

Impact of Nuclear Structure on Fusion–Fission Dynamics in Superheavy Element Synthesis

Y. Aritomo¹, K. Kawai¹, K. Nakajima¹, S. Takagi^{1,2}, A. Yumikura¹

¹*Faculty of Science and Engineering, Kindai University, Osaka, Japan*

²*RIKEN Center for Computational Science, Kobe, Japan*



24th COLLOQUE GANIL
21–25 Sept 2026
Bussang, France

24^{ème}
COLLOQUE GANIL
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**The University of Caen
and Kindai University
have signed an agreement for student and researcher
exchange.
July, 2026**

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SHE synthesis

2. Model

Two-center shell model

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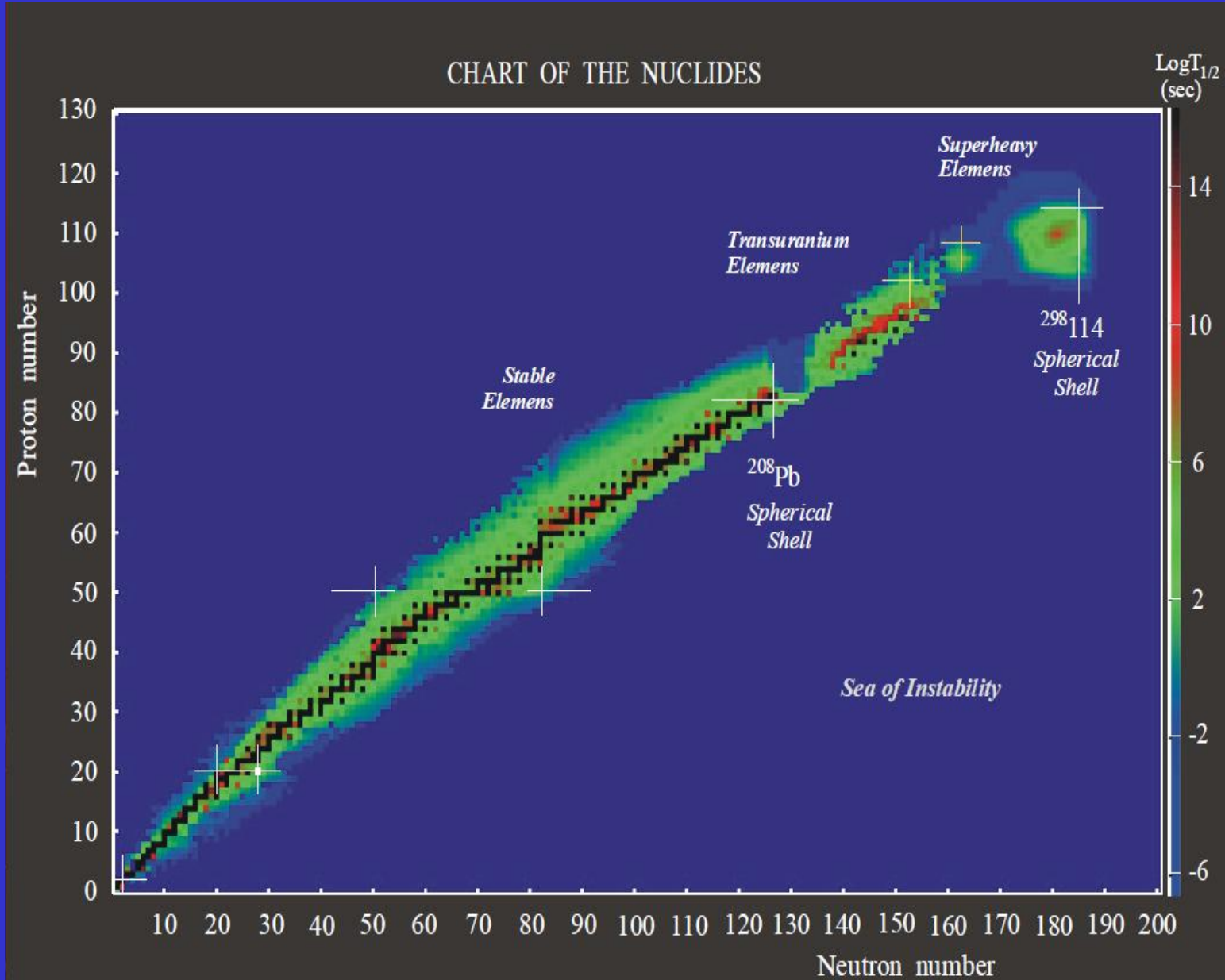
3. Discussion

Estimation for Synthesis of SHE

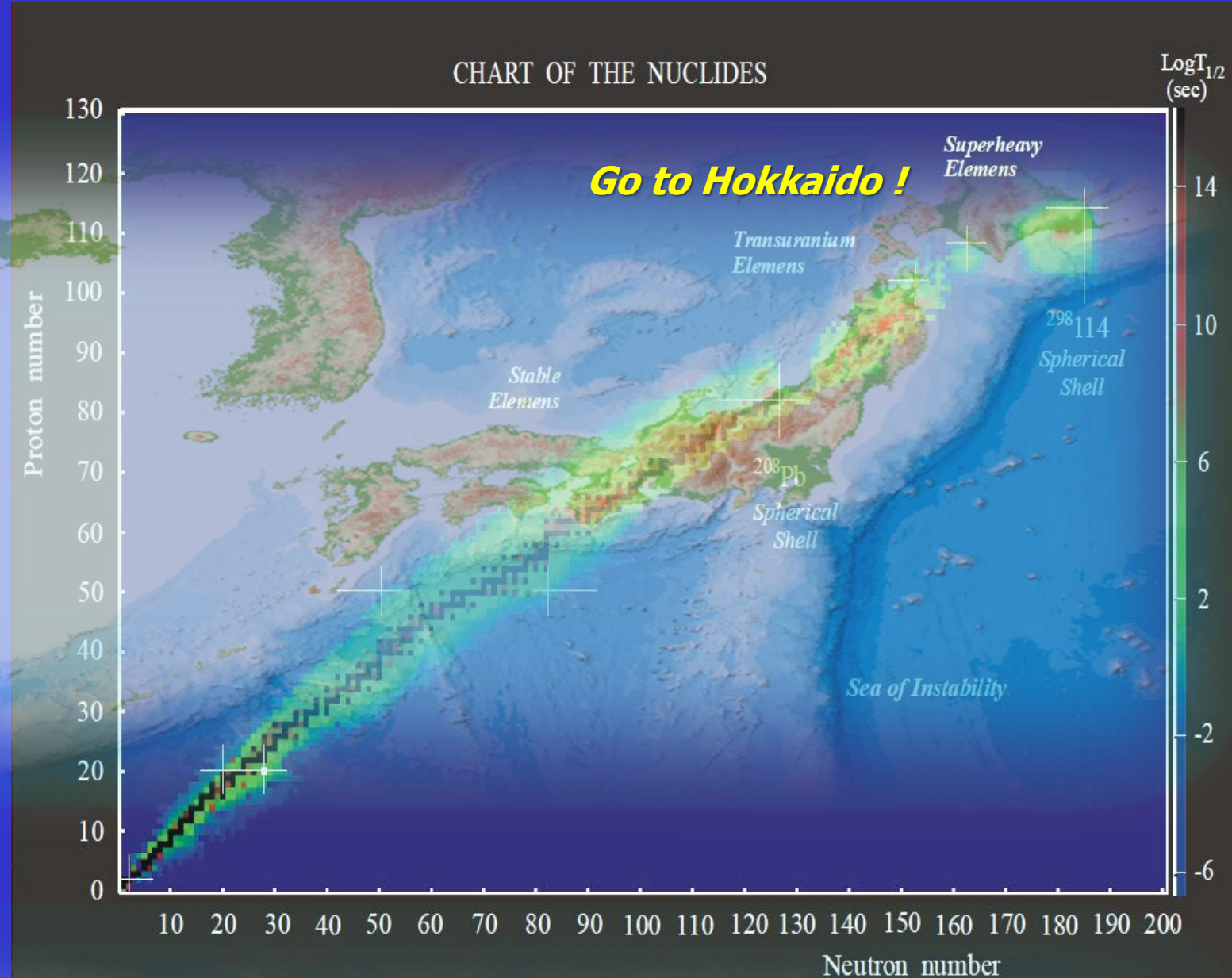
Future plan to **Synthesis of SHE**

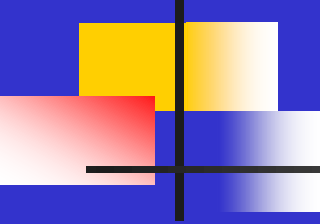
4. Summary

Nuclear Chart and Stability of Nuclei



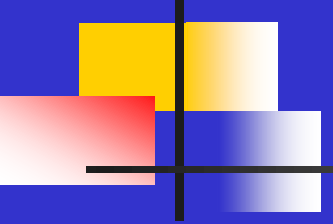
Nuclear Chart and Stability of Nuclei





Way for synthesizing new SHE

- 1) Ti, V, Cr, Fe etc. beams $\leftarrow$ ^{48}Ca beams
Actinide target
- 2) Secondary beams (RI beams)
- 3) Transfer reaction U+Th, U+Cm



Way for synthesizing new SHE

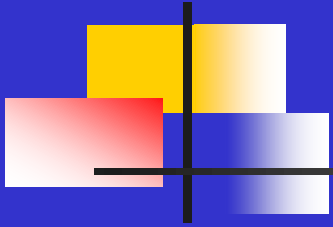
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$\leftarrow$ K. Kawai et.al.,
Phys. Rev. C 114, 014612 (2026)

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$\leftarrow$ K. Nakajima et.al.,
EPJ Web of Conferences 378, 02028 (2026)



Way for synthesizing new SHE

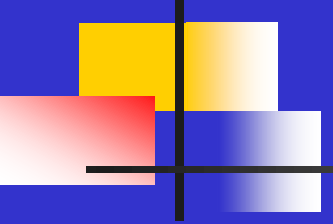
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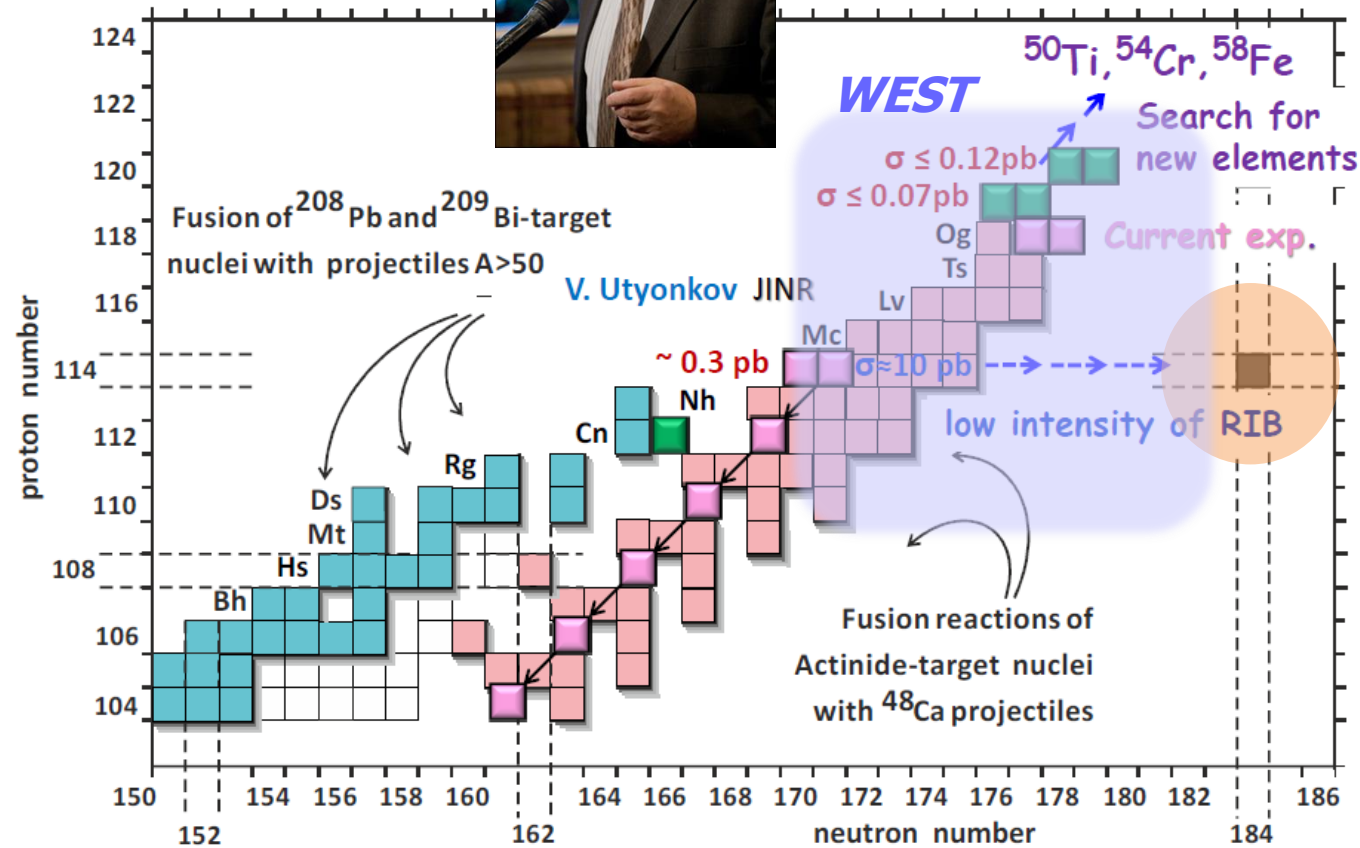
$\leftarrow$ What RI nuclei (Target or Projectile) should be used ?

- 3) Transfer reaction $\text{U}+\text{Th}$, $\text{U}+\text{Cm}$

$\leftarrow$ K. Nakajima et.al.,
EPJ Web of Conferences 378, 02028 (2026)



Oganessian



Yuri Oganessian SHE-2017, Sept. 10-14, 2017, Kazimierz Dolny, Poland



Cold fusion reaction Hot fusion reaction

1994



1996



1999



2000



2002



2003



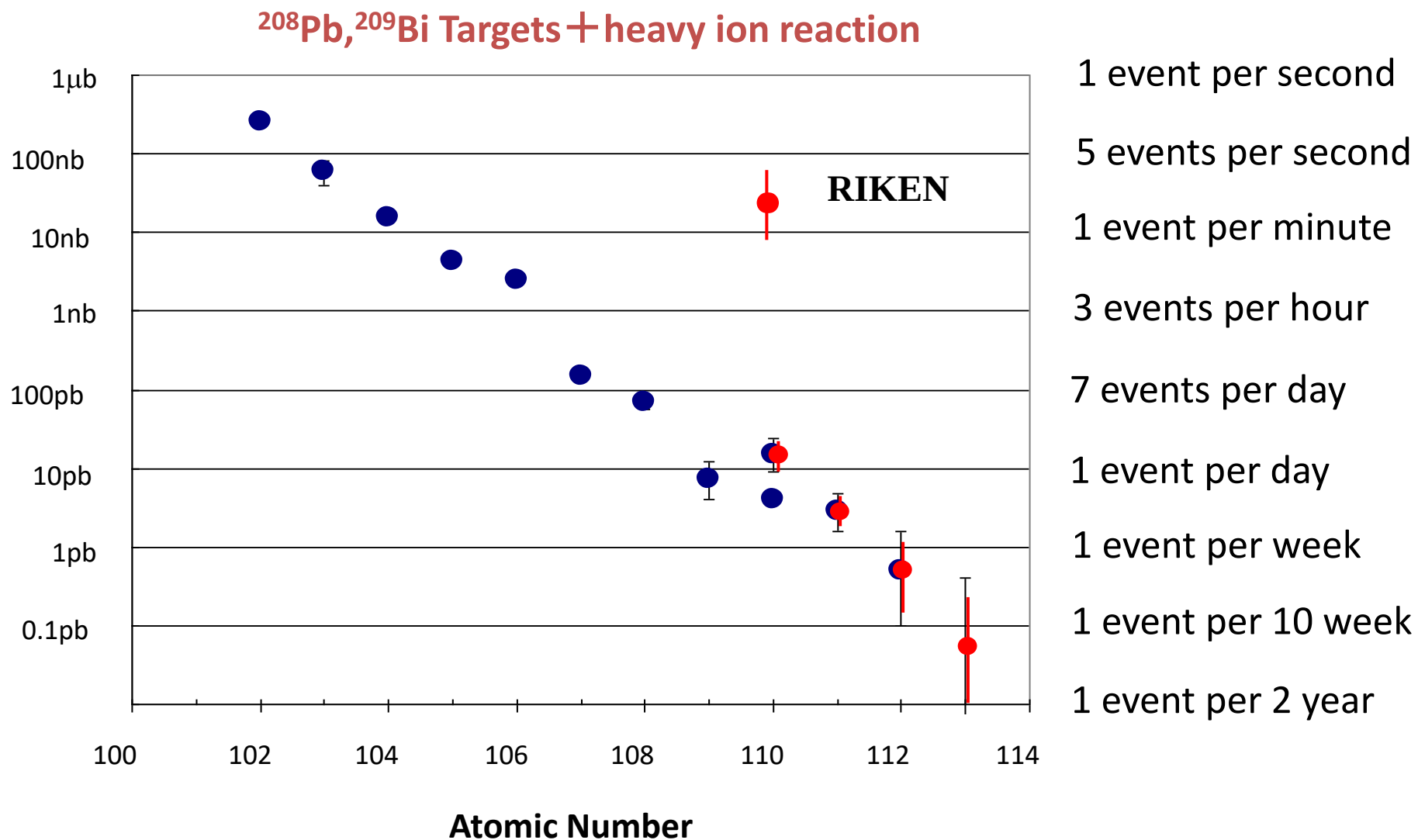
2004

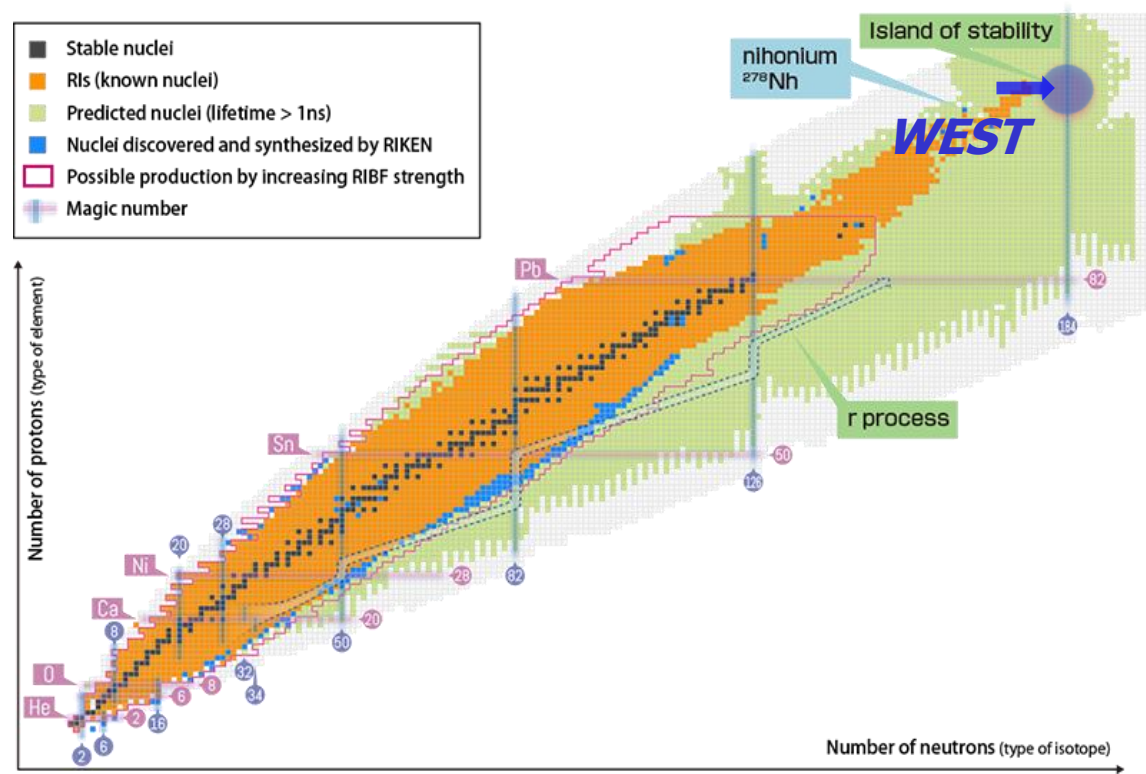


2010



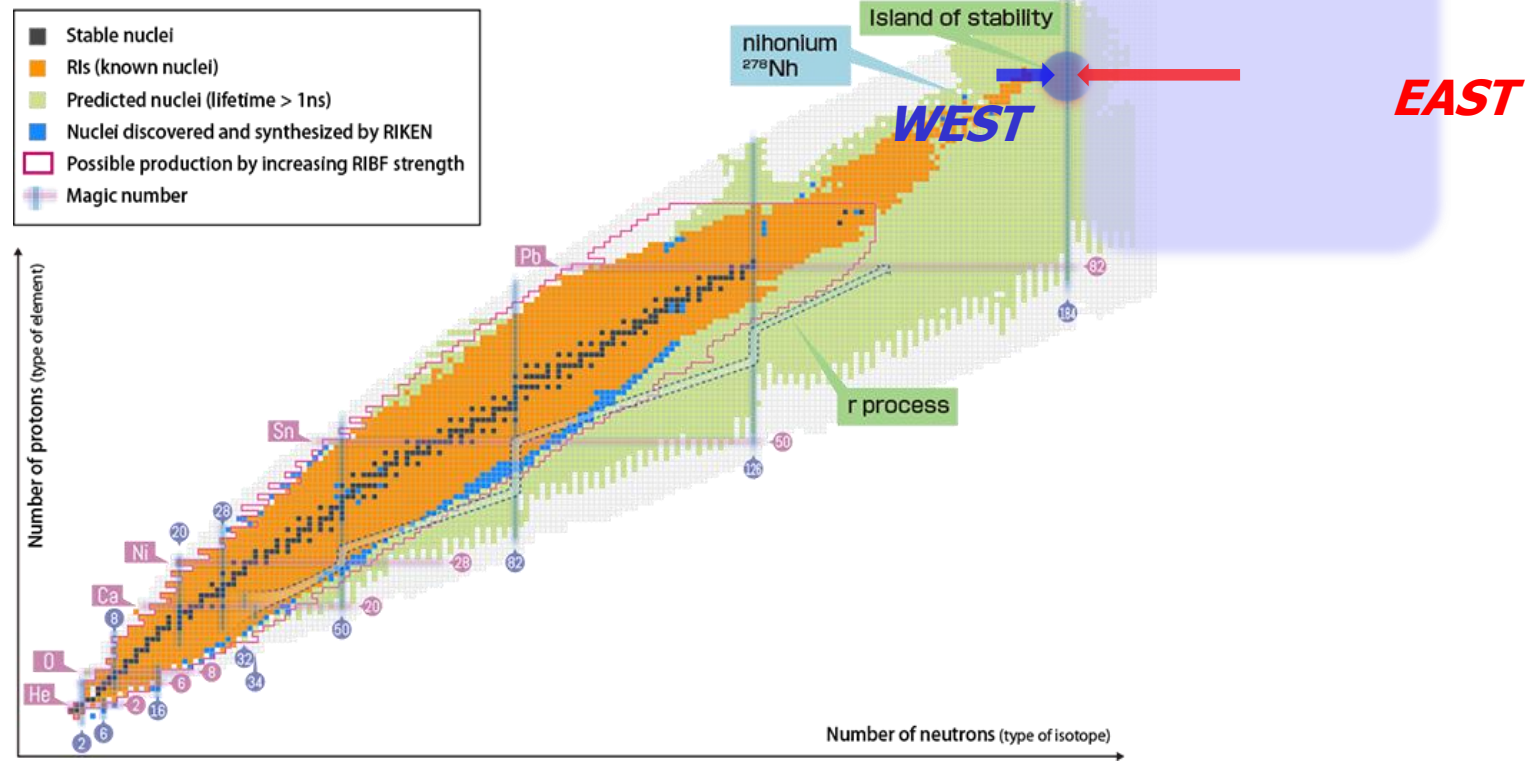
ease (or difficulty) of synthesis





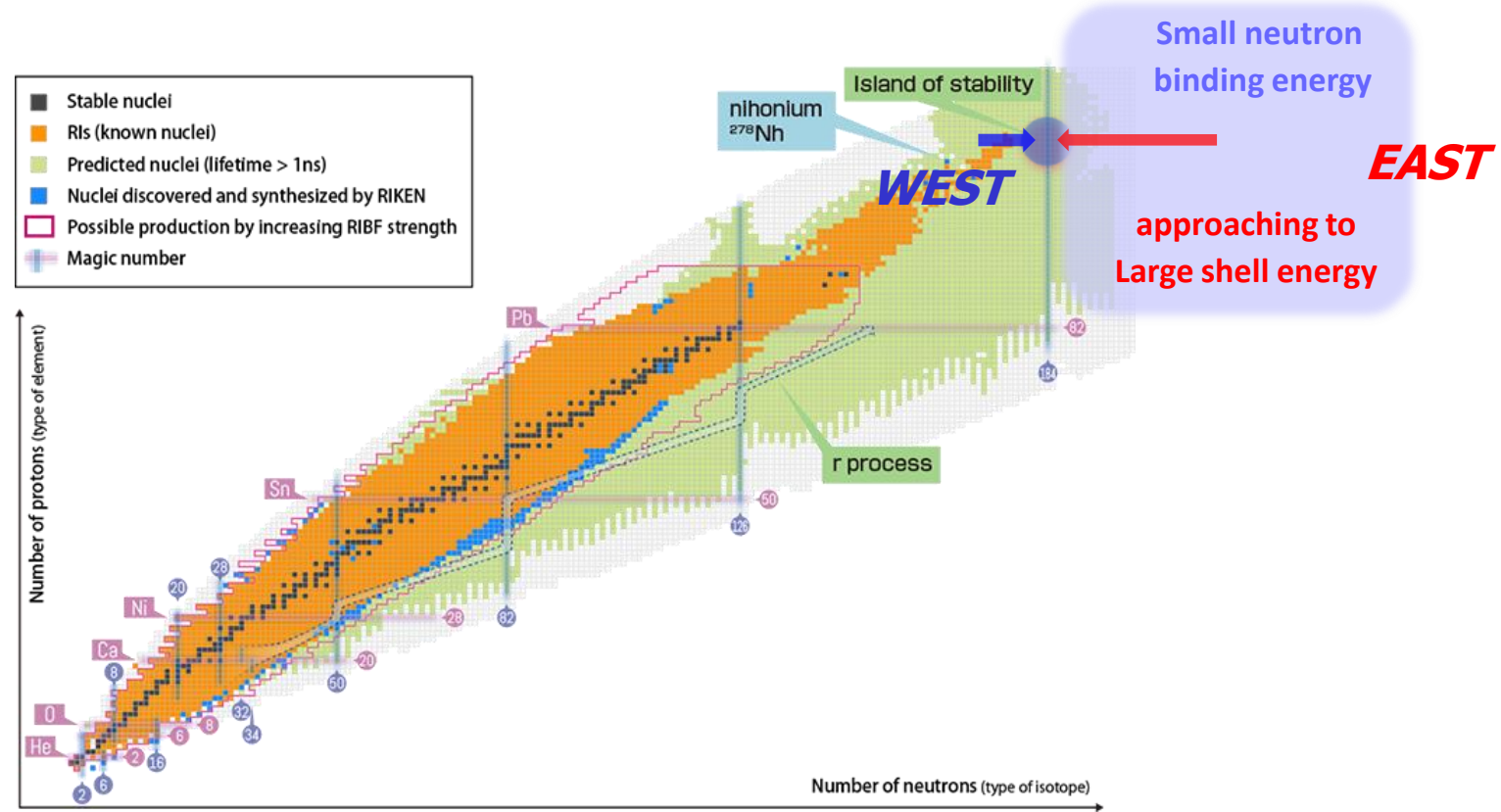
Riken Nishina HP: <https://www.nishina.riken.jp/ouen/en/factory.html>

Using RI beams

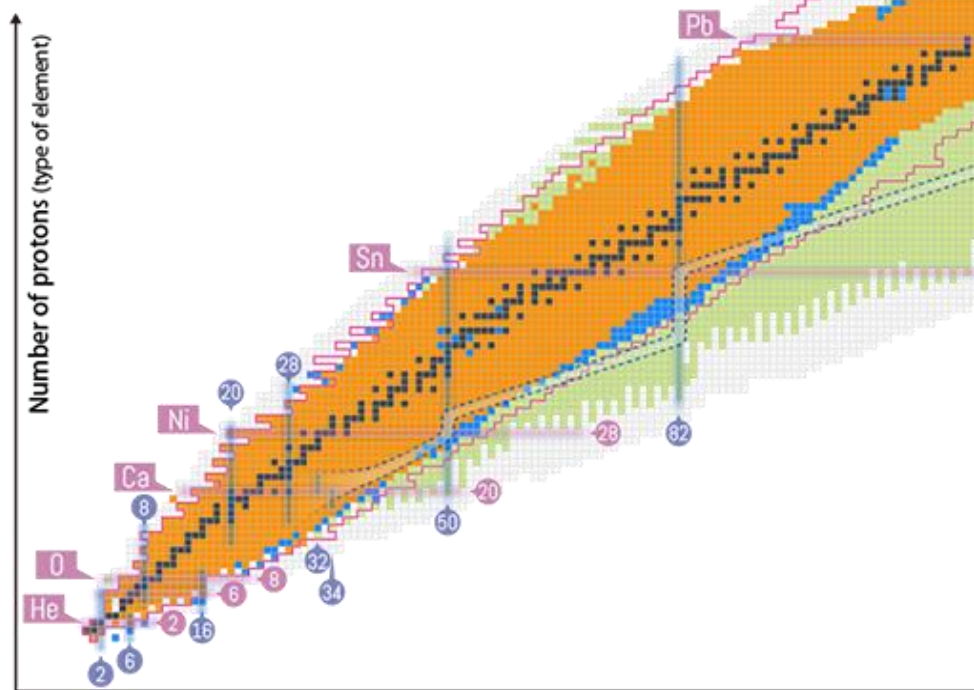
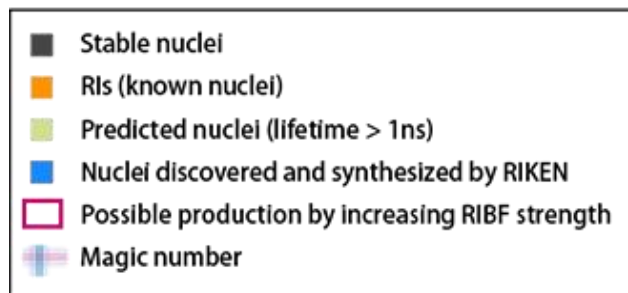


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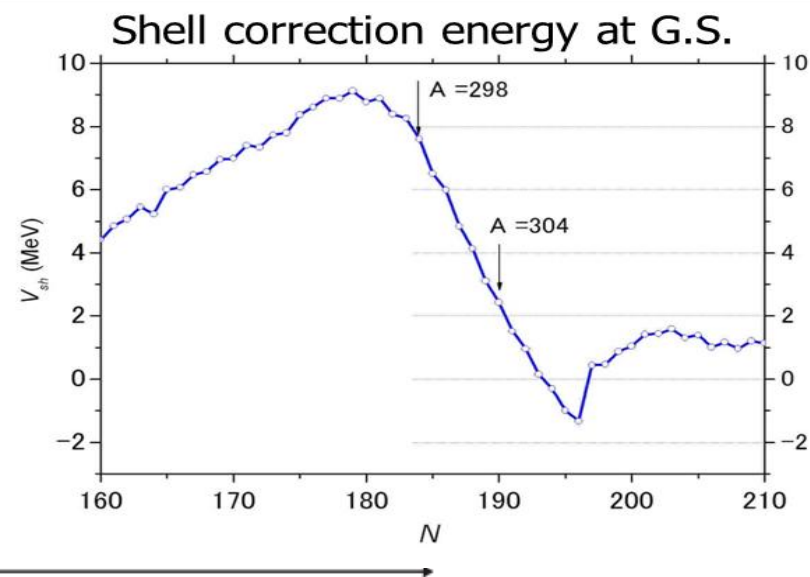
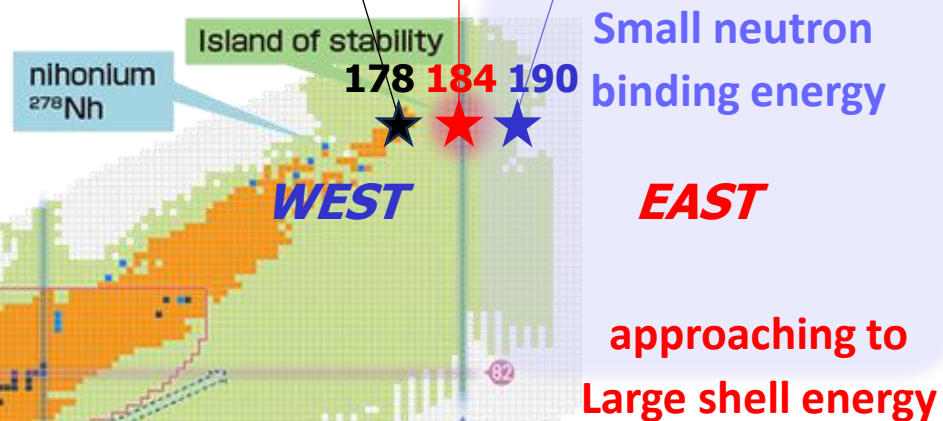
Using RI beams



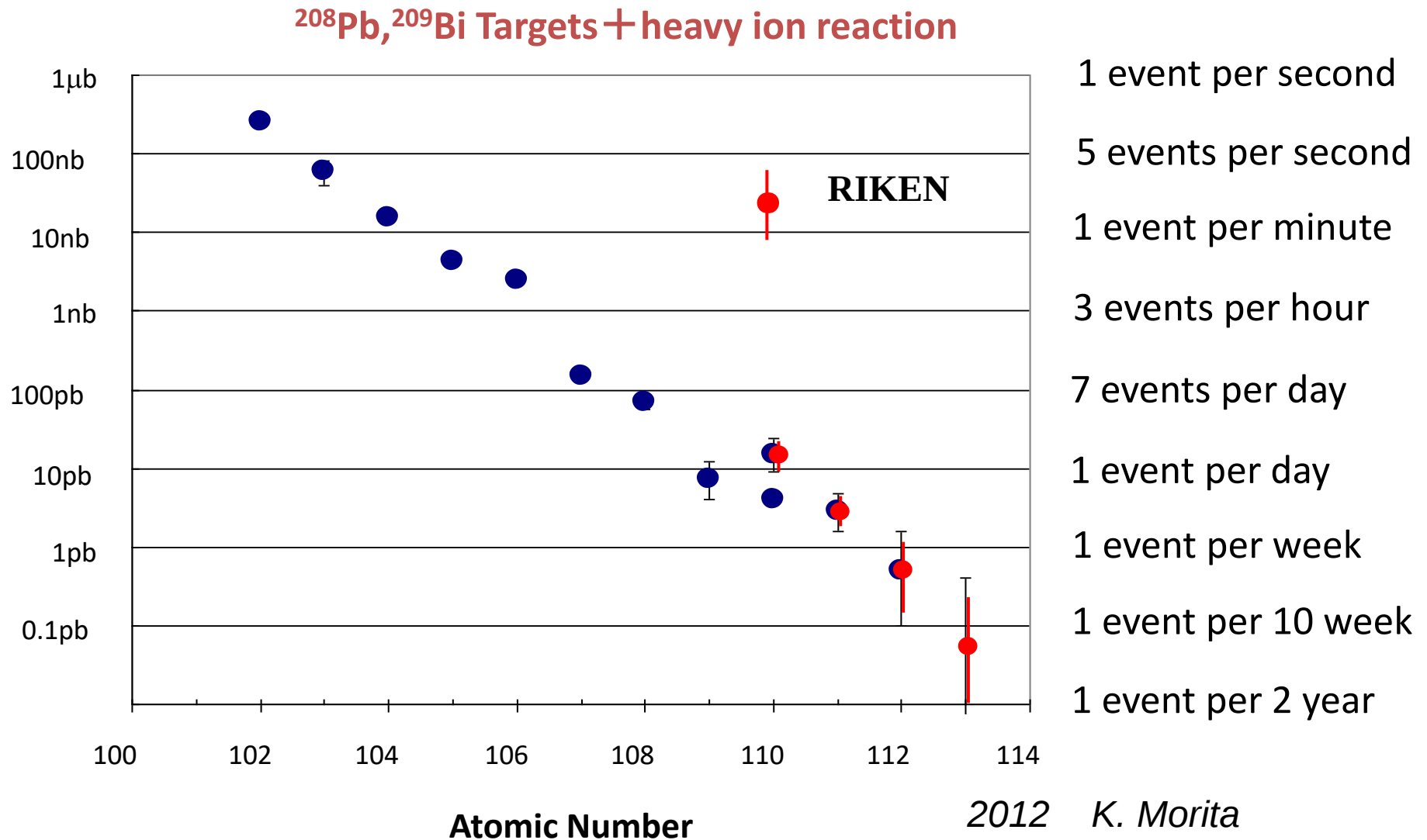
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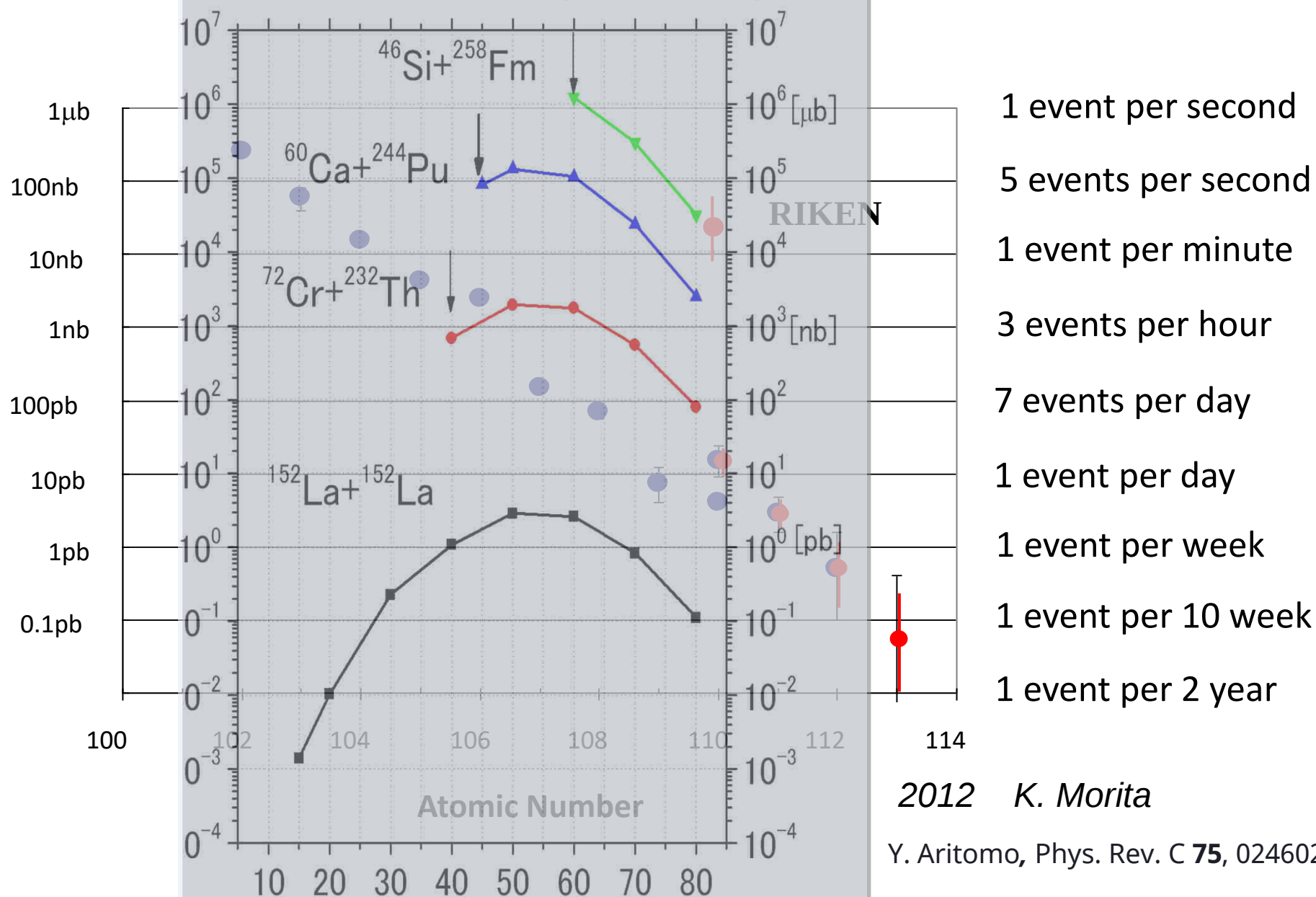
$S_n = 6 \quad 5 \quad 4 \text{ MeV}$ Using RI beams



ease (or difficulty) of synthesis

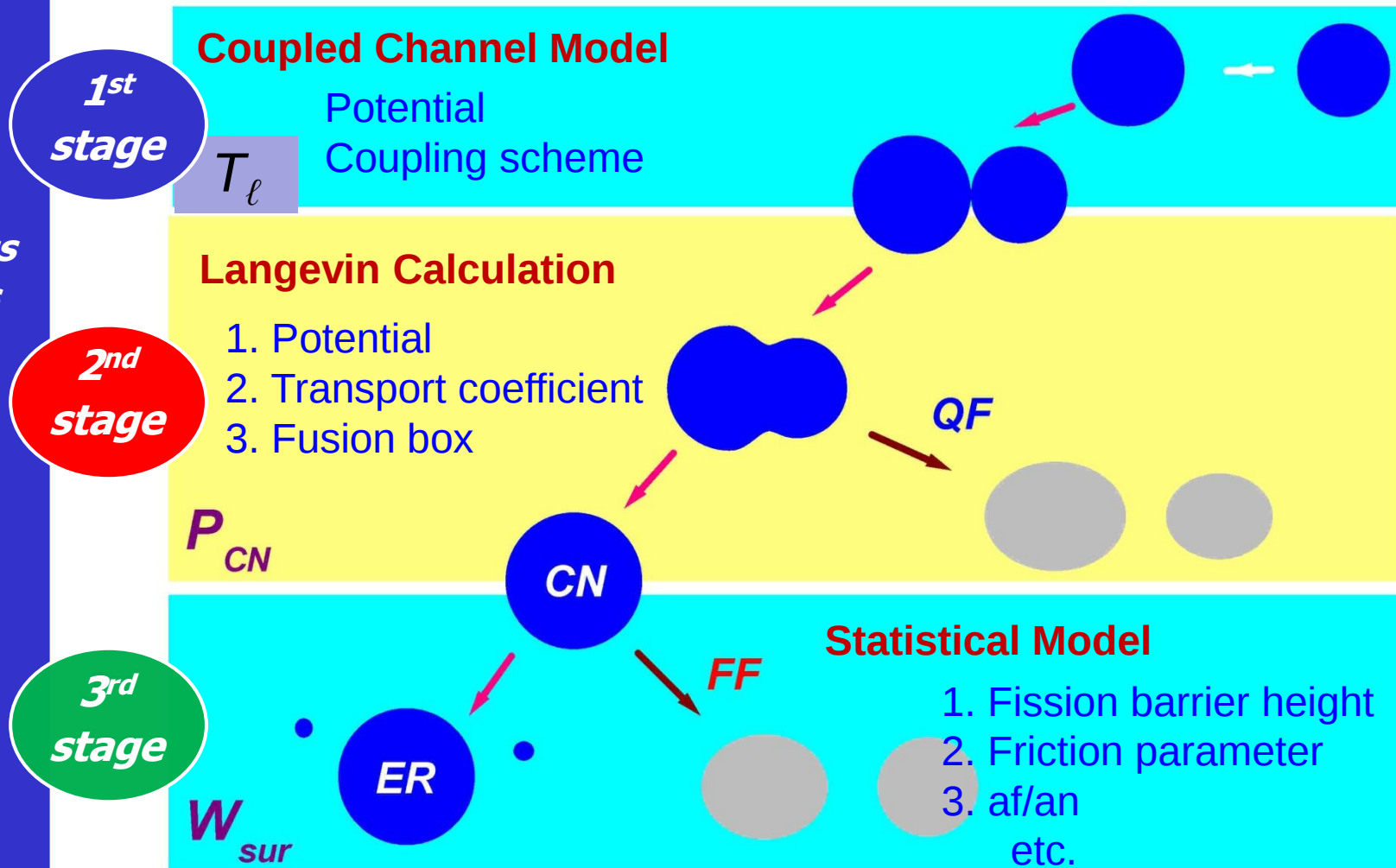


ease (or difficulty) of synthesis



$$\sigma_{ER} = \frac{\pi \hbar^2}{2\mu_0 E_{cm}} \sum_{\ell=0}^{\infty} (2\ell + 1) T_{\ell}(E_{cm}, \ell) P_{CN}(E^*, \ell) W(E^*, \ell)$$

*Divide
the whole process
into three stages*



Advantages of Each Stage

1. Suppression of incident energy dissipation

ADVANTAGE using Nuclei with **Strong Shell Structure**

1-stage

2. Use of the second pocket in fusion process

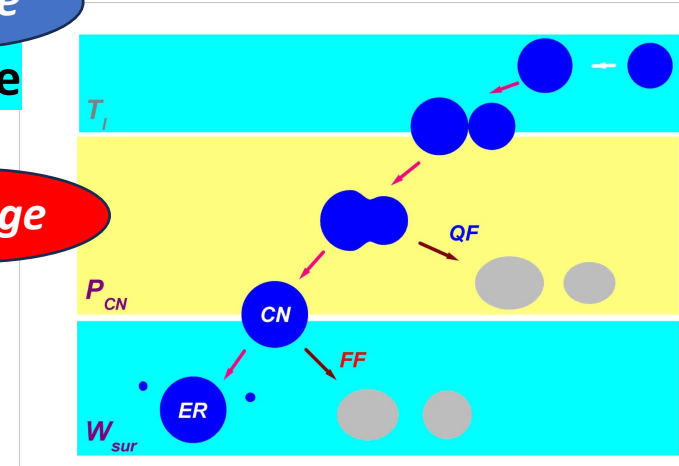
ADVANTAGE using the **Spherical Target**

2-stage

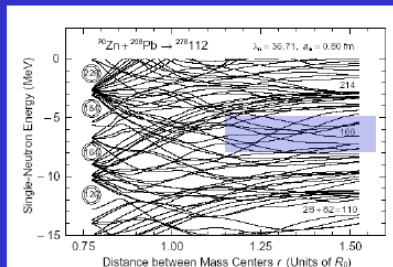
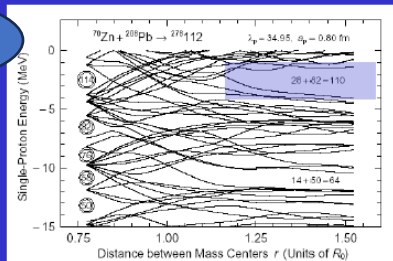
3. Rapid and many neutron emissions

ADVANTAGE using **RI beams**

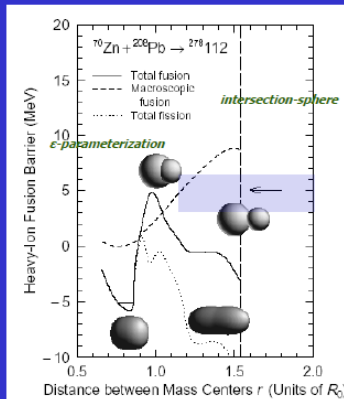
3-stage



1-stage



In dynamical model, we use
microscopic friction,
which depends on the temperature.

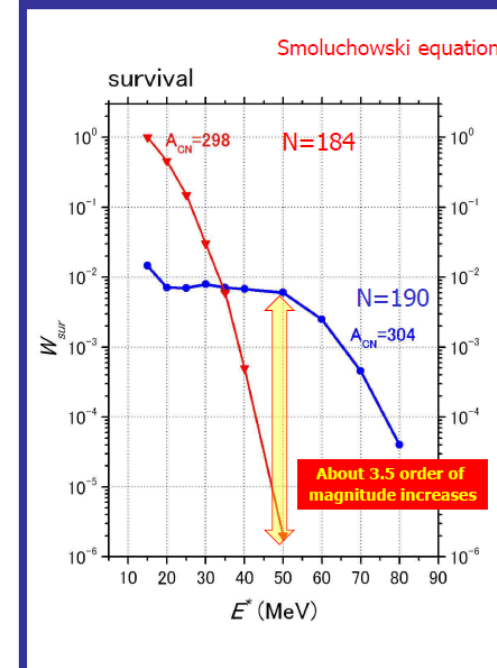


The original fragment cluster or shell structure is presented during most of the fusion process.

Little dissipation would occur until just outside the inner fusion and fission saddle points
→ reduce the extra energy in the entrance channel to reach the compound nucleus.

P. Möller, J.R. Nix, P. Armbruster, S. Hofmann, G. Munzenberg, Z. Phys. A 359, 251 (1997)
Single-particle enhancement of heavy-element production

3-stage



Due to many neutron emissions

① Approaching to **Island of Stability**
(large Vsh)

Due to many neutron emissions
→ E* of CN decreases

② Recovers of **shell correction energy**
Vsh

→ large fission Barrier

Advantages of Each Stage

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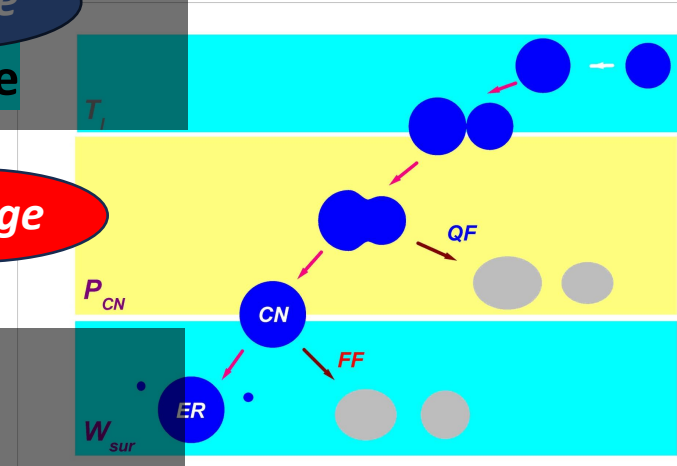
ADVANTAGE using the Spherical Target

2-stage

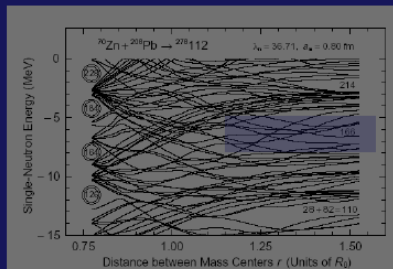
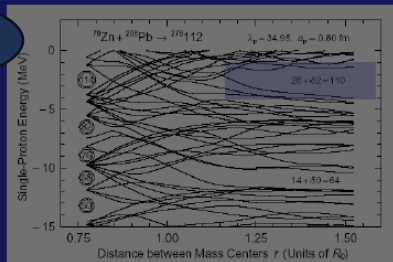
3. Rapid and many neutron emissions

ADVANTAGE using RI beams

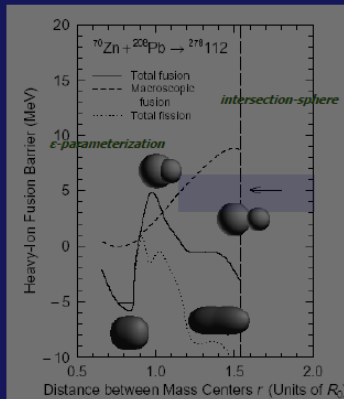
3-stage



1-stage



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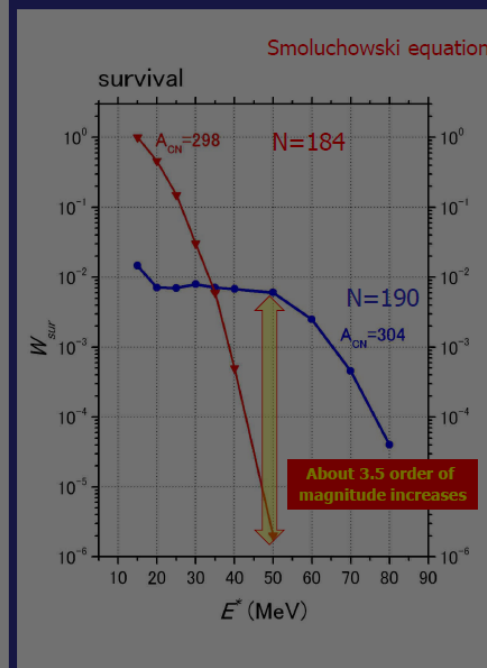


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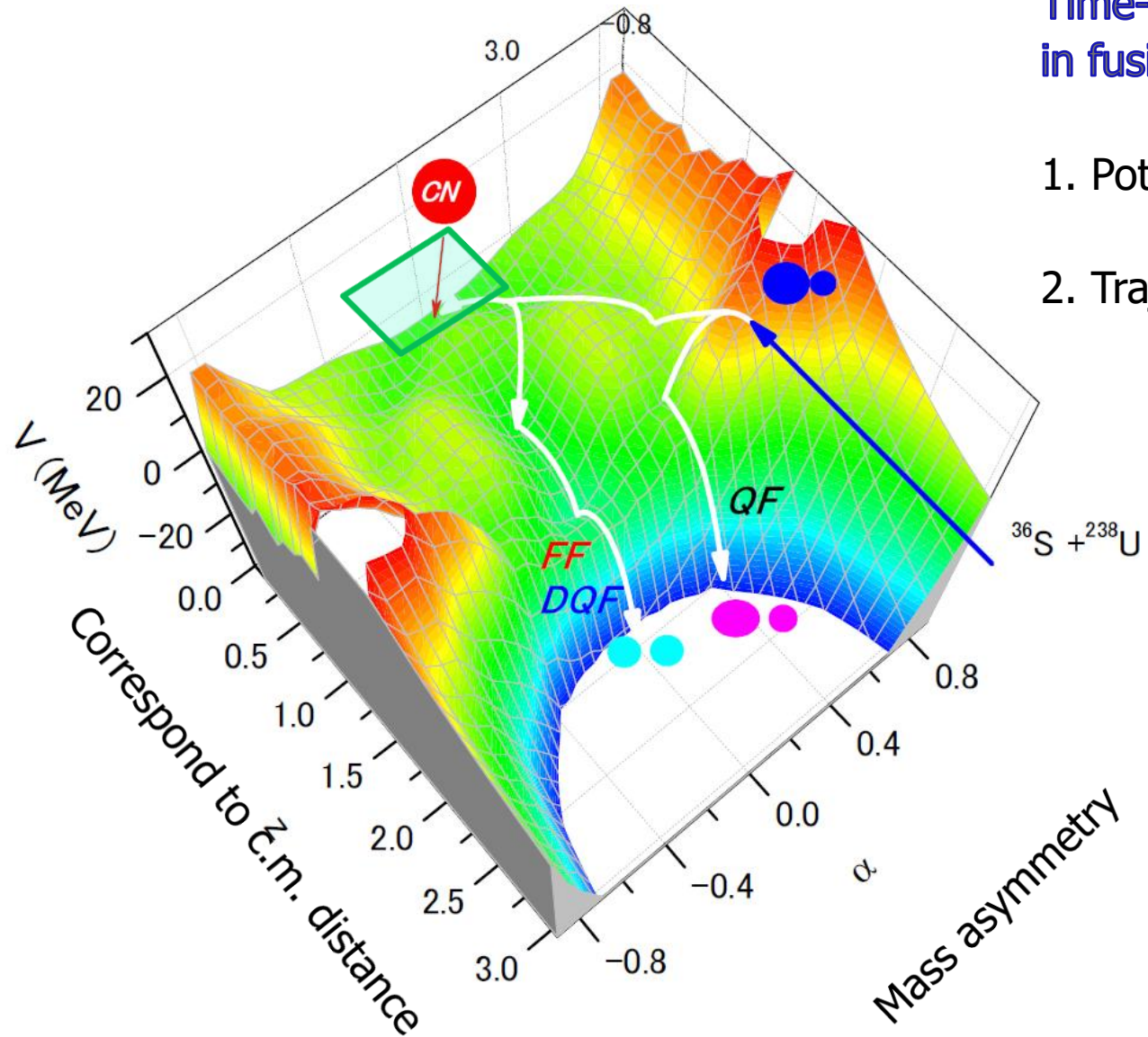
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Overview of Dynamical Process



Time-evolution of nuclear shape in fusion-fission process

1. Potential energy surface
2. Trajectory → described by equations

Nuclear shape

two-center parametrization (z, δ, α)

(Maruhn and Greiner,
Z. Phys. 251(1972) 431)

$$q(z, \delta, \alpha)$$

$$z = \frac{z_0}{BR}$$

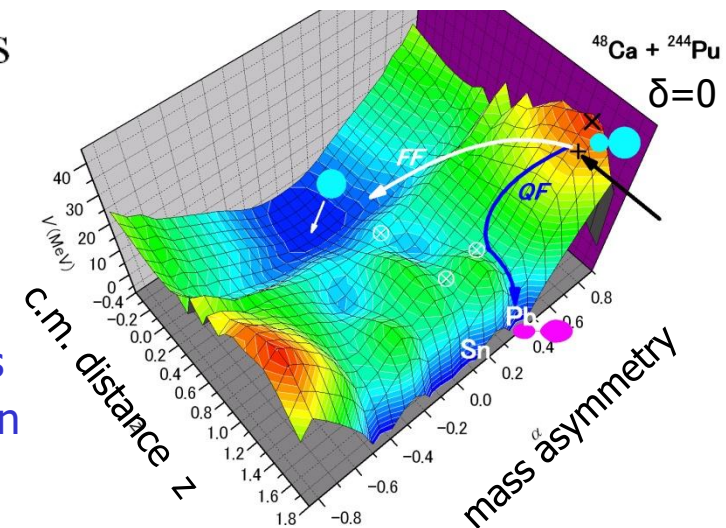
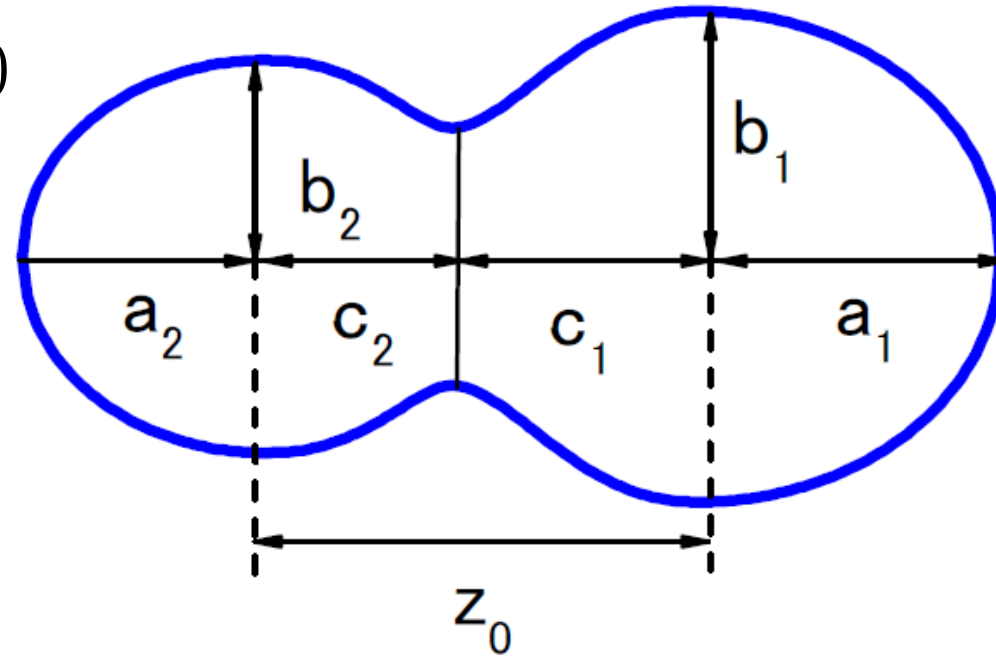
$$B = \frac{3 + \delta}{3 - 2\delta}$$

R : Radius of the spherical compound nucleus

$$\delta = \frac{3(a - b)}{2a + b} \quad (\delta_1 = \delta_2)$$

$$\alpha = \frac{A_1 - A_2}{A_{CN}}$$

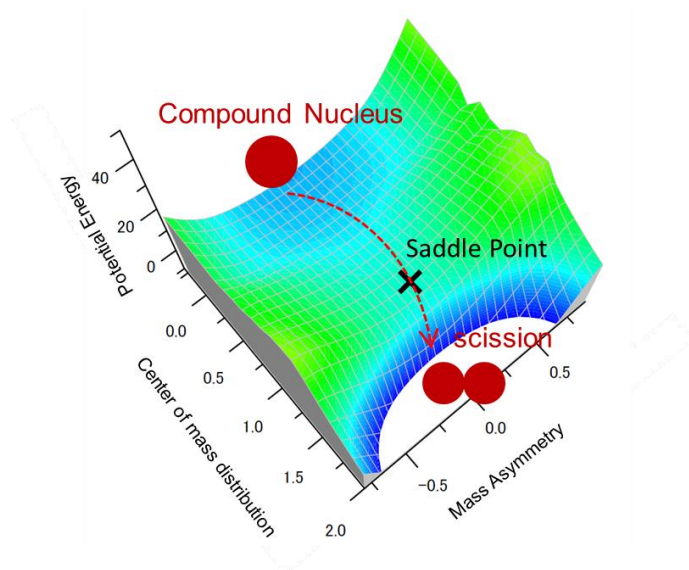
Trajectory which enters
into the spherical region
= fusion trajectory



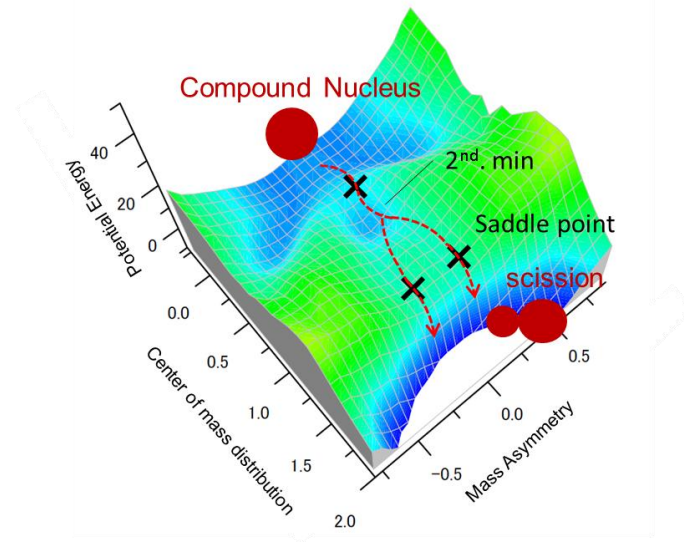
Potential energy

$$V(q, T) = V_{LD}(q) + V_{SH}(q, T)$$

Liquid drop model



Liquid drop and
Shell correction energy



Multi-dimensional Langevin Equation

$$\frac{dq_i}{dt} = (m^{-1})_{ij} p_j$$

$$\frac{dp_i}{dt} = -\frac{\partial V}{\partial q_i} - \frac{1}{2} \frac{\partial}{\partial q_i} (m^{-1})_{jk} p_j p_k - \underbrace{\gamma_{ij} (m^{-1})_{jk} p_k}_{\text{Friction dissipation}} + \underbrace{g_{ij} R_j(t)}_{\text{Random force fluctuation}}$$

Newton equation

ordinary differential equation

$\langle R_i(t) \rangle = 0$, $\langle R_i(t_1) R_j(t_2) \rangle = 2\delta_{ij} \delta(t_1 - t_2)$: white noise (Markovian process)

$$\sum_k g_{ik} g_{jk} = T \gamma_{ij}$$

Einstein relation

Fluctuation-dissipation theorem

q_i : deformation coordinate

(nuclear shape)

two-center parametrization (Z, δ, α)

(Maruhn and Greiner, Z. Phys. 251(1972) 431)

p_i : momentum

m_{ij} : Hydrodynamical mass

(inertia mass)

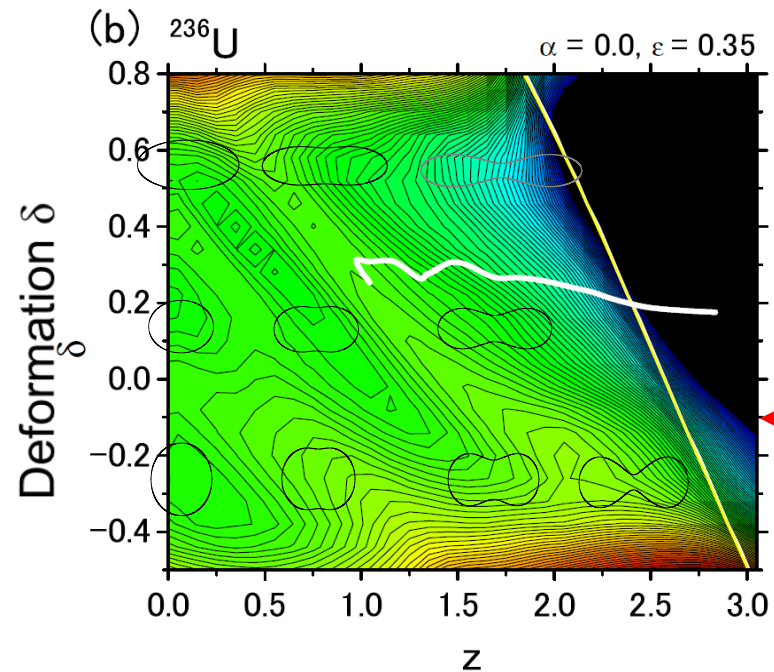
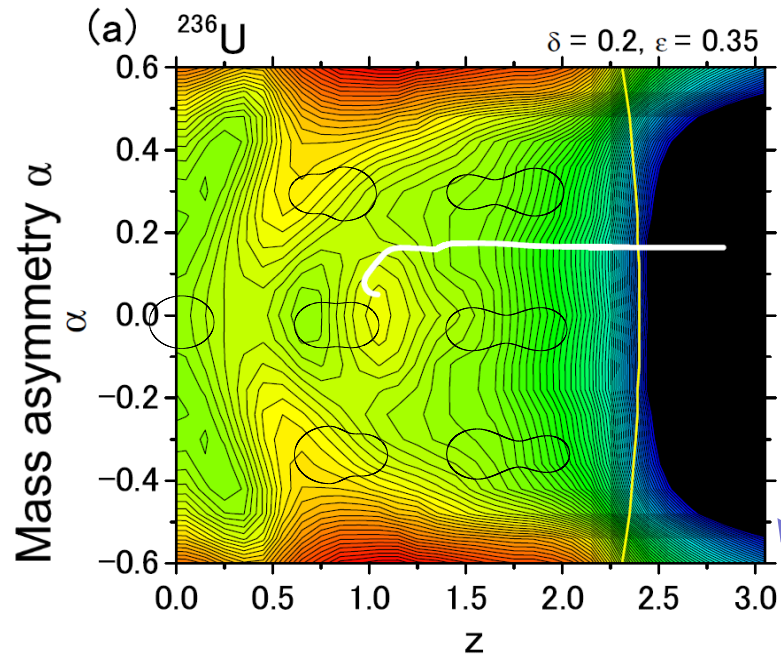
γ_{ij} : Wall and Window (one-body) dissipation

(friction)

$$E_{\text{int}} = E^* - \frac{1}{2} (m^{-1})_{ij} p_i p_j - V(q)$$

E_{int} : intrinsic energy, E^* : excitation energy

Without fluctuation



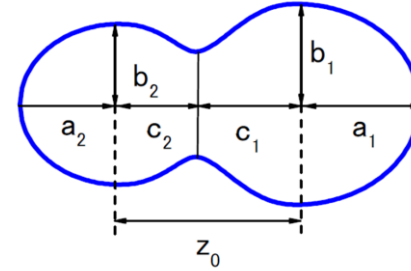
$$z = \frac{z_0}{BR}$$

$$B = \frac{3 + \delta}{3 - 2\delta}$$

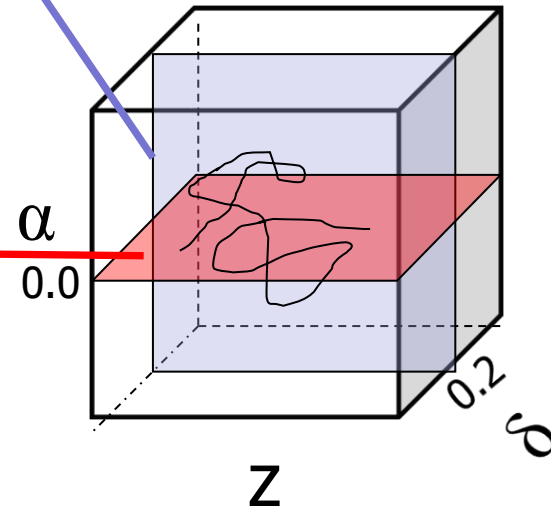
R : Radius of the spherical compound nucleus

$$\delta = \frac{3(a - b)}{2a + b}$$

$$\alpha = \frac{A_1 - A_2}{A_{CN}}$$

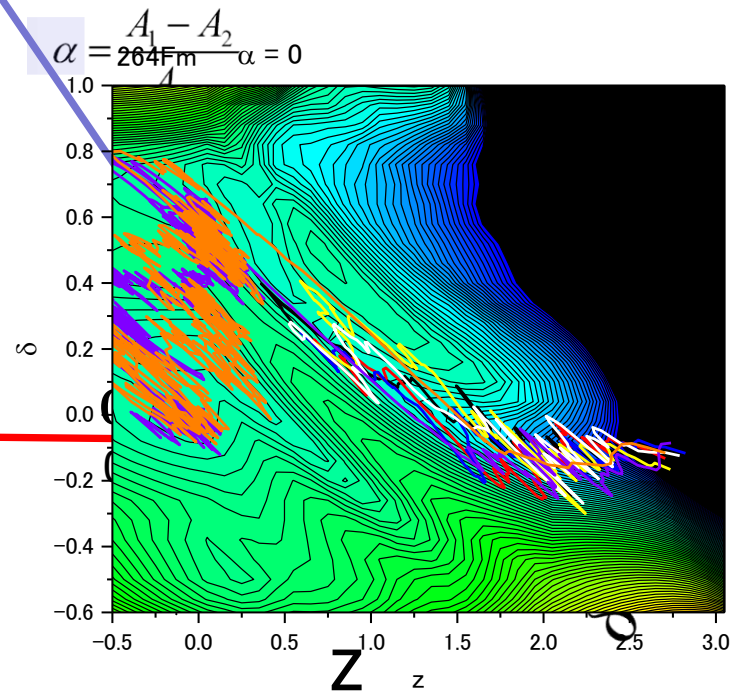
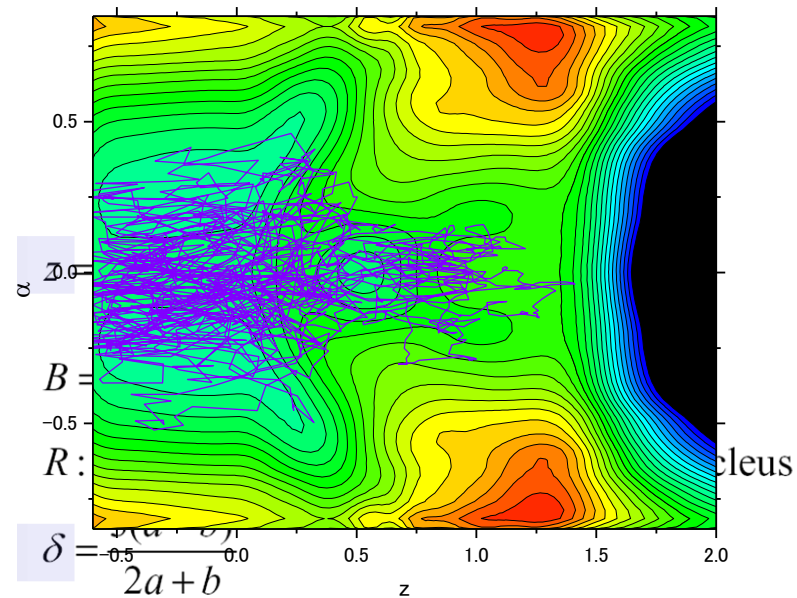
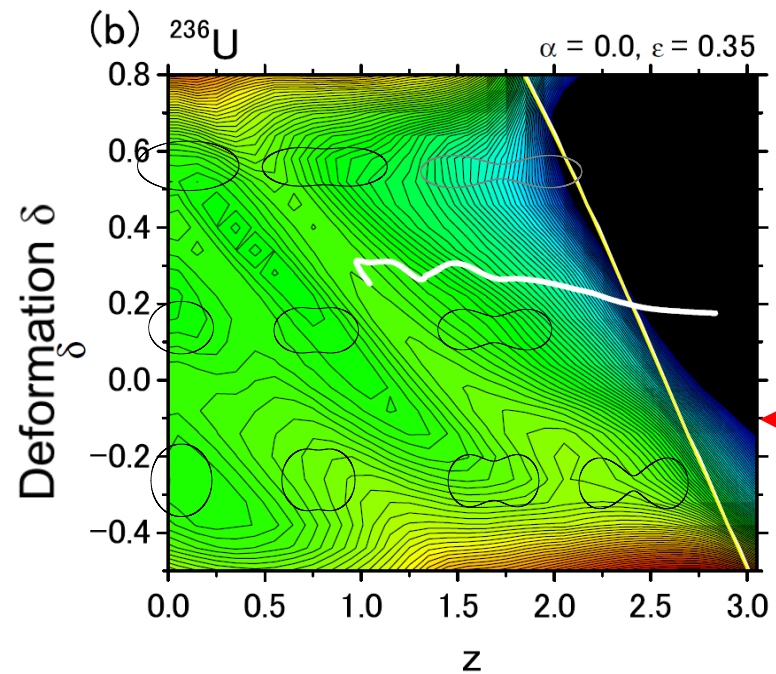
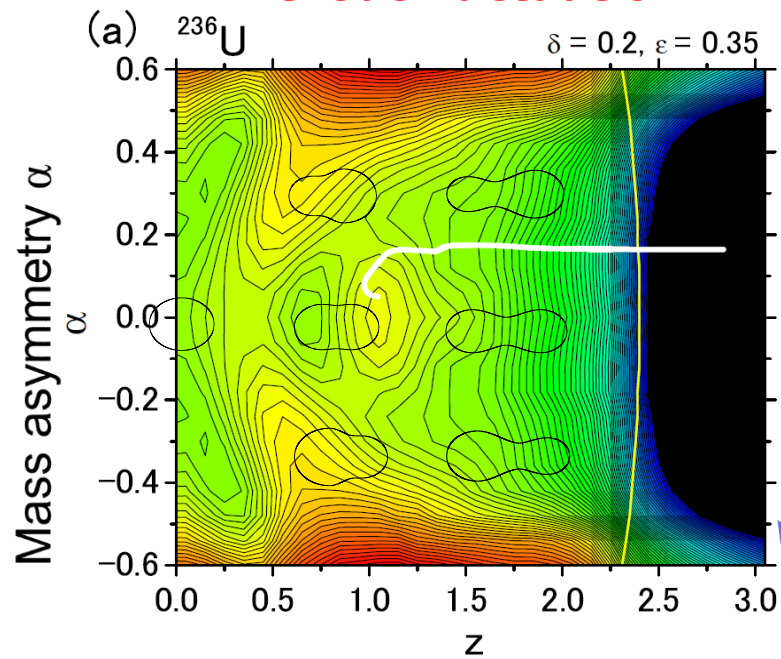


3D coordinate space



Projection on two-dim. plane

Without fluctuation



Projection on two-dim. plane

Fusion box

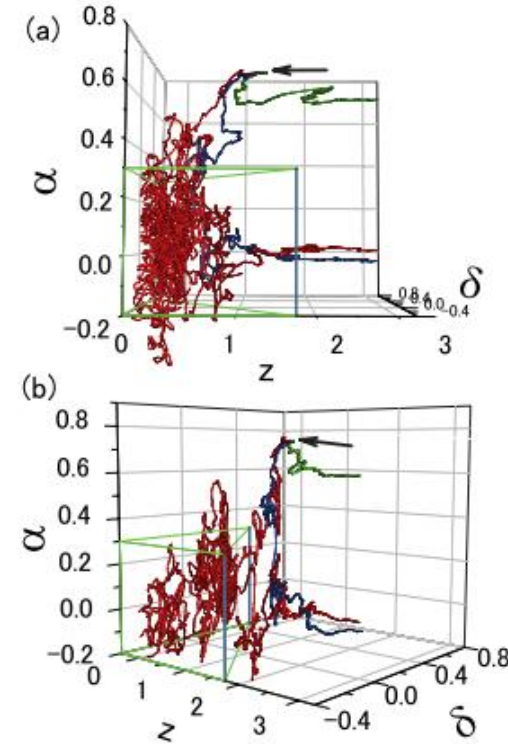
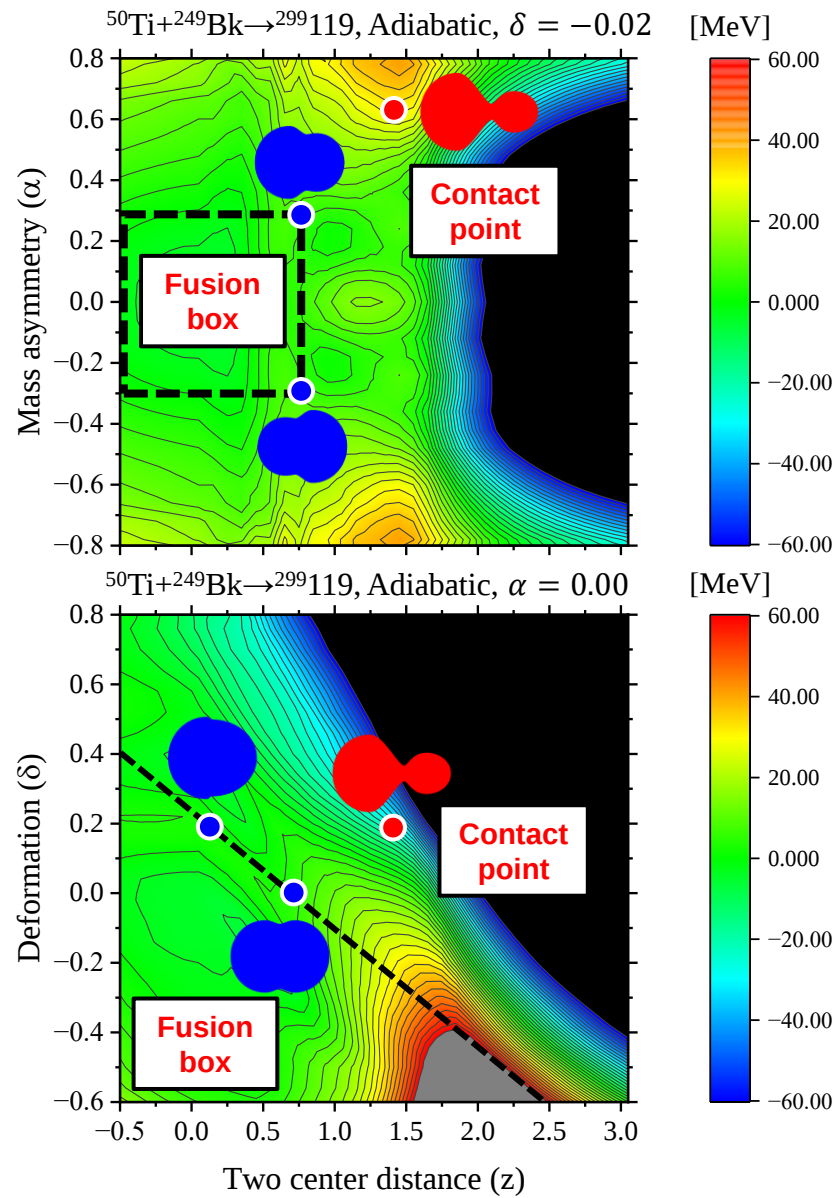


FIG. 11. (Color online) Sample trajectories in the three-dimensional coordinate space, $\{z, \delta, \alpha\}$, for the $^{36}\text{S} + ^{238}\text{U}$ reaction at $E^* = 35.5$ MeV. The arrow denotes the entrance point, where the Langevin calculations are started. The box represents the fusion box. The trajectories are plotted in the direction of the δ axis (a) and also in a different angle (b). The green, blue, and red lines represent QF, DQF, and FF, respectively.

Y. Aritomo, *et al.*, Phys. Rev. C **85**, 044614 (2012)

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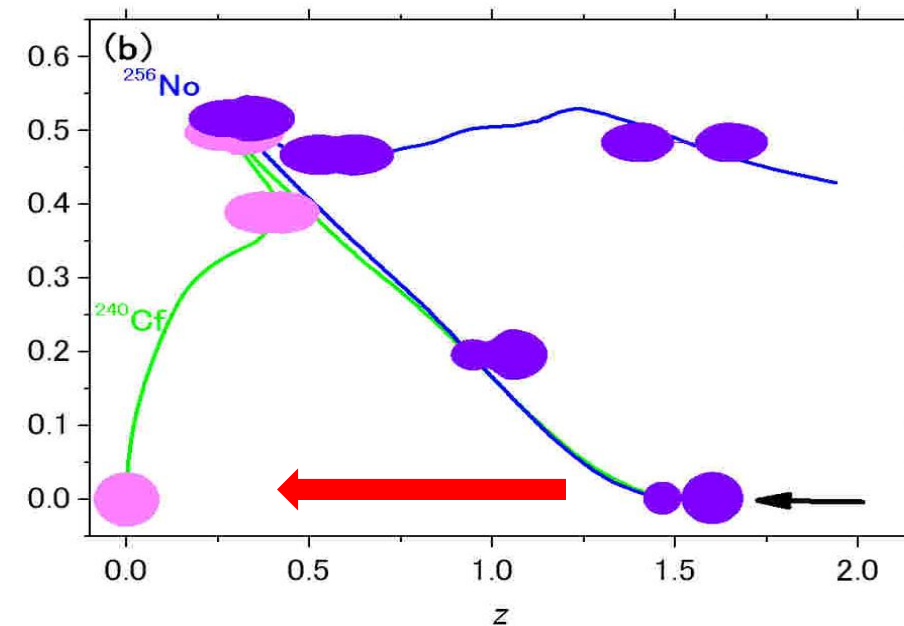
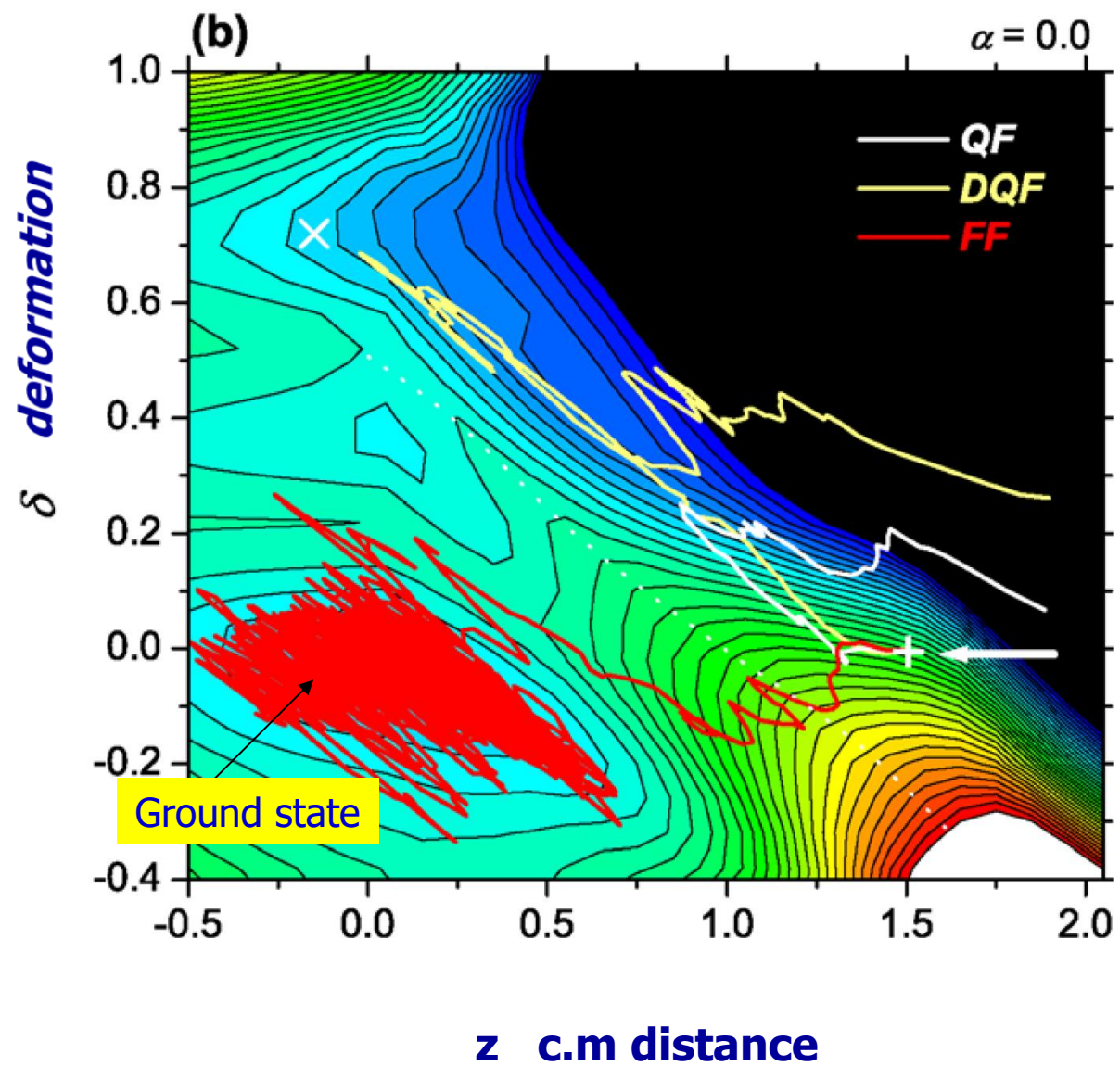
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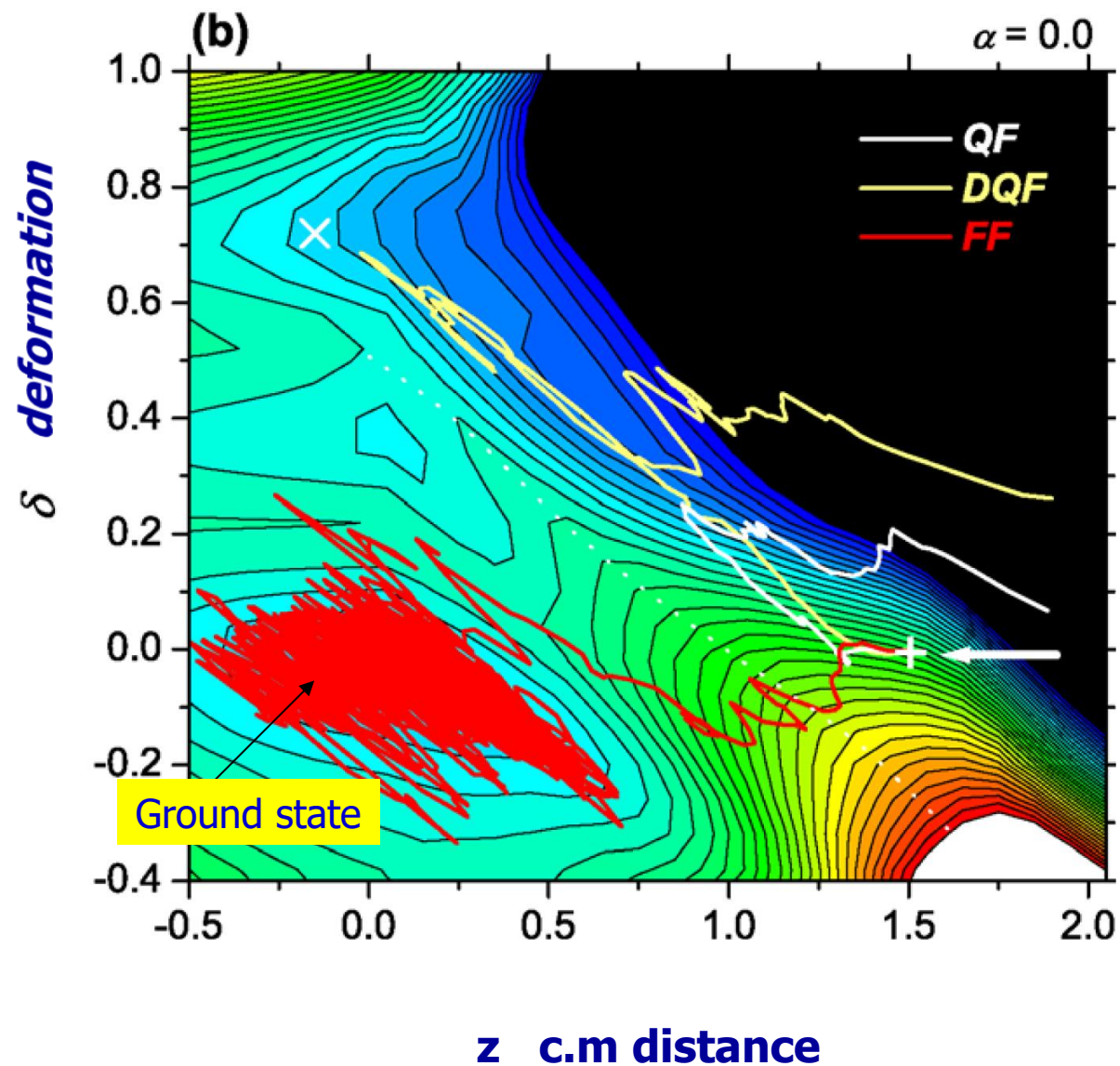
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4. Summary

$^{48}\text{Ca} + ^{244}\text{Pu}$



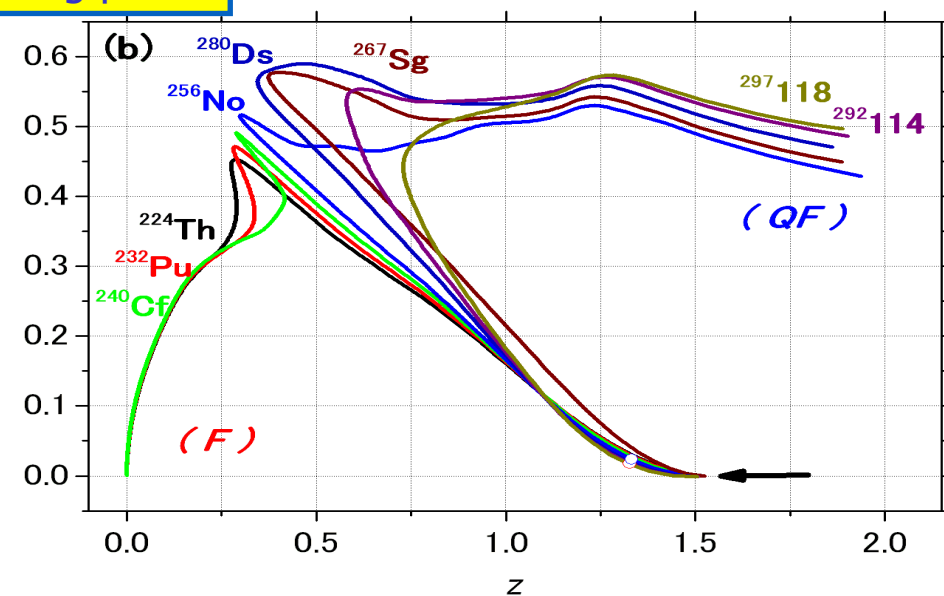
$^{48}\text{Ca} + ^{244}\text{Pu}$



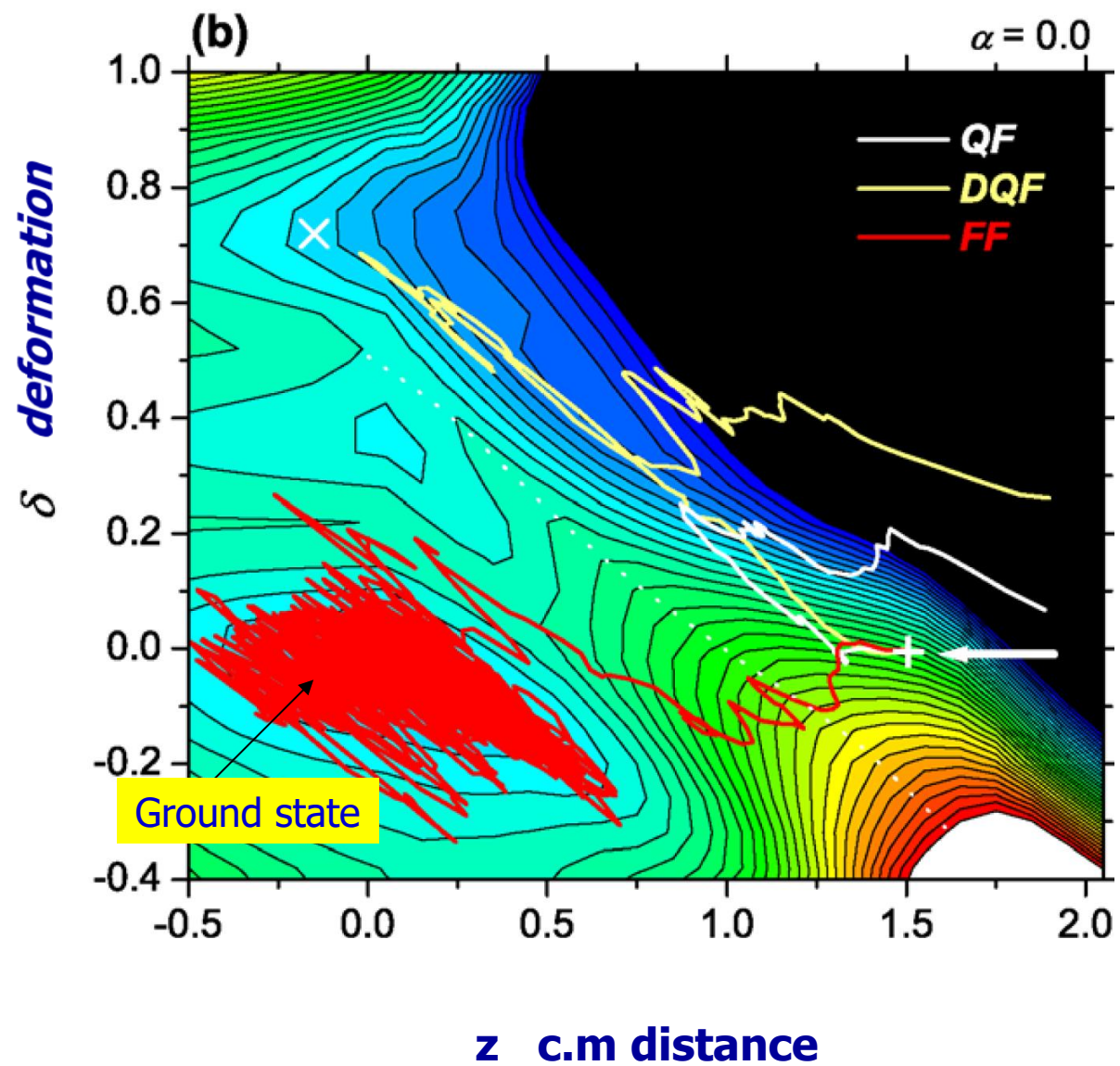
To produce Th, Pu, Cf, No, Sg, Ds, Fl, Og

Gross tendency of the trajectories in fusion-fission process

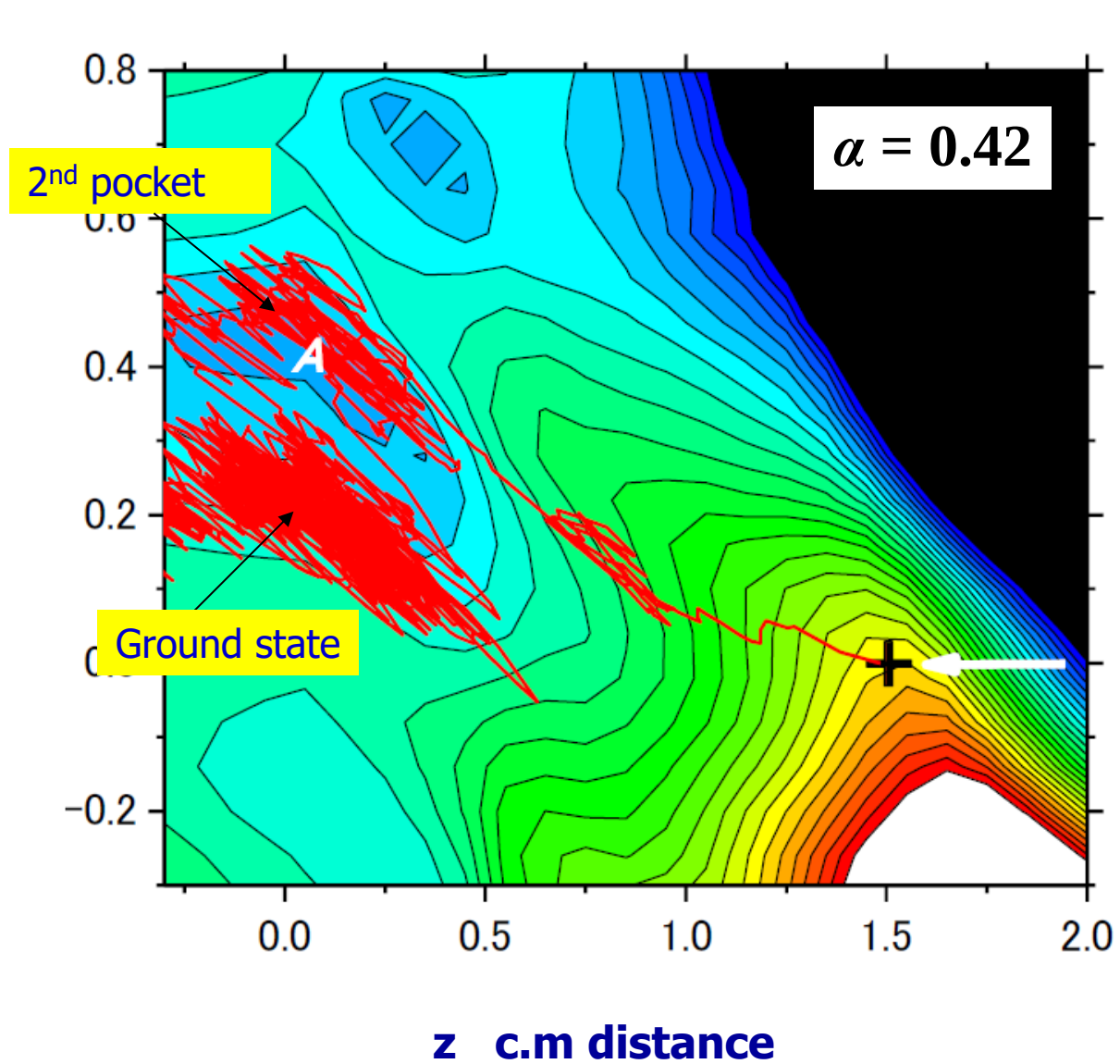
turning point

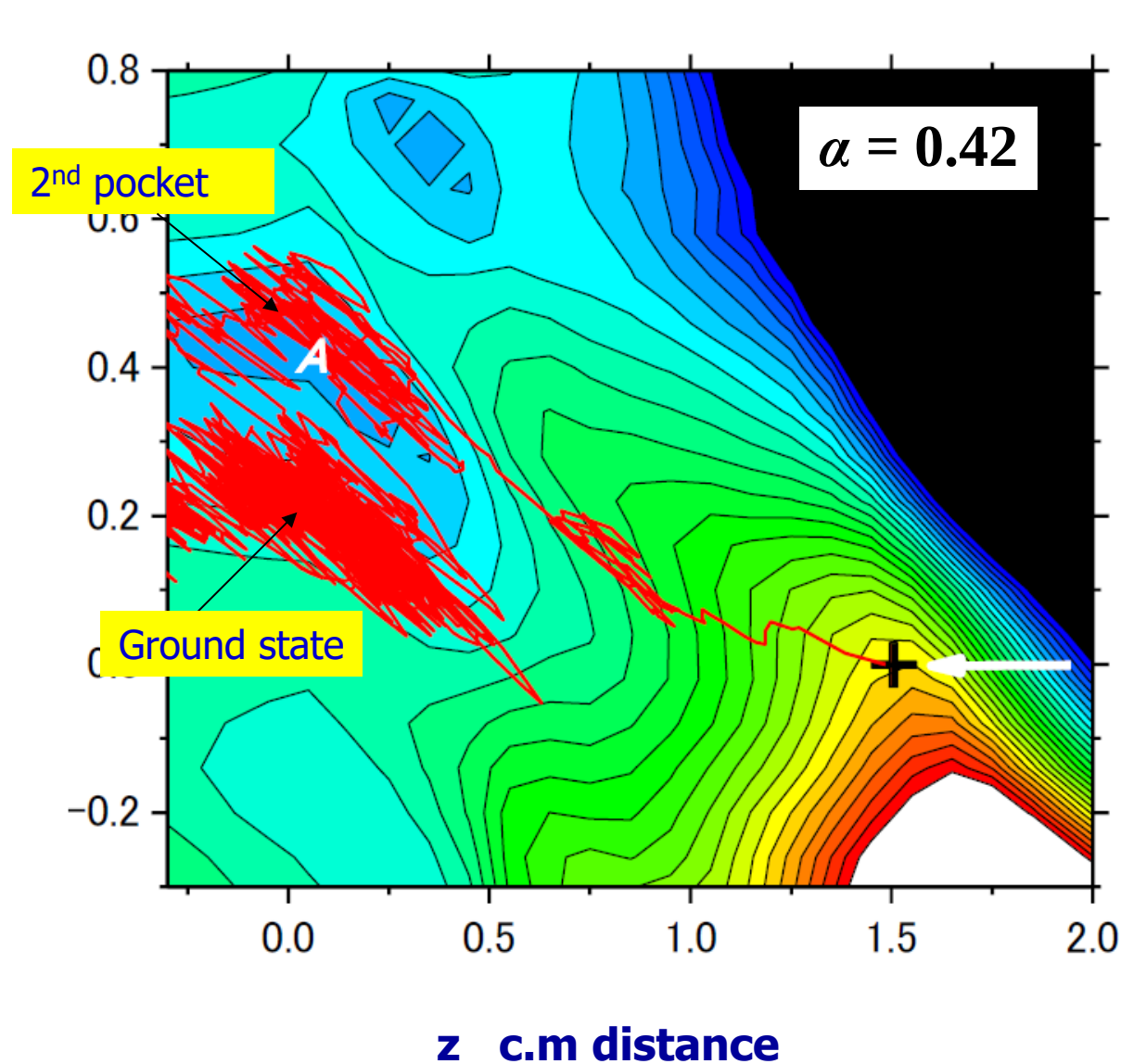
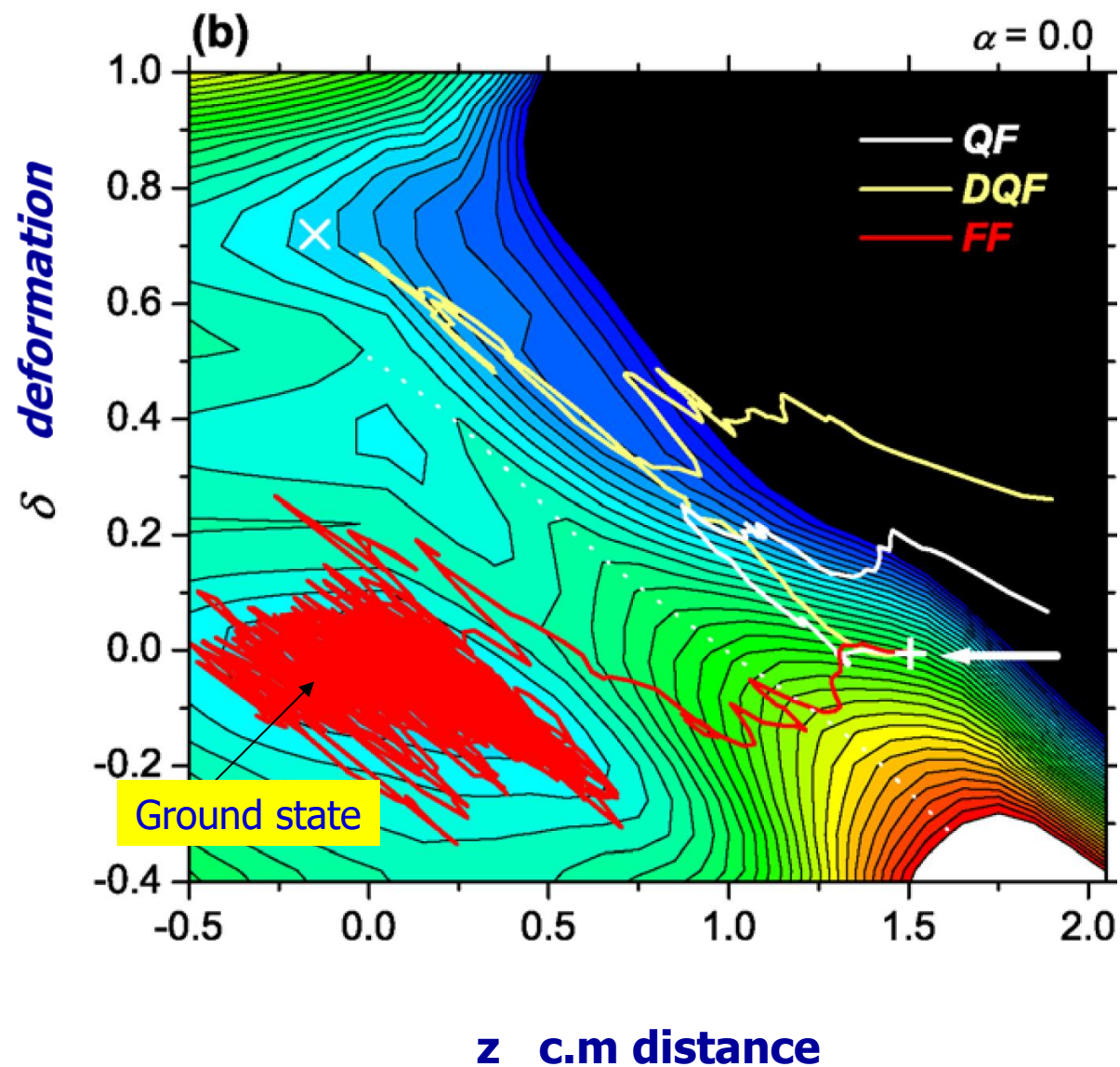


$^{48}\text{Ca} + ^{244}\text{Pu}$



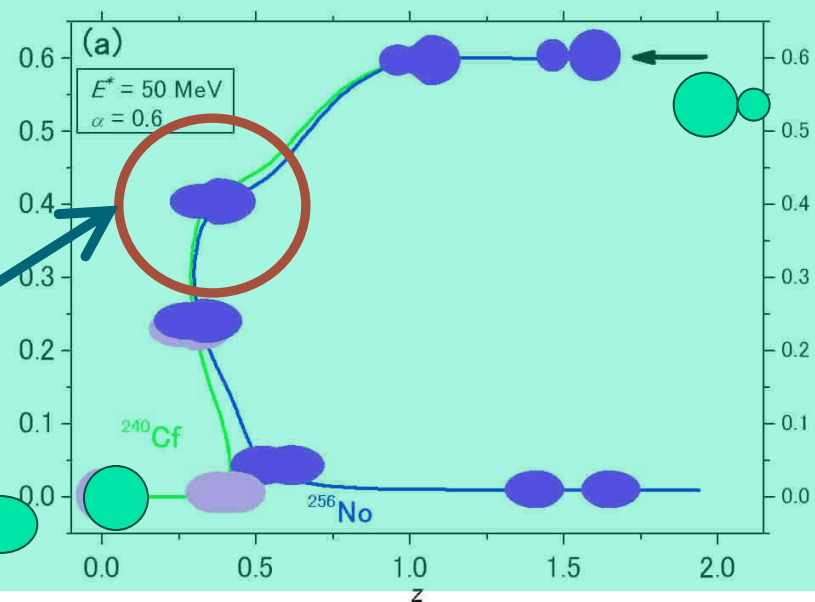
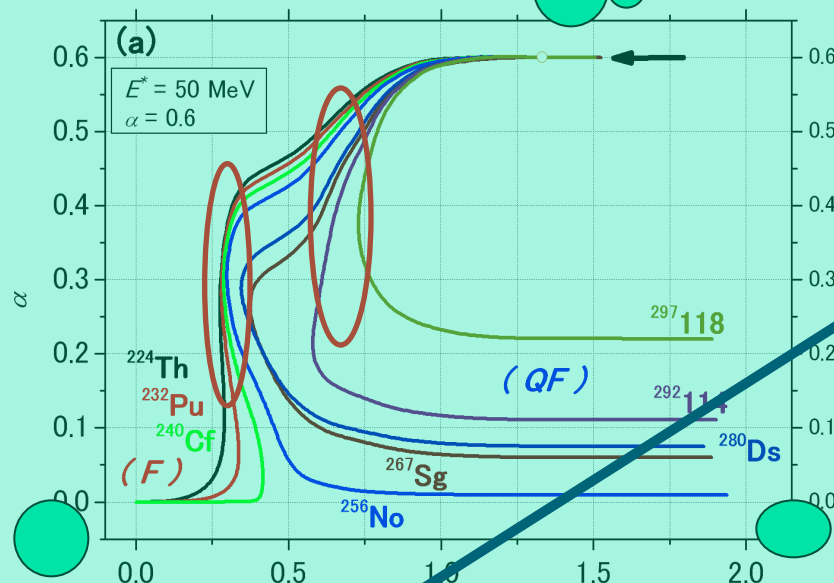
$^{48}\text{Ca} + ^{208}\text{Pb}$



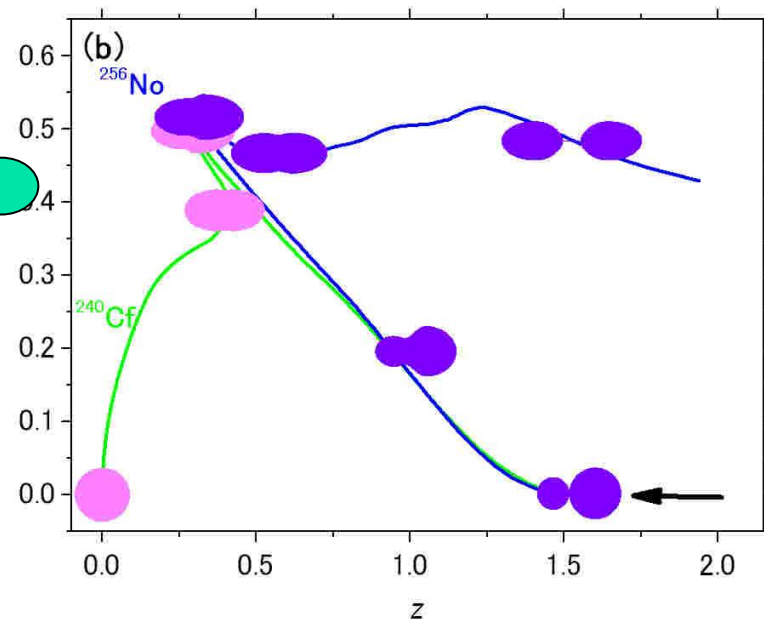
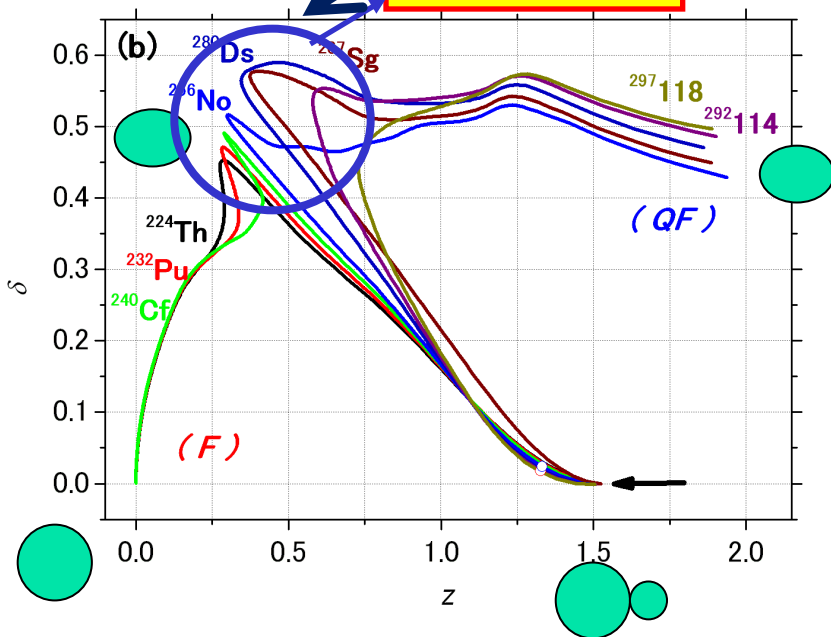


Mass Asymmetry α

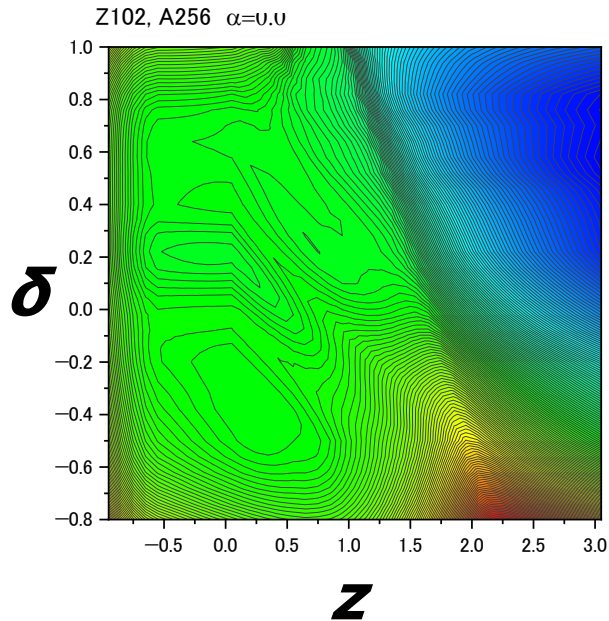
V_{LD} mean trajectory



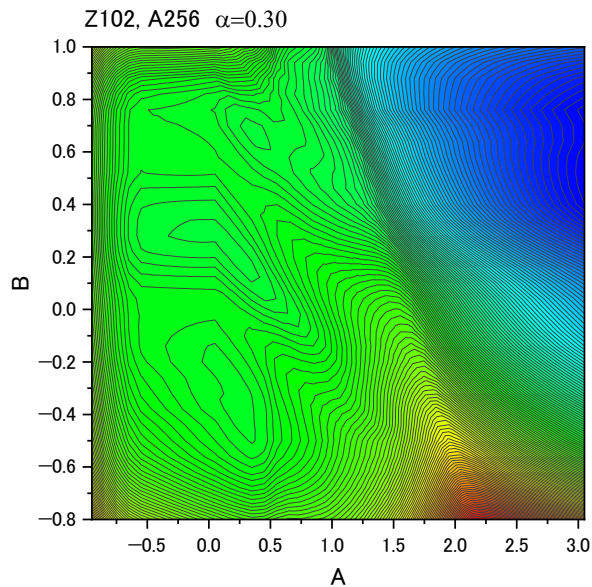
Deformation δ



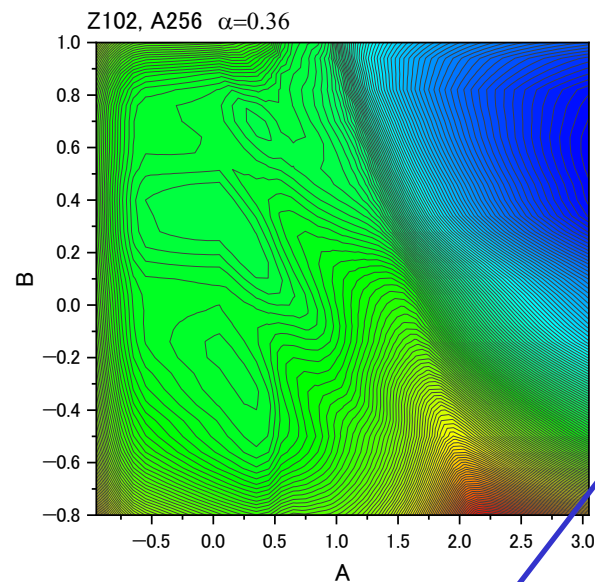
$\alpha = 0.0$



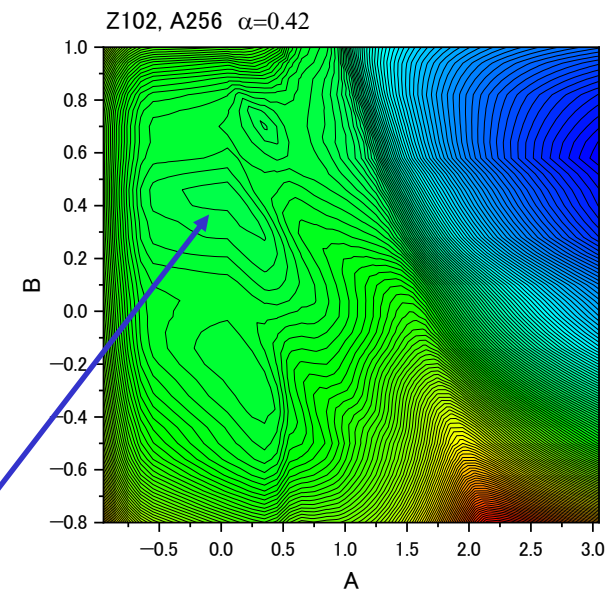
$\alpha = 0.30$



$\alpha = 0.36$

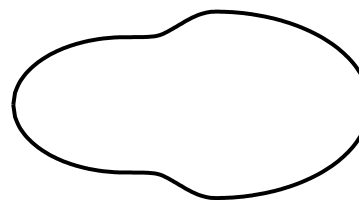


$\alpha = 0.42$



$\alpha = 0.42$

$\delta = 0.40$



2nd Pocket

$\alpha=0.42$

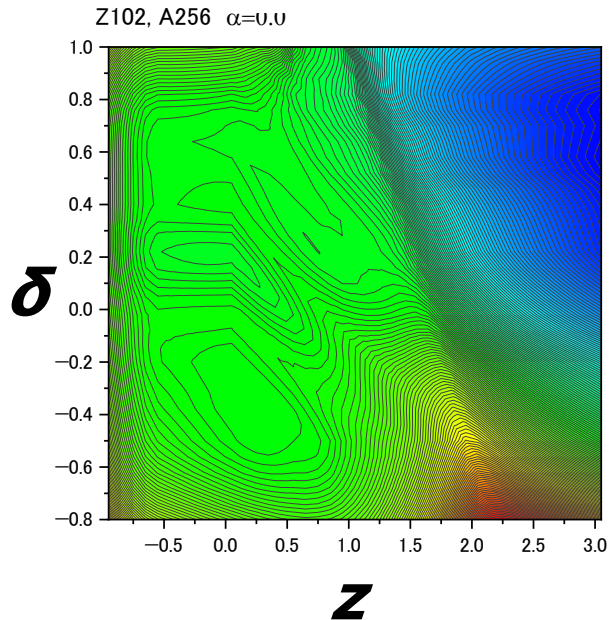
Corresponds to

$N=110$ deformed shell

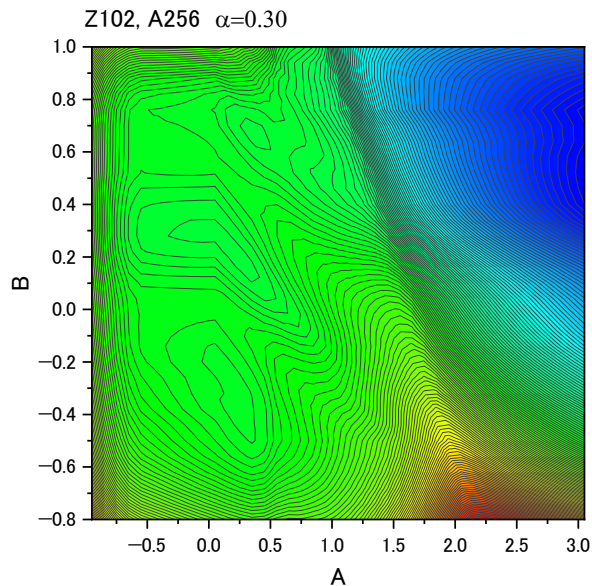
^{184}W ($Z=74$, $N=110$)

^{186}Os ($Z=76$, $N=110$)

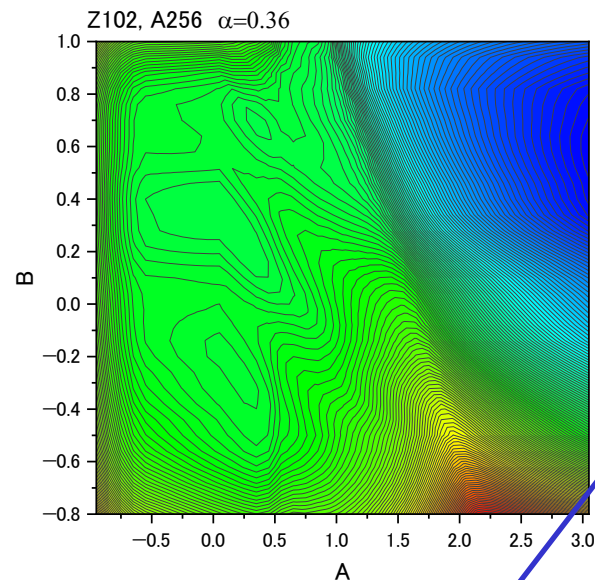
$\alpha = 0.0$



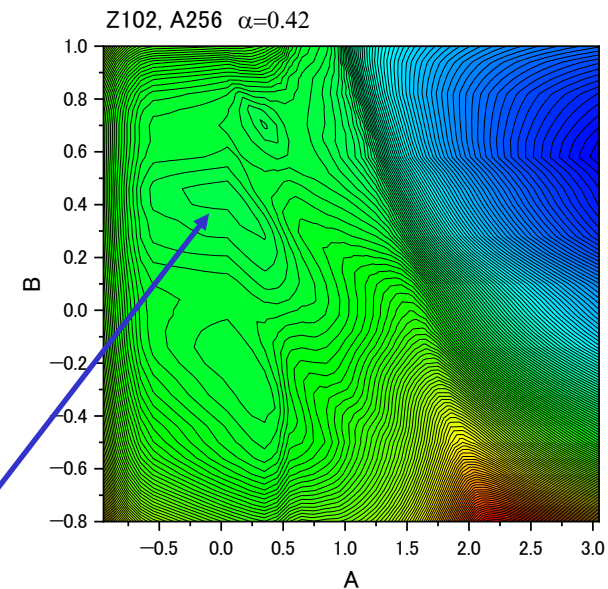
$\alpha = 0.30$



$\alpha = 0.36$



$\alpha = 0.42$



$\alpha = 0.42$

$\delta = 0.40$



2nd Pocket

$\alpha=0.42$

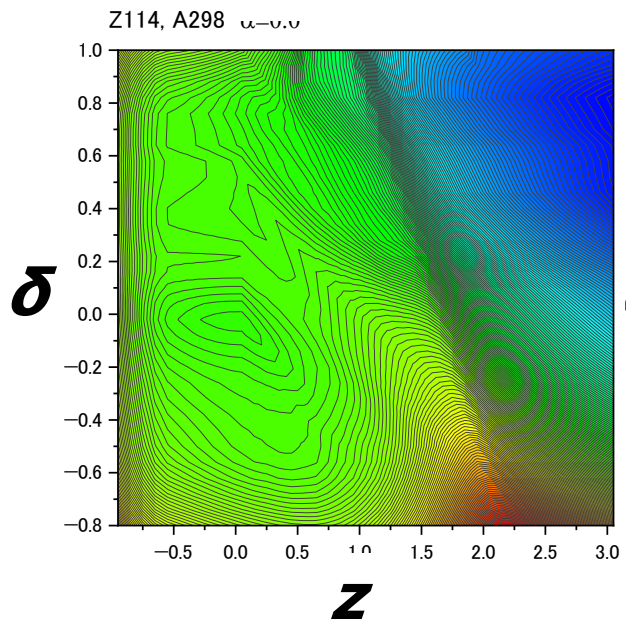
Corresponds to

$N=110$ deformed shell

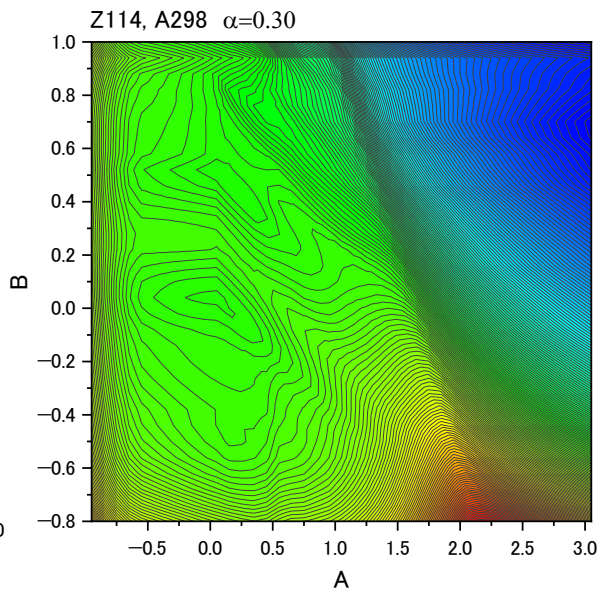
^{184}W ($Z=74$, $N=110$)

^{186}Os ($Z=76$, $N=110$)

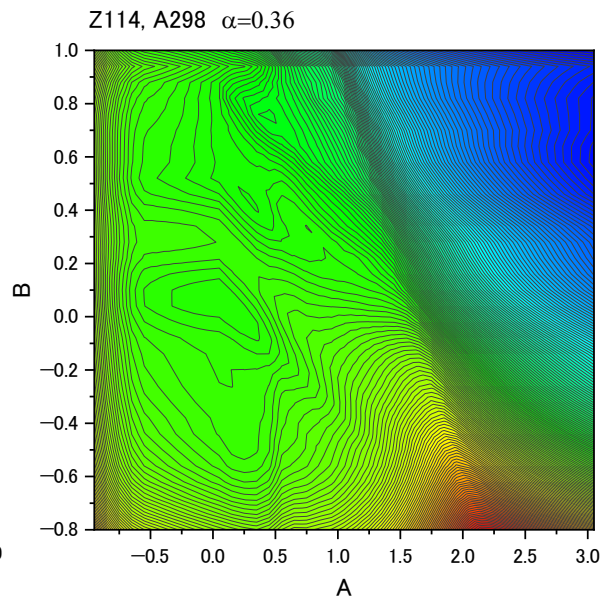
$\alpha = 0.0$



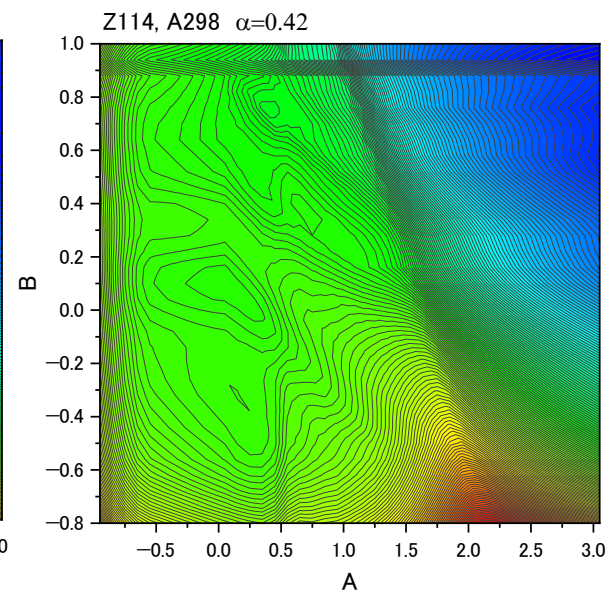
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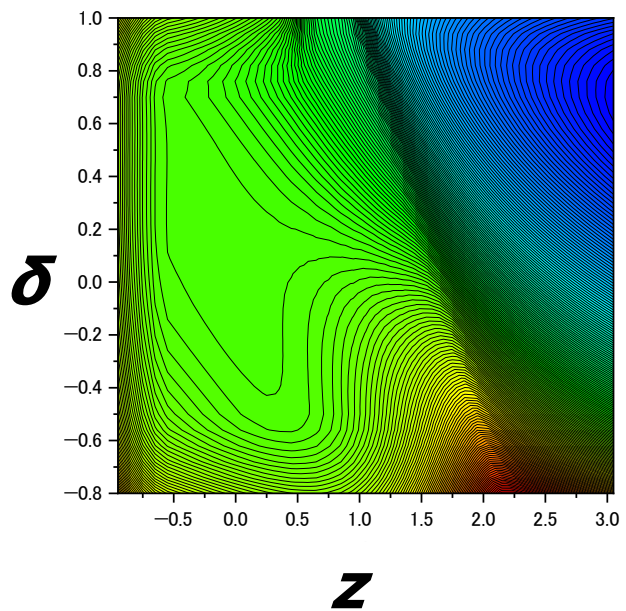
$\alpha = 0.36$



$\alpha = 0.42$

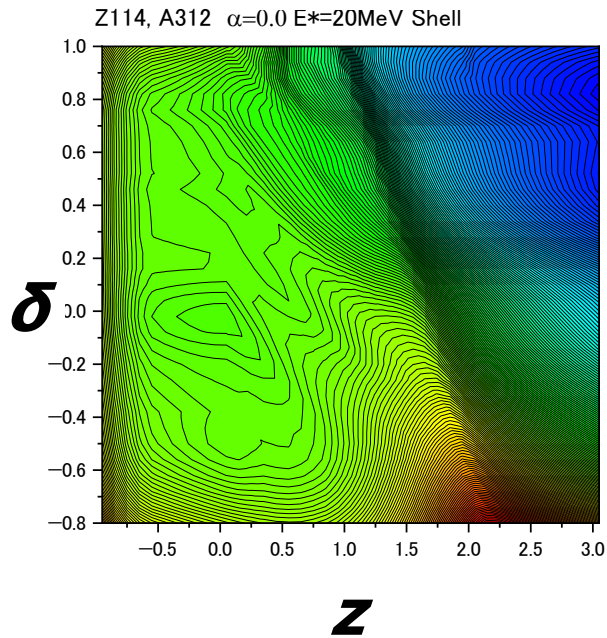


Z114, A298 $\alpha=0.0$

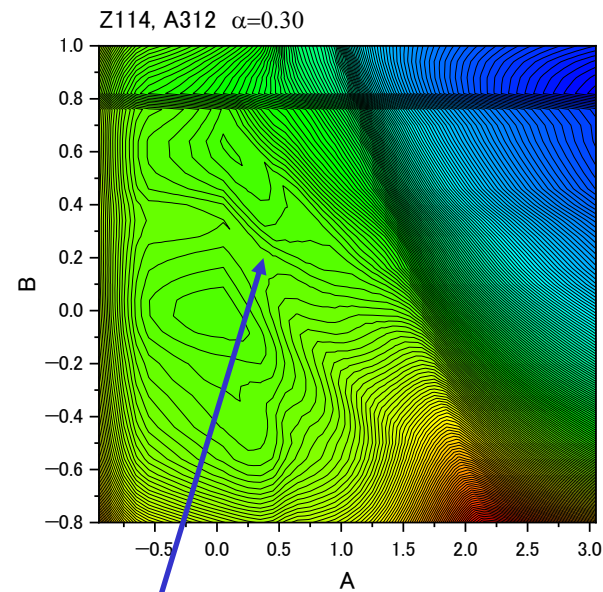




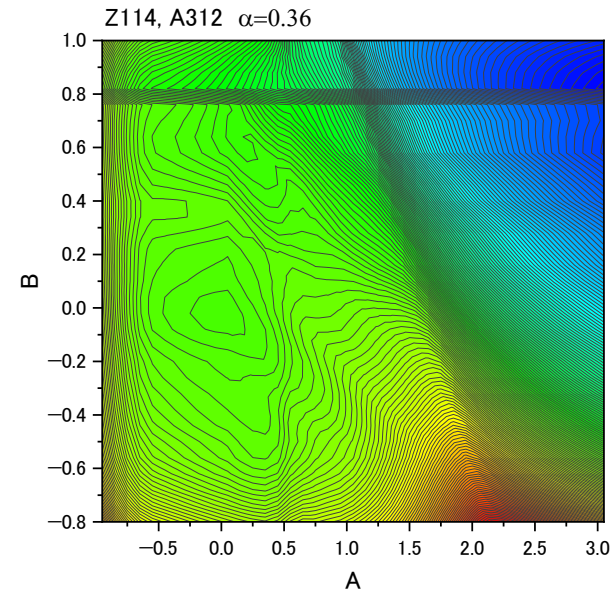
$\alpha = 0.0$



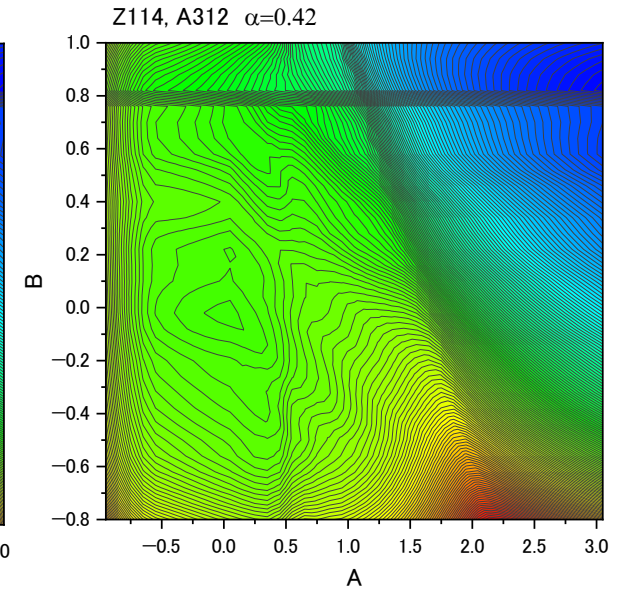
$\alpha = 0.30$



$\alpha = 0.36$



$\alpha = 0.42$

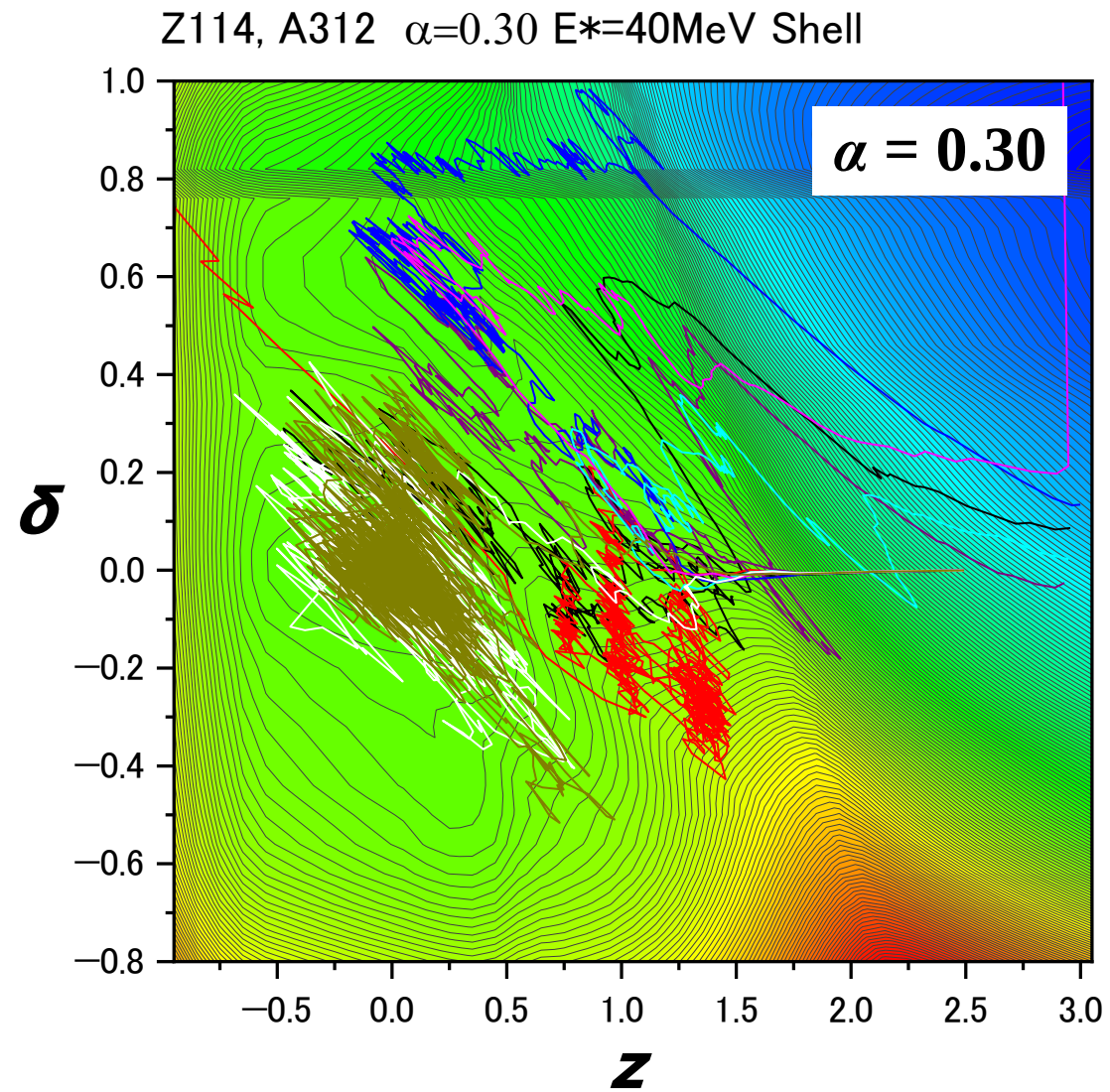


$\alpha = 0.30$

$\delta = 0.10$



Flat region
 $\alpha=0.30$
Corresponds to
N=126 Spherical shell
 ^{208}Pb (Z=82, N=126)



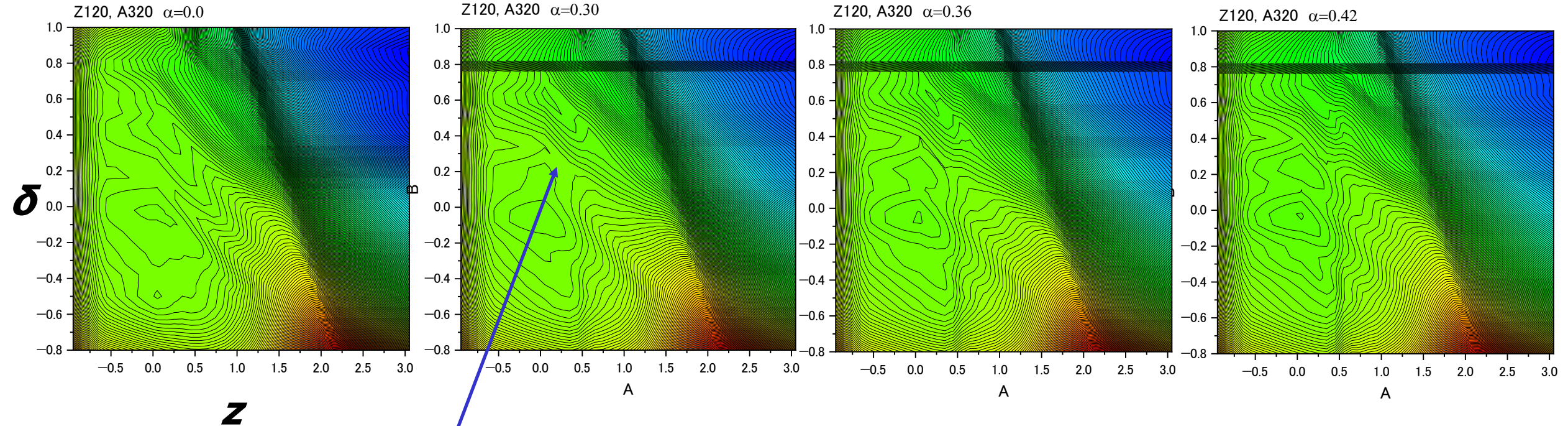


$$\alpha = 0.0$$

$$\alpha = 0.30$$

$$\alpha = 0.36$$

$$\alpha = 0.42$$

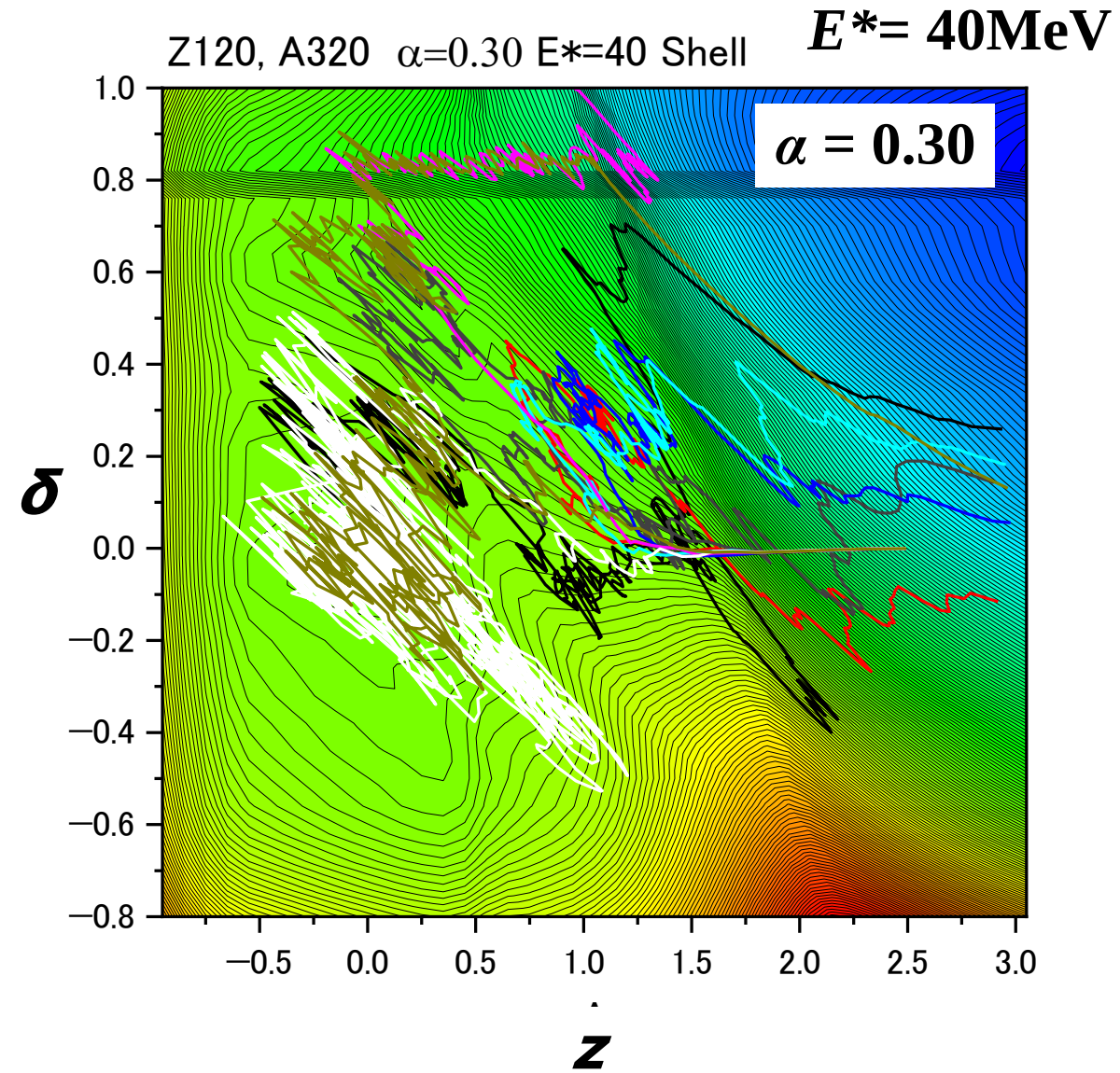


$$\alpha = 0.30$$

$$\delta = 0.10$$



Flat region
 $\alpha=0.30$
Corresponds to
 $N=126$ Spherical shell
 ^{208}Pb ($Z=82, N=126$)



Summary and Conclusion

ADVANTAGE using Nuclei with **Strong Shell Structure**, **Spherical Target**, **RI beams**

1. **Suppression of incident energy dissipation**
2. **Use of the second pocket in fusion process**
3. **Rapid and many neutron emissions**

We need information

on the **highly accurate properties** of SHE in the **neutron-rich region**

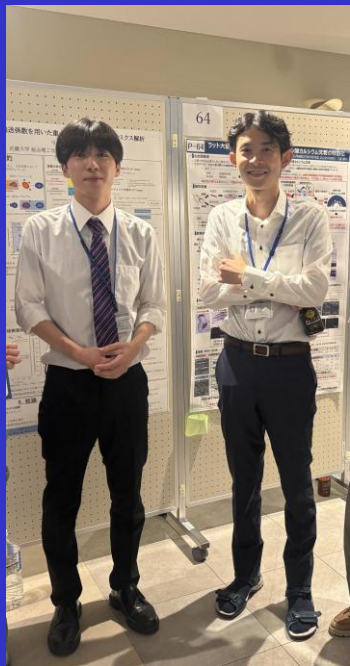
← Study of **Nuclear Structure**

Shell correction energy

Deformation of g.s.

mass, neutron separation energy → more accurate mass table for unknown region

Collaborators



K. Kawai, K. Nakajima
A. Yumikura
Kindai University



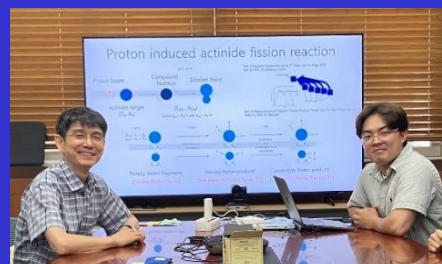
S. Takagi
RIKEN



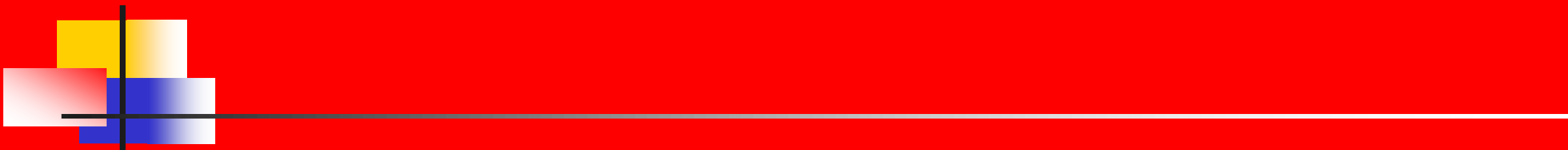
N. Nishimura
Kogakuin Univ.



Y. Kim,
I. Shin
IBS, Korea



C. Song,
C. Lee



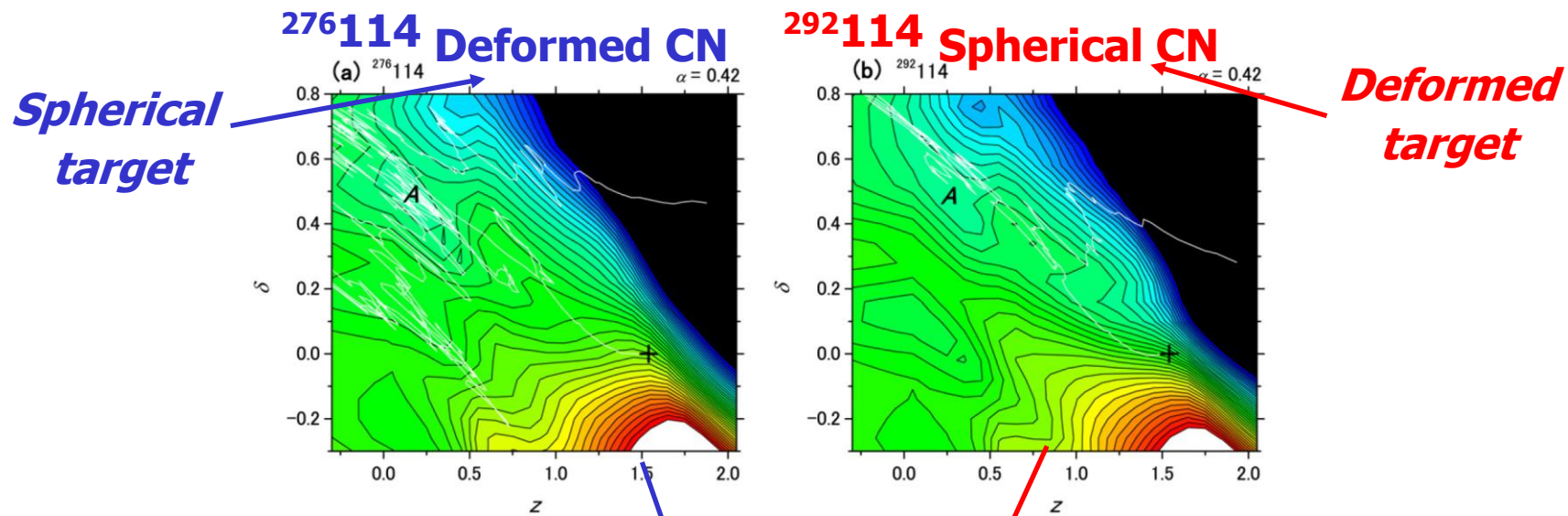
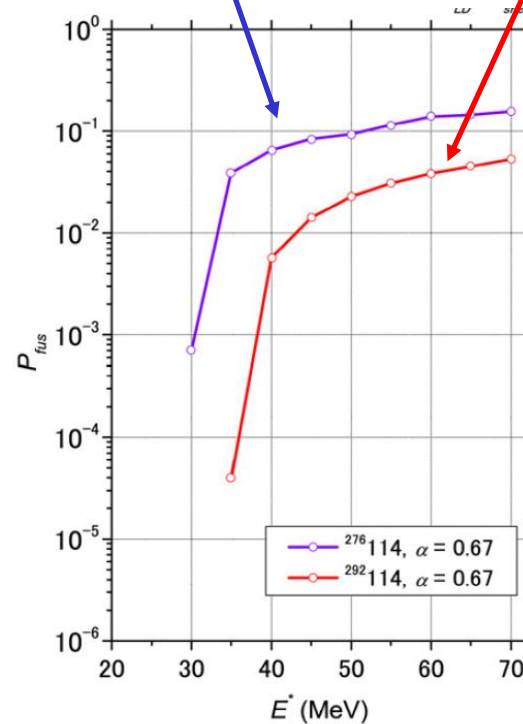
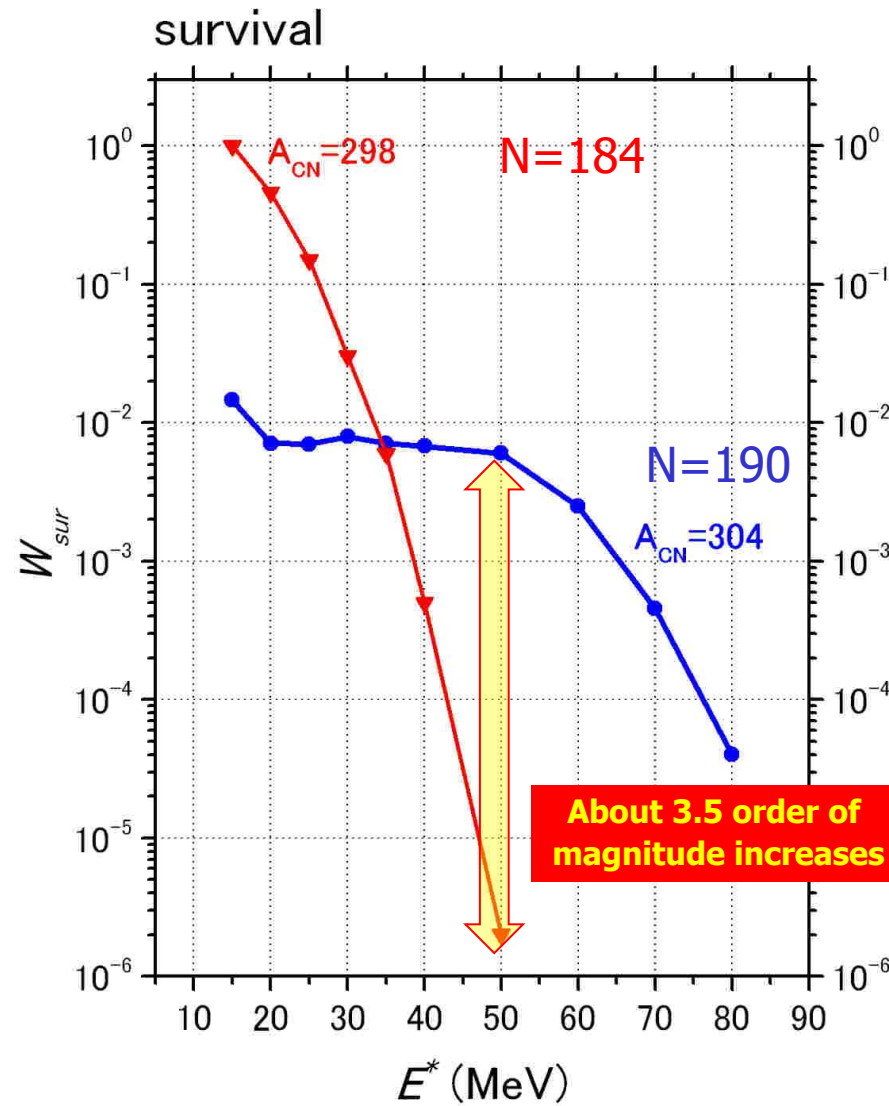


Fig. 8. (Colour online.) Sample trajectory projected onto the z - δ plane at $\alpha = 0.42$ of $V_{LD} + E_{shell}^0$ for (a) $^{276}_{114}$ (deformed nucleus) and (b) $^{292}_{114}$ (spherical one). The trajectory starts at $\alpha = 0.67$ and $E^* = 40$ MeV. Symbols are given in the text.



Y. Aritomo
Nucl. Phys. A 780
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Smoluchowski equation



Due to many neutron emissions

① Approaching to **Island of Stability**
(large V_{sh})

Due to many neutron emissions
→ E^* of CN decreases

② Recovers of **shell correction energy**
 V_{sh}

→ large fission Barrier

deformation of the nucleus

