
		3.5	5.8	7.7	61	18	23
120	2.3	1.5	14.0	10.5	846	254	334
		3.5	30.7	23.1	245	74	88
60	2	1.5	8.4	11.1	707	212	288
		3.5	17.0	22.3	176	53	68

e.g. Static stresses are much higher in Al

AIBeMET

Beam Energy (GeV)	Beam Power (MW)	Beam Sigma (mm)	Deposited Energy (kJ/spill)	Time Averaged Power (kW)	Peak Energy Density (J/cc/spill)	Max. ΔT per spill (K)	Max. Von-Mises Stress (MPa)
120	0.7	1.5	6.2	4.7	321	98	105
		3.5	15.7	11.8	108	33	30
60	0.7	1.5	3.8	5.0	299	91	104
		3.5	8.6	11.3	77	23	25
120	2.3	1.5	20.6	15.5	1069	326	351
		3.5	52.5	39.5	359	110	101
60	2	1.5	11.0	14.5	869	265	302
		3.5	25.0	32.8	223	68	73

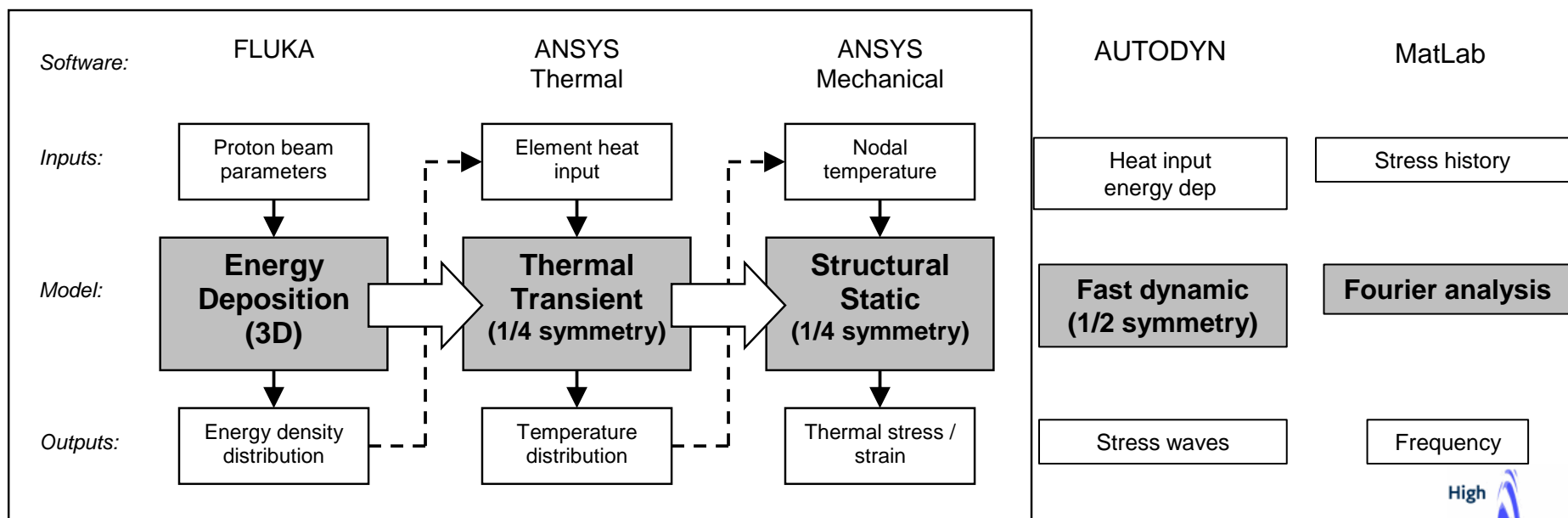
Aluminium

Beam Energy (GeV)	Beam Power (MW)	Beam Sigma (mm)	Deposited Energy (kJ/spill)	Time Averaged Power (kW)	Peak Energy Density (J/cc/spill)	Max. ΔT per spill (K)	Max. Von-Mises Stress (MPa)
120	0.7	1.5	12.2	9.2	537	221	158
		3.5	35.1	26.4	269	110	71
60	0.7	1.5	6.3	8.3	472	190	158
		3.5	16.6	21.8	155	60	43
120	2.3	1.5	40.8	30.7	1789	736	525
		3.5	117.1	88.1	898	365	236
60	2	1.5	18.2	24.0	1374	551	459
		3.5	48.2	63.4	451	175	124



Engineering Analysis Procedure

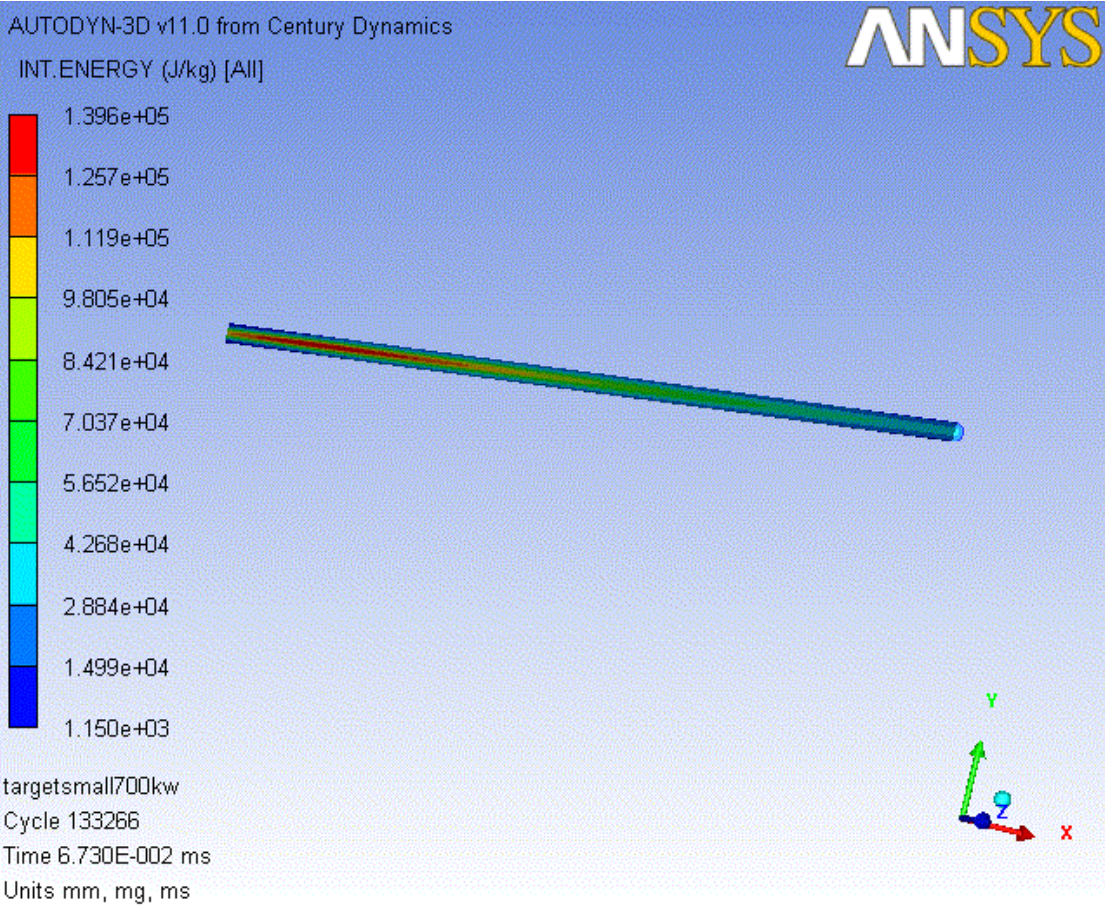
- Multi-stage process involving linked FLUKA, ANSYS and AUTODYN simulations
 - Can choose whether or not to include inertial effects. This enables one to isolate the consequences of various stress mechanisms:
 - “Quasi-static” thermal stress
[thermal conduction timescales of the order ~seconds]
 - Inertial stress due to bulk oscillations (“violin modes”)
[1st mode period typically of the order ~milliseconds]
 - Elastic stress wave propagation
[characteristic time period of the order ~microseconds]



Process flow diagram: beam induced heating



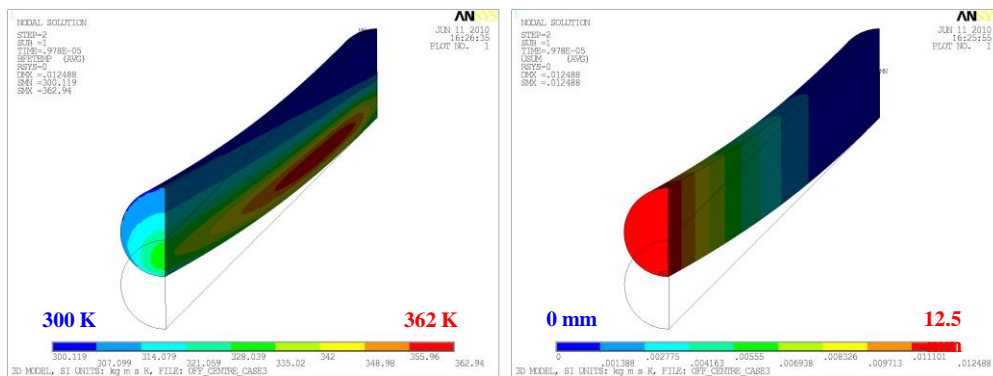
Drilling down on different effects: Static – dynamic – off-centre beam



Dynamic stresses can be as much as double the static ones and then grow by another 50% if off-centre beam effects are included



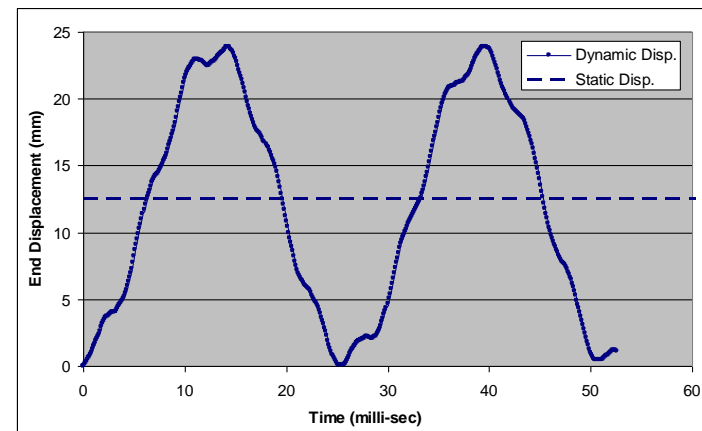
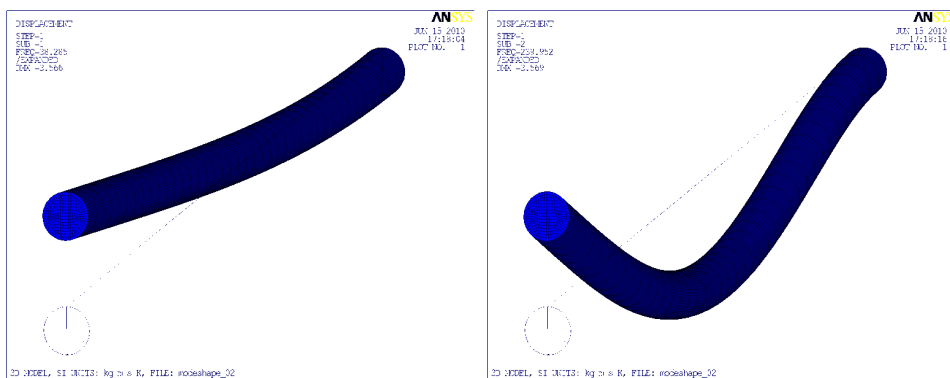
Worse case scenario: off-centre beam (not that uncommon?!) static stresses & resonance



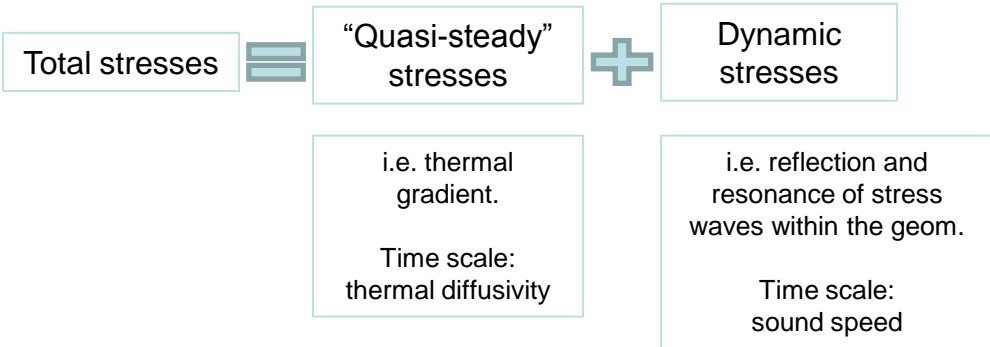
Off-centre effects include:

- thermal gradient (with associated residual stresses and deformation)
- Inertial stress waves and stress resonance

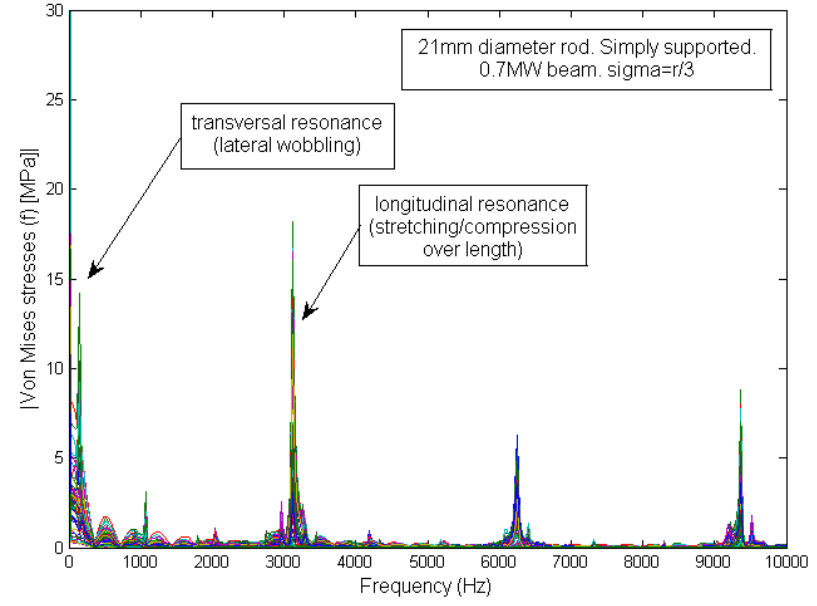
P Loveridge



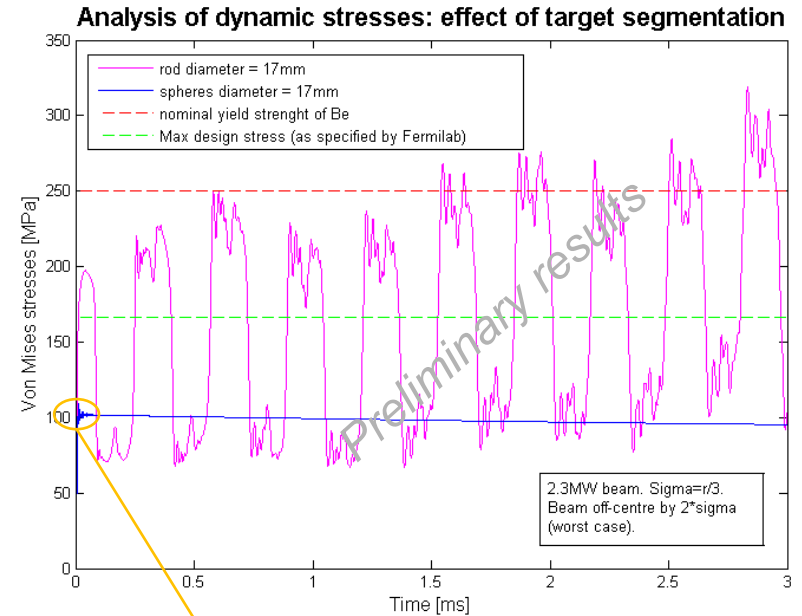
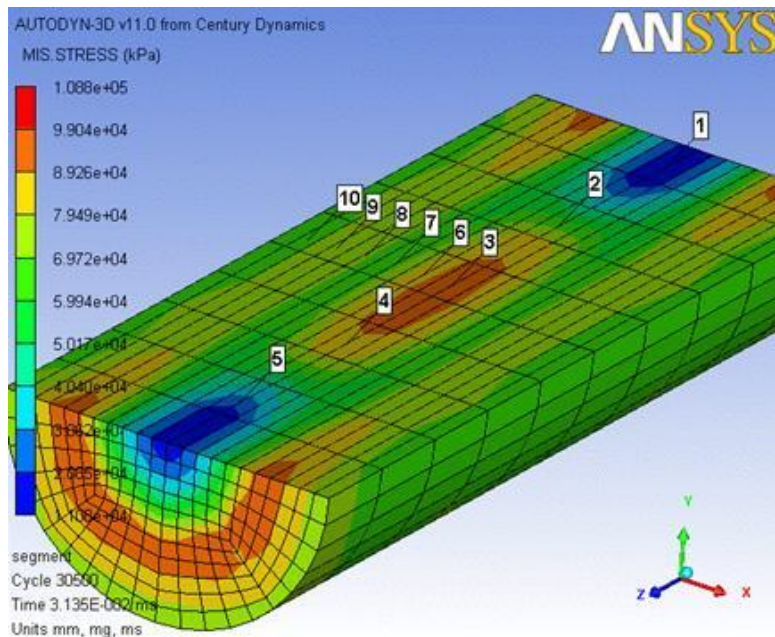
A look at dynamic stresses



Amplitude Spectrum analysis of Von Mises stress throughout the target rod

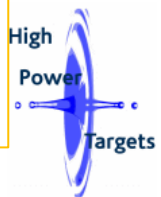


Target segmentation reduces the stresses



Segmentation of the target minimises the dynamic components quickly resolving to the “quasi-steady” stress field

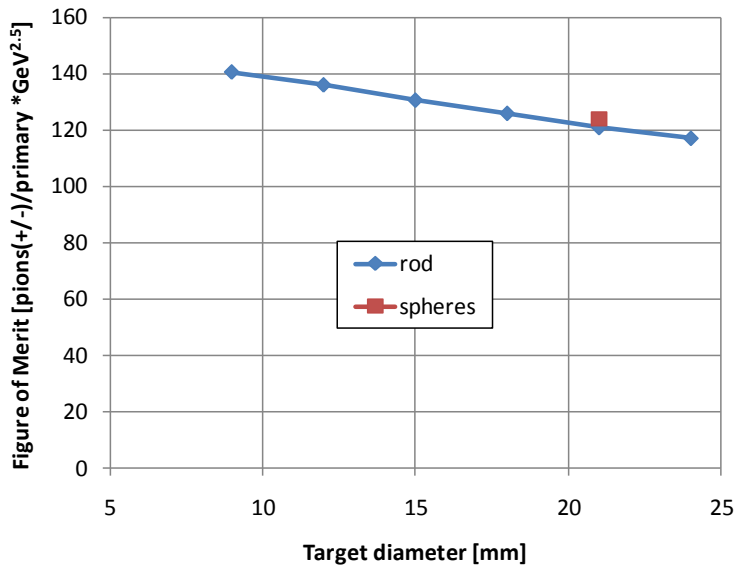
Avoiding sharp edges in the target geometry reduces both stress concentrations and constructive wave interference



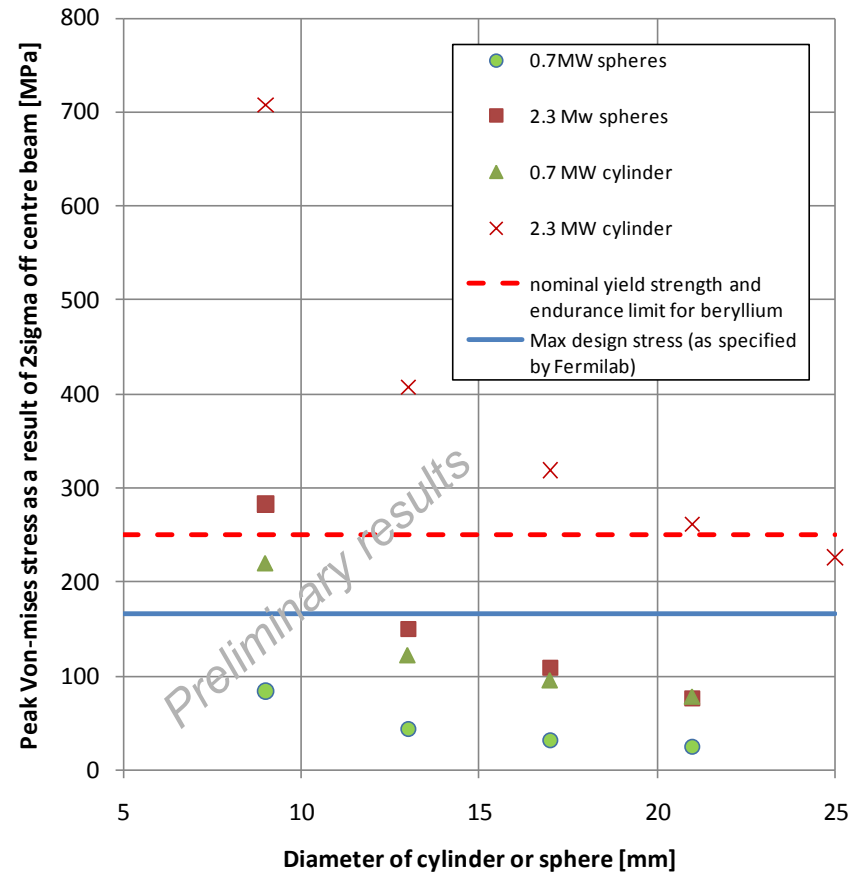
Stresses as a function of rod/spheres diameter

- Design Selection Parameters
 - Peak stress with off centre beam & FoM
- Design choice
 - Diameter & Shape (Rod vs Segments)

Figure of Merit as a function of target diameter (1 m long cylinders; $\sigma=r/3$)



Peak stress with off centre beam



1. Reducing target diameter gives better pion yield but more stress.
2. Beam induced dynamic stress in the form of longitudinal stress waves and from induced vibrations are significant in a beryllium rod ruling it out for 2.3 MW operation.
3. Segmenting the target (a series of spheres for example) has been identified as a potential option for achieving the desired diameter with reasonable stress levels.

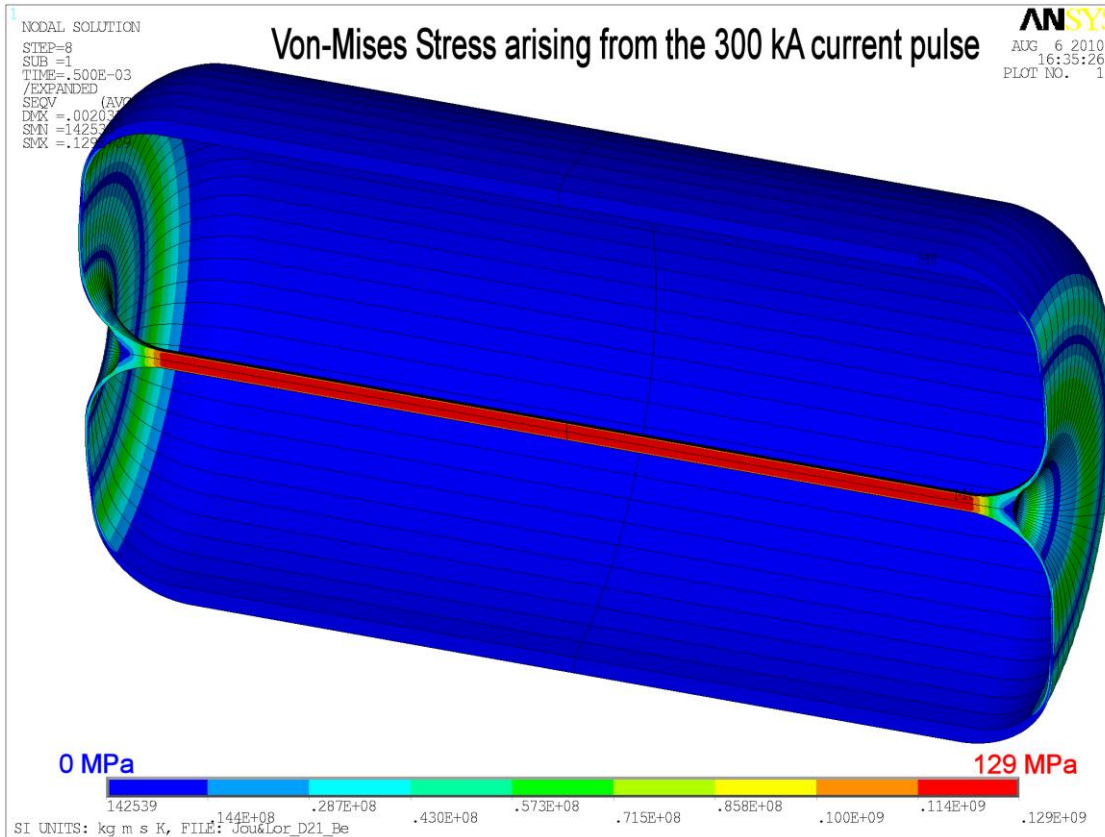
4. FoM is comparable between spheres and rod.

Ottone Caretta, Krakow, October 2010

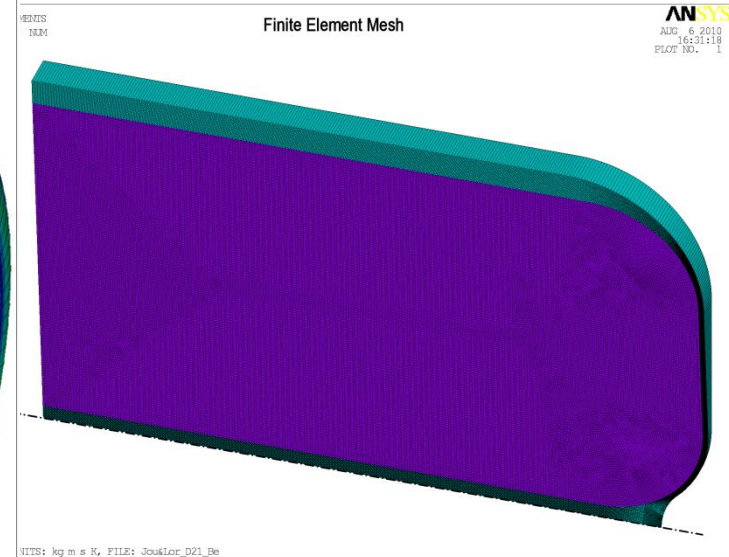


Progress on Combined target and horn concept

- Electromagnetic – Thermal – Structural modelling
 - Including the horn “end bells” allows the axial Lorentz forces transmitted by the inner conductor to be captured in the simulation

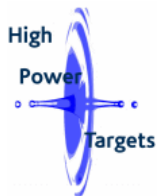


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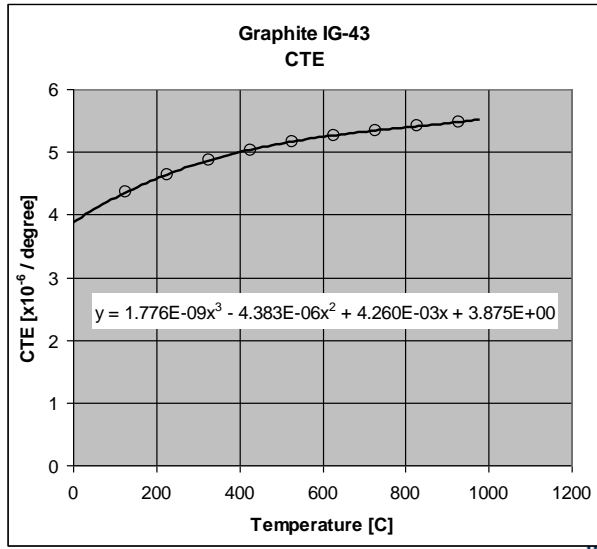
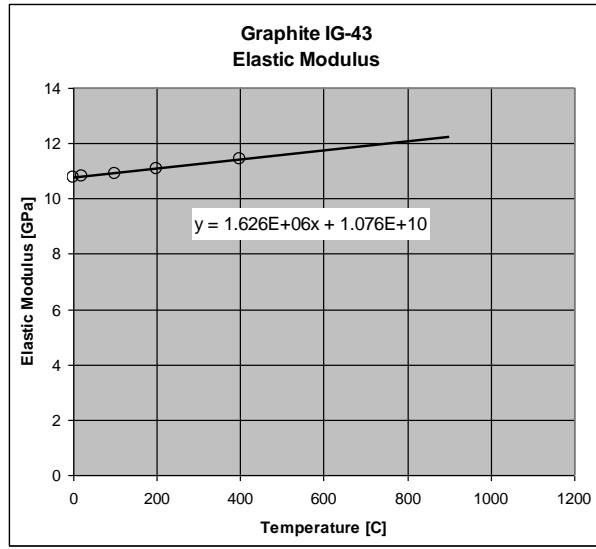
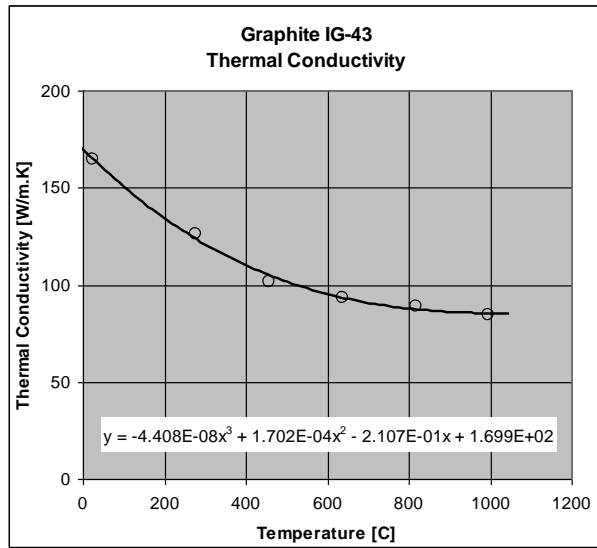
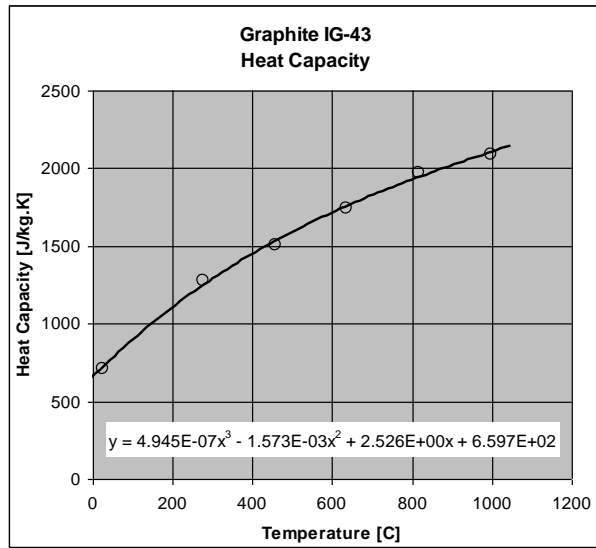
ANSYS model of the combined target / inner conductor concept.

Axial Lorentz forces induce a significant tensile stress component in the solid inner conductor.



Preliminary work on the EURONu-SPL baseline graphite rod

Temperature Dependent Properties of Graphite IG-43



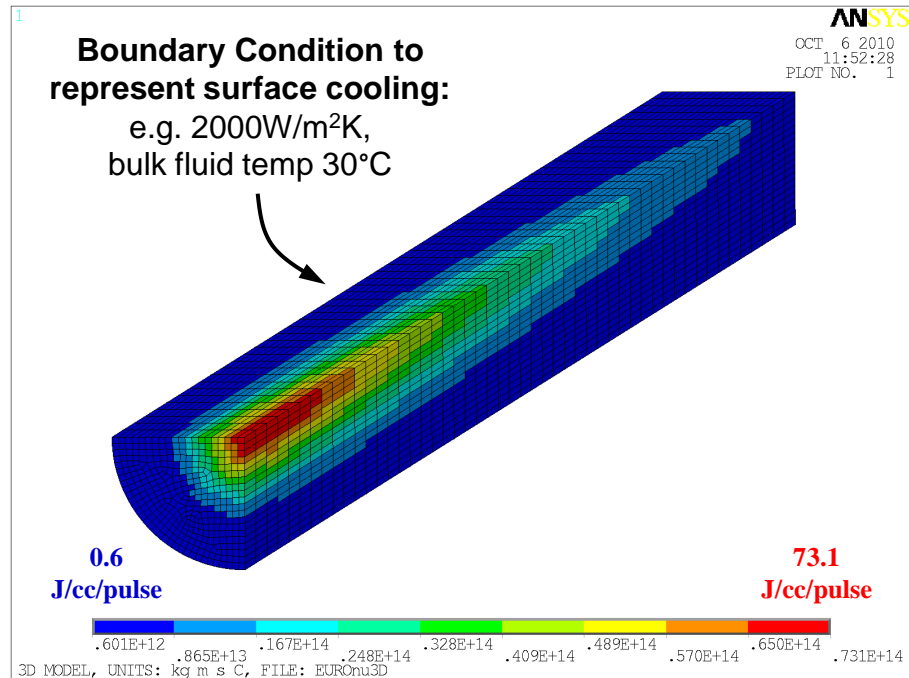
Beam Heating Model (ANSYS)

- 78 cm long, 3 cm diameter cylindrical graphite target
- $\frac{1}{4}$ symmetry 3D finite element model
- “Instantaneous” power density used as input heat load
- Convection heat transfer applied at outer surface

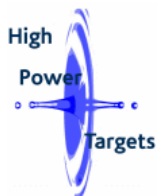
Integrated Energy Deposition:
4.1 kJ/pulse

Time averaged Power on Target:
4.1 kJ/pulse x 12.5 Hz = **51 kW**

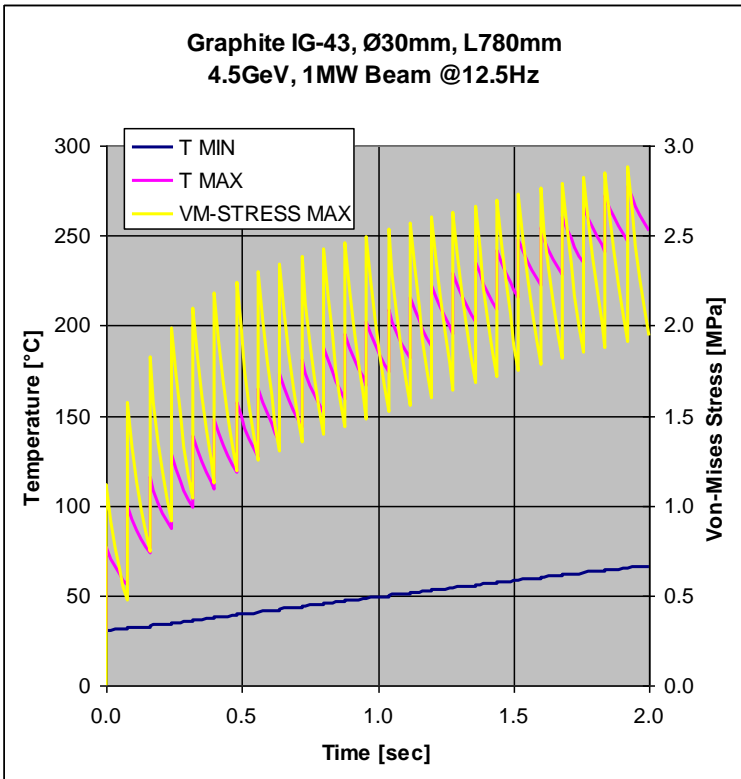
Peak Energy Density in Target:
73 J/cc/pulse



Beam Heat Load Input to ANSYS Thermal Simulation

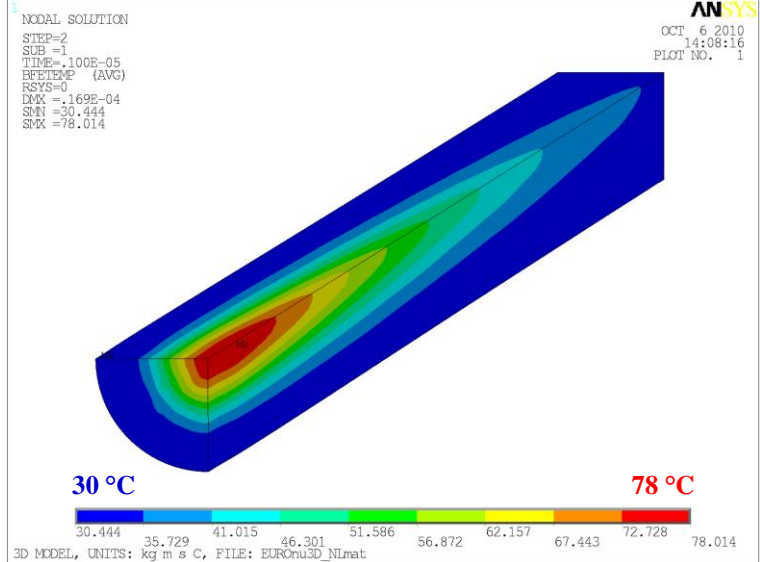


Transient Analysis Results (ANSYS)

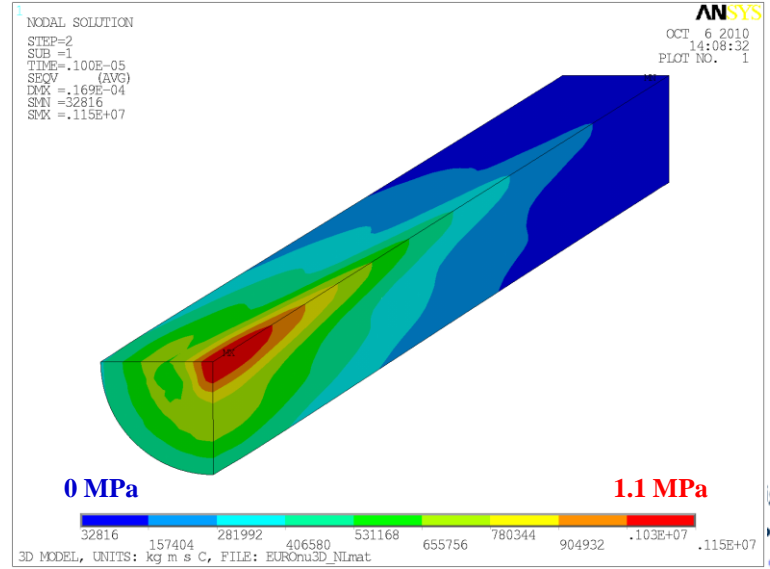


Transient Results Summary

- But many more pulses required to reach steady-state conditions...



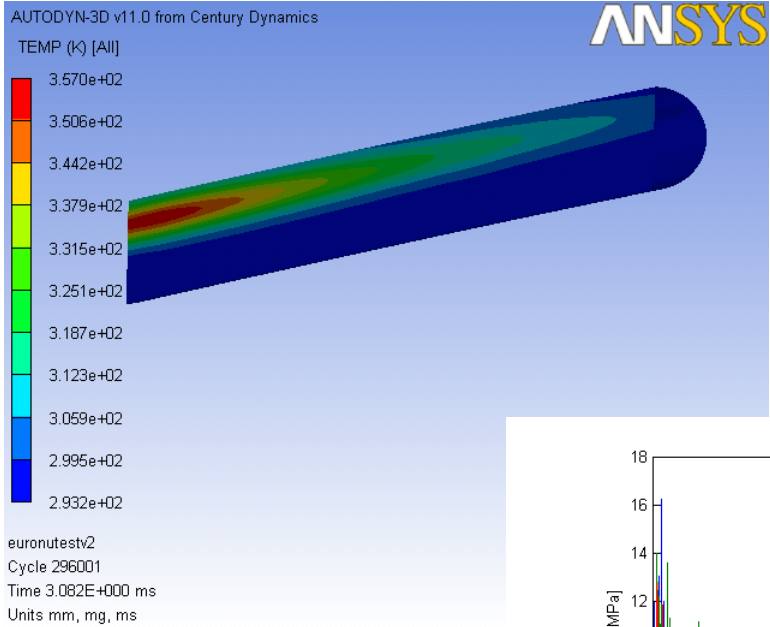
Temperature at End of 1st Pulse



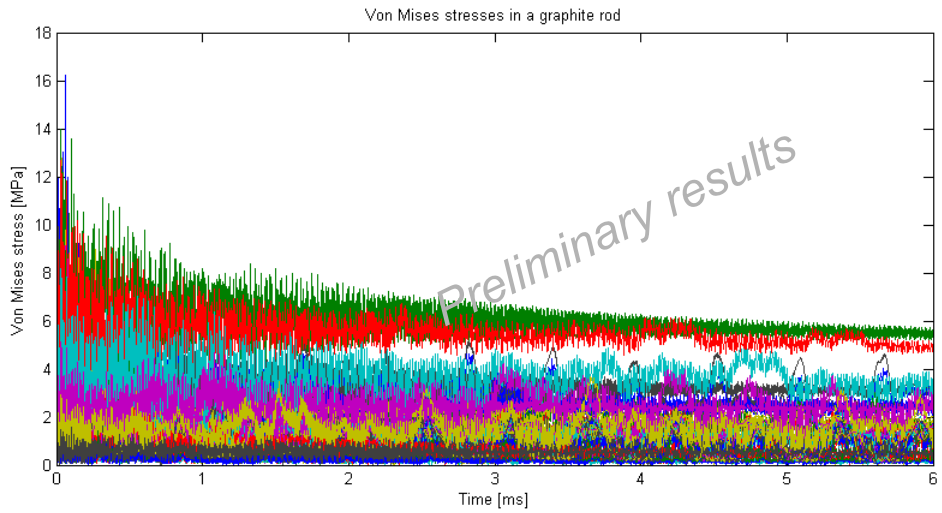
Von-Mises Stress at End of 1st Pulse



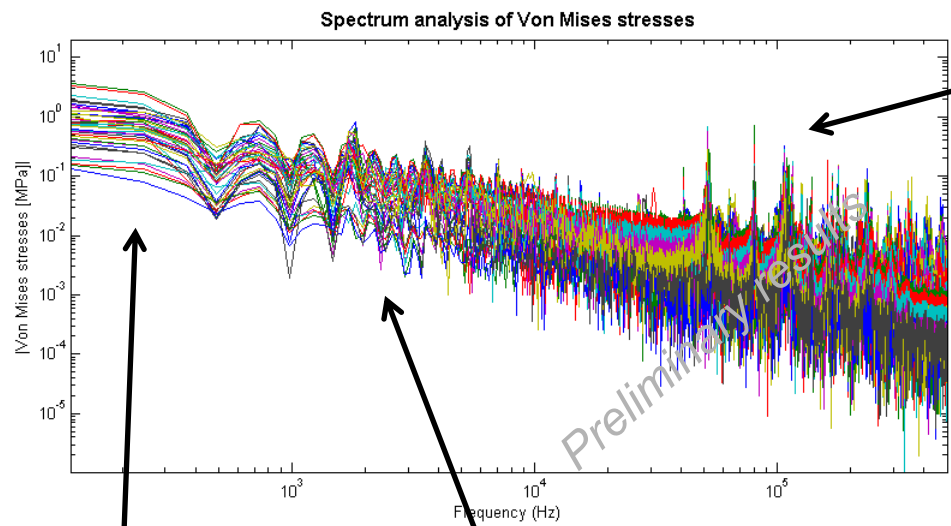
Preliminary analysis of dynamic stresses in a EUROnu SPL graphite rod



4.5 GeV beam. 4mm sigma. 1MW beam
30mm diameter rod. 11mm off-centre beam



Preliminary analysis of dynamic stresses in a EUROnu SPL graphite rod

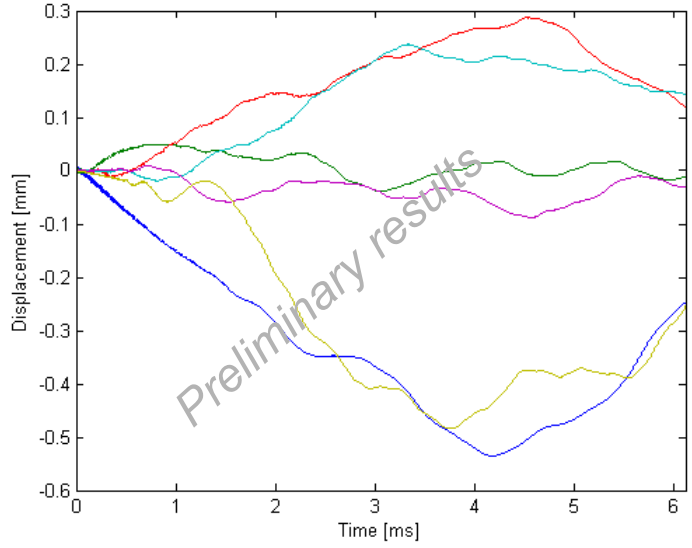


Transverse resonance
bowing

Longitudinal resonance
Stretching/compression over length

Radial resonance
Expansion/ contraction of radius

Y-Displacement (due to bowing) of gauge points along the graphite rod



Conclusions

- There is more to the target than just the physics e.g:
 - Structural integrity
 - Heat removal
 - Ancillaries such as support structure, cooling channels, etc (this also has an affects on the pion yield!)
 - Safety & chemical compatibility
 - Etc.
- Preliminary analysis indicates that the stresses in the EUROnu SPL baseline graphite rod for 1 bunch train look significant
- At high rep rate (12.5Hz) the effects of subsequent bunch trains may constructively interfere (quasi-static stresses, attenuation coefficient for stress waves?)
- Cooling will not be trivial: 50kW may not seem much but the surface area available for heat transfer is rather small!
- Segmentation of the target may help to reduce stresses (see LBNE example)
- Beryllium may be a better candidate material (e.g. Better yield strength)?

