



GroundBIRD: Preliminary Results on Polarization Angle Calibration with a Sparse Wire Grid

Miku Tsujii on behalf of the GroundBIRD collaboration

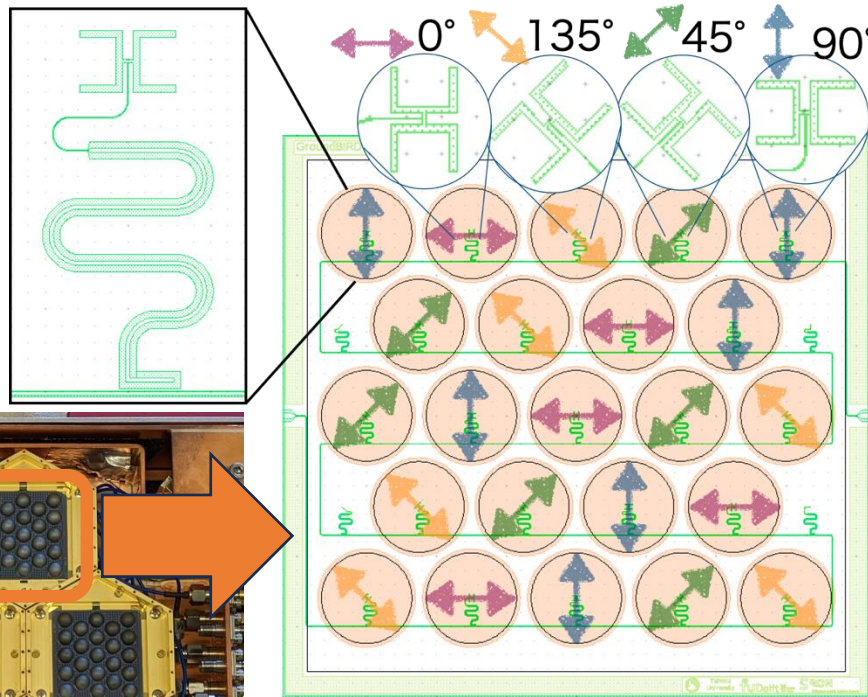
Outline

1. Detector design & calibration need
2. Choice of Calibration Method
3. Physics: how a wire generates polarization
4. Wire grid design
5. Preliminary results
6. Summary & next steps

Detector Design & Calibration Need

145 GHz 6 arrays $\times$ 23 kids, 220 GHz 1 array $\times$ 23 kids

Each detector has one of 4 antenna orientations: 0° / 45° / 90° / 135°



- The scan direction is aligned to the pixel arrangement (ref. Suzuki)
- Designed to sample all Stokes parameters across the focal plane
- Actual sky-projected angle can deviate from design due to instrumental and optical effects

→ **Polarization angle calibration is essential!**

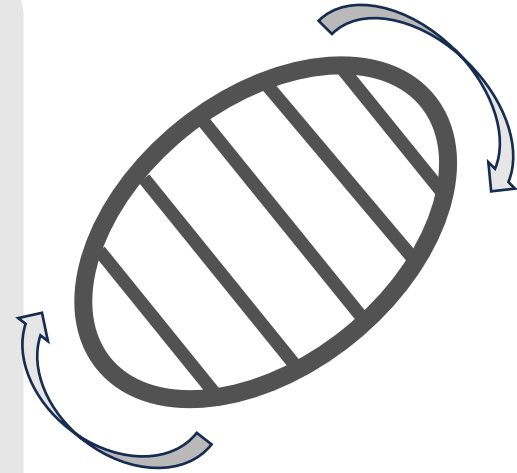
Choice of Calibration Method

Astronomical sources are difficult for GroundBIRD

- Tau A: wide beam $\rightarrow$ requires long integration time
- Moon: extended source, requires intensity correction

$\rightarrow$ **We use a sparse wire grid (SWG)**

- Metal wires spaced much wider than the observing wavelength
- An artificial source: usable anytime, with a proven track record



Target accuracy

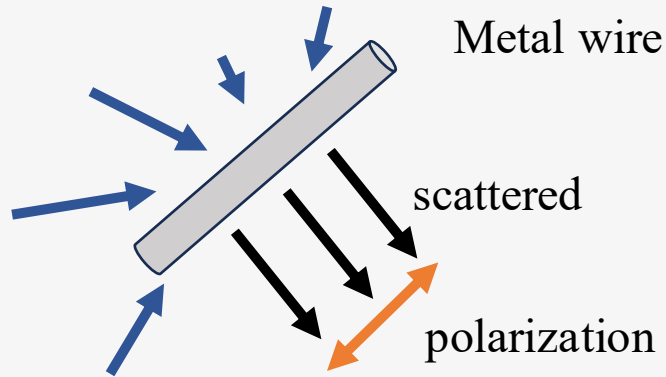
- We plan to do a joint analysis with QUIJOTE
- QUIJOTE's angle accuracy is $0.5^\circ - 0.96^\circ \rightarrow$ **Choose $0.5^\circ - 0.96^\circ$ as our target**

How a Wire Generates Polarization?

Polarization is generated along the wire direction

Wire scattering schematic

Ambient radiation



Light sources scattered by the wire

$\tau B(T = 300 \text{ K}) \sim B(T = 40 \text{ K})$:

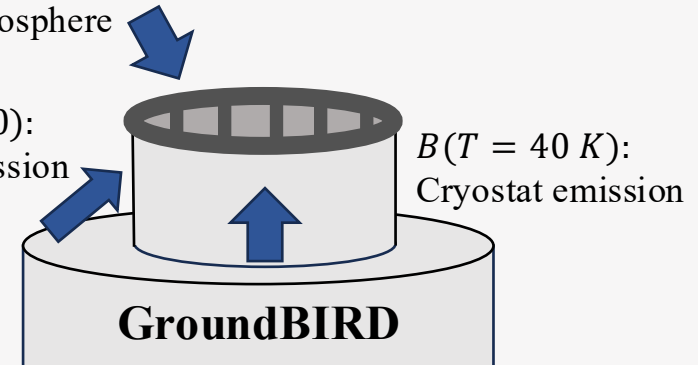
Thermal emission
from the atmosphere

$B(T = 300)$:

Baffle emission

$B(T = 40 \text{ K})$:

Cryostat emission



Overview

1. Ambient radiation is scattered along the wire axis
 - Wire-perpendicular component: transmitted light, from the atmosphere
 - Wire-parallel component: scattered light, mostly from sources warmer than the atmosphere (e.g. baffle)
 - polarized along the wire
2. Rotating the wire within the field of view modulates the detected polarization signal
3. Fit the modulation → recover detector sensitivity angle

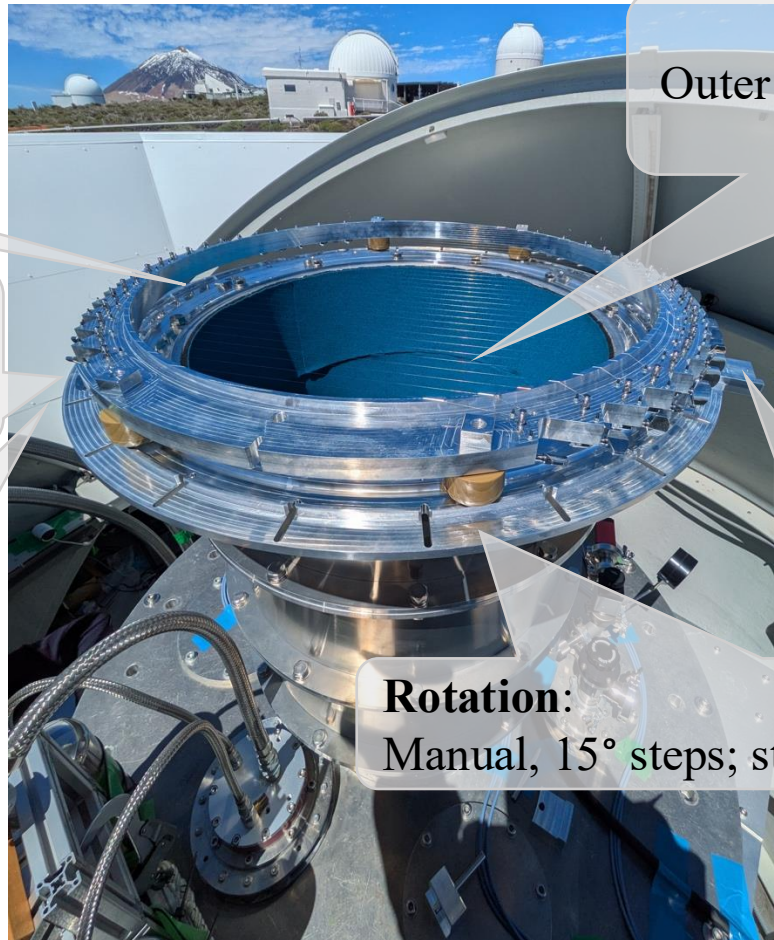
Wire grid design

Wire grid — overview

Wires: 39 × tungsten,
ø0.3 mm, 15 mm pitch

Tensioning
: Guitar pegs (one side)
+ bead stopper (other)

Tension control:
chromatic tuner



Frame:
Outer ø700 mm / inner ø600 mm
(A5052 Al)

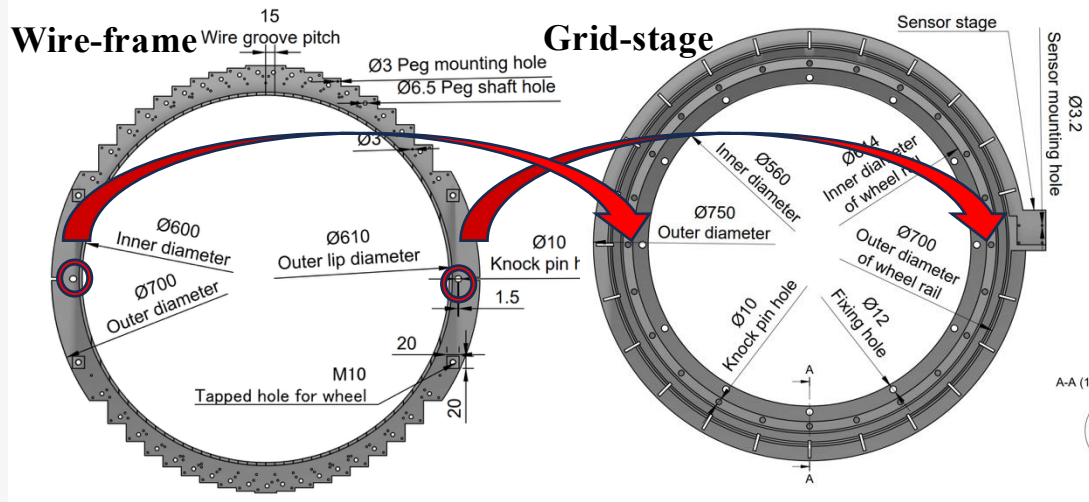
Angle sensor:
Gravity sensor →
absolute wire angle

Rotation:
Manual, 15° steps; stage + wheels + knock pins

Combined instrumental angular uncertainty: $\sim 0.31^\circ$

Wire Grid — Design Details

Wire-frame & grid-stage drawings



Rotate the wire-frame by hand.

- Two knock pins engage with the stage holes to lock the rotation angle.

Wires: 39 × tungsten, 15 mm pitch

- Pitch $\gg$ wavelength
→ keeps wires "sparse"
 - Smaller pitch → more wires
→ stronger signal
- 15 mm pitch: a balance between these two

Wire attachment

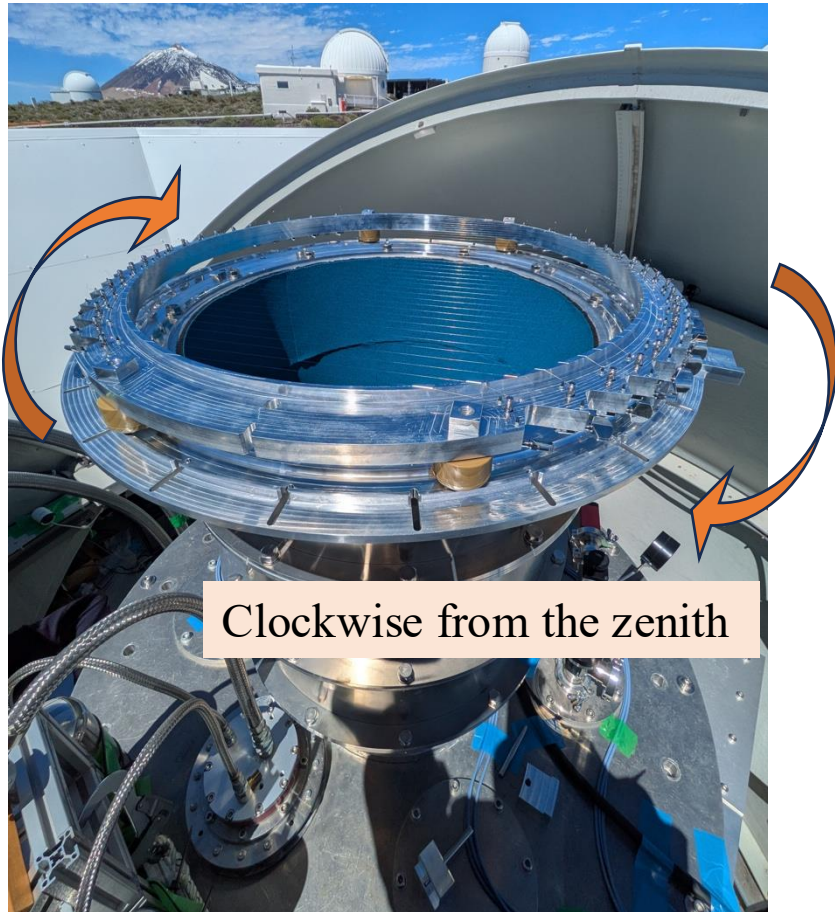
Keep the wires straight and field-serviceable by a single person

→ Guitar pegs+ bead stopper



Preliminary results

Measurement Procedure



Observation sequence

- 01 Point telescope to zenith and keep it fixed
- 02 Mount wire grid on aperture
- 03 Rotate the wire grid by hand in $30^\circ (= \Delta\theta)$ steps, clockwise from the zenith
- 04 Lock each step using the knock pins, which fix the relative rotation angle
- 05 At each angle, hold the wire grid still and record detector data (stare-mode)
- 06 Repeat for all steps to cover a full 360° rotation (~ 12 positions, ~ 1 min per step)

Analysis Pipeline

1

Select range

Manually select time segments with shadows excluded and low noise

2

Median per angle

Compute median detector output at each wire rotation angle

3

Initial fit

Fit with the model using weighted least squares to obtain initial $\{a, p, b, c\}$

4

Common-mode noise subtraction

Group detectors by angle ($0^\circ/45^\circ/90^\circ/135^\circ$)
Estimate & subtract shared noise $C(\theta)$

5

Re-fit & iterate

Repeat steps 3–4 until convergence
→ final amplitude a and sensitivity angle p

Fitting model

$$y(\theta) = a \sin\left(\frac{2(\theta - p)}{180} \pi\right) + \underline{b + c\theta}$$

linear baseline for drifts during observation (e.g., thermal fluctuations)

Parameter	Description	Constraint
a	Amplitude	$a \geq 0$
p	Detector angle (phase offset) [deg]	none
b	Constant baseline	none
c	Linear drift coefficient	none
θ	Wire grid angle	

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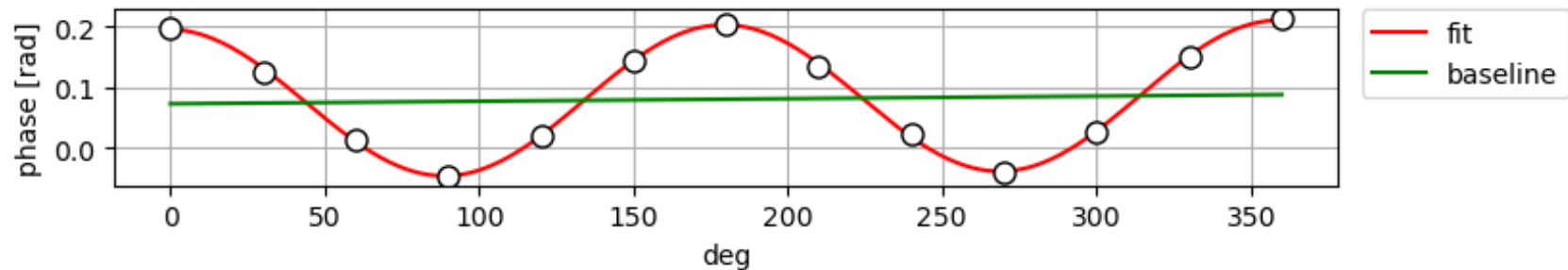
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Wire grid angle



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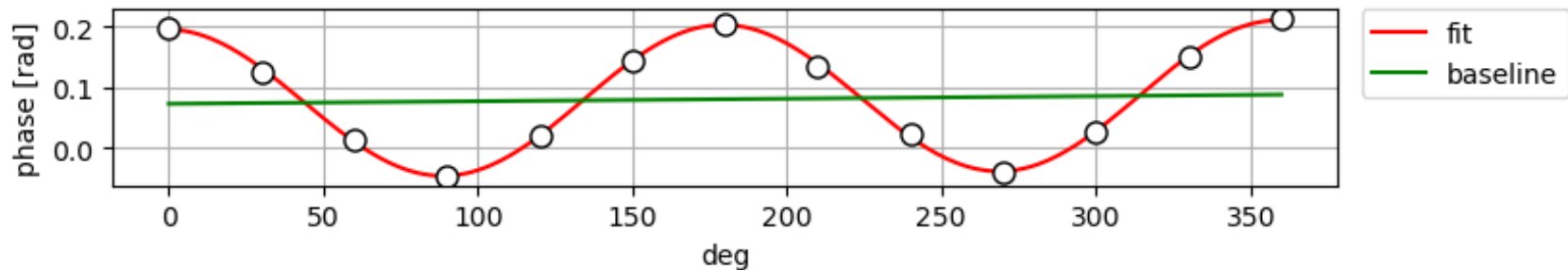
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Wire grid angle



Common-Mode Noise: Definition and Example

How common-mode noise $C(\theta)$ is estimated from the residuals:

$$r_k(\theta) = \frac{y_k(\theta) - \text{fit}_k(\theta)}{a_k} = C(\theta) + \epsilon_k(\theta)$$

Common-mode noise source image



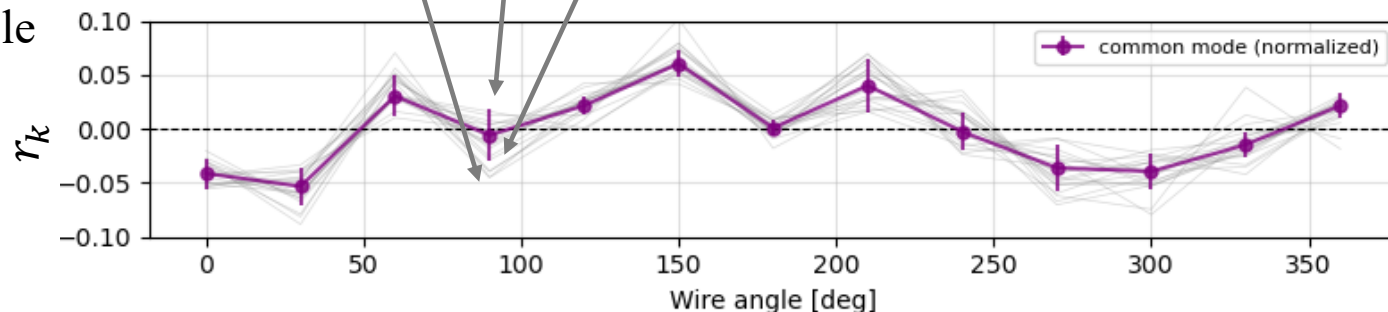
Common-mode noise $C(\theta)$

- Shared by all detectors at wire angle θ
- From common effects (e.g. atmosphere)

Detector-specific noise $\epsilon_k(\theta)$

- Residuals different for each kid

Example

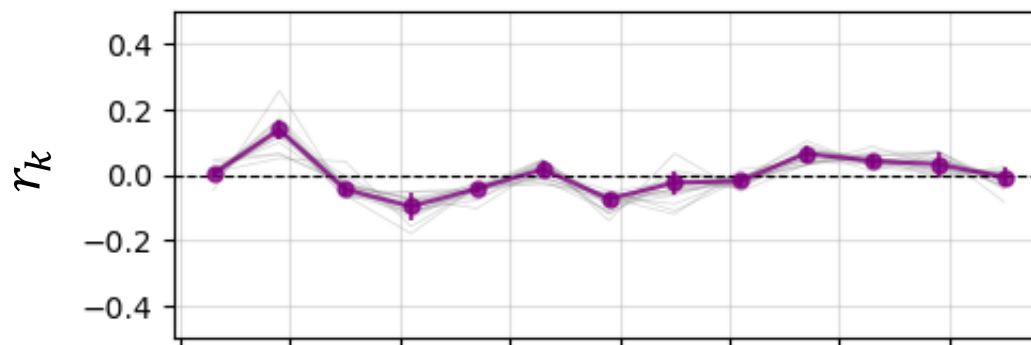


Preliminary Results — Common-Mode Noise vs. Atmospheric Conditions

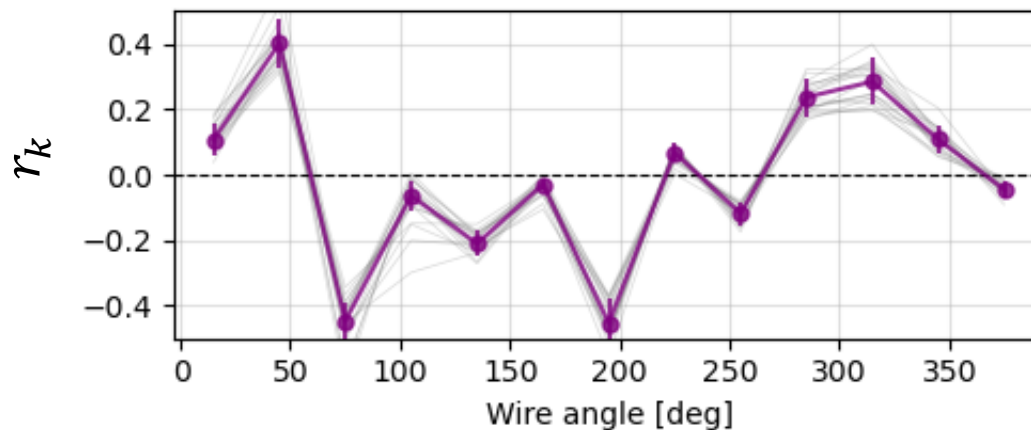
The 220 GHz common mode is visibly larger than the 145 GHz common mode

2026-05-16, ~04:00 UTC, PWV:~3.2 [mm]

common mode at
145 GHz



common mode at
220 GHz

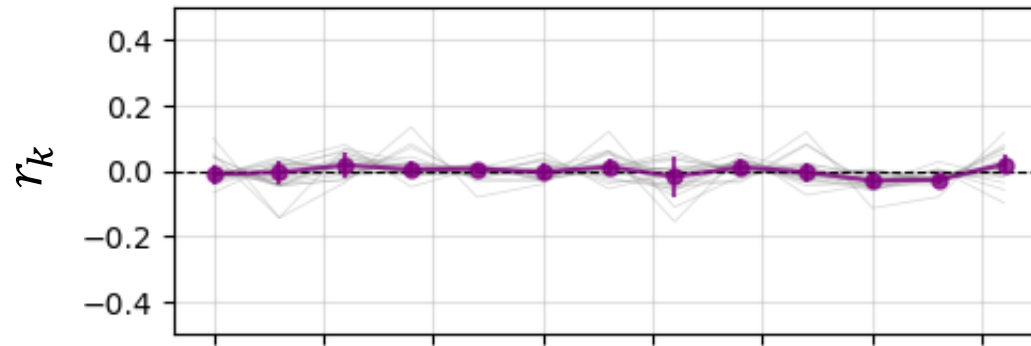


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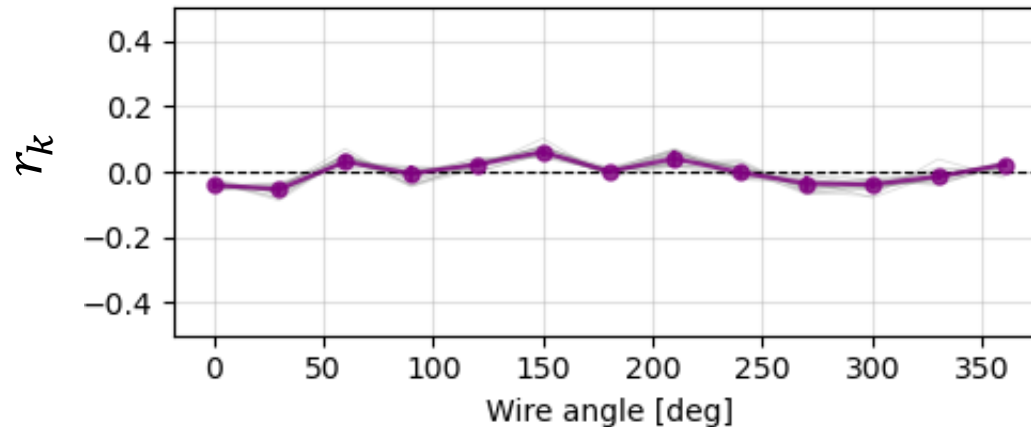
Under good atmospheric conditions, the common-mode noise amplitude is small

2026-05-09, ~05:00 UTC, PWV: 0.3~2 [mm]

common mode at
145 GHz



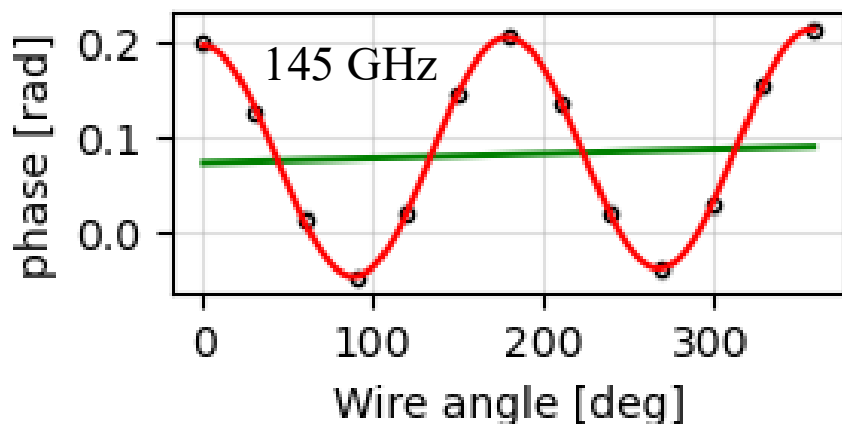
common mode at
220 GHz



→ At 145 GHz, it is small enough to be buried in individual detector noise, with no clear common pattern.

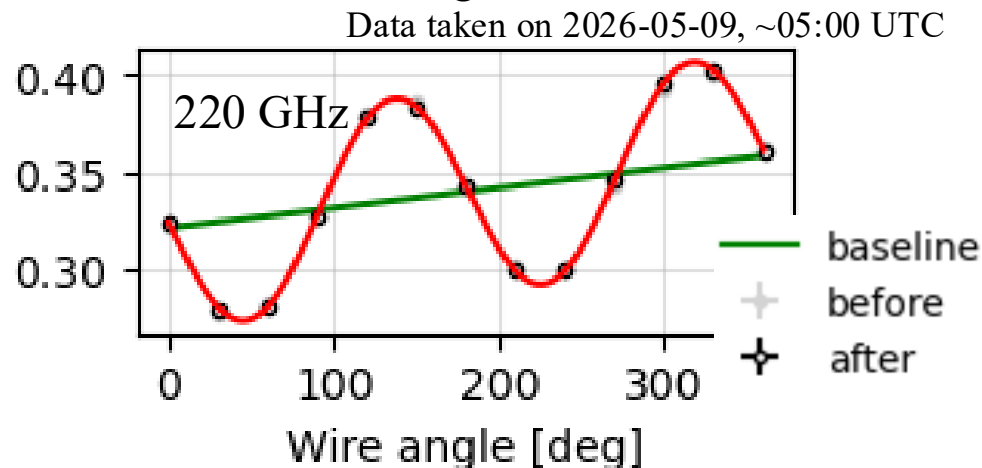
Preliminary Results — Fit Examples (145 & 220 GHz)

Example detector fits show clear periodic modulation with wire angle



Before CMN subtraction (initial fit)

	p	$\tilde{\chi}^2$
145 GHz detector	133.98 ± 0.13	10.2
220 GHz detector	91.57 ± 0.21	4.9



After CMN subtraction (converged)

	p	$\tilde{\chi}^2$
145 GHz detector	133.92 ± 0.18	2.0
220 GHz detector	91.59 ± 0.22	0.5

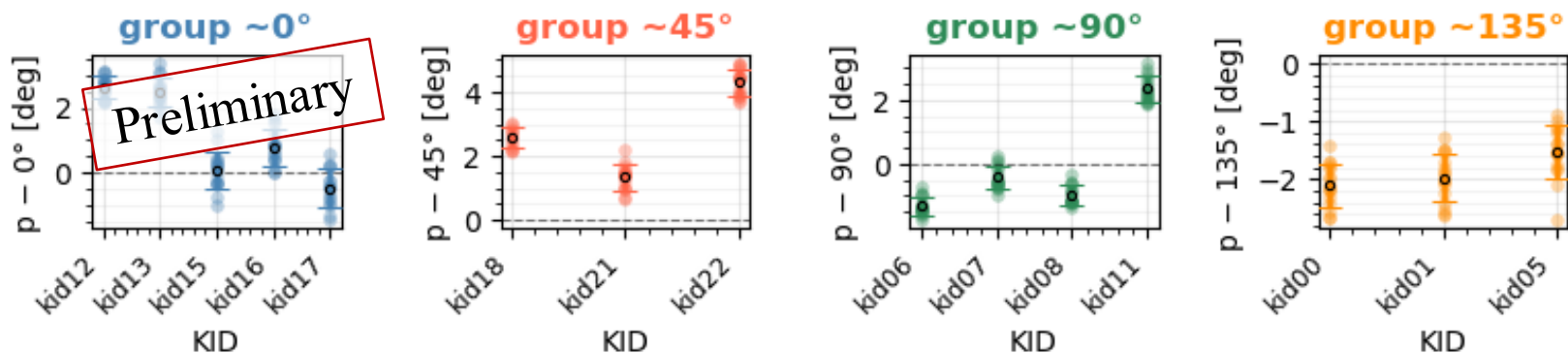
- p remains stable before and after subtraction
- $\tilde{\chi}^2$ drops confirming noise removal

Preliminary Results — Per-Detector Angle Distribution

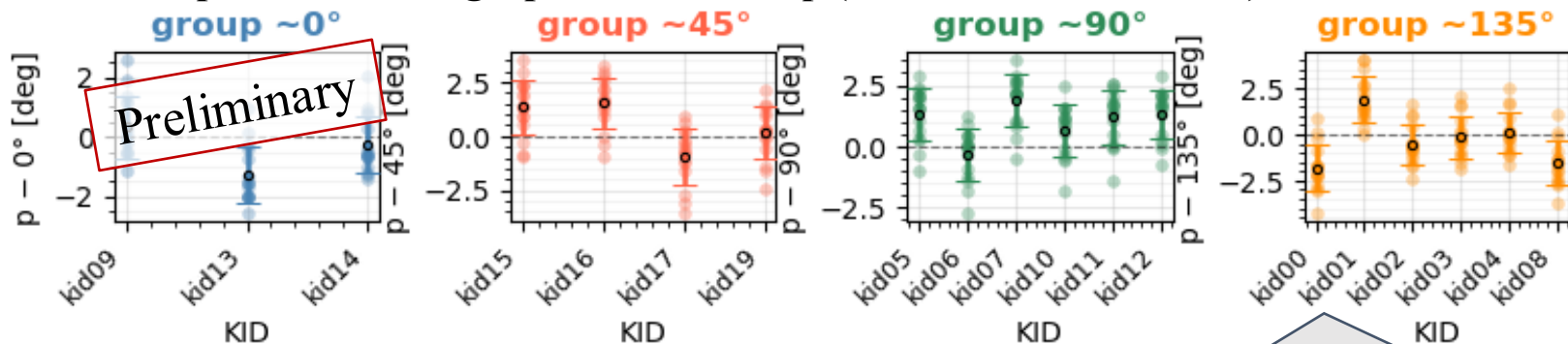
Per-KID polarization angle p , grouped by design angle.

Error bars ($\pm$ SD) show the spread across multiple measurements.

Per-KID polarization angle p -145 GHz chip (with CMN subtraction)



Per-KID polarization angle p - 220 GHz chip (with CMN subtraction)

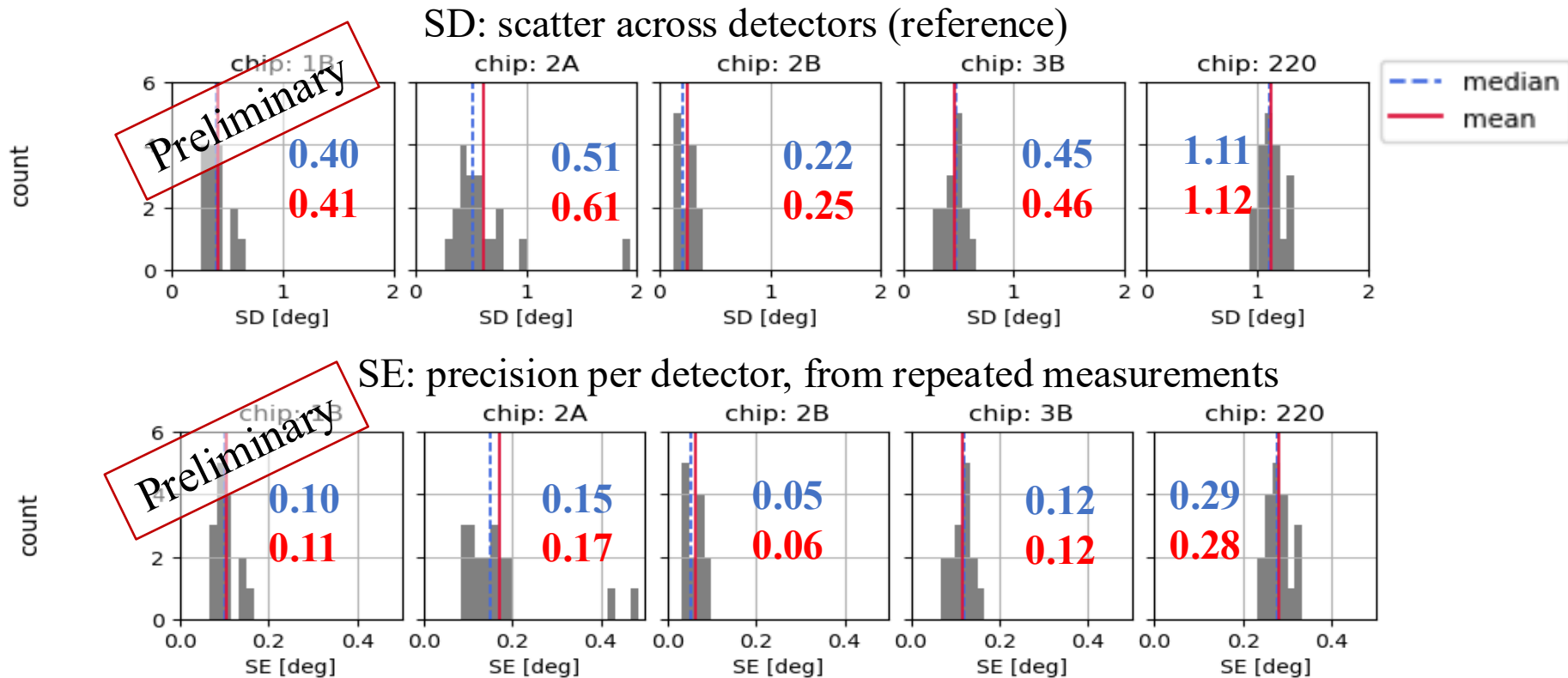


Each detector clusters around a consistent value

Data period: May 7–9, 2026
(PWV: 0–3.5 mm; not available on May 7)

Per-Detector Precision: SD and SE by Chip

Per-detector SD and SE, by chip $\left\{ \begin{array}{l} \bullet \text{ SD reflects detector-to-detector scatter} \\ \bullet \text{ SE reflects the precision from repeated measurements} \end{array} \right.$



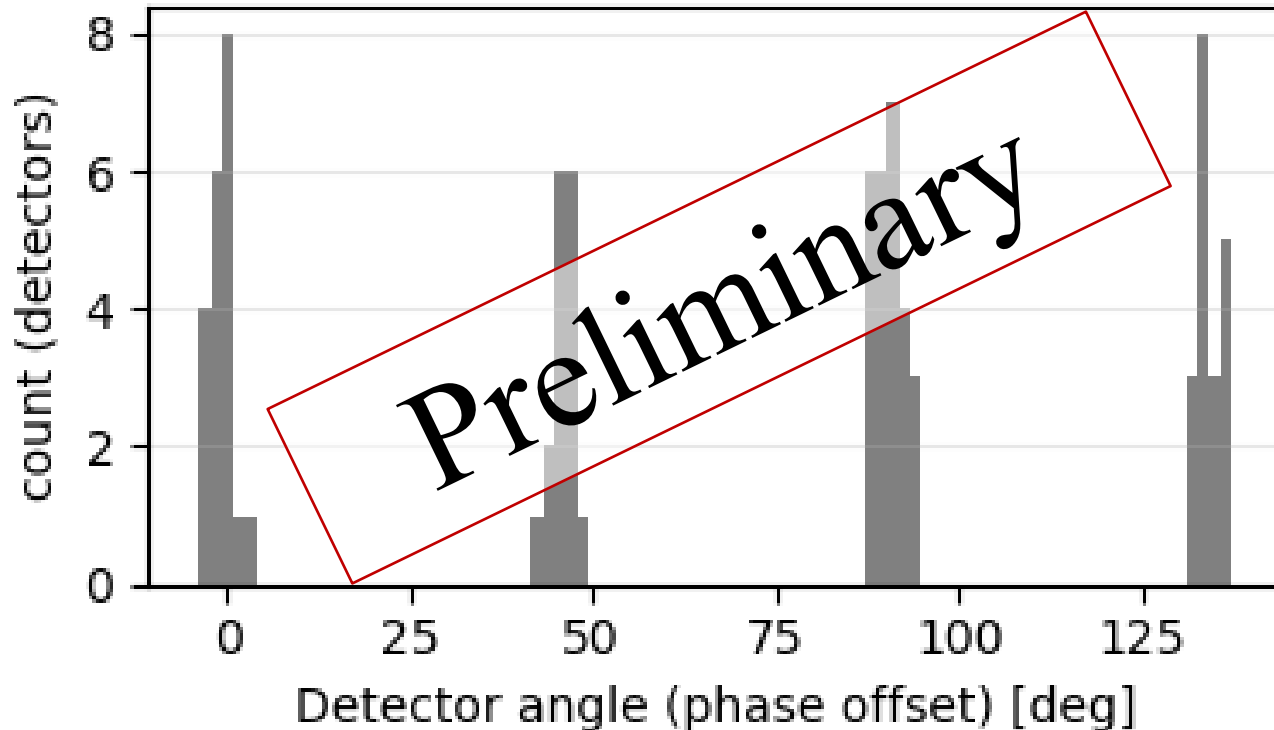
SE is expected to shrink as more measurements accumulate

→ Precision will improve with more statistics

→ Our preliminary results indicate that the $0.5^\circ - 0.96^\circ$ target accuracy is within reach

All Detectors Resolve into Four Design Angles

Distribution of fitted sensitivity angles p , all chips combined



The four design orientations (0° / 45° / 90° / 135°) are clearly separated

Summary & Next steps

• What was achieved

- Designed, built, and operated a sparse wire-grid calibrator for polarization angle calibration of GroundBIRD
- Obtained preliminary per-detector sensitivity angles for both 145 and 220 GHz detectors
- Developed a common-mode noise subtraction method, and found that its impact depends strongly on atmospheric conditions (PWV)
- Preliminary results suggest our target is achievable, with further improvement expected as we accumulate more data

• Next steps

- Extend the analysis to all detectors and multiple datasets to obtain final sensitivity angles
- Cross-check the results with simulations
- Repeat measurements over time to assess the long-term stability of detector angles