



Mitigation of the Flexing Filtering Effect in TDI for LISA

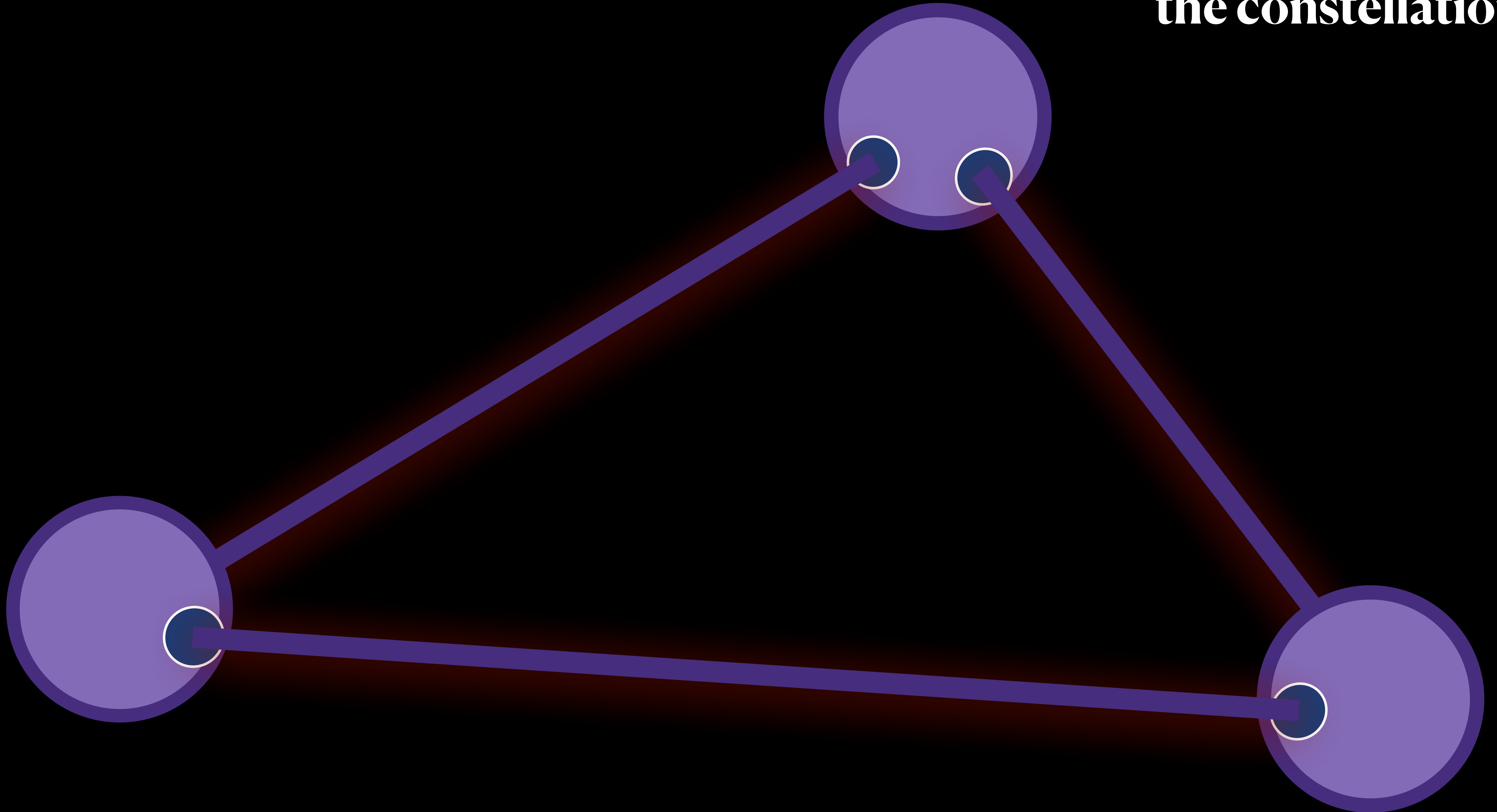
S. HARER¹, M.STAAB ^{2,3}, H.HALLOIN¹

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LISA France

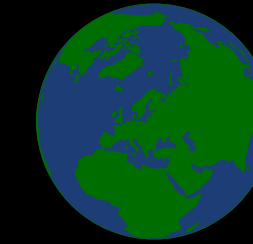
¹APC Paris ²LTE Paris ³GRASP Utrecht

the constellation



the measurement

i

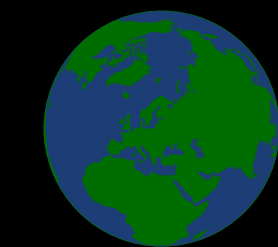
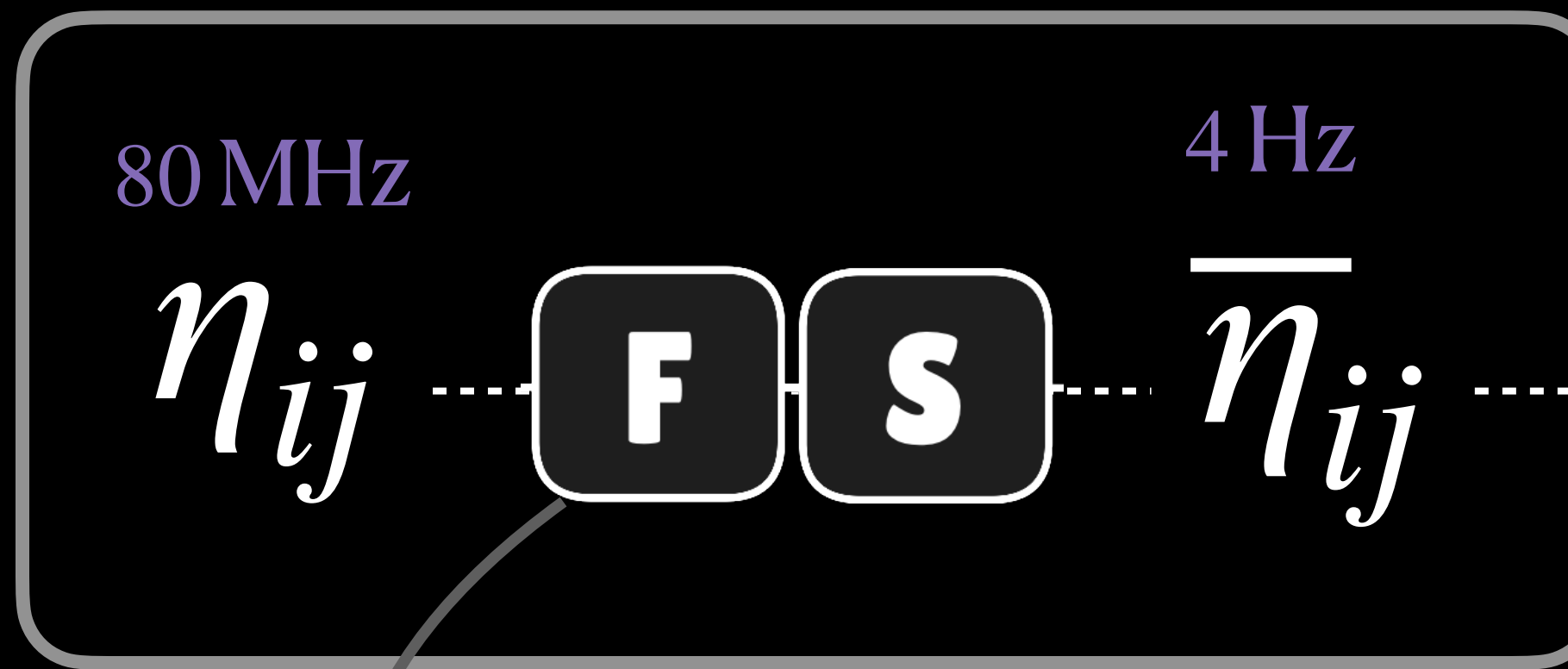
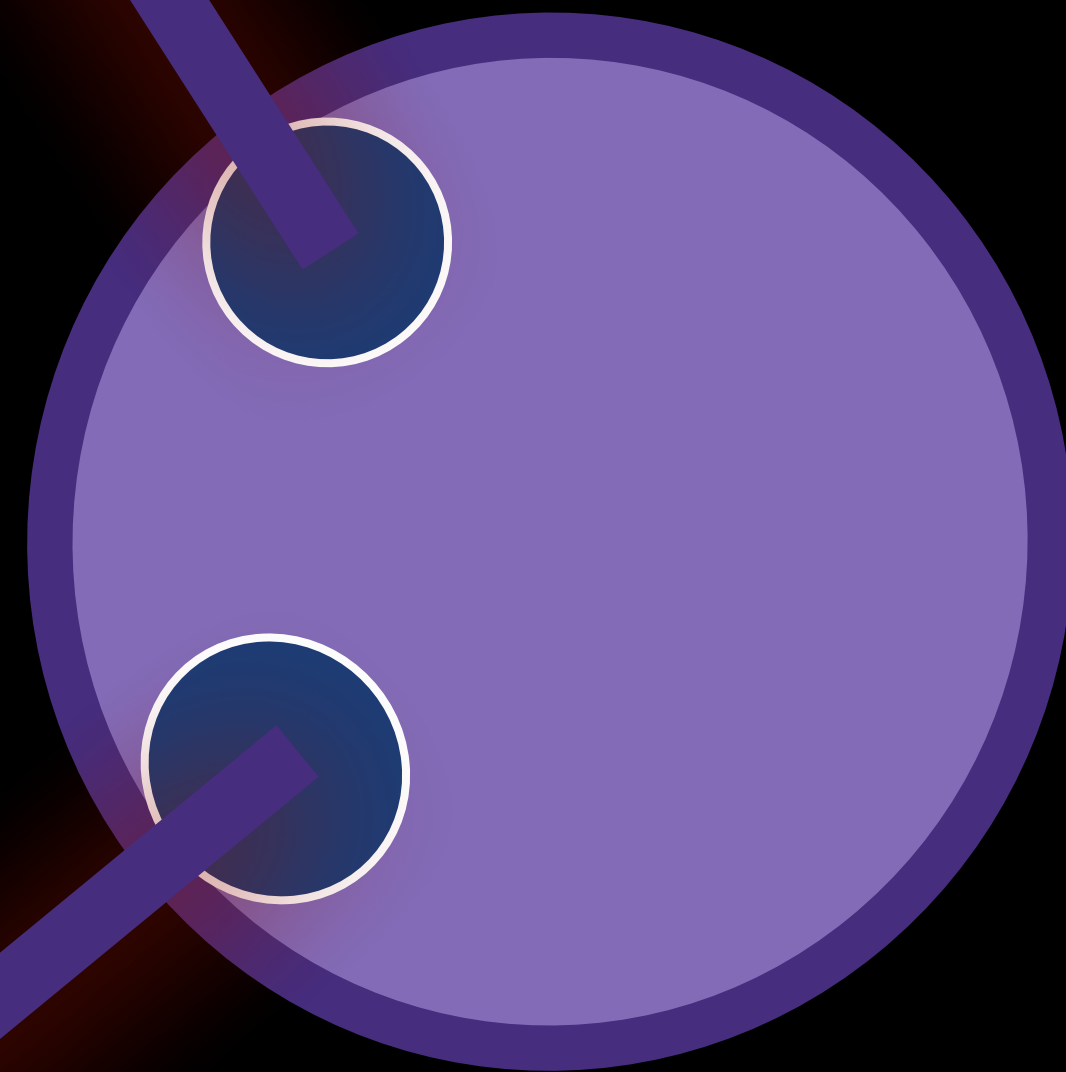


transmitted to Earth

$$\eta_{ij} = \mathbf{D}_{ij} p_j - p_i$$

j

we need to reduce the sampling rate of the data before transmission

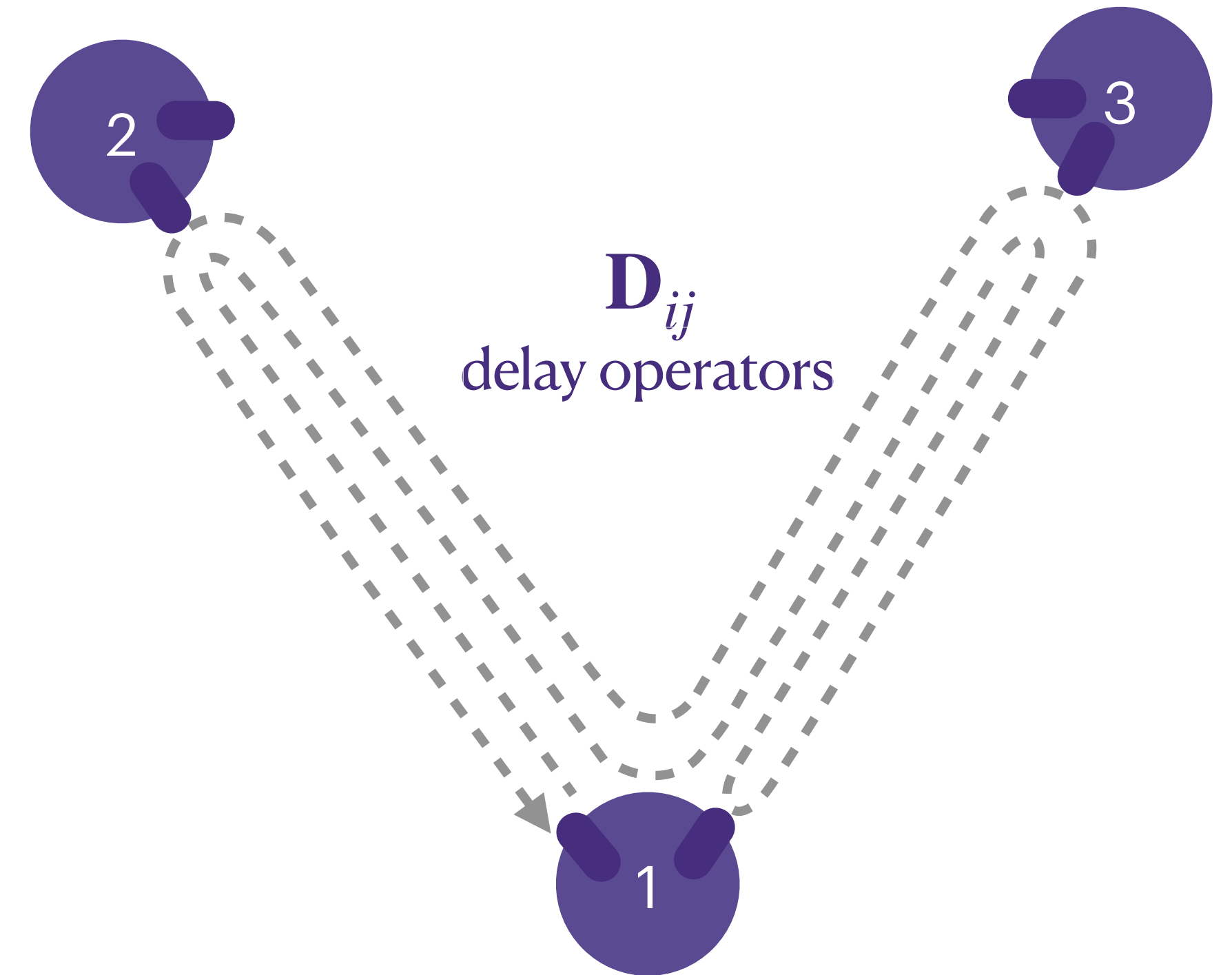


data preprocessing
and analysis

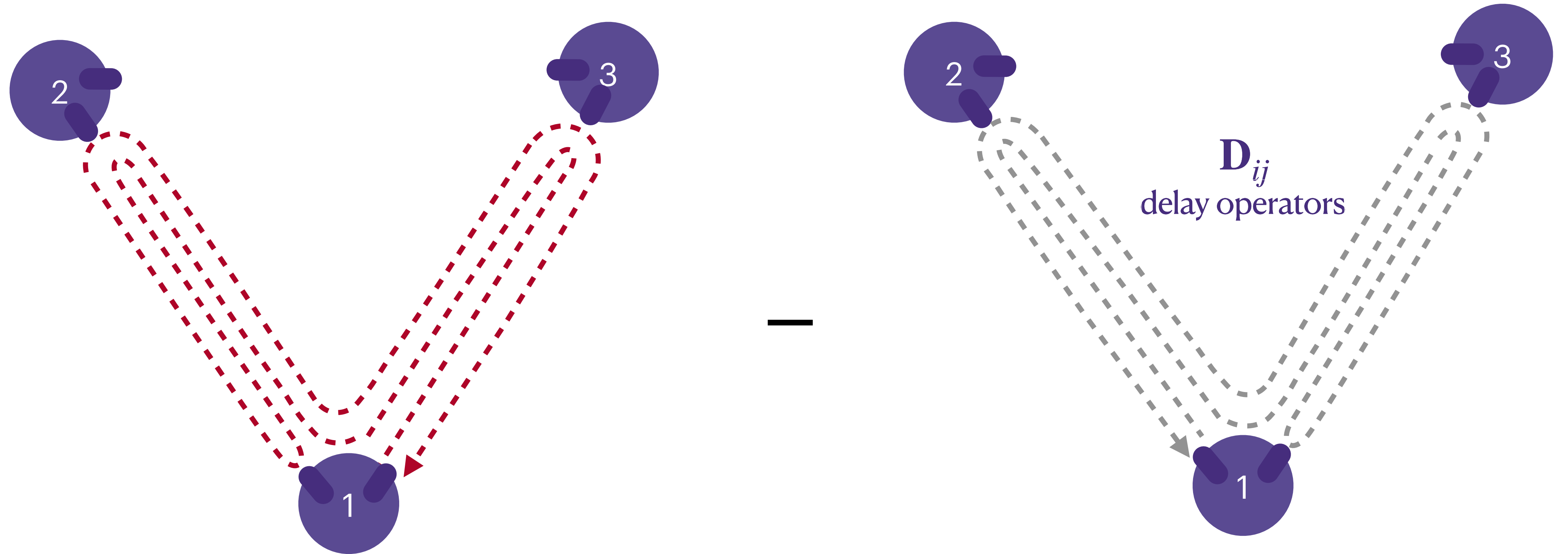
anti-aliasing filters

why do we need to do preprocessing?

- largest source of noise in LISA is laser frequency noise
- does not get automatically suppressed as in ground-based detectors because of varying arm length
- we apply a technique : **Time-Delay Interferometry (TDI)** on ground to suppress laser frequency noise.



why do we need to do preprocessing?



$$X = \sigma_{13} - \sigma_{12}$$

TDI variable (Y, Z centered on spacecraft 2,3)

However, the filter on the spacecraft and delay operator of TDI do not commute.

$$\bar{\eta}_{ij} = \mathbf{F} \mathbf{D}_{ij} p_j - \mathbf{F} p_i$$

$$\bar{\eta}_{ij} = \mathbf{F} \mathbf{D}_{ij} p_j - \mathbf{F} p_i + \underbrace{[\mathbf{F}, \mathbf{D}_{ij}] p_j}_{\text{flexing filtering}^1}$$

residual

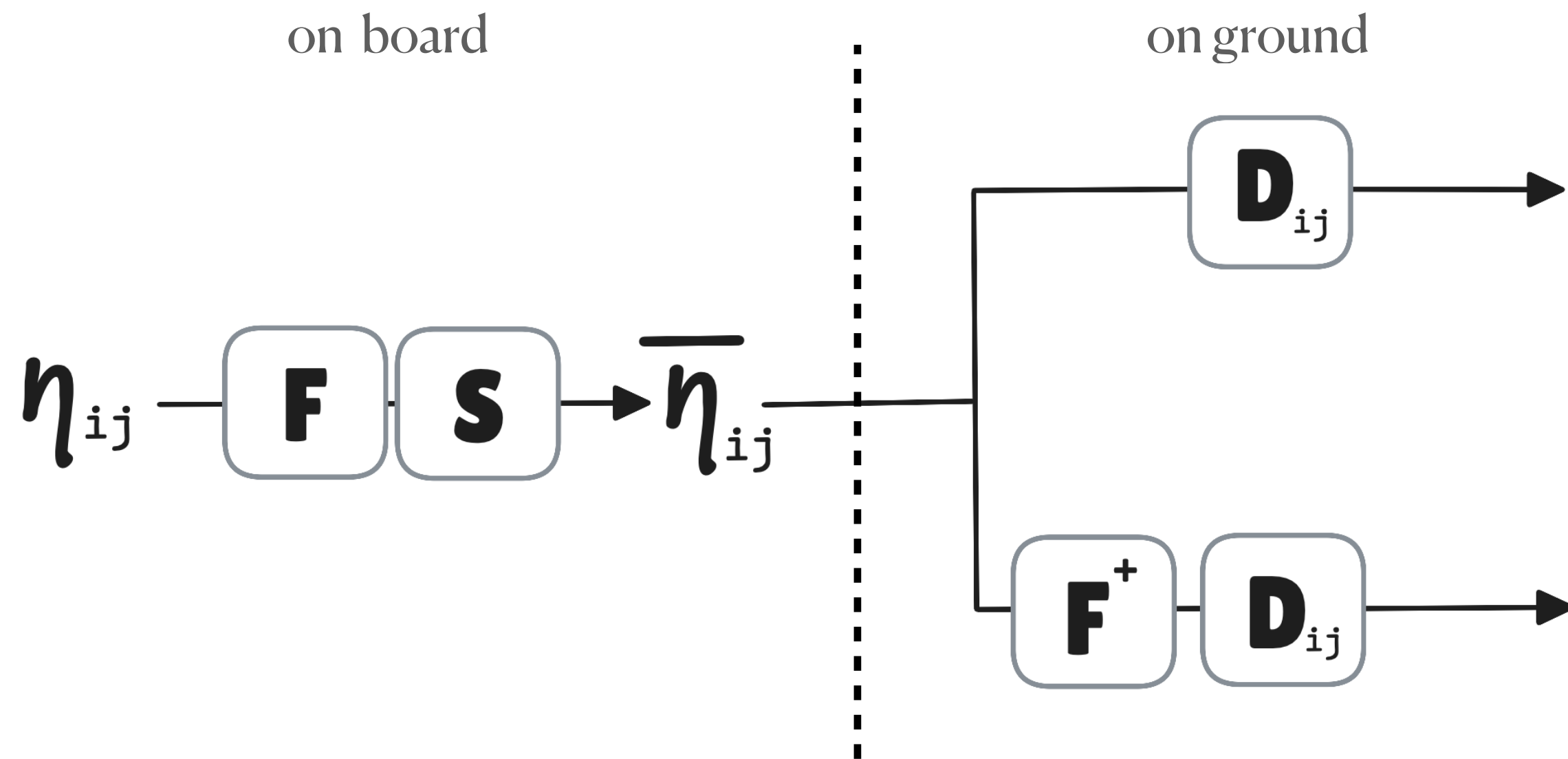
The amplitude of flexing-filtering residual* depends on:

1. the delay derivative \dot{d}
2. the “flatness” of the filter in-band

* to leading order

$$\frac{\dot{d}}{2\pi} \cdot \frac{d\tilde{h}_{\mathbf{F}}(f)}{df}$$

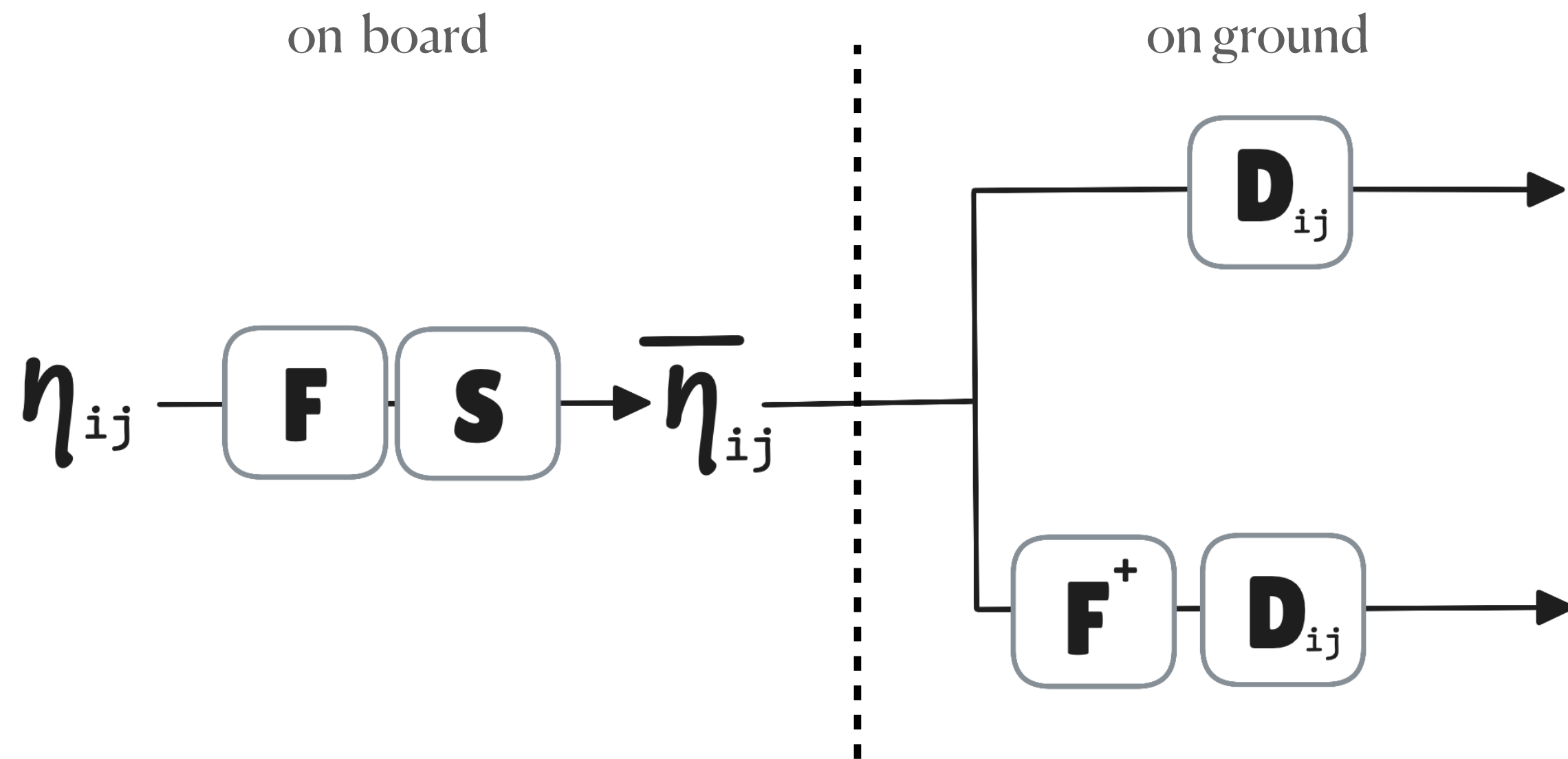
how we currently keep the “flatness” of the filter (in-band)



1. **Standard TDI**: using long, flat kaiser filters (145 taps).
2. **TDI with Compensation²**: using a quasi-inverse filter \mathbf{F}^+ to “lift” non-unity frequency response in-band.

$$\mathbf{F}^+ \bar{\eta}_{ij} = \mathbf{F}^+ \mathbf{S} \mathbf{F} (\mathbf{D}_{ij} \phi_j - \phi_i) \approx \eta_{ij}$$

how we currently keep the “flatness” of the filter (in-band)



1.

the gap : A flat filter chain on the spacecraft is computationally expensive and causes additional group delay.

2.

the gap : Needs accurate inverse filter, adds to filter chain and causes additional group delay.

Q. Can we reduce flexing filtering noise without compromising on data quality or overburdening the spacecraft's computational resources?

modify the delay operator : modified TDI

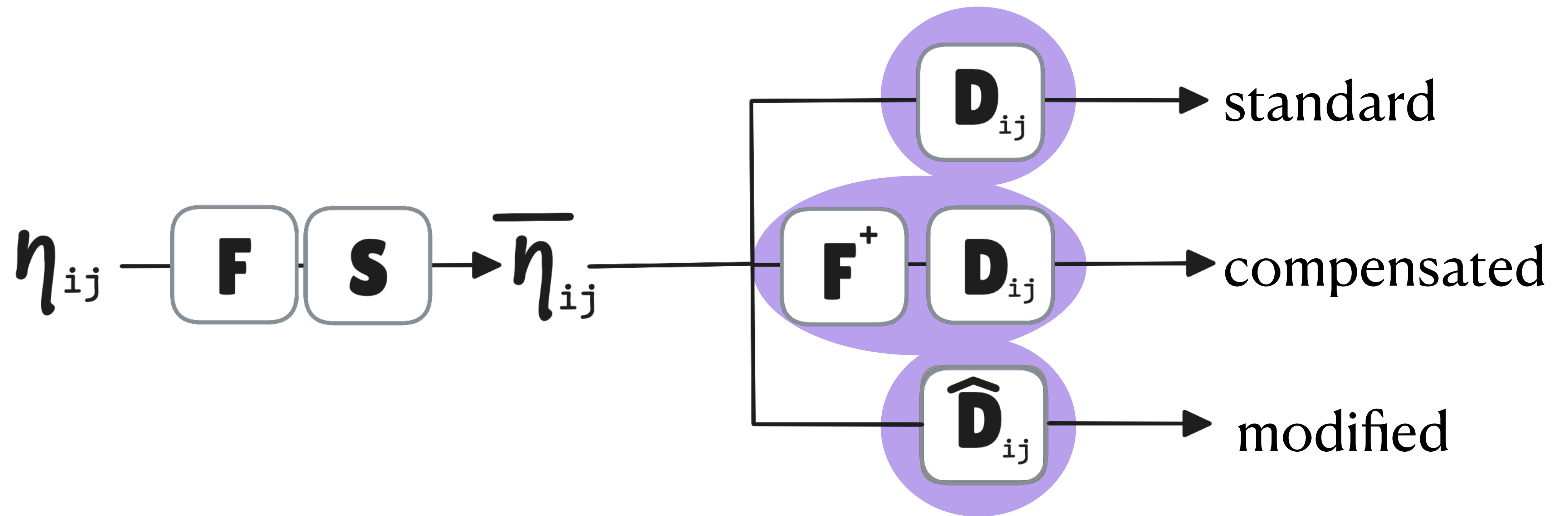
$$\bar{\eta}_{ij} = \mathbf{F} \hat{\mathbf{D}}_{ij} \mathbf{F}^{-1} \mathbf{F} p_j - \mathbf{F} p_i$$

modified delay
operator $\hat{\mathbf{D}}_{ij}$

modify the delay operator : modified TDI

The modified delay operator is approximated as a sum of the normal delay operator and a **small correction** scaled by d

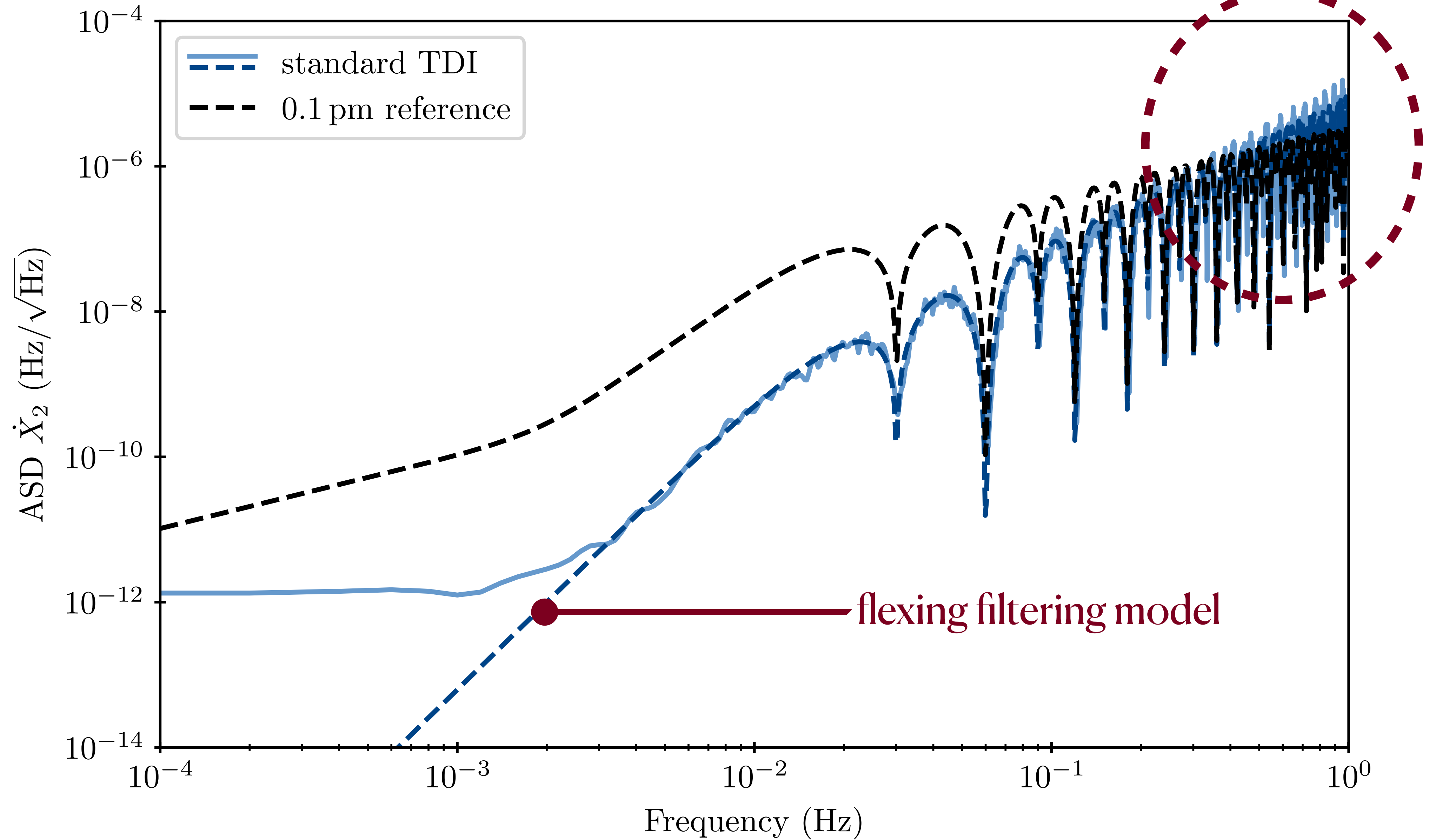
$$\begin{aligned}\widehat{\mathbf{D}} &= \mathbf{F}\mathbf{D}_{ij}\mathbf{F}^{-1} \\ &\approx \mathbf{D} + d \cdot \underbrace{\mathbf{D} \frac{d}{dt} \mathbf{G}\mathbf{F}^{-1}}_{\mathbf{H}} \\ &\quad h_{\mathbf{G}}(\tau) = \tau \cdot h_{\mathbf{F}}(\tau)\end{aligned}$$



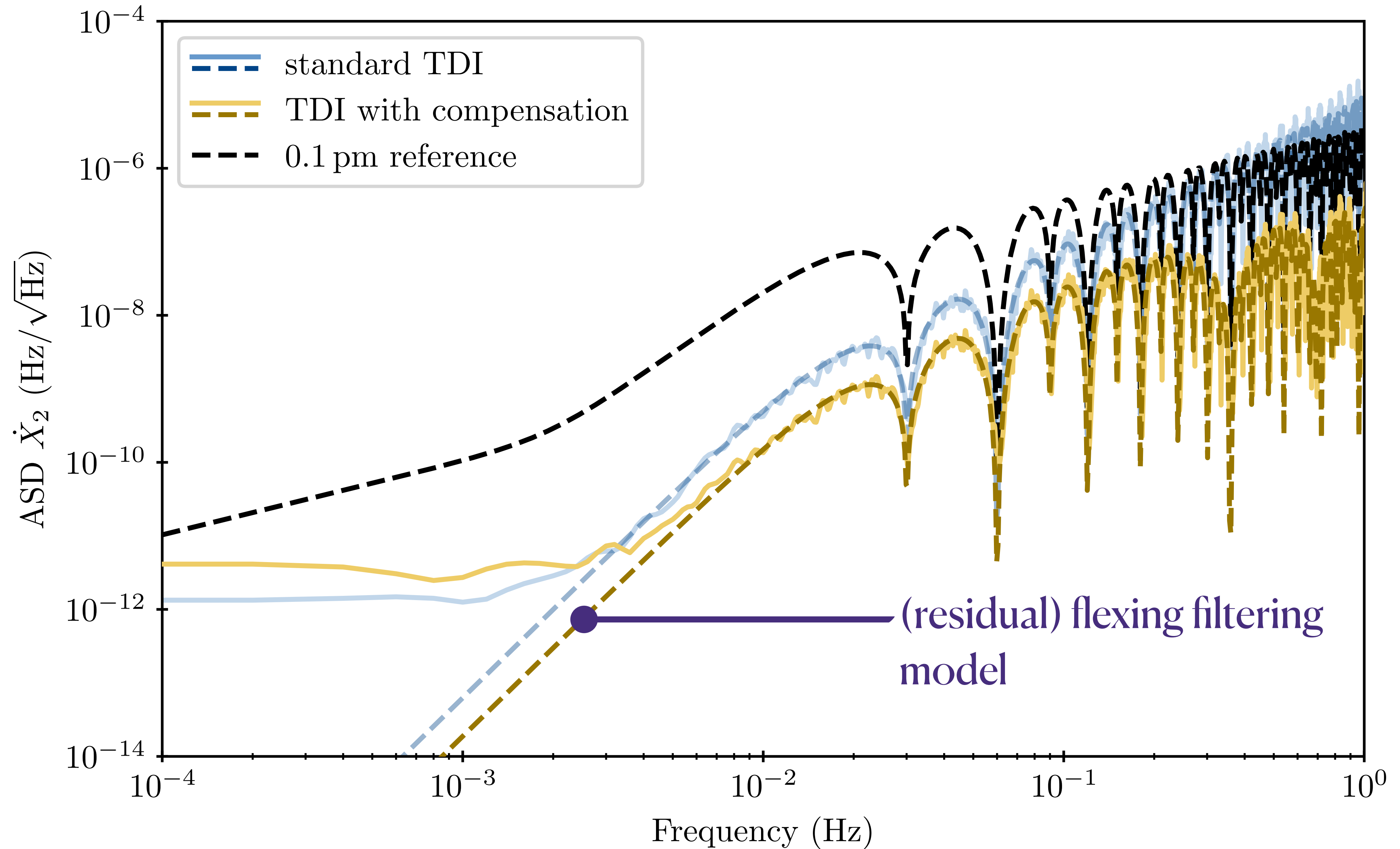
performance review

comparing the three topologies while using a non-flat filter on board

Standard TDI

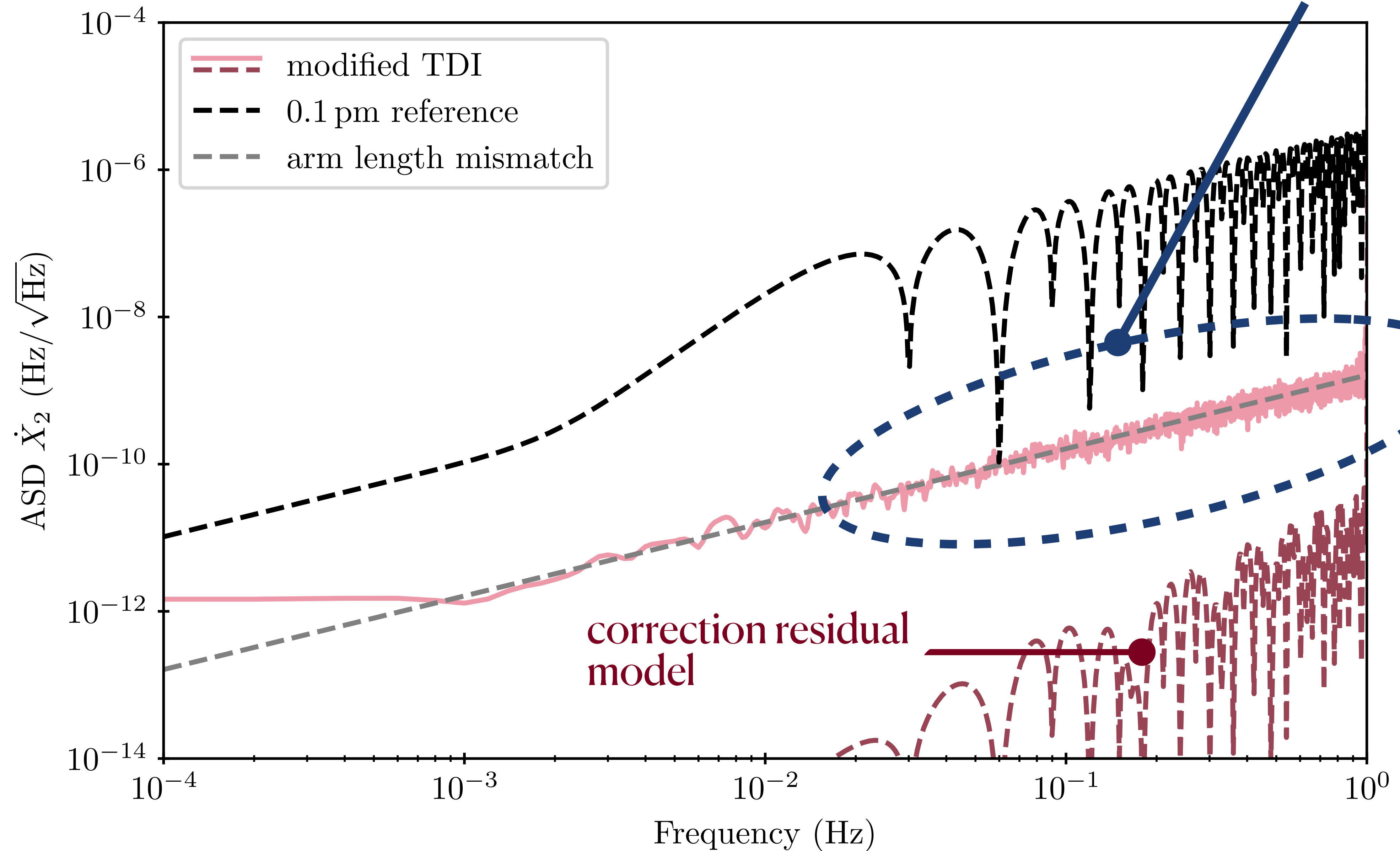


TDI with Compensation

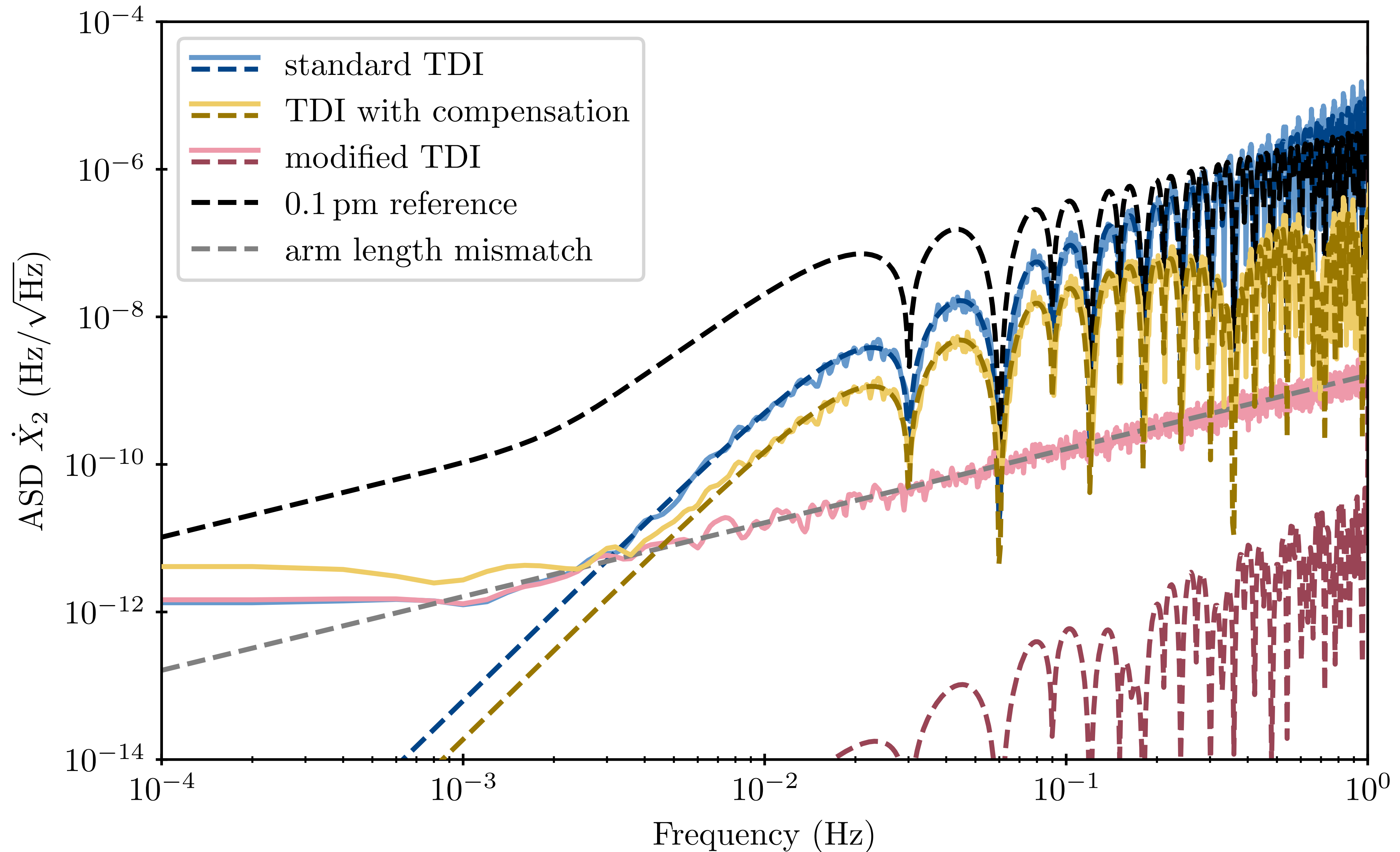


Modified TDI

fundamental noise floor X_2



Modified TDI outperforms the other two topologies



summary and conclusion

Q. Can we reduce flexing filtering noise without compromising on data quality or overburdening the spacecraft's computational resources?

Yes.

Modified TDI allows for 6 order of noise reduction , contributes no additional group delay and keeps on-board computational cost low via an inexpensive anti-aliasing filter.

Follow up studies : other locking configurations, include primary noise sources, effect on other secondary noises (clock noise)

thanks :)

If you're interested, you can find our paper on CQG and [arXiv:2506.04316](https://arxiv.org/abs/2506.04316)

backup slides

We need to **approximate the correction \mathbf{H}** to apply it on discrete data.

Similar to the pure delay operation
i.e. a **discrete convolution** between the data and
this **approximate correction \mathcal{H}** .

$$y(nT_s) = \sum_{m=-\infty}^{\infty} x((n-m)T_s) \cdot h_{\mathcal{H}}(mT_s - d)$$

The kernel $h_{\mathcal{H}}$ is designed using cosine-sum kernels ³

$$h_{\mathcal{H}}(t) = \text{rect} \left(\frac{t}{NT_s} \right) \sum_{n=0}^{N-1} a_n \cdot \cos \left(2\pi f_s \frac{n}{N} t \right)$$

where the coefficients a_n are approximated using the Parks-McClellan algorithm.

Residual Noise in Modified TDI

Errors between the exact operator $\widehat{\mathbf{D}}$ and the approximate design $\widehat{\mathcal{D}}$ result in noise residues.

$$\underbrace{(\mathbf{D} - \mathcal{D})\phi}_{\text{interpolation error}} + \underbrace{\dot{d} \cdot (\mathbf{H} - \mathcal{H})\phi}_{\text{correction residual}}$$

LISA Instrument³ parameters

- i. three laser lock
- ii. white laser noise, ASD of $30 \text{ Hz}/\sqrt{\text{Hz}}$
- iii. sampling: 4 Hz for 25000 s
- iv. anti-aliasing filter: filter at 4 Hz with **9 taps**
- v. interpolation: Lagrange ($N = 62$)
- vi. ESA Trailing Orbits
- vii. $t_0 = 2.0813 \times 10^9 \text{ s}$; to maximize \dot{d}

What contributes to the residual noise?

Topology	Noise source
Standard TDI	flexing filtering [\mathbf{F} , \mathbf{D}]
TDI with compensation	(residual) flexing filtering [$\mathbf{F}^+\mathbf{F}$, \mathbf{D}]
Modified TDI	correction ($\mathbf{H} - \mathcal{H}$)