



MAX PLANCK INSTITUTE  
FOR GRAVITATIONAL PHYSICS  
(ALBERT EINSTEIN INSTITUTE)



## LISA Instrumentation III: instrument modelling, TDI, L0-L1

LISA School for Early-career Scientists  
11th of October 2025, Les Houches  
Olaf Hartwig

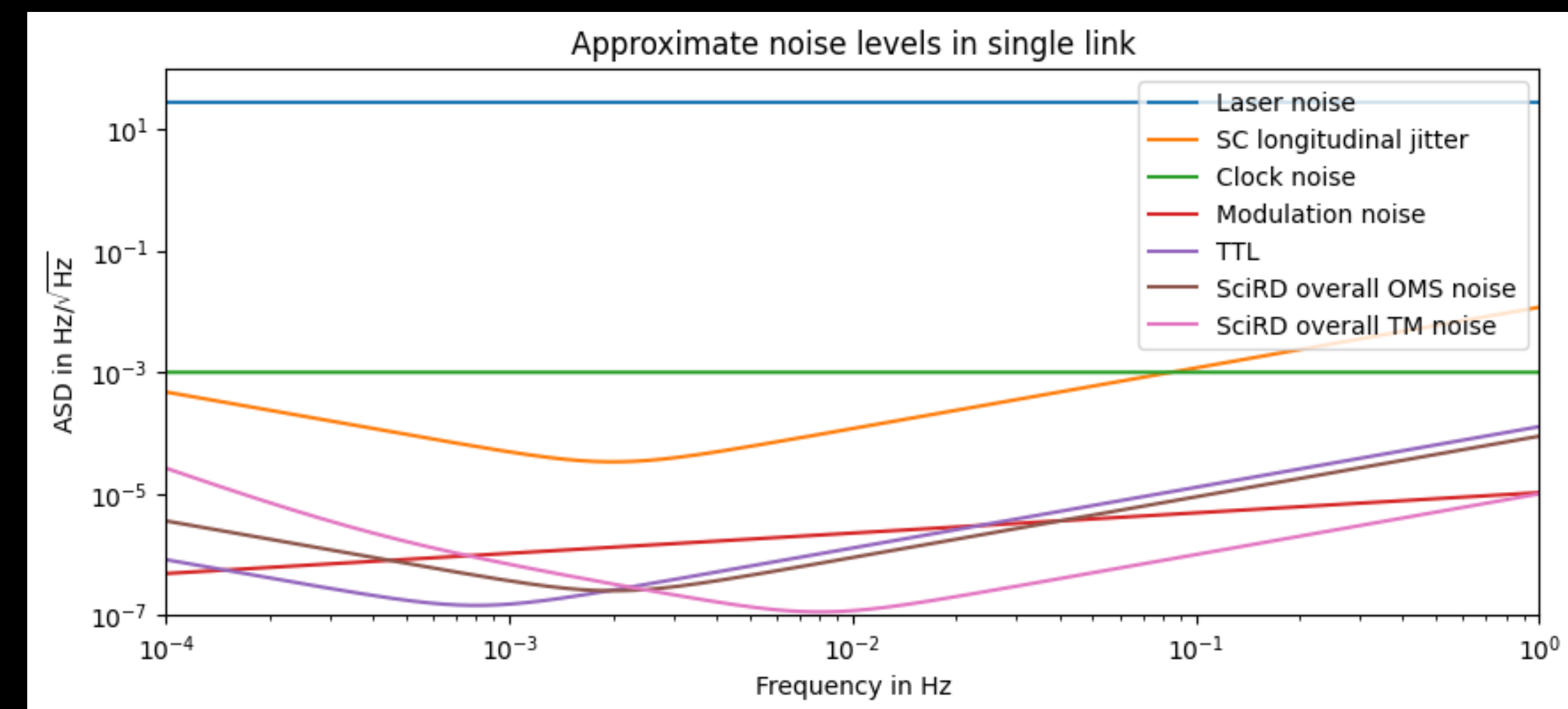
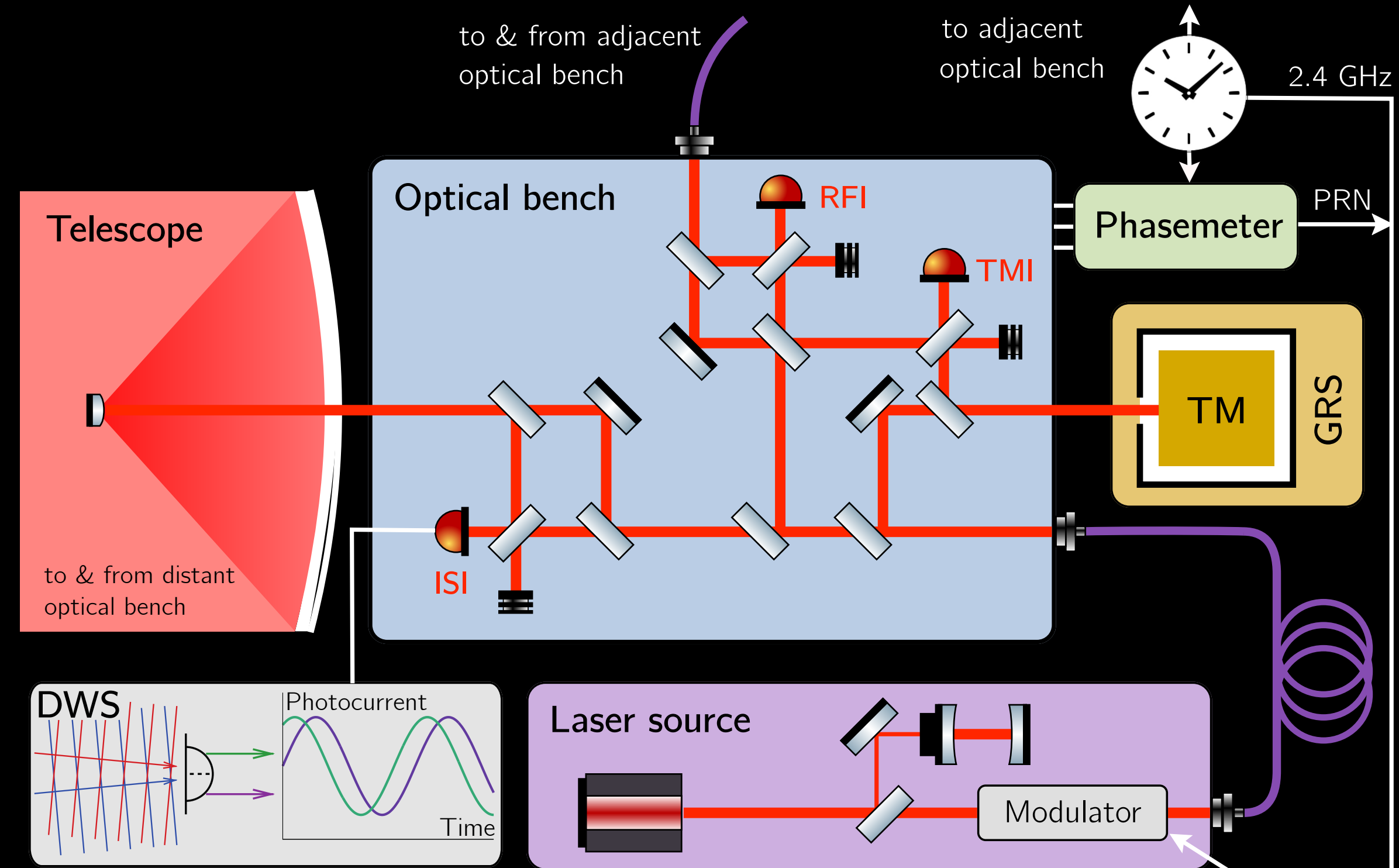
# Summary on instrument

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- LISA is not exactly ‘LIGO in Space’, but faces unique technical challenges
- LISA data pre-processing (‘L0.5-L1’):
  - Combines  $\approx 66$  main scientific interferometric measurements with ground tracking information and auxiliary sensors
- Outputs:
  - 3 synchronized scientific variables, 2 ‘Michelson-like’, one ‘null-channel’
  - Other quantities needed for DA: spacecraft positions, time couples, light-travel times, noise estimates
- We will try to summarise how these processing steps work
- Not covered in this talk: countless technical details and engineering!

# LISA measurements

- The main LISA measurements:
  - 3 main interferometry signals (SCI, RFI, TMI)
  - Auxiliary sideband beatnotes in the SCI for clock noise exchange
  - Auxiliary sideband beatnotes in the RFI for local frequency distribution correction
  - Absolute ranging via additional pseudo-random noise (PRN) code modulation (+ local codes)
  - Angular jitter correction via differential wavefront sensing (DWS)
- Dominant noise sources to be suppressed:
  - Laser noise
  - S/C longitudinal jitter
  - Clock noise in main phase measurements
  - Timing noise in clock distribution chain
  - and angular jitter (TTL)



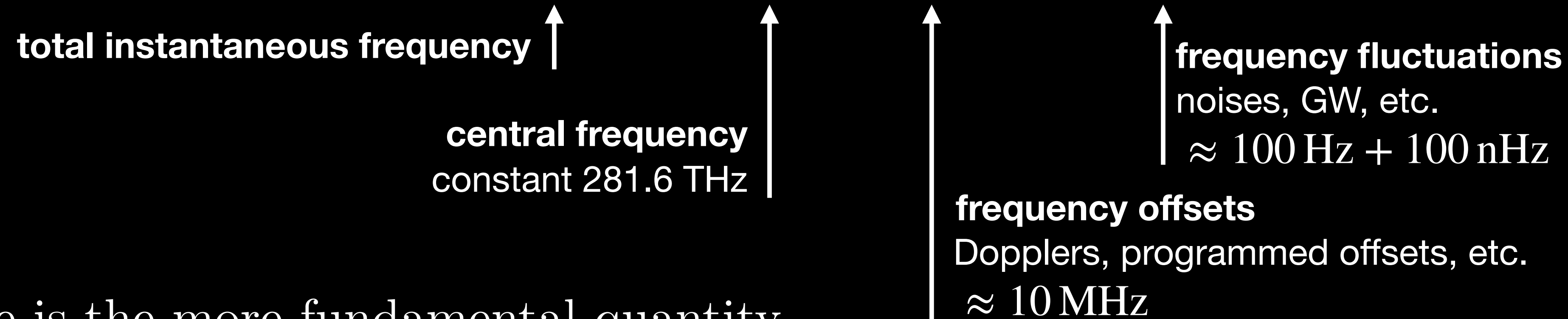
# LISA Measurements: high-level model



# Laser Beams

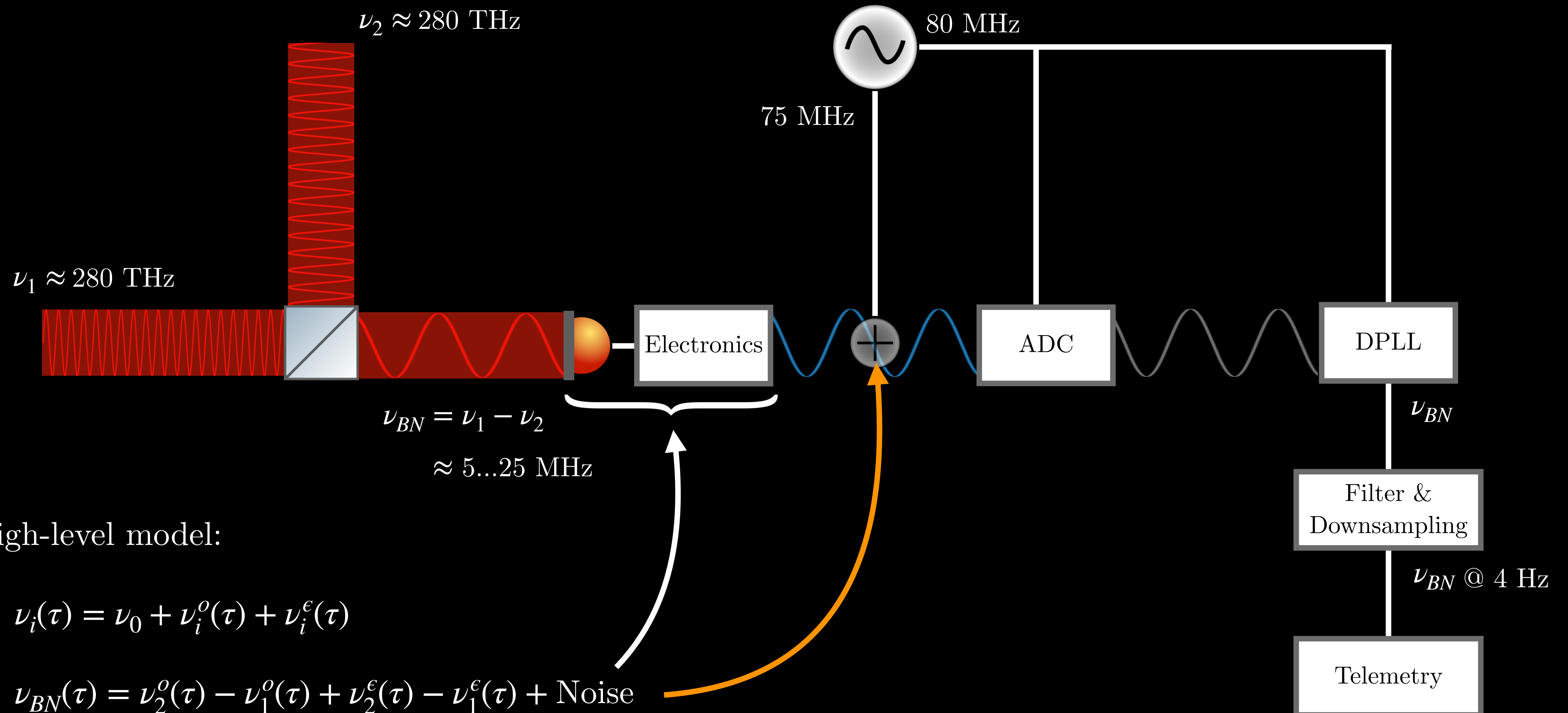
- Electromagnetic field of the laser beams in a fixed point, using the plane wave approximation:  $E(\tau) = E_0(\tau)\cos(2\pi\Phi(\tau)) = \text{Re} [E_0(\tau)e^{i2\pi\Phi(\tau)}]$
- $\Phi(\tau)$  is rapidly evolving:

$$\dot{\Phi}(\tau) = \nu(\tau) = \nu_0 + \nu^o(\tau) + \nu^\epsilon(\tau)$$



- Phase is the more fundamental quantity
- However: frequency usually easier to work with in practice, almost same information (modulo integration constant)
- Often useful to use complex field amplitude:  $E(\tau) \equiv E_0(\tau)e^{i2\pi\Phi(\tau)}$

# Measurement chain



- High-level model:

- $\nu_i(\tau) = \nu_0 + \nu_i^o(\tau) + \nu_i^\epsilon(\tau)$

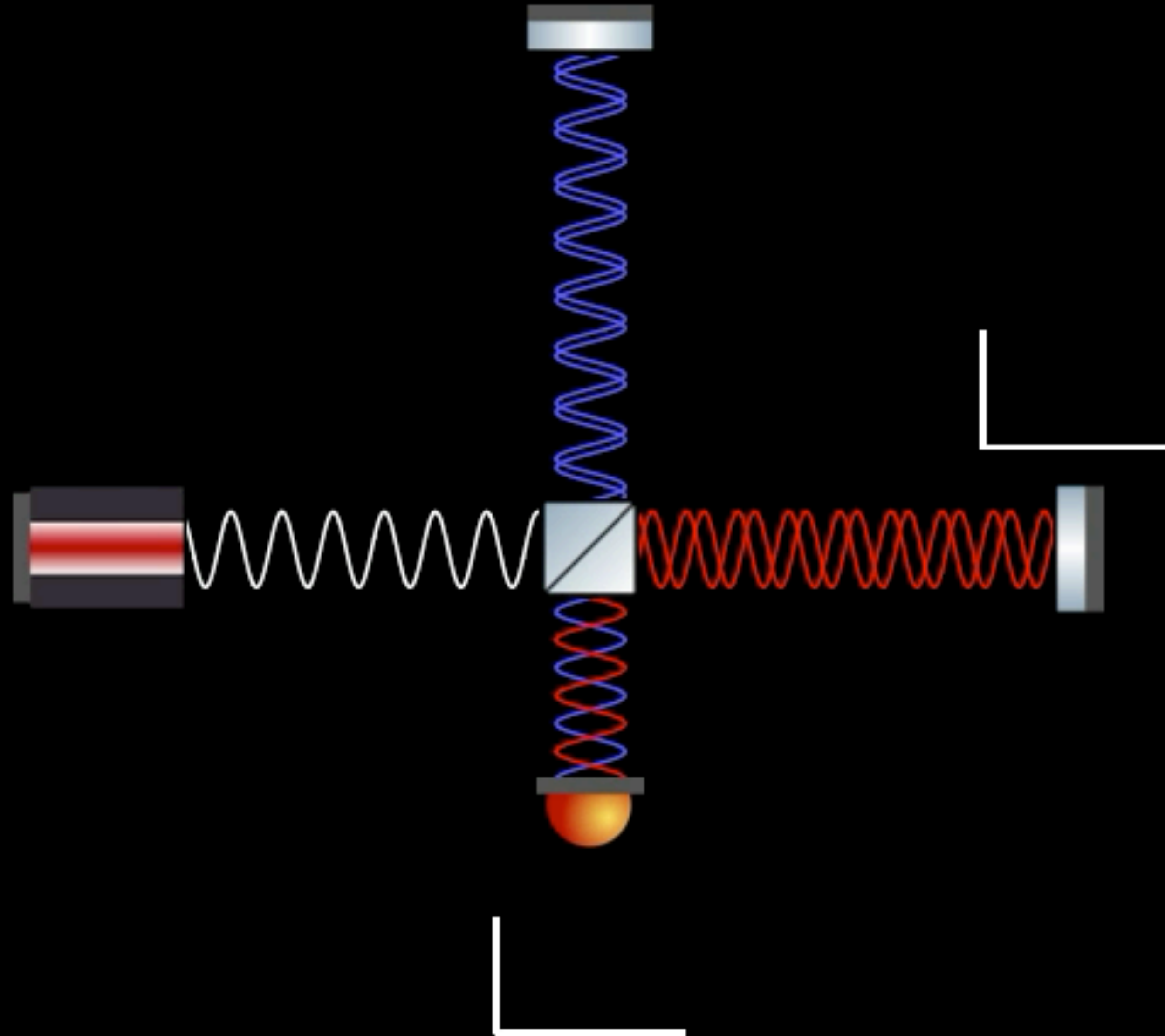
- $\nu_{BN}(\tau) = \nu_2^o(\tau) - \nu_1^o(\tau) + \nu_2^\epsilon(\tau) - \nu_1^\epsilon(\tau) + \text{Noise}$

- First: focus on in-band laser fluctuations in  $\nu_i^\epsilon(\tau)$

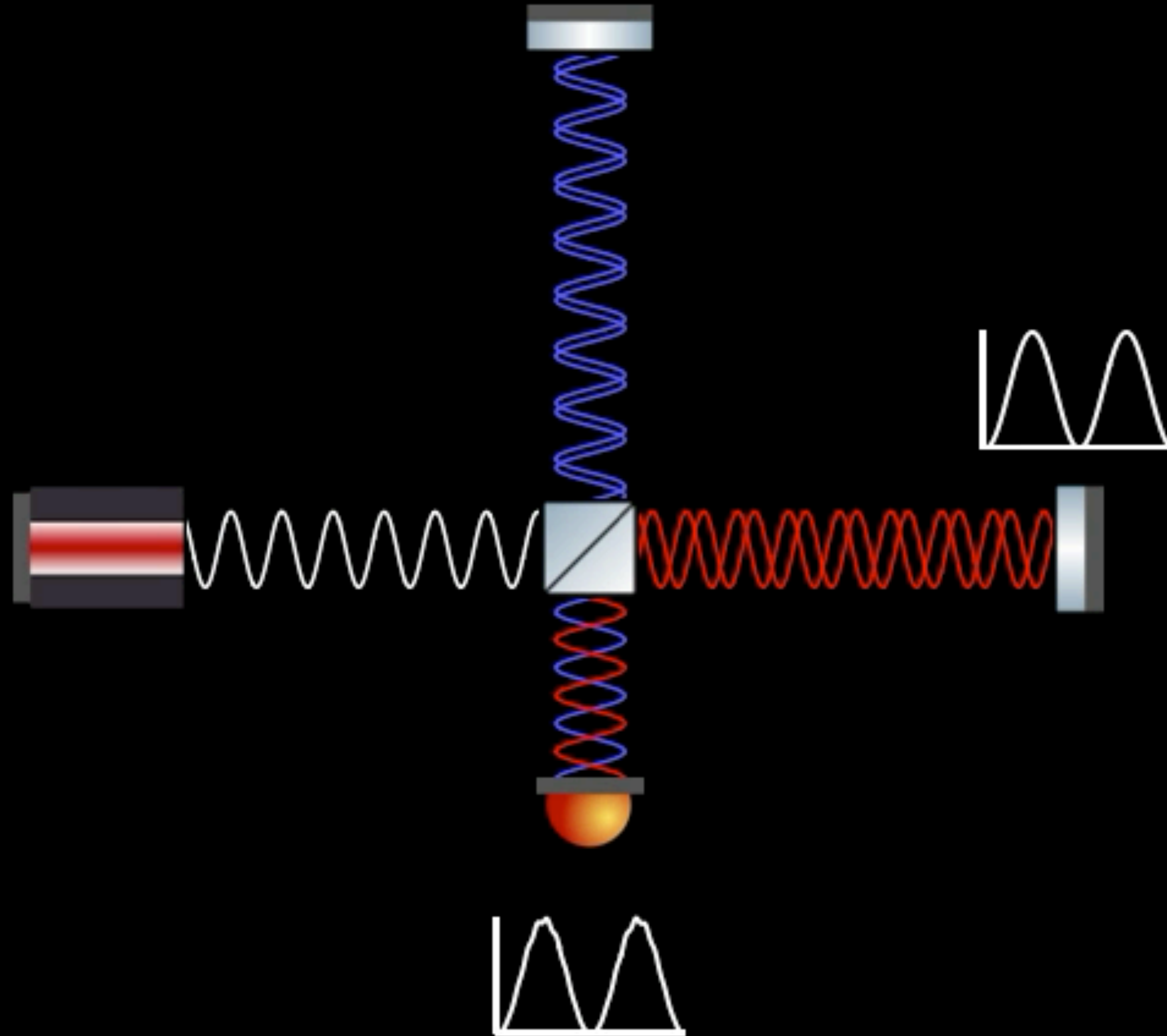
Note: Illustrative, numbers to be seen as placeholders

# Laser noise cancellation in LISA

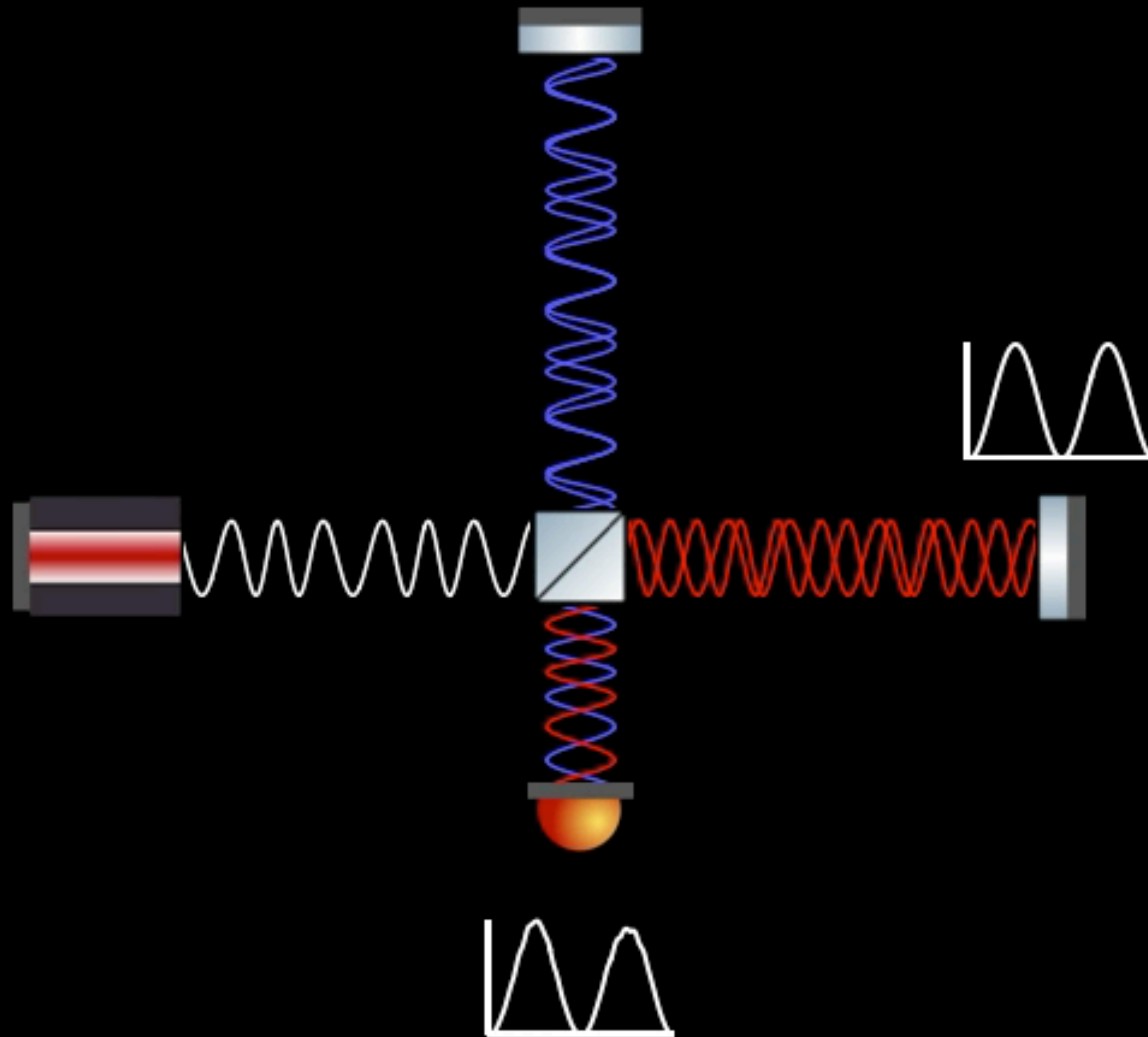
# Laser noise cancellation in interferometers



# Laser noise cancellation in interferometers

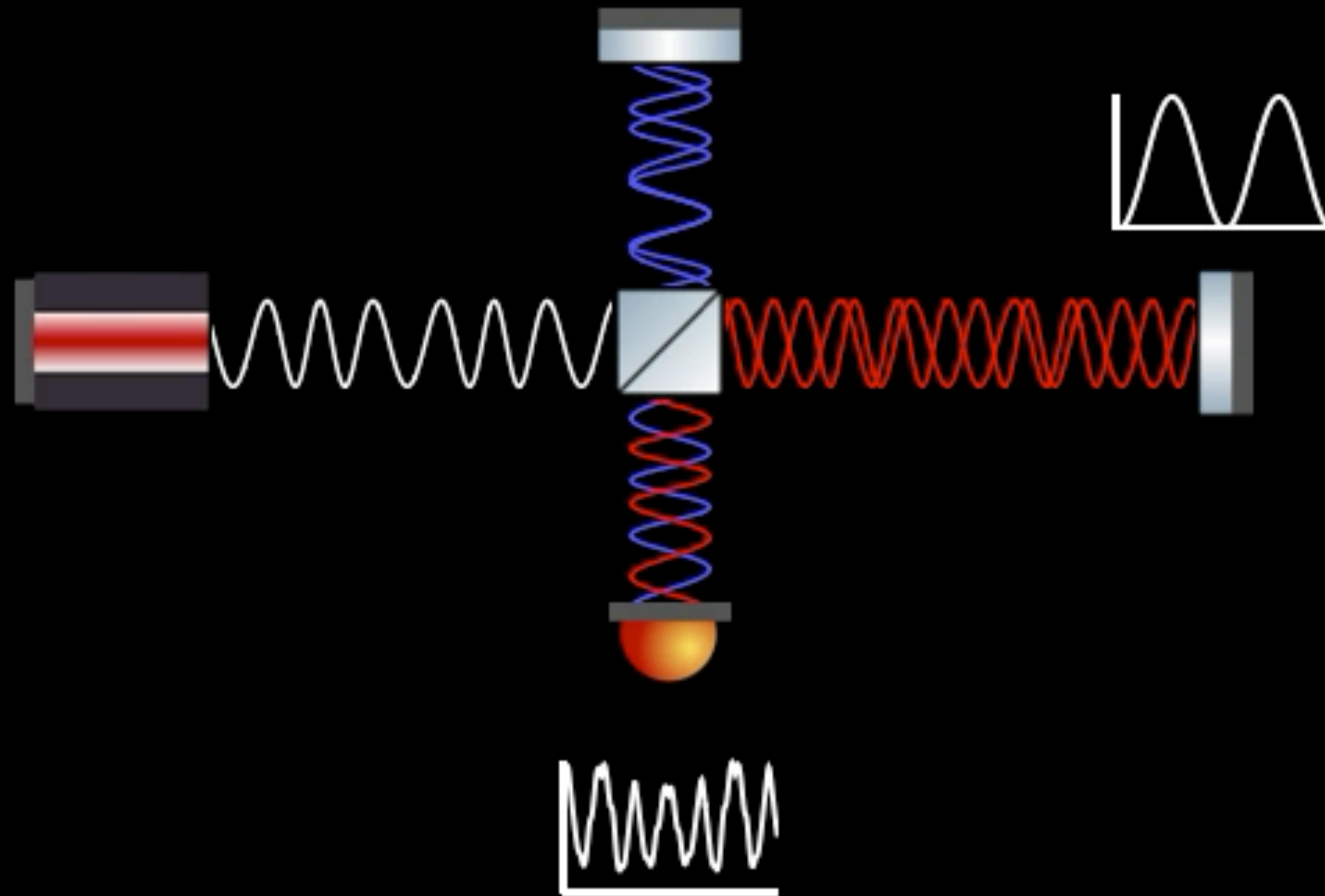


# Laser noise cancellation in interferometers

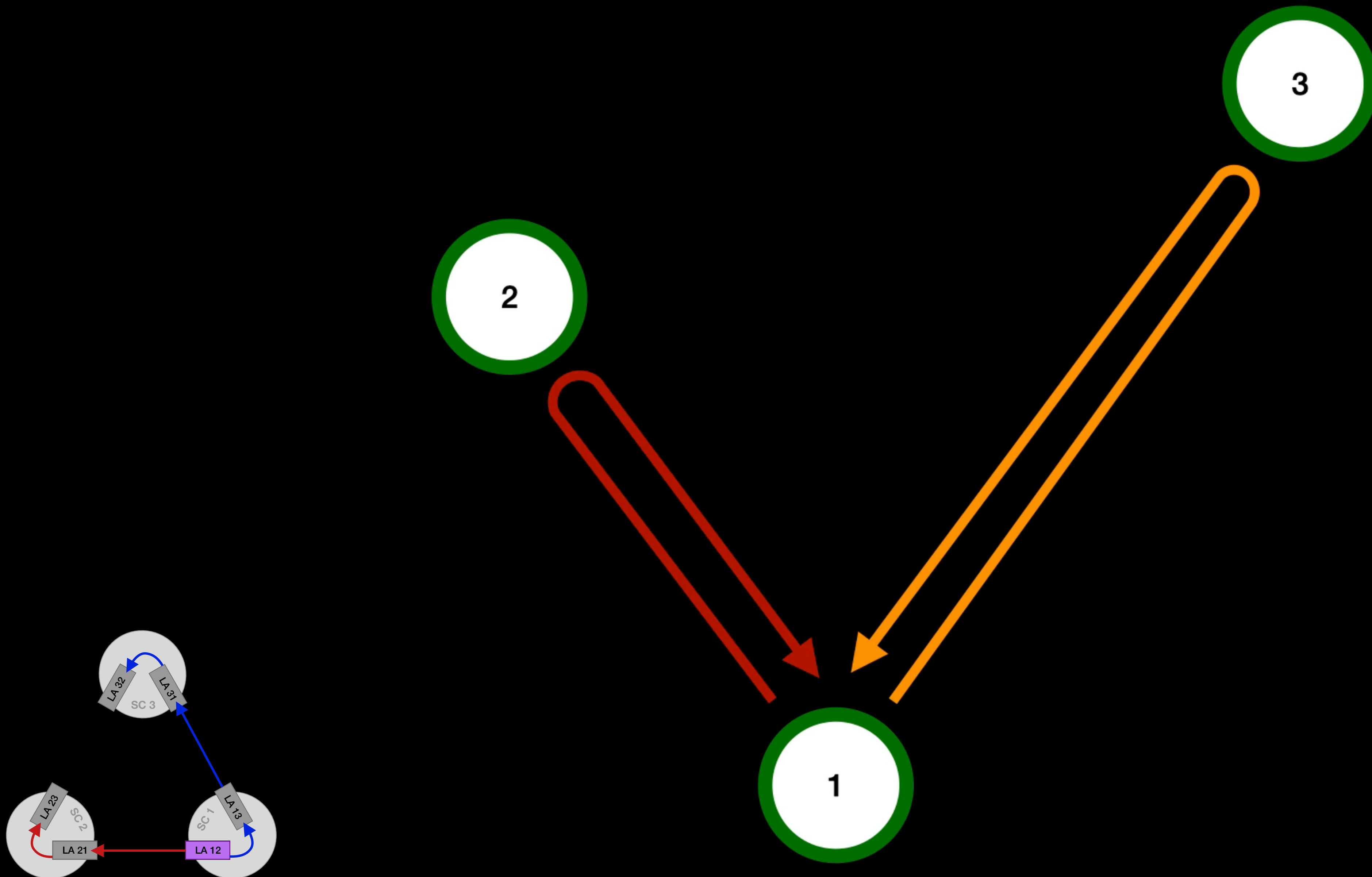




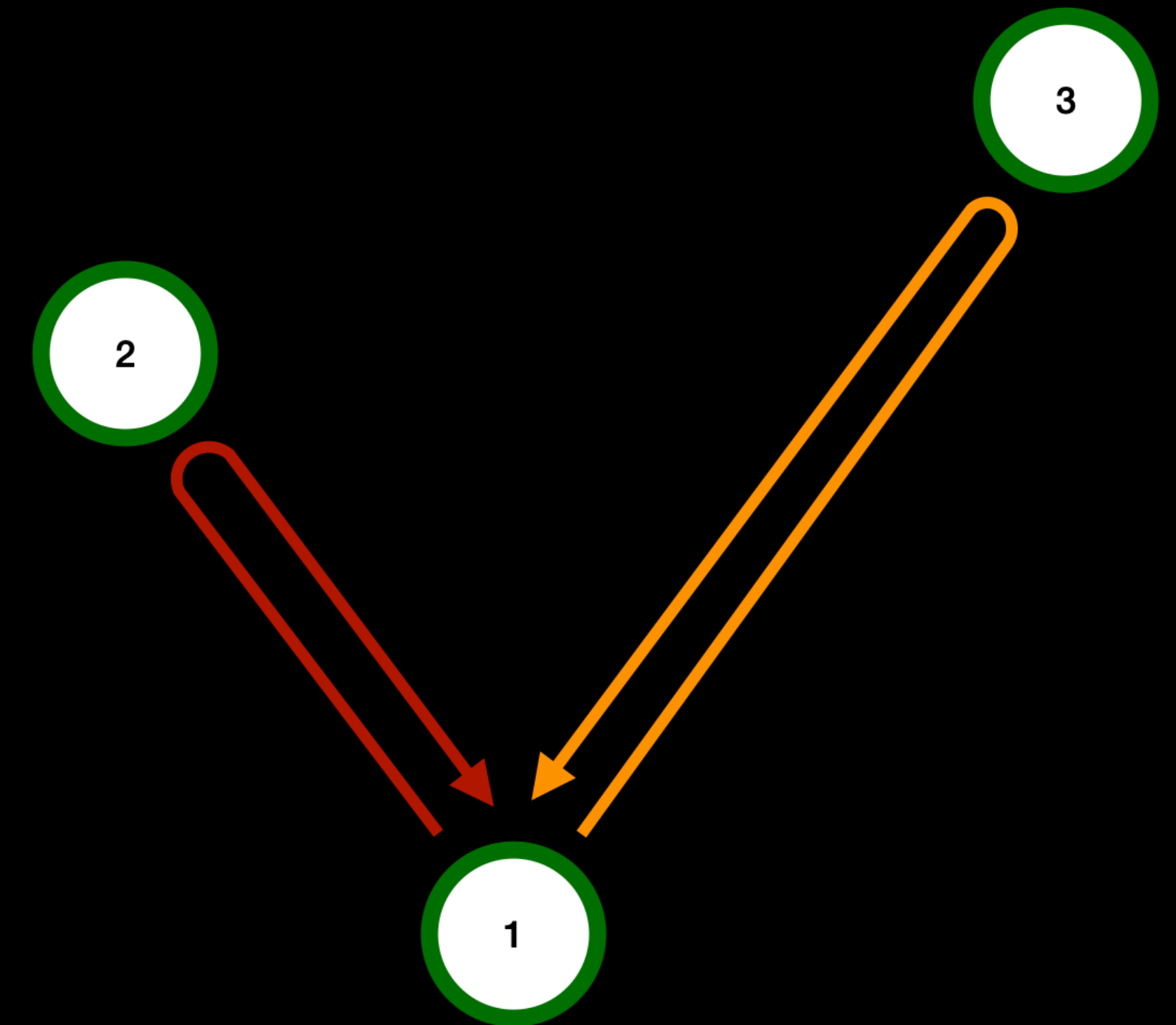
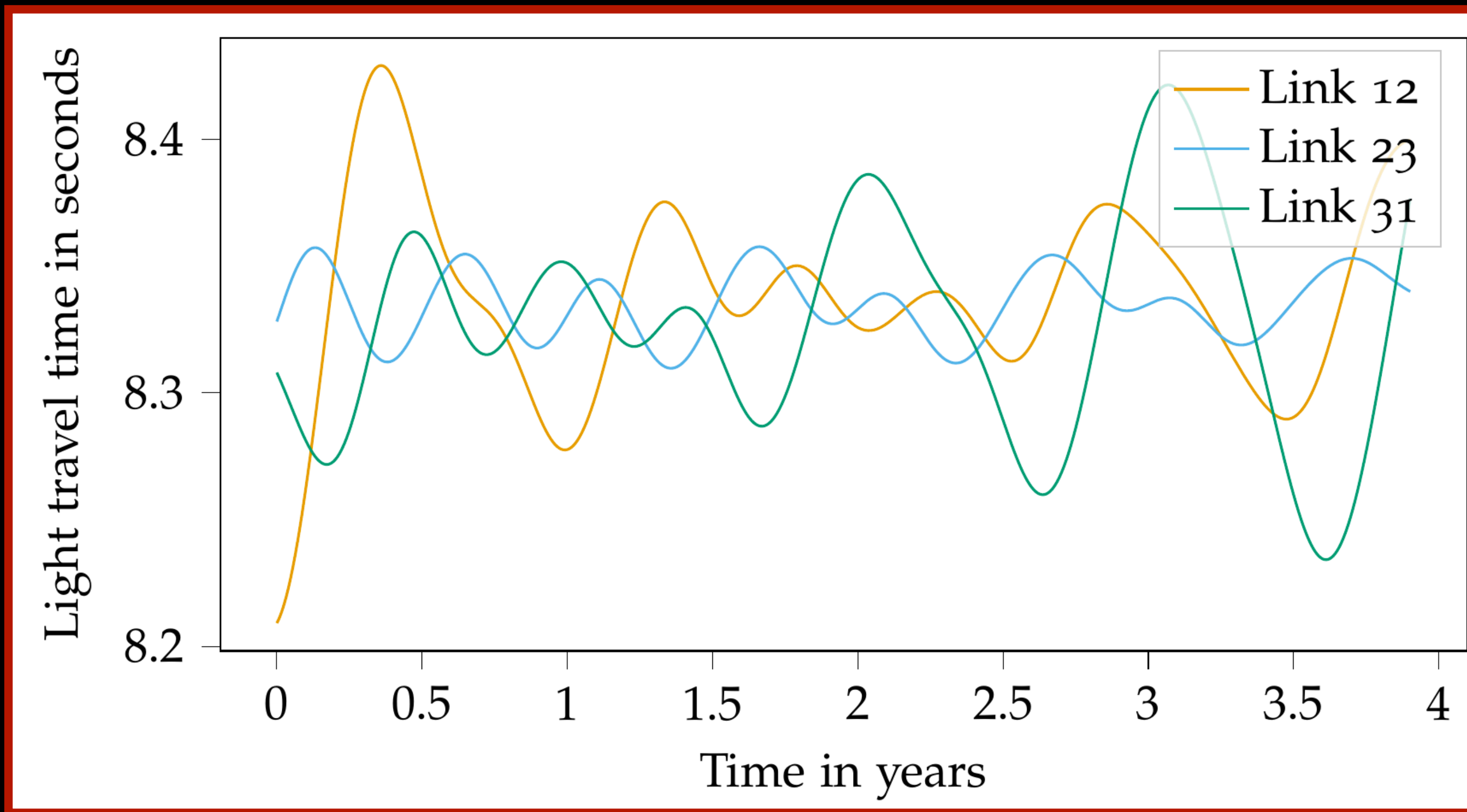
# Laser noise cancellation in interferometers



# Laser noise cancellation in LISA



# Laser noise cancellation in LISA

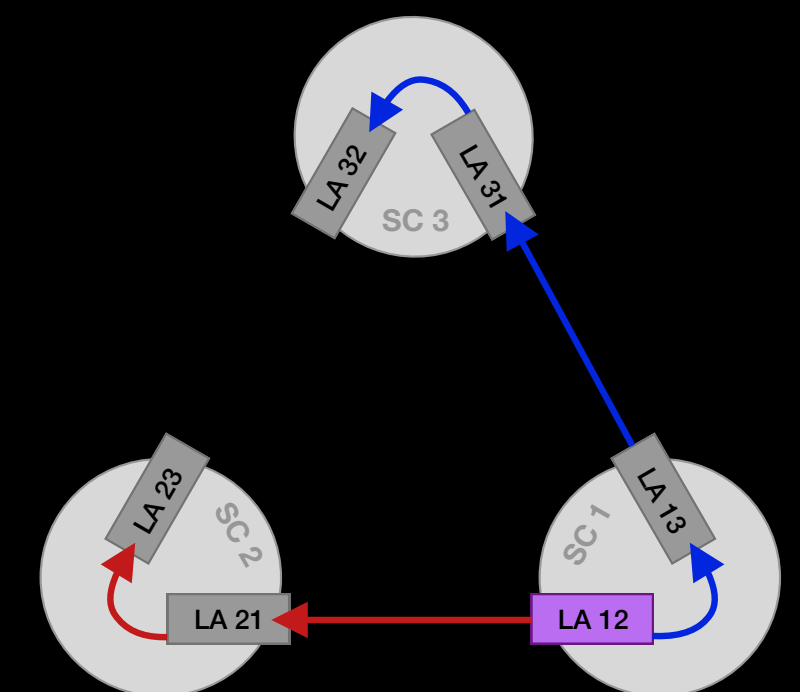
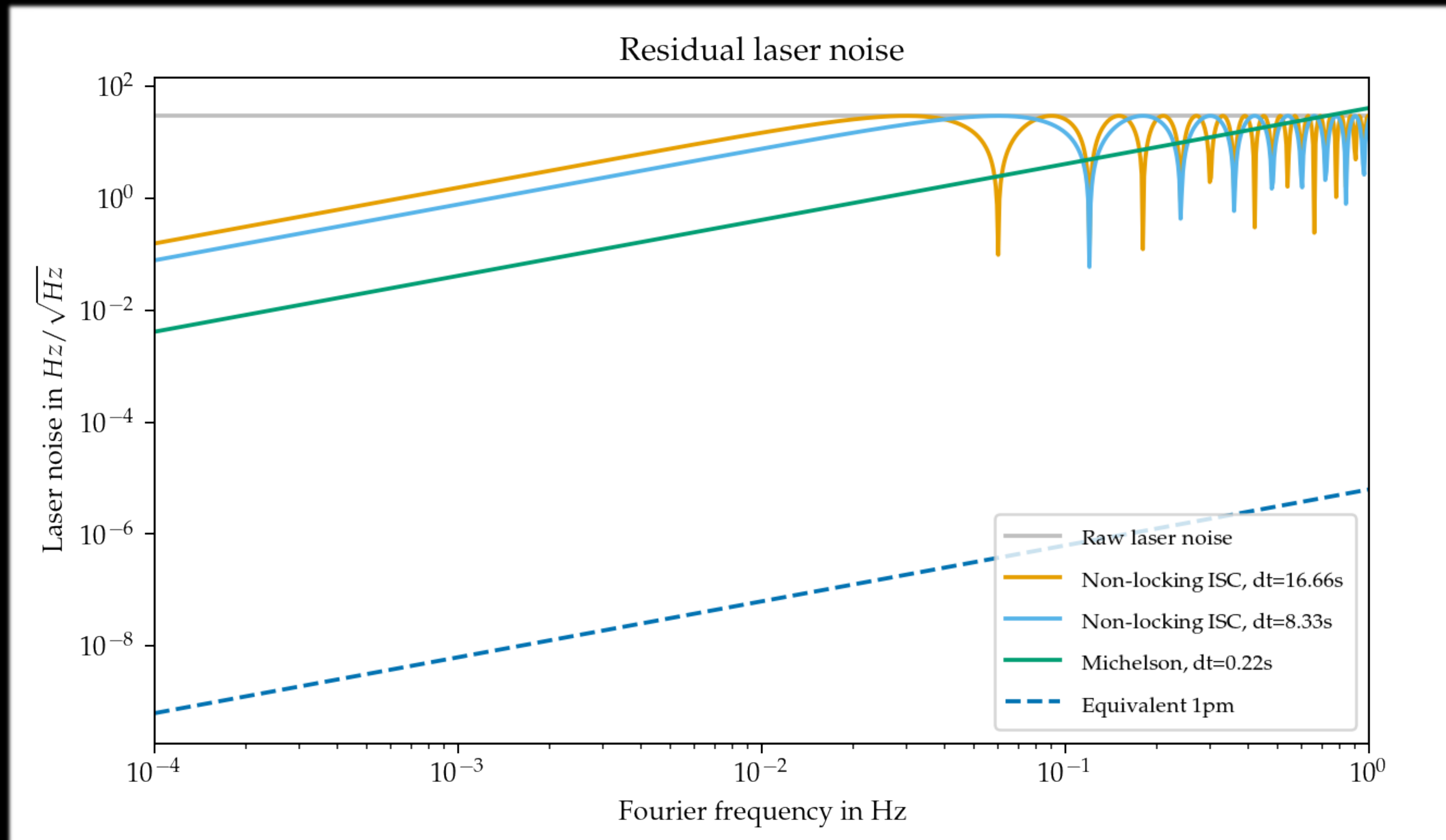


- Laser noise will enter as  $\Phi(t - \delta t_1) - \Phi(t - \delta t_2)$ , which in the frequency domain becomes (with  $\delta t = \delta t_1 - \delta t_2$ )

$$S_{\Phi, \text{TDI}} = 4 \sin(\pi f \delta t)^2 S_{\Phi} \approx (2\pi f)^2 \delta t^2 S_{\Phi}$$

# Residual laser noise in LISA

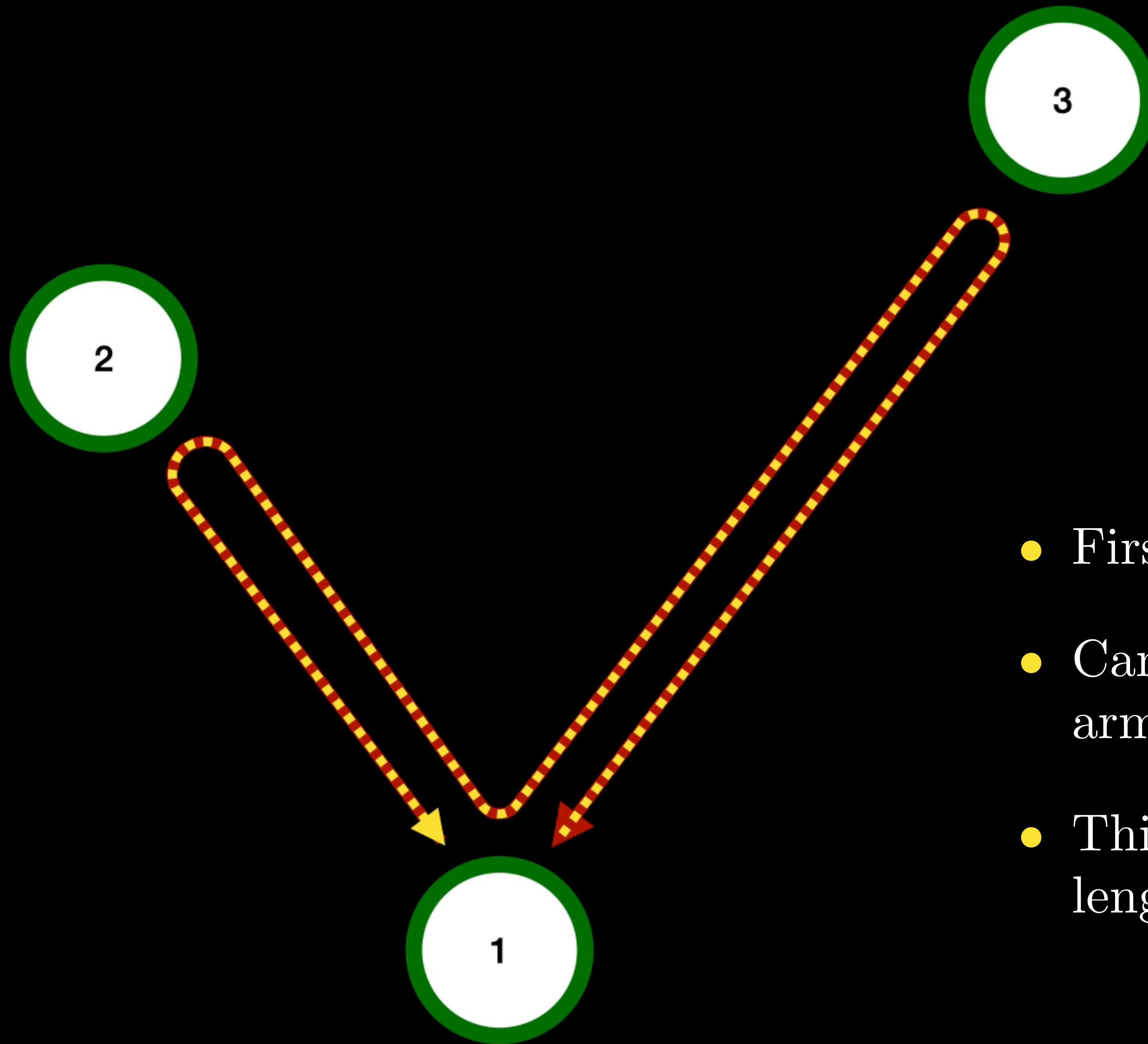
$$S_{\Phi, \text{TDI}} = 4 \sin(\pi f \delta t)^2 S_{\Phi} \approx (2\pi f)^2 \delta t^2 S_{\Phi}$$



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# Time delay interferometry

# Time-Delay Interferometry



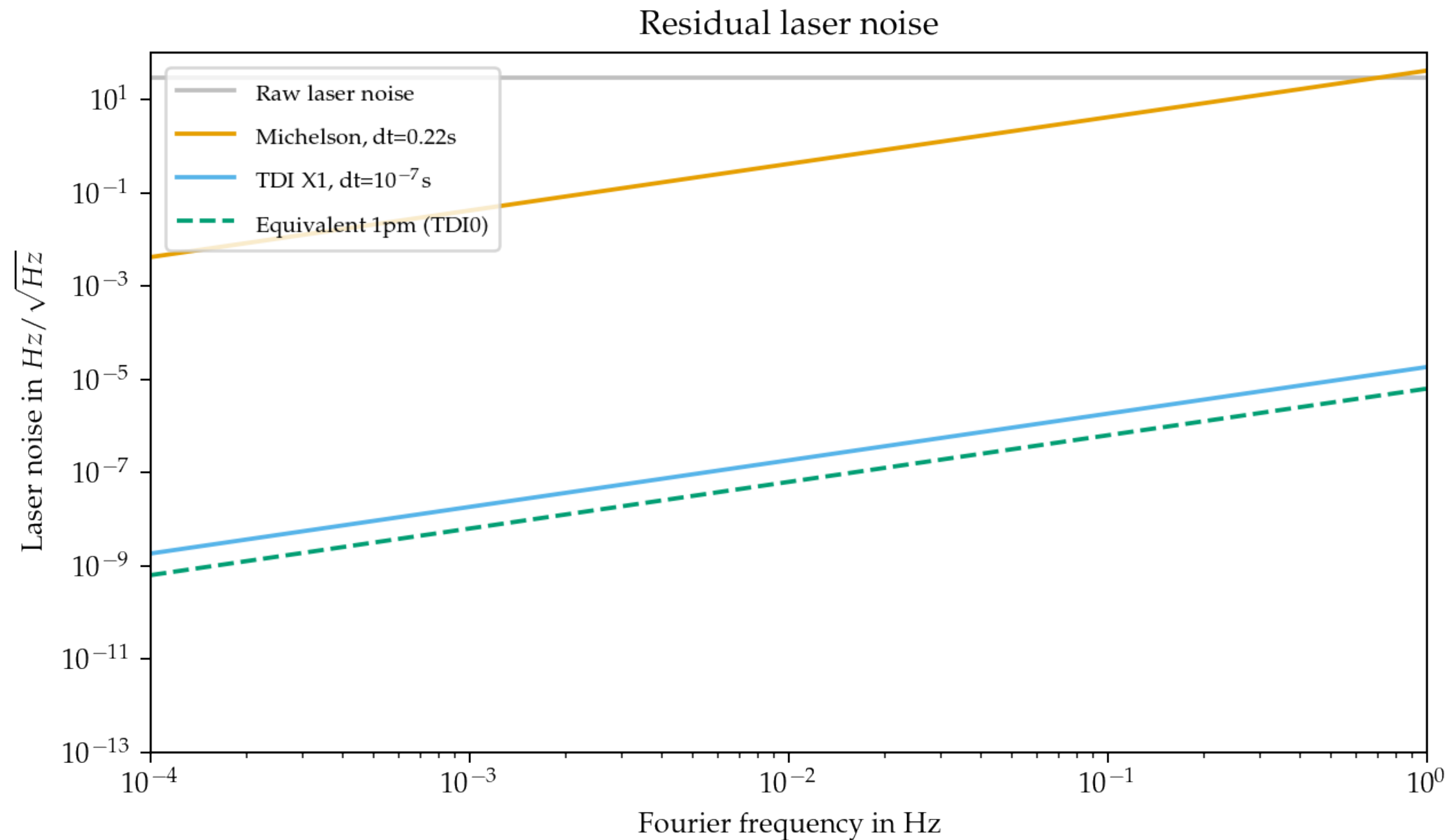
- First proposed in [Tinto et al., 1999]
- Cancel laser noise by constructing equal arm interferometer in post-processing
- This is an example for constant arm lengths (1st generation TDI)

See living review [Tinto & Dhurandhar, 2020] for detailed references on TDI  
First reference in history section (not quite TDI): [Faller and Bender, 1984]

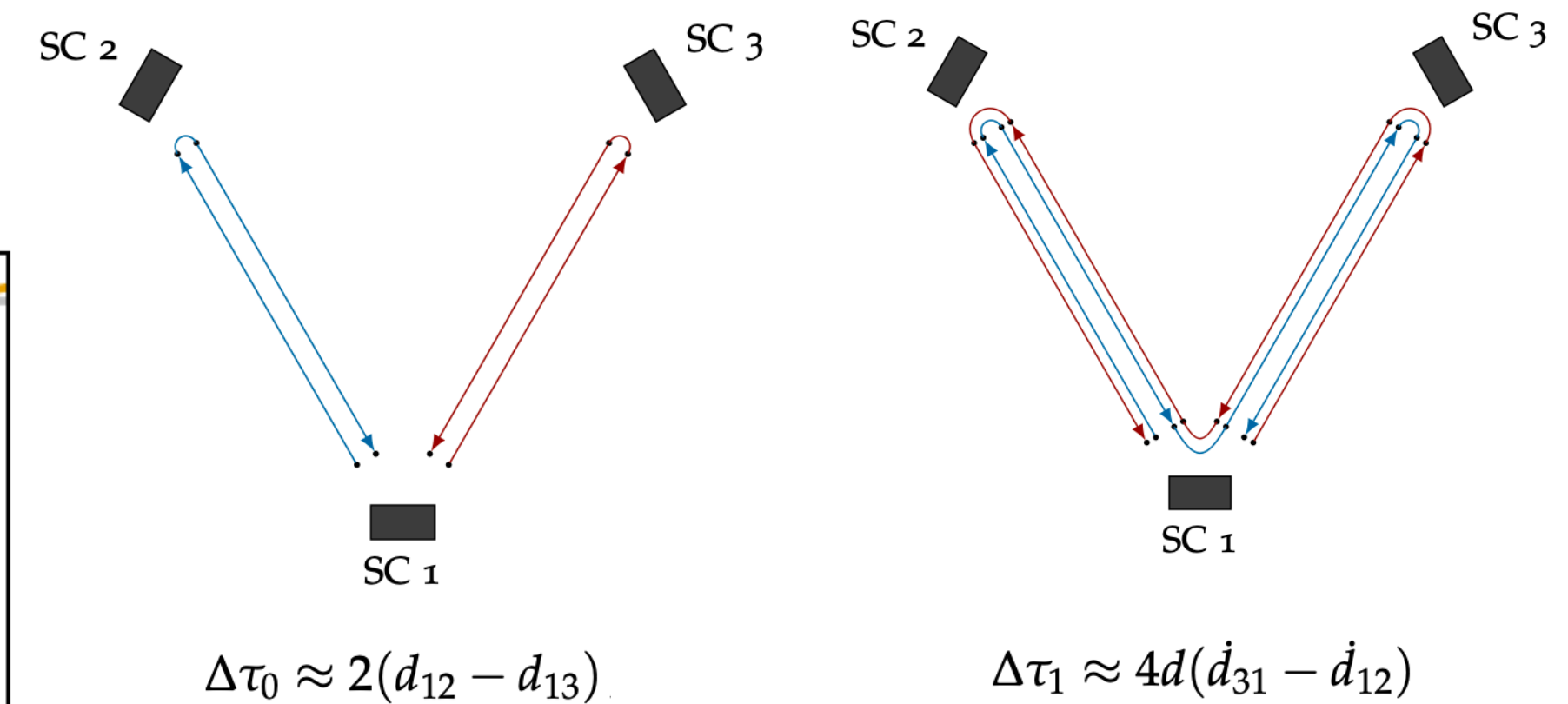


# Residual laser noise in LISA

$$S_{\Phi, \text{TID}} \approx (2\pi f)^2 \delta t^2 S_{\Phi}$$



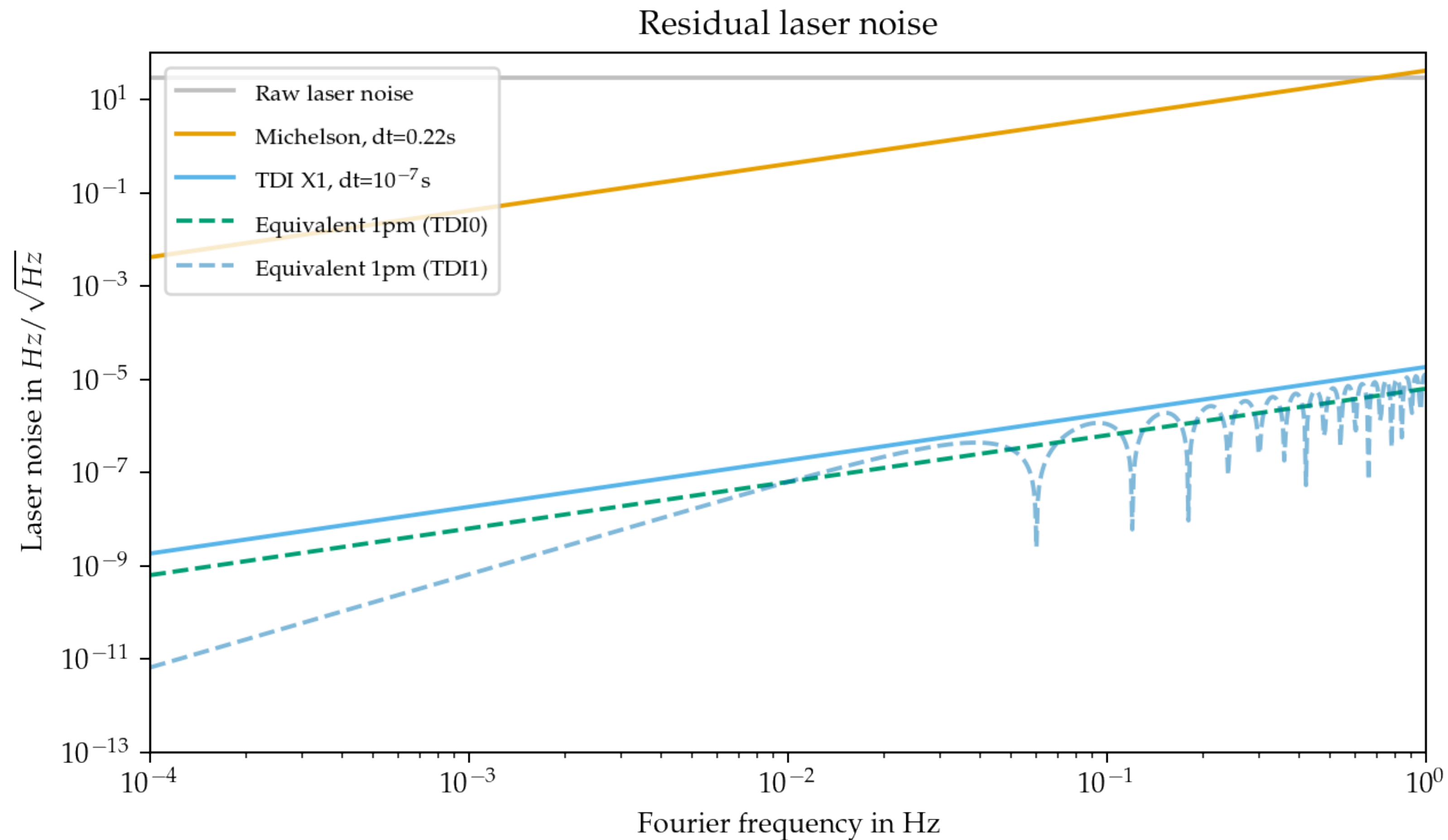
Average light travel times with ESA orbits:  $d_A \approx 8.3\text{s}$ ,  $\dot{d}_A \approx 10^{-9}$  and  $\ddot{d}_A \approx 10^{-15}\text{s}^{-1}$



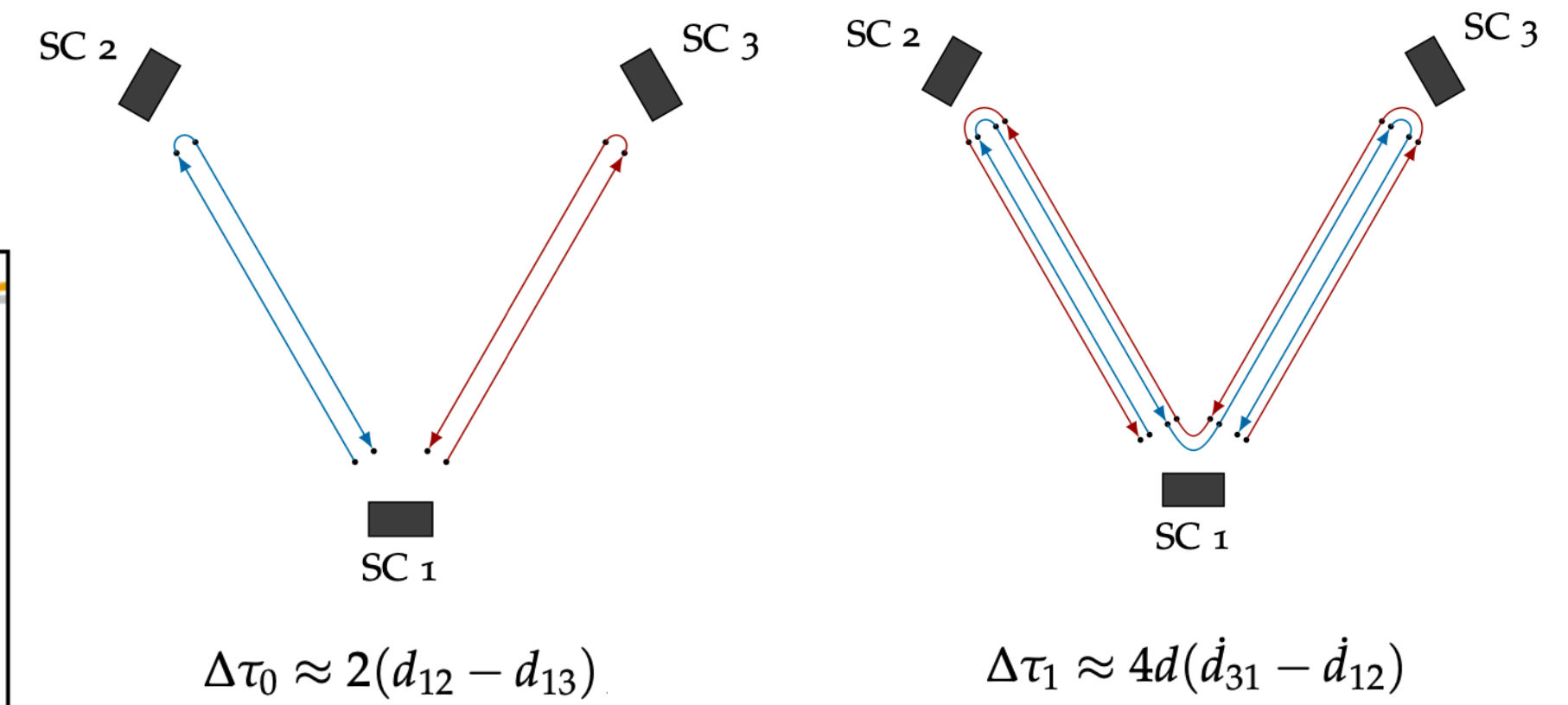
Note: Illustrative, neither laser noise nor actual requirement are white across the band

# Residual laser noise in LISA

$$S_{\Phi, \text{TDI}} \approx (2\pi f)^2 \delta t^2 S_{\Phi}$$



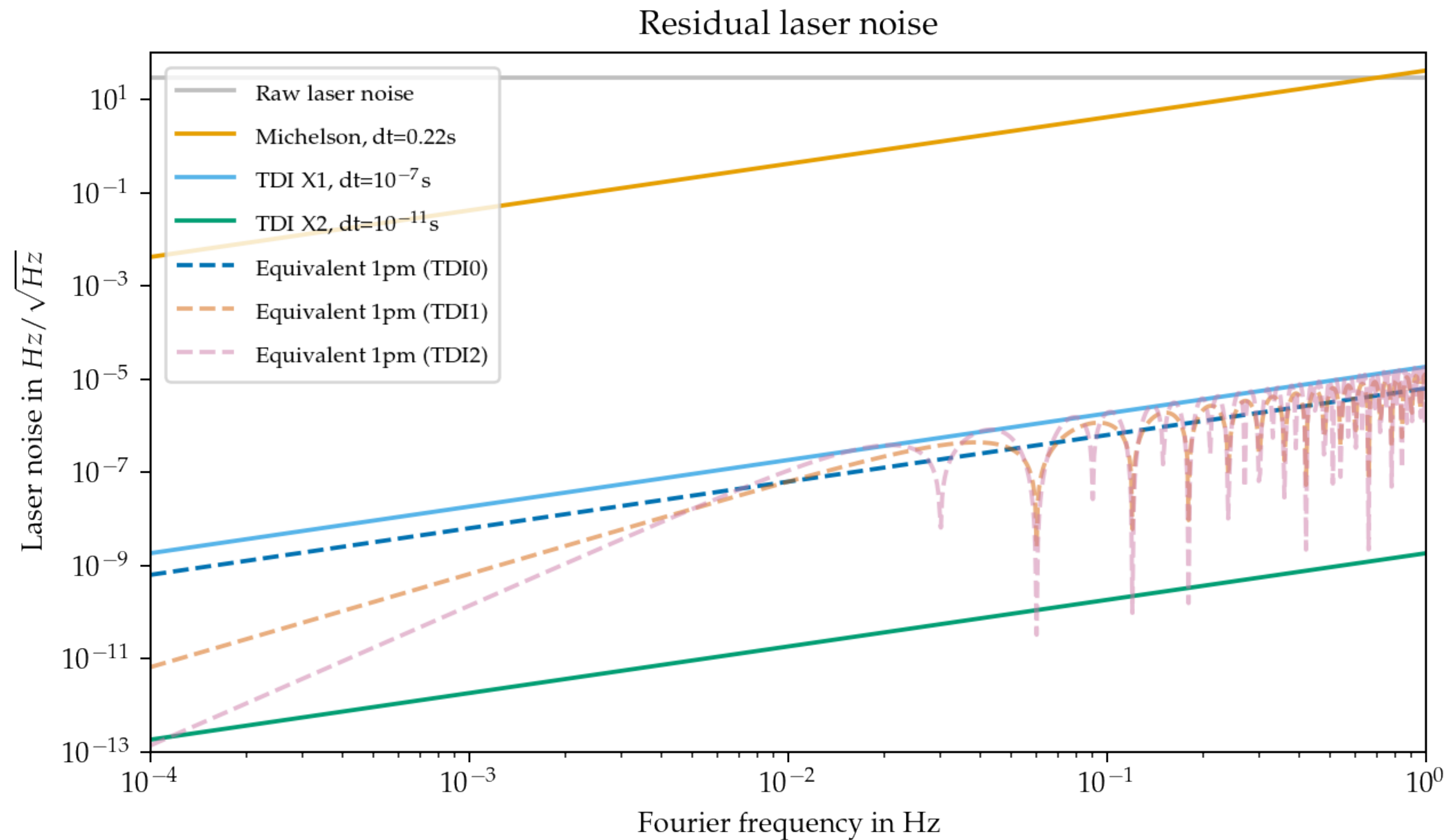
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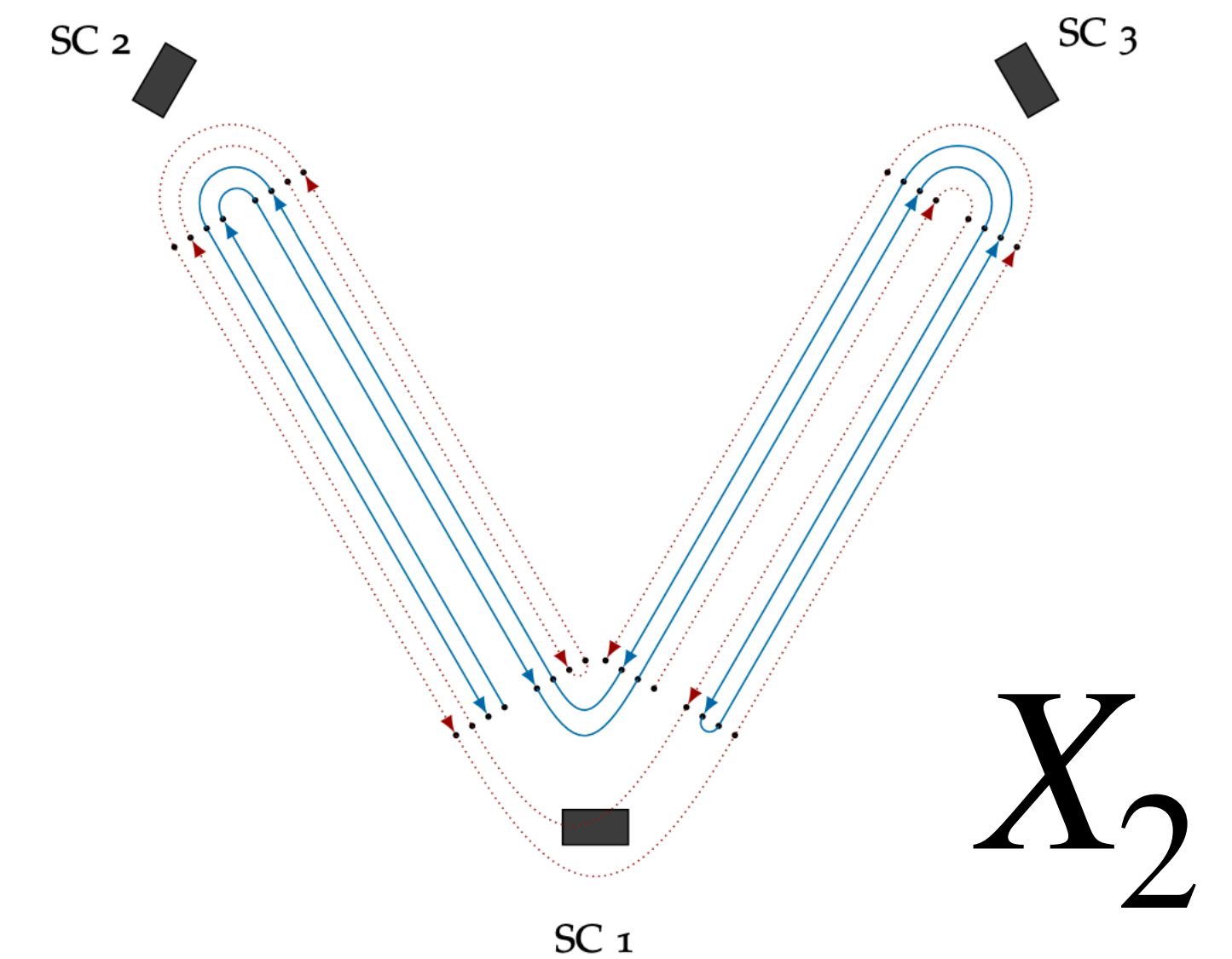
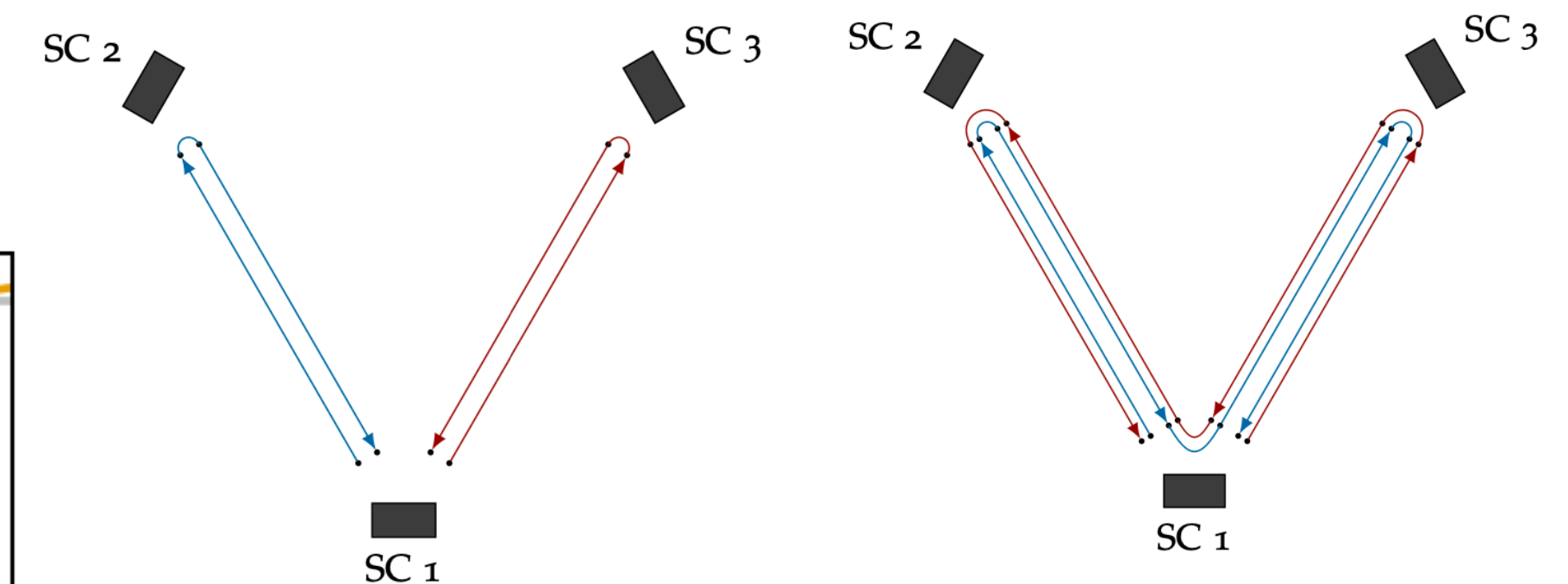
Note: Illustrative, neither laser noise nor actual requirement are white across the band

# Residual laser noise in LISA

$$S_{\Phi, \text{TDI}} \approx (2\pi f)^2 \delta t^2 S_{\Phi}$$



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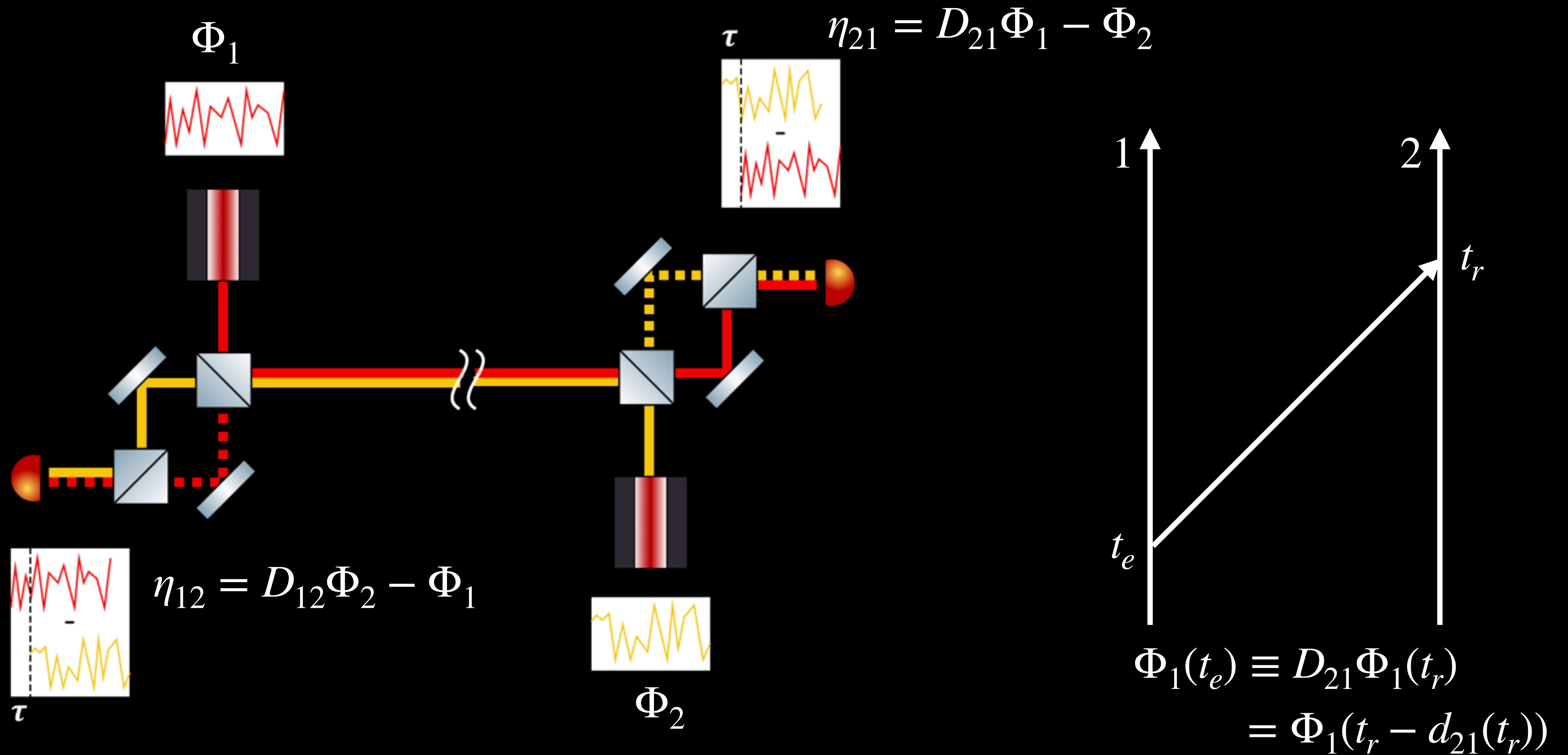


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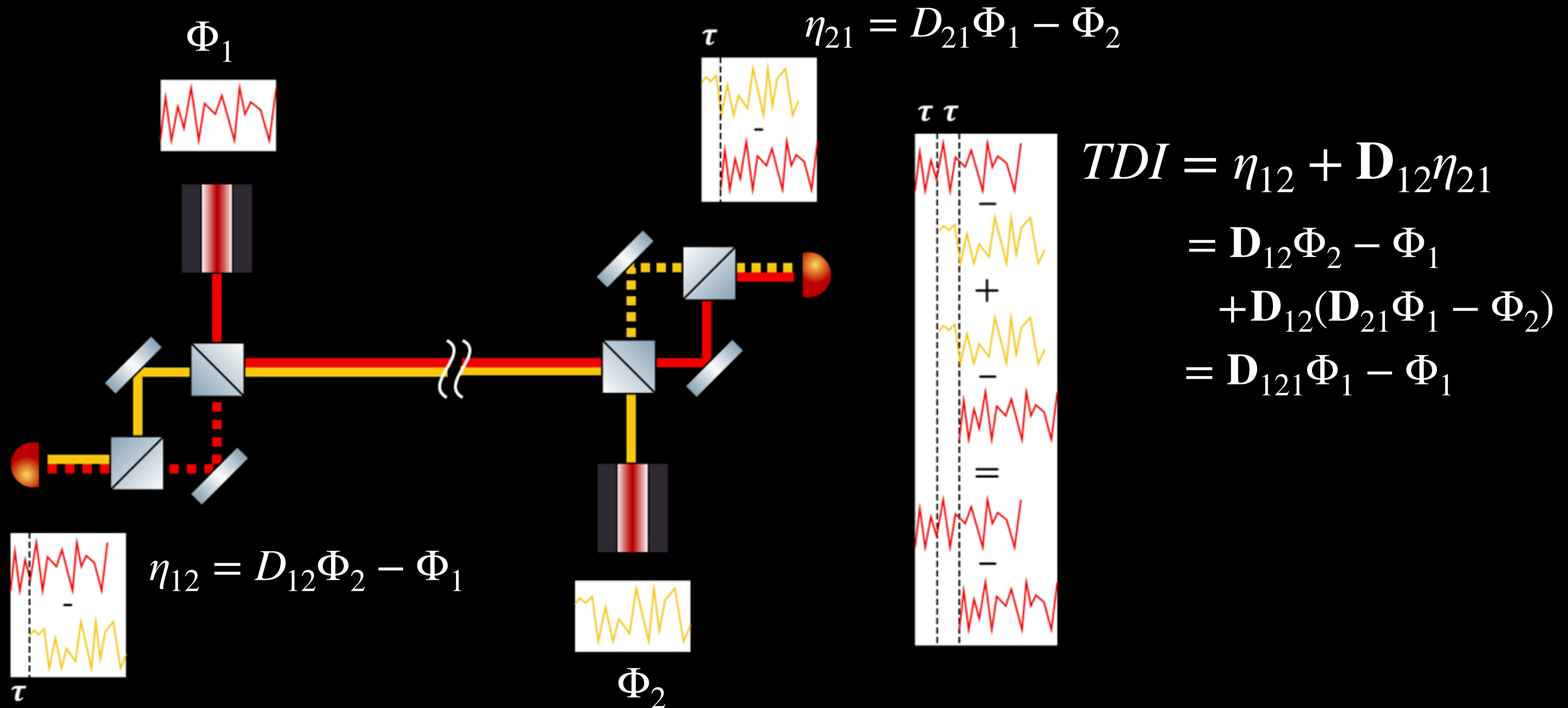
How does TDI work, in practice?

# TDI toy model



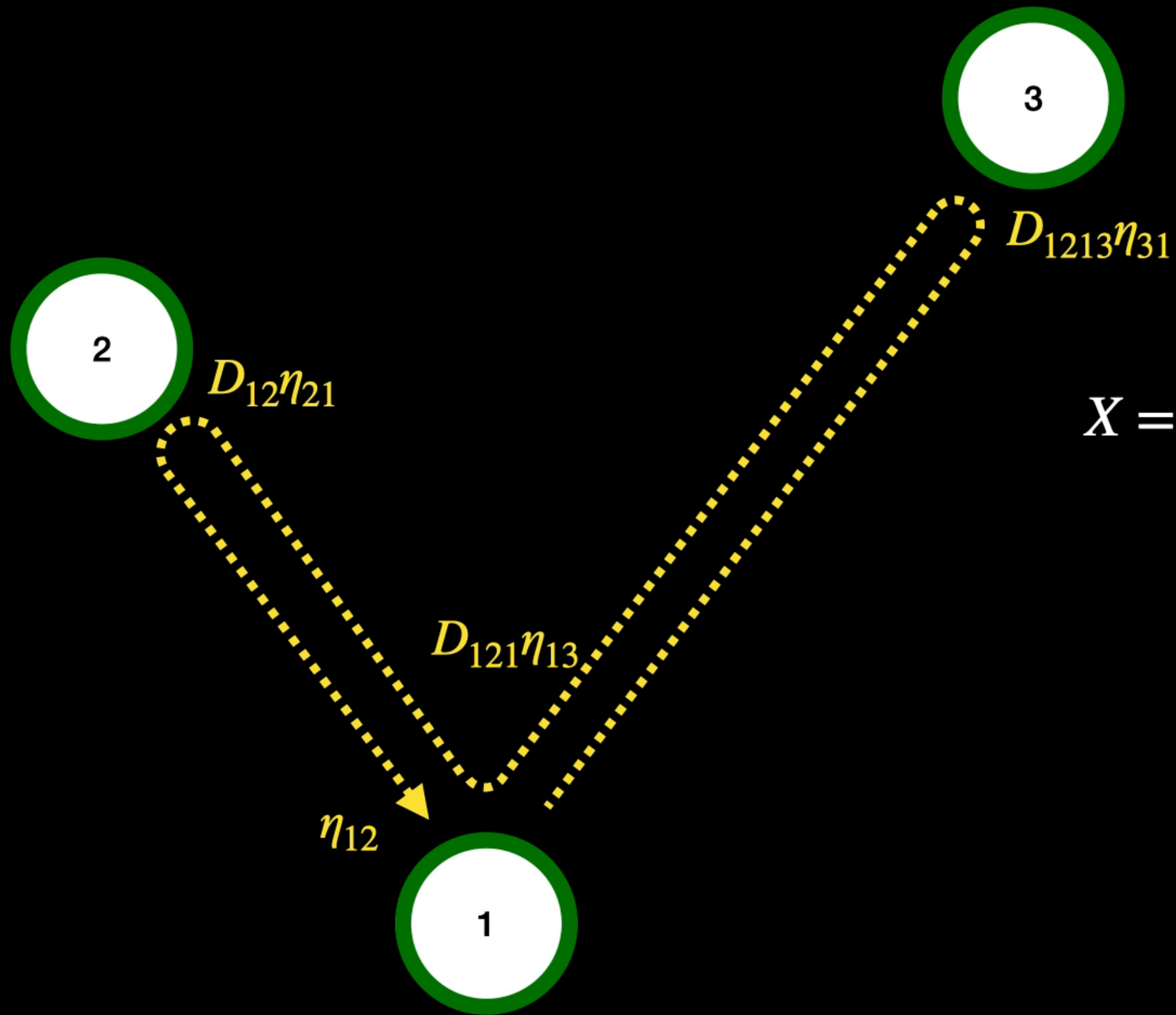


# TDI toy model



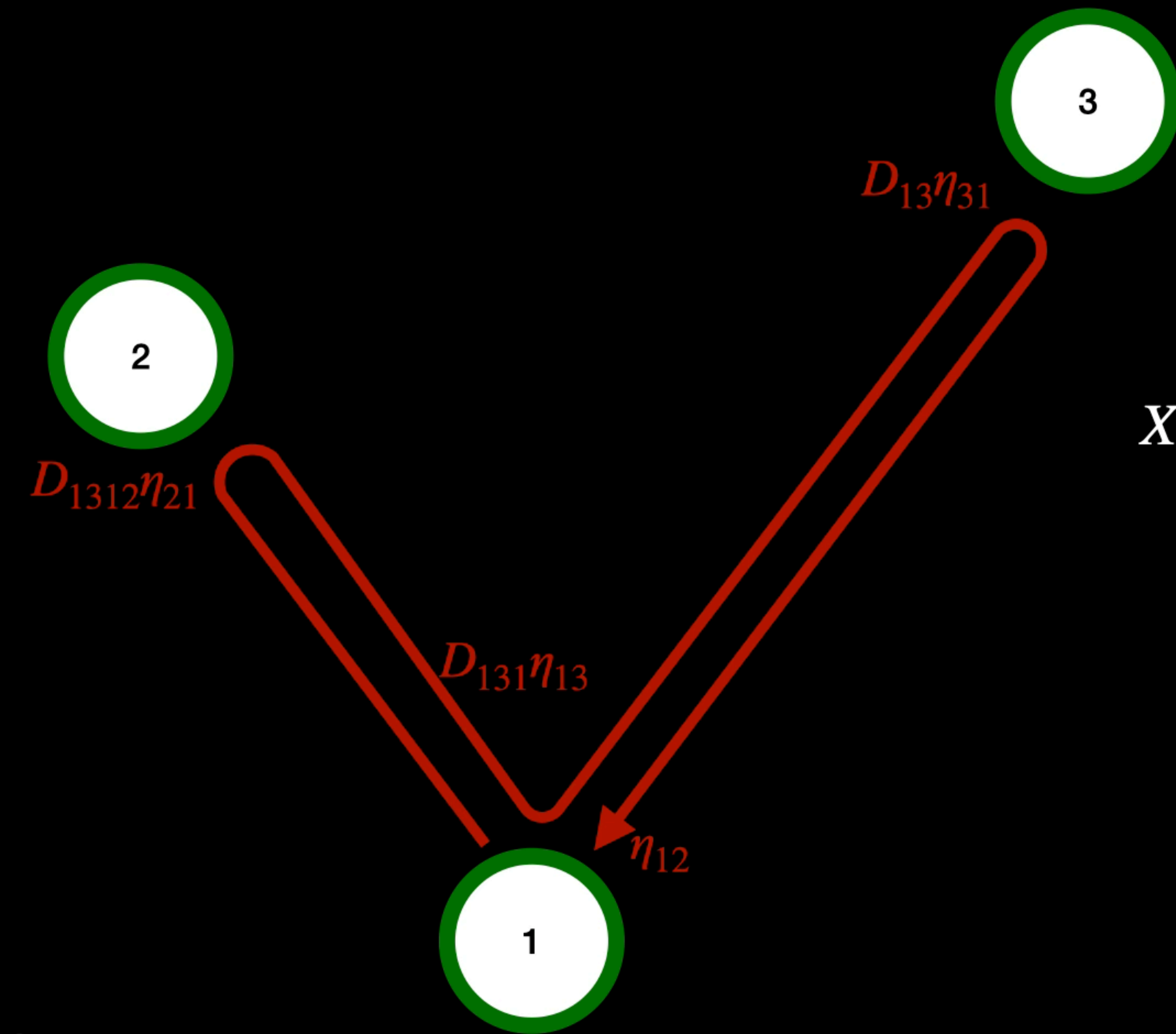


# Full first generation TDI



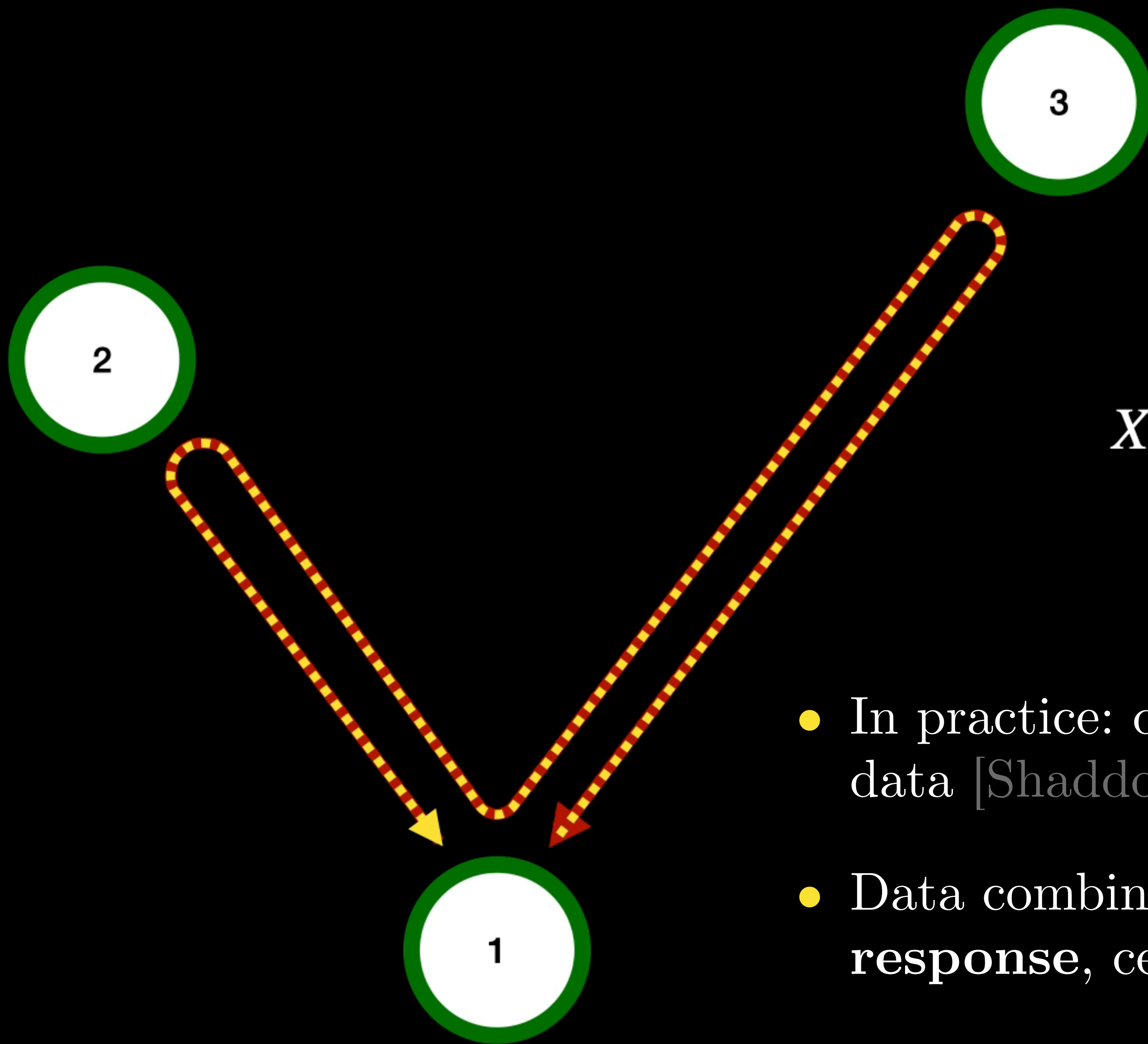
$$X = \eta_{12} + D_{12}\eta_{21} + D_{121}\eta_{13} + D_{1213}\eta_{31}$$

# Full first generation TDI



$$X = \eta_{12} + D_{12}\eta_{21} + D_{121}\eta_{13} + D_{1213}\eta_{31} \\ - \eta_{12} - D_{13}\eta_{31} - D_{131}\eta_{13} - D_{1312}\eta_{21}$$

# Full first generation TDI



$$\begin{aligned} X = & \eta_{12} + D_{12}\eta_{21} + D_{121}\eta_{13} + D_{1213}\eta_{31} \\ & - \eta_{12} - D_{13}\eta_{31} - D_{131}\eta_{13} - D_{1312}\eta_{21} \\ = & (D_{12131} - D_{13121})\Phi_1 \end{aligned}$$

- In practice: delays realised by interpolating 4 Hz data [Shaddock et al., 2004].
- Data combination has **strong impacts on GW response**, central to LISA data analysis

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TDI variables, how to find them I: algebraic solution

# Algebraic approach to TDI - framework

- Consider the single link equations  $\eta_{ij} = D_{ij}p_j - p_i$
- $\eta_{ij}, p_{ij}$ : time series, living in  $\mathcal{T} = \{x : \mathbb{R} \rightarrow \mathcal{K}\}$ , where  $\mathcal{K}$  is a field (usually  $\mathbb{R}$ )
- $D_{ij} : \mathcal{T} \rightarrow \mathcal{T}$ : operator/function, mapping time-series into time-series
- Set of our 6 delay operators:  $D_{set} = \{D_{ij} | ij \in \mathcal{J}_2\}$ , equipped with natural multiplication through function composition (ie., apply multiple delays in sequence)
- Set of monomials  $M$ : the set of all finite (ordered) products of elements in  $D_{set}$  (semi-group)
- Set of polynomials of delay operators:

$$P = \left\{ \sum_k c_k M_k \mid c_k \in \mathcal{K}, M_k \in M \right\}$$

- Equipped with natural addition and multiplication, forms the **ring**  $\mathcal{K}[D_{set}]$
- We can also interpret  $P$  as a space of maps  $P_i : \mathcal{T} \rightarrow \mathcal{T}$ , acting on time series as

$$\left( \sum_k c_k M_k \right) x(t) = \sum_k c_k (M_k x(t))$$

# Algebraic approach to TDI - formulation

- We can write the single link expression in matrix form:

$$\vec{p} = \begin{pmatrix} p_1 \\ p_2 \\ p_3 \end{pmatrix} \in \mathcal{T}^3, \quad \vec{\eta} = \begin{pmatrix} \eta_{12} \\ \eta_{23} \\ \eta_{31} \\ \eta_{13} \\ \eta_{32} \\ \eta_{21} \end{pmatrix} \in \mathcal{T}^6, \quad D = \begin{pmatrix} -1 & D_{12} & 0 \\ 0 & -1 & D_{23} \\ D_{31} & 0 & -1 \\ -1 & 0 & D_{13} \\ 0 & D_{32} & -1 \\ D_{21} & -1 & 0 \end{pmatrix} : \mathcal{T}^3 \rightarrow \mathcal{T}^6$$
$$\implies \vec{\eta} = D\vec{p}$$

- For laser noise suppression, construct  $\text{TDI} = \sum_{ij \in \mathcal{J}_2} P_{ij} \eta_{ij} = \vec{P} \vec{\eta} = \vec{P} D \vec{p} \equiv 0$
- For arbitrary  $p_i$ : need  $\vec{P} D \equiv 0 \implies D^T \vec{P}^T \equiv 0$
- Now: interpret  $D^T$  as a map  $D^T : \mathcal{K}[D_{set}]^6 \rightarrow \mathcal{K}[D_{set}]^3$  between ‘vectors’ of polynomials

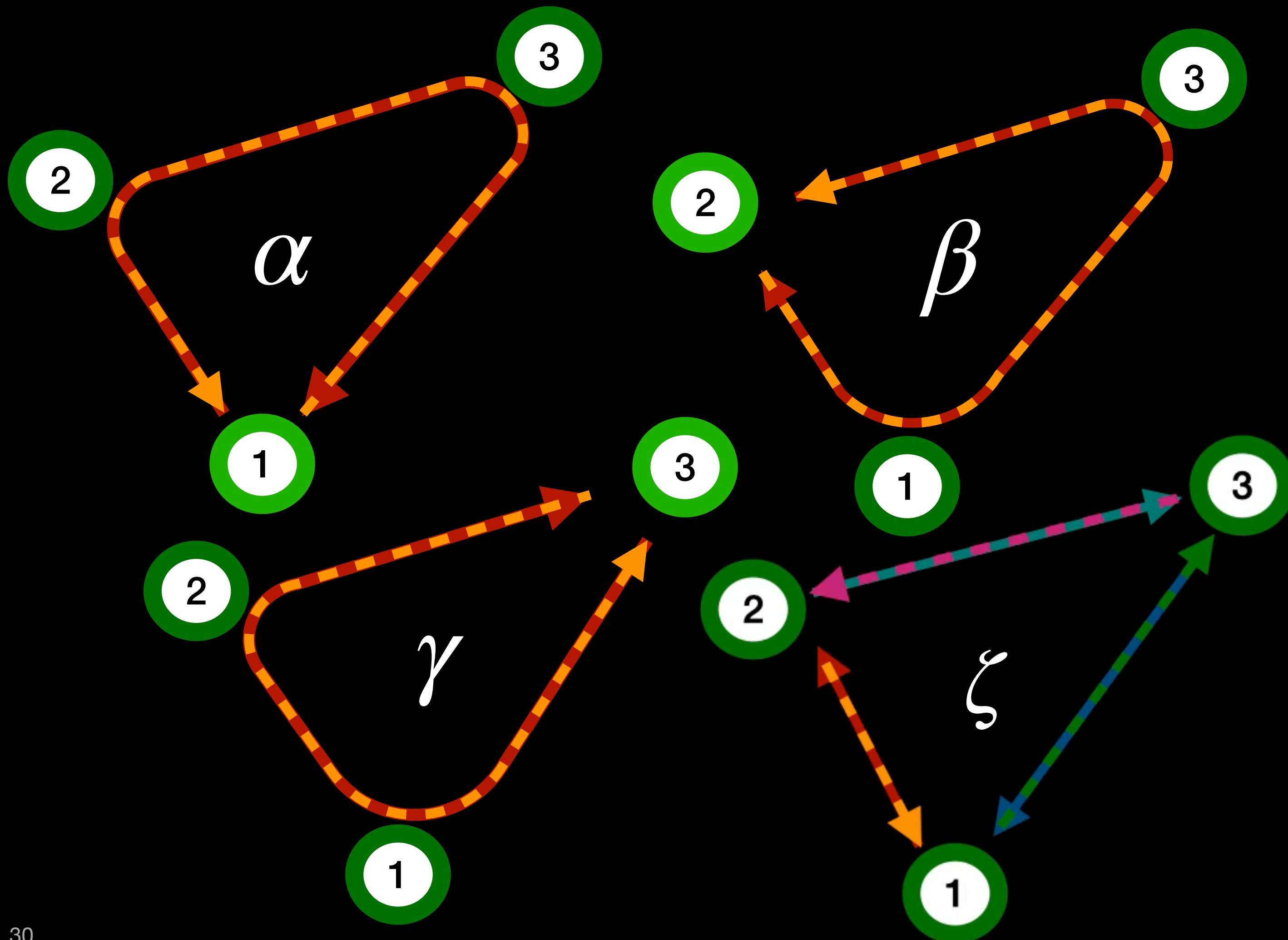


# Algebraic approach to TDI - formulation

- Space of TDI combinations: simply the kernel of  $D^T : \mathcal{K}[D_{set}]^6 \rightarrow \mathcal{K}[D_{set}]^3$
- Note:  $\mathcal{K}[D_{set}]$  is a ring, not a field
- Consequently:  $\mathcal{K}[D_{set}]^6$  is not a vector space, but a **module** over that ring.
- TDI solutions form a **sub-module** of  $\mathcal{K}[D_{set}]^6$ ,  $\approx$  first module of syzygy
- This is a well framed algebraic problem, can be solved for the case of constant (commutative) delays using standard algorithms or specialized software (e.g., Macauly2)
- Number of generators to generate the sub-module depend on assumptions:
  - ‘0th generation’ TDI: All delays equal,  $D_{ij} = D$
  - ‘1st generation’ TDI: Static constellation,  $D_{ij} = D_{ji}$
  - ‘Modified 1st generation’/‘1.5th generation’ TDI: Rotating but rigid constellation,  $D_{ij} \neq D_{ji}$

# Which variables to use?

- For a static constellation, all TDI variables can be build from 4 generators [Dhurandhar et al., 2002]
- Only three independent:  $(1 - D_{12}D_{23}D_{31})\zeta = (D_{23} - D_{31}D_{12})\alpha + (D_{31} - D_{12}D_{23})\beta + (D_{12} - D_{23}D_{31})\gamma$



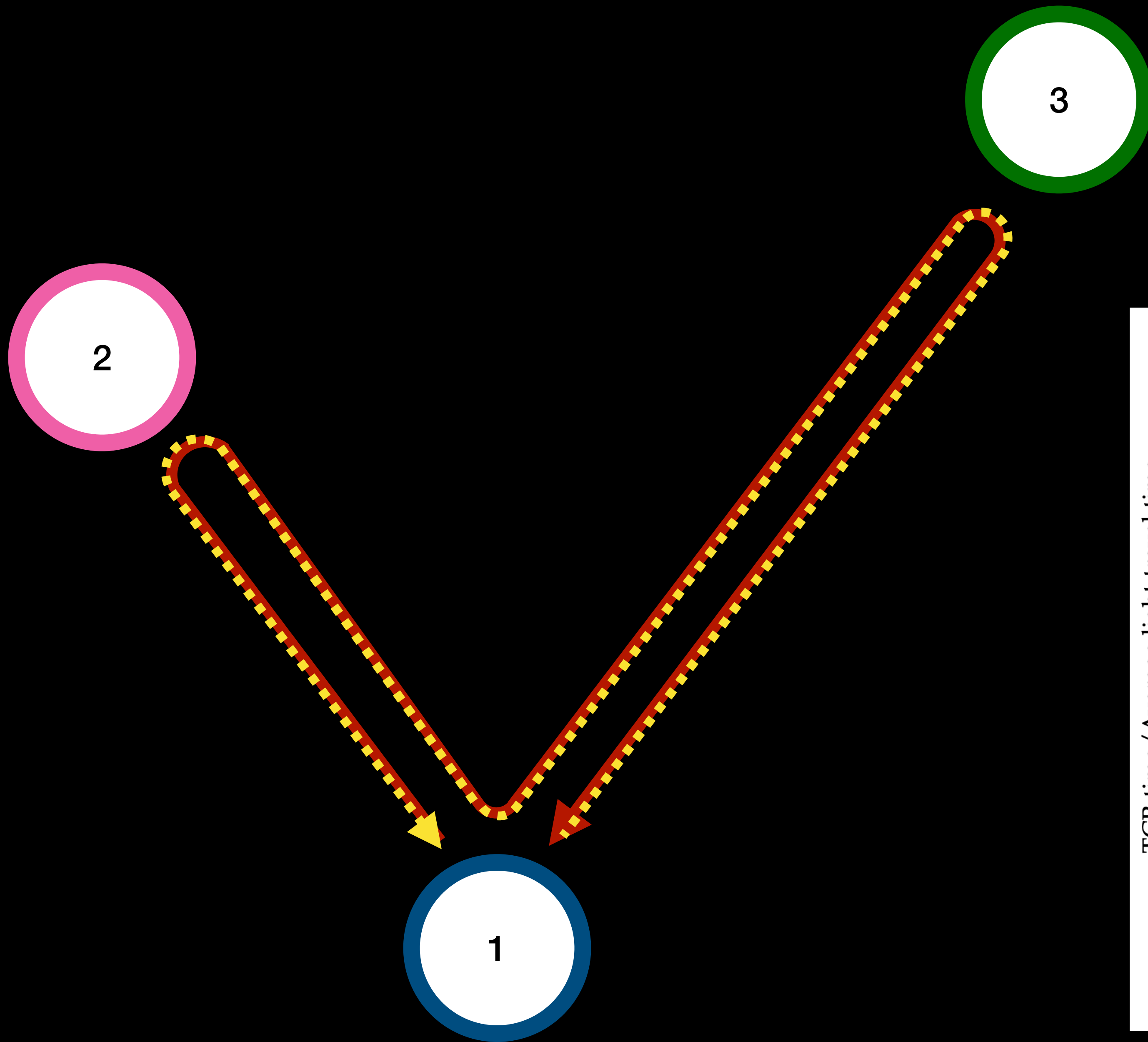
- In ‘good’ (?) approximation:
  - Only 3 channels independent even in realistic scenarios (time-varying orbits)
  - Popular choice: 3 Michelson combinations ( $X_2, Y_2, Z_2$ )
  - Under (strong) assumptions: easy to construct noise- and signal orthogonal (A, E, T)
  - At low frequency: only A,E sensitive to GWs, and  $S_h^A \simeq S_h^E \simeq S_h^X$

# 2nd generation TDI

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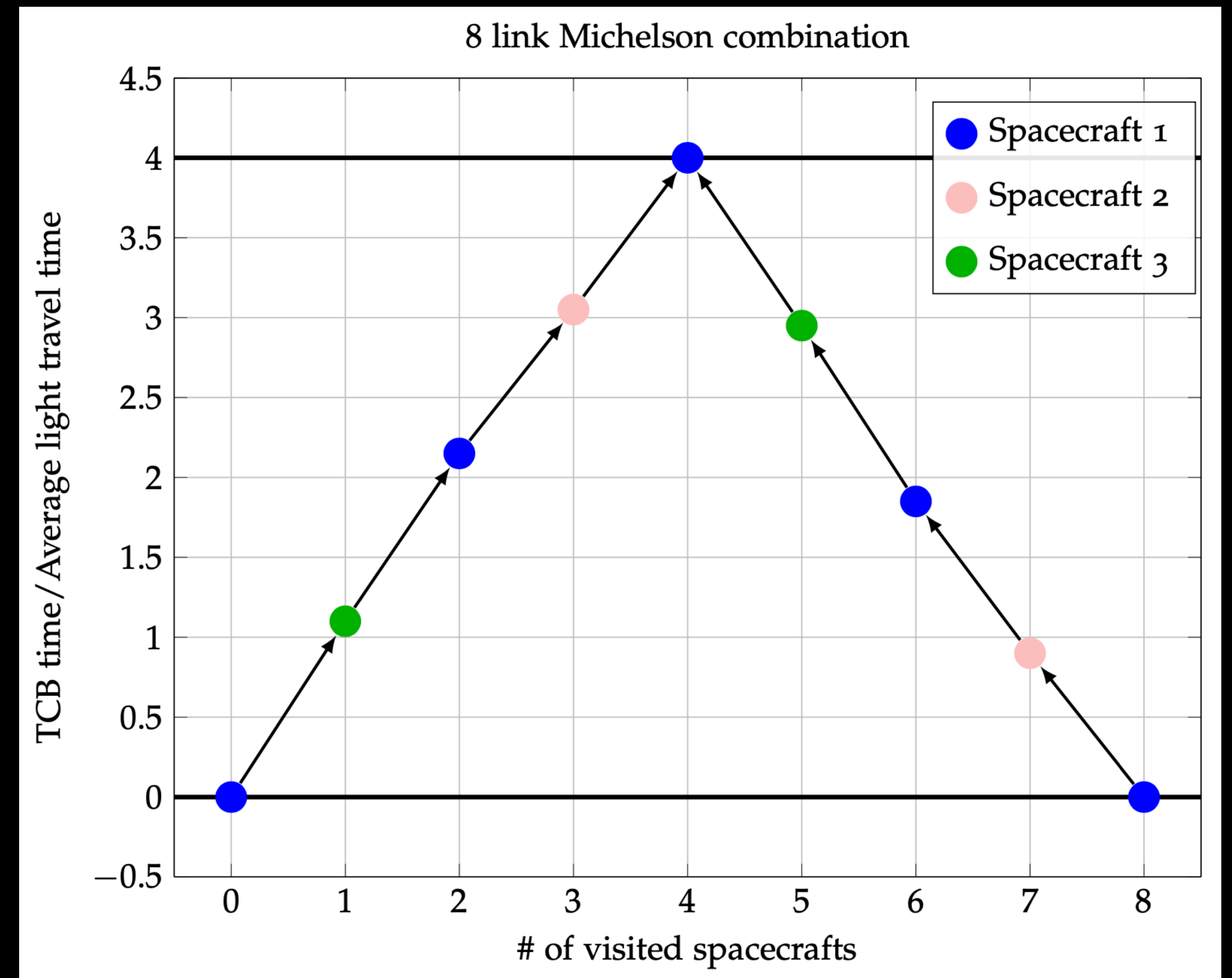
- With time-varying arms, algebraic solution for TDI is not known [Tinto 2021].
- Solutions were first discovered by modifying existing 1st generation variables [Tinto et al.]
- Many more solution found using ‘Geometric TDI’, using linear approximation of light travel times [Vallisneri]
- Recently revisited by different groups (e.g., [Muratore et al.]), who found more combinations using a symmetry in the LISA orbits

# Geometric TDI



“13 31 12 21 -13 -31 -12 -21”

“13121 -13121”



# Search algorithm for 2nd generation TDI

- Solutions can be found by exhaustive computation of all possible strings:
  - Generate all possible strings up to a certain length,
  - Compute time difference  $\delta t$  between first and last event in chain,
  - Discard combinations for which  $\delta t > \text{threshold}$ .
- $\delta t$  can first be evaluated assuming constant arm lengths (1st gen TDI)
  - Simple counting is sufficient (all links have to enter equal times in forward and backward time direction)
  - This allows to discard a vast number of strings.
- For 2nd generation TDI, one can use an analytical expansion  $L_{ij}(t) = L_{ij} + \dot{L}_{ij}t$  and require cancellation to first order in  $\dot{L}_{ij}$ 
  - Performing this expansion in the TCB [Vallisneri 2005] does not account for certain symmetries, and excludes Sagnac-like combinations
  - [Muratore et al.] showed that additional combinations can be found by doing the expansion in the Fermi-normal frame
  - Alternatively,  $\delta t$  can also be evaluated numerically



# TDI Combinations: overview

- Many solutions to the problem of 2nd generation TDI:
  - [Vallisneri] added many 16+ link combinations
  - [Muratore et al.] added additional 12, 14 and 16 link combinations
- Table reduced by various symmetries:
  - Rotation, reflection of constellation
  - String-reversal
  - Time reversal
- 34 core combinations up to 16 links represent 210 distinct variables

$\alpha_2 \rightarrow$

$X_2 \rightarrow$

Name	Normal string	$\dot{L}$ closed	M.S.	T.S.	Trivial
$C_1^{12}$	"1231321 -1321231"		✓	✓	
$C_2^{12}$	"12321 -1321 131 -1231"			✓	
$C_3^{12}$	"121 -13 32 -21 13 -323 31 -12 23 -31"		✓	✓	
$C_1^{14}$	"121321 -13212 231 -1231"				
$C_2^{14}$	"1213 -3213 32 -2123 3123 -31"			✓	
$C_3^{14}$	"1213 -32 21 -13 32 -2123 31 -12 23 -31"			✓	
$C_1^{16}$	"121313121 -131212131"	✓	✓	✓	
$C_2^{16}$	"121323121 -132121231"			✓	
$C_3^{16}$	"123121321 -132121231"			✓	
$C_4^{16}$	"12121 -13121 13131 -12131"	✓	✓	✓	✓
$C_5^{16}$	"1213121 -13121 131 -12131"	✓		✓	
$C_6^{16}$	"1213212 -23121 132 -21231"	✓		✓	
$C_7^{16}$	"123123 -31321 1313 -32131"	✓		✓	
$C_8^{16}$	"12313123 -31321 13 -32131"	✓		✓	
$C_9^{16}$	"12121 -13212 23132 -21231"			✓	
$C_{10}^{16}$	"1213121 -13212 232 -21231"			✓	
$C_{11}^{16}$	"12312321 -1321 13 -321231"				
$C_{12}^{16}$	"1231321 -13123 313 -32131"			✓	
$C_{13}^{16}$	"12121 -1321 132 -212 231 -1231"			✓	
$C_{14}^{16}$	"1213121 -13 32 -2123212 23 -31"		✓	✓	
$C_{15}^{16}$	"12132 -2123 3121 -13212 23 -31"		✓		
$C_{16}^{16}$	"1213 -3212 232 -2123 3121 -131"		✓	✓	
$C_{17}^{16}$	"12132 -21321 1312 -2312 23 -31"				
$C_{18}^{16}$	"1213 -321 1321 -1312 231 -1231"			✓	
$C_{19}^{16}$	"1232321 -1321 13 -323 31 -1231"			✓	
$C_{20}^{16}$	"1232321 -1323 31 -121 13 -3231"			✓	
$C_{21}^{16}$	"12123 -3121 13 -32 213 -3212 23 -31"	✓			
$C_{22}^{16}$	"1213 -3212 23 -3121 13 -32 2123 -31"	✓	✓		
$C_{23}^{16}$	"12121 -13 32 -2123 313 -3212 23 -31"			✓	
$C_{24}^{16}$	"1231 -121 13 -321 1321 -131 12 -231"		✓		✓
$C_{25}^{16}$	"12321 -1323 31 -12 232 -21 13 -3231"			✓	
$C_{26}^{16}$	"12121 -13 32 -21 13 -32123 31 -12 23 -31"			✓	
$C_{27}^{16}$	"12132 -21 13 -32 21 -13123 31 -12 23 -31"			✓	
$C_{28}^{16}$	"121 -132 21 -13 32 -21 131 -123 31 -12 23 -31"		✓		✓

# TDI Combinations: overview

Name	Normal string	$\dot{L}$ closed	M.S.	T.S.	Trivial
$C_1^{12}$	"1231321 -1321231"		✓	✓	
$C_2^{12}$	"12321 -1321 131 -1231"			✓	
$C_3^{12}$	"121 -13 32 -21 13 -323 31 -12 23 -31"		✓	✓	
$C_1^{14}$	"121321 -13212 231 -1231"				
$C_2^{14}$	"1213 -3213 32 -2123 3123 -31"			✓	
$C_3^{14}$	"1213 -32 21 -13 32 -2123 31 -12 23 -31"			✓	
$C_1^{16}$	"121313121 -131212131"	✓	✓	✓	
$C_2^{16}$	"121323121 -132121231"			✓	
$C_3^{16}$	"123121321 -132121231"			✓	
$C_4^{16}$	"12121 -13121 13131 -12131"	✓	✓	✓	✓
$C_5^{16}$	"1213121 -13121 131 -12131"	✓		✓	
$C_6^{16}$	"1213212 -23121 132 -21231"	✓		✓	
$C_7^{16}$	"123123 -31321 1313 -32131"	✓		✓	
$C_8^{16}$	"12313123 -31321 13 -32131"	✓		✓	
$C_9^{16}$	"12121 -13212 23132 -21231"			✓	
$C_{10}^{16}$	"1213121 -13212 232 -21231"			✓	
$C_{11}^{16}$	"12312321 -1321 13 -321231"				
$C_{12}^{16}$	"1231321 -13123 313 -32131"			✓	
$C_{13}^{16}$	"12121 -1321 132 -212 231 -1231"			✓	
$C_{14}^{16}$	"1213121 -13 32 -2123212 23 -31"		✓	✓	
$C_{15}^{16}$	"12132 -2123 3121 -13212 23 -31"		✓		
$C_{16}^{16}$	"1213 -3212 232 -2123 3121 -131"		✓	✓	
$C_{17}^{16}$	"12132 -21321 1312 -2312 23 -31"				
$C_{18}^{16}$	"1213 -321 1321 -1312 231 -1231"			✓	
$C_{19}^{16}$	"1232321 -1321 13 -323 31 -1231"			✓	
$C_{20}^{16}$	"1232321 -1323 31 -121 13 -3231"			✓	
$C_{21}^{16}$	"12123 -3121 13 -32 213 -3212 23 -31"	✓			
$C_{22}^{16}$	"1213 -3212 23 -3121 13 -32 2123 -31"	✓	✓		
$C_{23}^{16}$	"12121 -13 32 -2123 313 -3212 23 -31"			✓	
$C_{24}^{16}$	"1231 -121 13 -321 1321 -131 12 -231"		✓		✓
$C_{25}^{16}$	"12321 -1323 31 -12 232 -21 13 -3231"			✓	
$C_{26}^{16}$	"12121 -13 32 -21 13 -32123 31 -12 23 -31"			✓	
$C_{27}^{16}$	"12132 -21 13 -32 21 -13123 31 -12 23 -31"			✓	
$C_{28}^{16}$	"121 -132 21 -13 32 -21 131 -123 31 -12 23 -31"		✓		✓

Name	Timeshift	Expression
$C_1^{12}$	1	$(1 - xyz)\alpha$
$C_2^{12}$	$xy^2$	$(y - xz)\alpha$
$C_3^{12}$	$yz$	$(y - xz)\zeta$
$C_1^{14}$	$xy$	$(1 - z^2)\alpha$
$C_2^{14}$	$yz$	$(1 - z^2)\gamma$
$C_3^{14}$	$y$	$(1 - z^2)\zeta$
$C_1^{16}$	1	$(1 - y^2z^2)(\alpha - z\beta - y\gamma + yz\zeta)$
$C_2^{16}$	1	$(1 - xyz^3)\alpha - z(1 - xyz)\beta$
$C_3^{16}$	1	$(1 - xyz^3)\alpha$
$C_4^{16}$	$y^4z^2$	$(y - z)(y + z)(\alpha - z\beta - y\gamma + yz\zeta)$
$C_5^{16}$	$y^2$	$(1 - z^2)(\alpha - z\beta - y\gamma + yz\zeta)$
$C_6^{16}$	$xy$	$(1 - z^2)(z\alpha - \beta)$
$C_7^{16}$	$xy^3$	$(y - xz)(y\alpha - \gamma)$
$C_8^{16}$	$y$	$(1 - xyz)(y\alpha - \gamma)$
$C_9^{16}$	$x^2y^2z^2$	$(xy - z^3)\alpha + (z^2 - xyz)\beta$
$C_{10}^{16}$	$x^2y$	$(x - yz^3)\alpha + (yz^2 - xz)\beta$
$C_{11}^{16}$	$y$	$(1 - x^2z^2)\alpha$
$C_{12}^{16}$	$y^2$	$(1 - xyz)\alpha + (xz - y)\gamma$
$C_{13}^{16}$	$x^2yz$	$(xy - z^3)\alpha$
$C_{14}^{16}$	$y$	$(xyz^2 - z)\gamma + (1 - xyz^3)\zeta$
$C_{15}^{16}$	$xz^2$	$(xy - z)\gamma + (1 - xyz)\zeta$
$C_{16}^{16}$	$yz^2$	$(xy - z^3)\gamma + (-xyz + z^2)\zeta$
$C_{17}^{16}$	$xy^2z^2$	$(y - xz)\beta$
$C_{18}^{16}$	$x$	$(x - yz)\alpha$
$C_{19}^{16}$	$xy^2$	$(y - x^3z)\alpha$
$C_{20}^{16}$	$xy^2$	$(y - x^3z)\alpha + (x^2z - xy)\zeta$
$C_{21}^{16}$	$yz^2$	$(xz - y)(\gamma - z\zeta)$
$C_{22}^{16}$	$yz^2$	$(1 - z^2)(\gamma - z\zeta)$
$C_{23}^{16}$	$y^2z^2$	$(xz^2 - yz)\gamma + (y - xz^3)\zeta$
$C_{24}^{16}$	$xyz^3$	$(z^2 - y^2)\alpha$
$C_{25}^{16}$	$x^2y$	$(y - xz)\alpha + (z - xy)\zeta$
$C_{26}^{16}$	$yz$	$(y - xz^3)\zeta$
$C_{27}^{16}$	$x$	$(1 - xyz)\zeta$
$C_{28}^{16}$	$y^3z$	$(y - z)(y + z)\zeta$

- Going back to the assumption of 3 constant arms, all these variables can be represented in terms of 4 generators  $\alpha, \beta, \gamma, \zeta$
- This is often sufficient to describe instrumental noises + GW response

$$x \approx D_{23} \approx D_{32}$$

$$y \approx D_{31} \approx D_{13}$$

$$z \approx D_{12} \approx D_{21}$$



- Standard TDI formulation: continuous time
- Actual data: sampled time series
- TDI- $\infty$ : re-formulate TDI on sample-space

$$\mathbf{y} = \begin{bmatrix} y_1(t_1) \\ y_2(t_1) \\ y_1(t_2) \\ \dots \\ y_1(t_n) \\ y_2(t_n) \end{bmatrix} \quad \mathbf{p} = \begin{bmatrix} p(t_1) \\ p(t_2) \\ \dots \\ p(t_n) \end{bmatrix} \quad \mathbf{y} = \mathbf{M}\mathbf{p} + \mathbf{h} + \mathbf{n} \rightarrow \mathbf{M}\mathbf{p}$$

Similar to algebraic approach: define observable as  $\mathbf{o} = \mathbf{T}\mathbf{y} = \mathbf{T}\mathbf{M}\mathbf{p}$ , look for solutions of  $\mathbf{T}\mathbf{M} = \mathbf{0}$

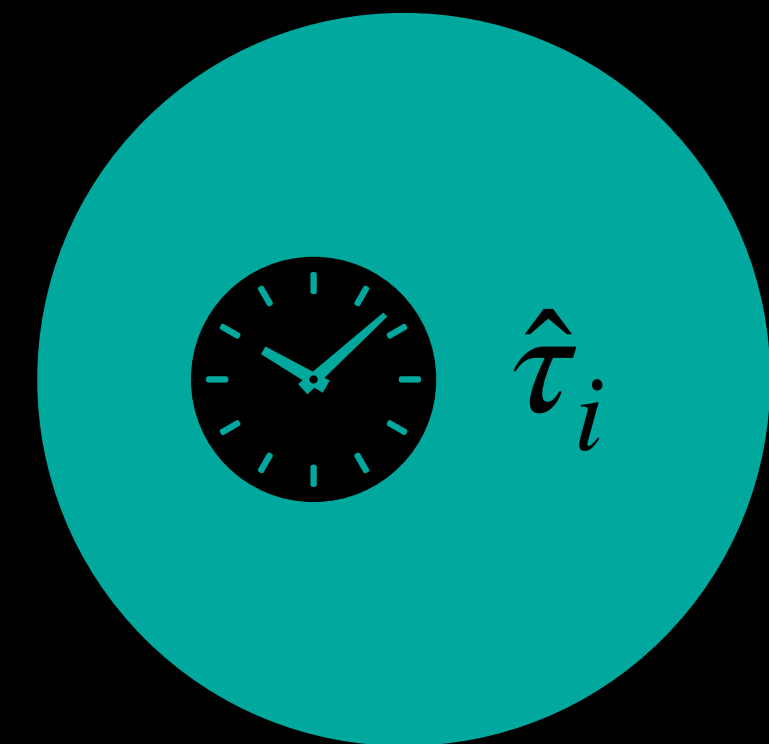
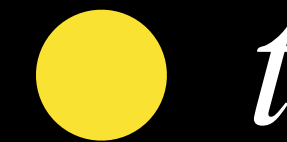
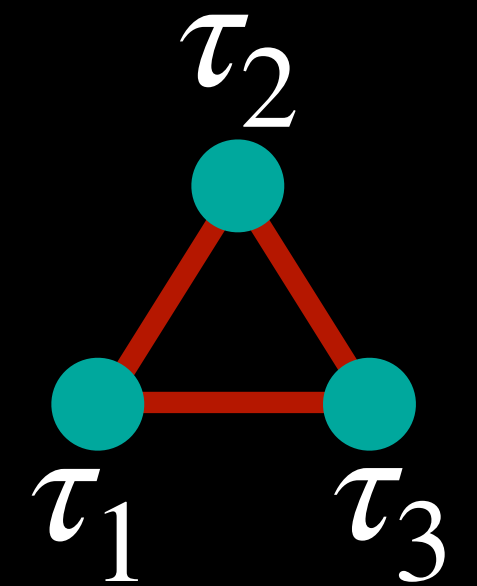
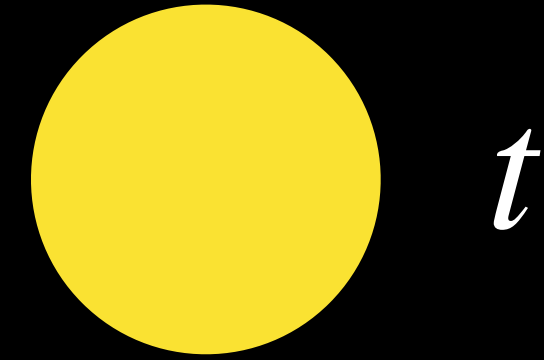
- Difference: problem on regular vector space, ‘standard’ linear algebra!
- Disadvantage: computational complexity (large matrix), interpretability

[Vallisneri et al, 2020]

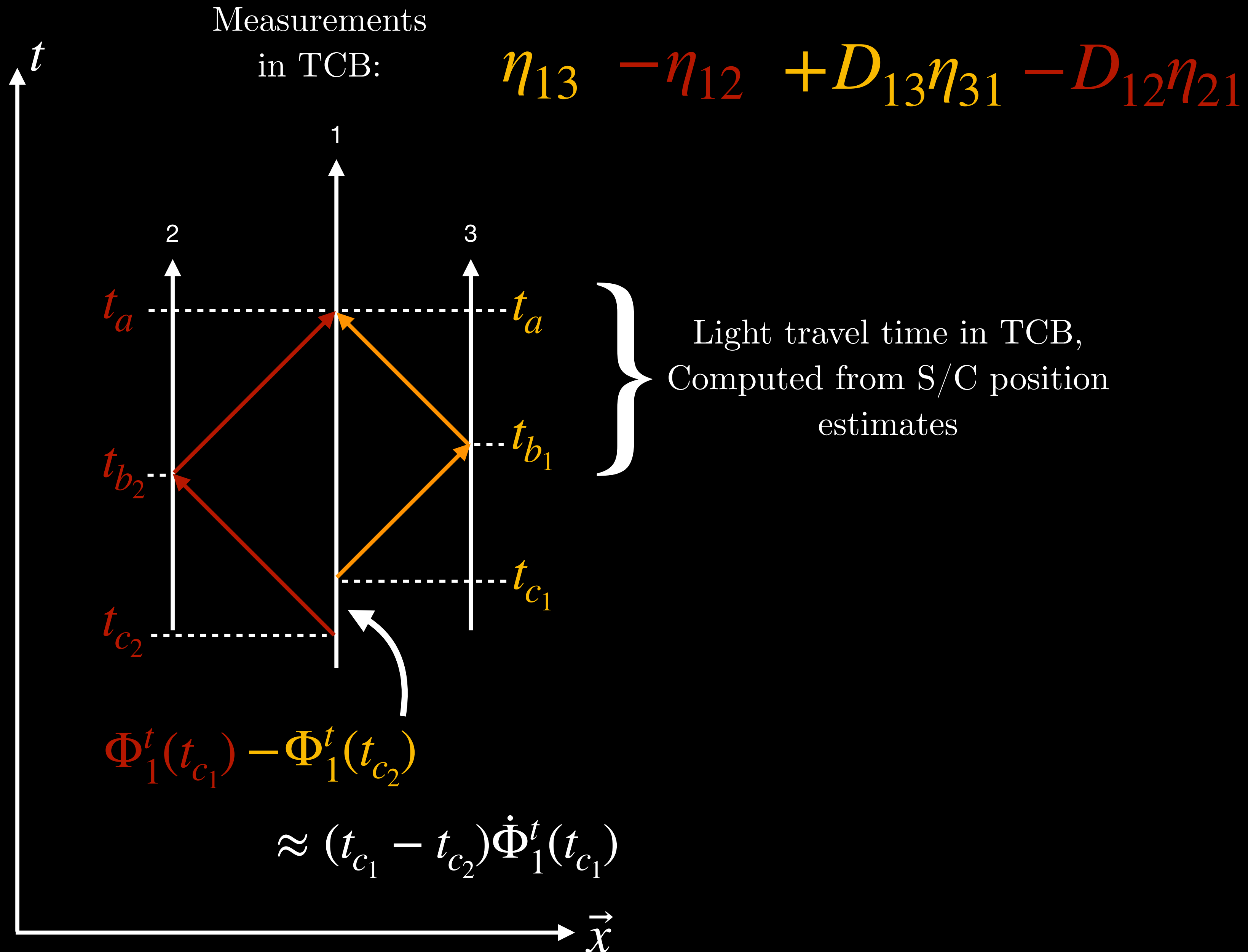
# TDI with desynchronized clocks

# Timescales in LISA

- TCB time  $t$ 
  - Defined as the time shown of a **perfect** clock sitting at the solar system baricenter
  - Global timescale, used for data analysis + ‘standard’ formulation of TDI
- One proper time  $\tau_i$  for each spacecraft  $i$  ( $i = 1,2,3$ )
  - Defined as the time shown of a **perfect** clock sitting in spacecraft  $i$
  - Related to  $t$  (and each other) by General Relativity
  - Used for describing physics inside one spacecraft
- One onboard clock time  $\hat{\tau}_i$  for each spacecraft  $i$  ( $i = 1,2,3$ )
  - Defined as the time shown of the **actual** clock sitting in spacecraft  $i$
  - Differs from  $\tau_i$  by instrumental imperfections
  - **Only timescale directly accessible by the satellites**

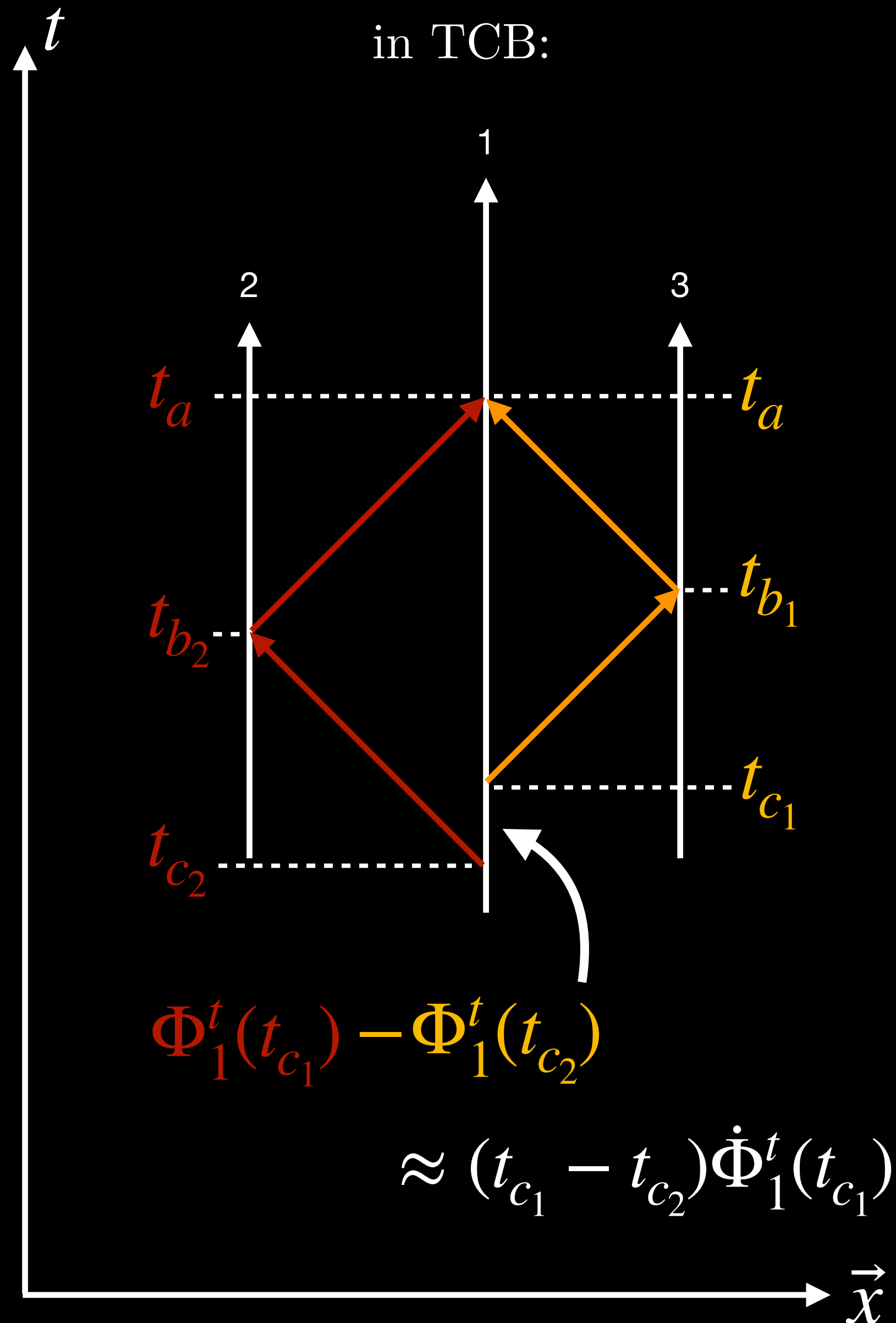


# Geometric TDI with clock times

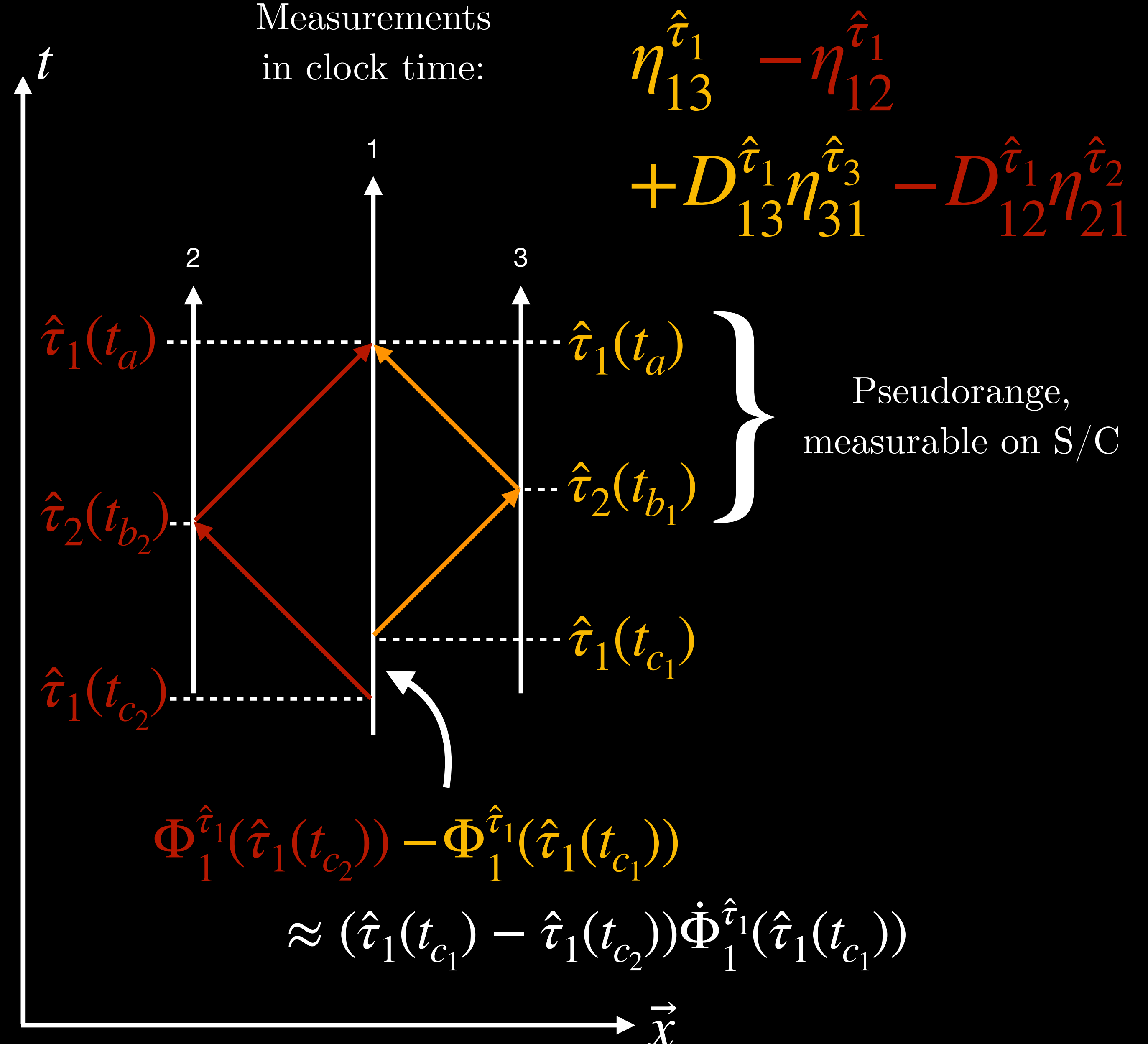


# Geometric TDI with clock times

Measurements  
in TCB:



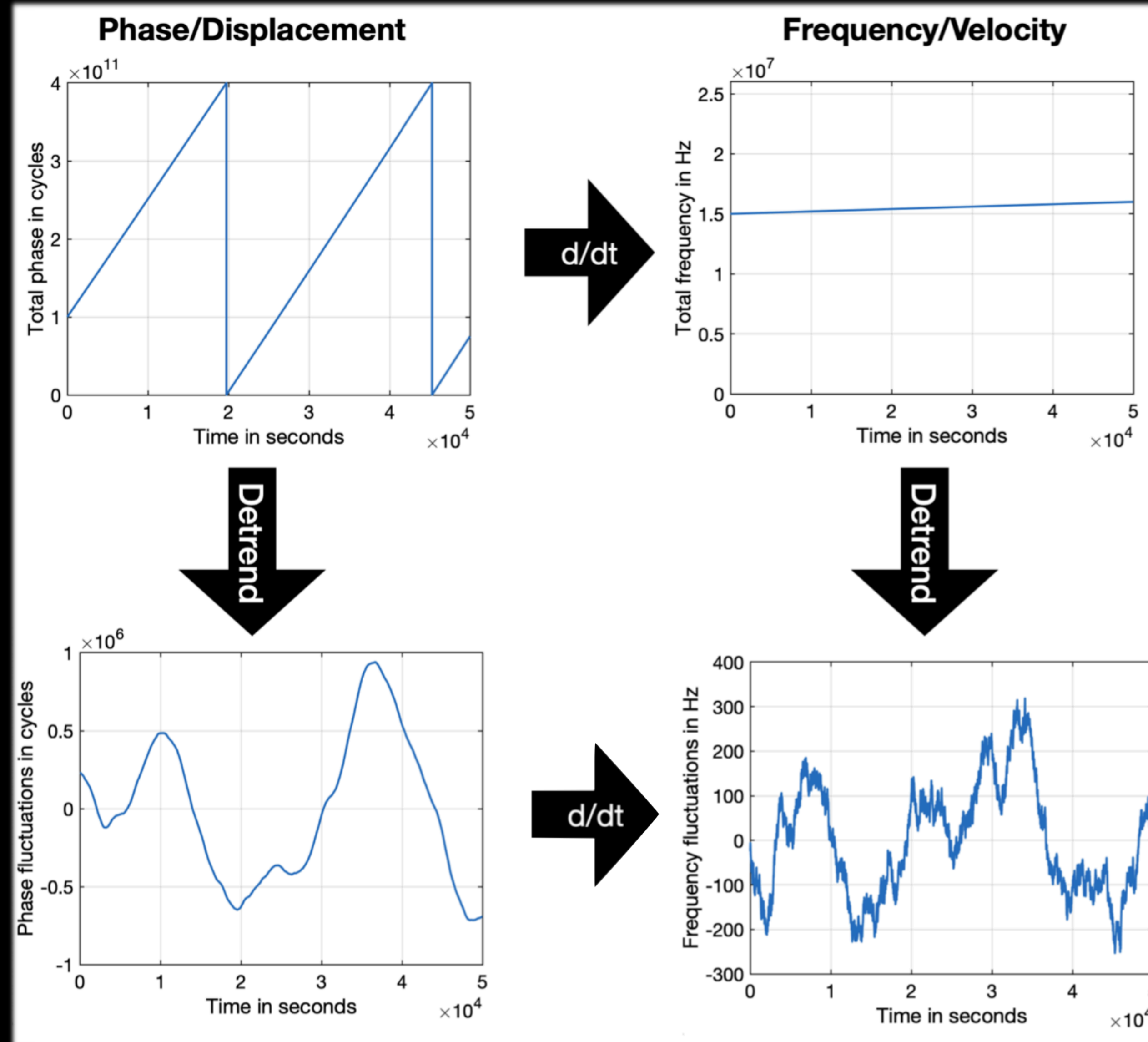
Measurements  
in clock time:



# TDI: Phase vs. Frequency



# Different units: overview



# TDI with frequency

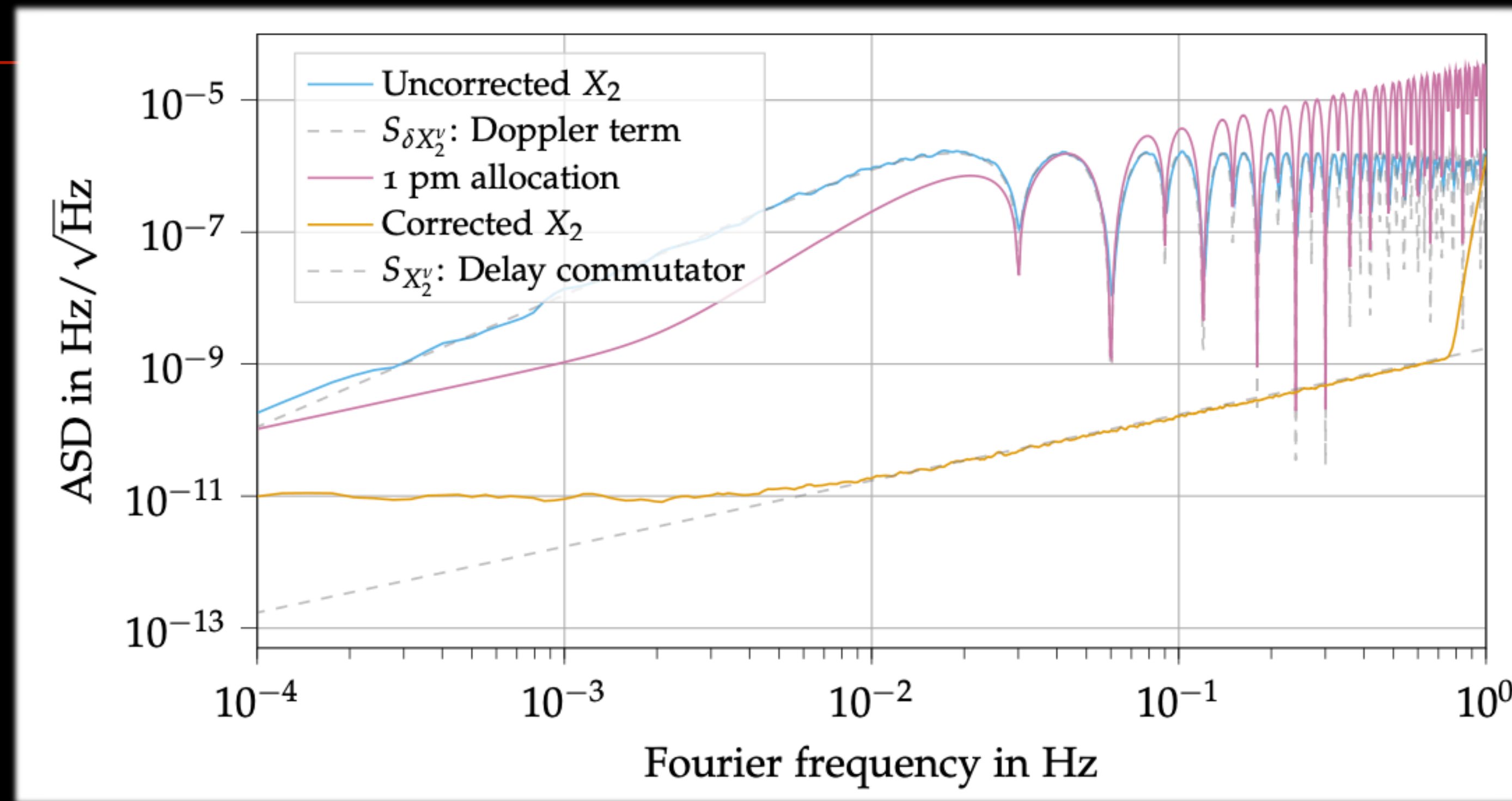
- TDI is usually formulated in terms of phase, where we have

$$\begin{aligned}\eta_{12}(t) &= D_{12}\Phi_2(t) - \Phi_1(t) \\ &= \Phi_2(t - d_{12}(t)) - \Phi_1(t)\end{aligned}$$

- In terms of frequency, we get instead

$$\begin{aligned}\dot{\eta}_{12}(t) &= (1 - \dot{d}_{12}(t)) \times \dot{\Phi}_2(t - d_{12}(t)) - \dot{\Phi}_1(t) \\ &\equiv \dot{D}_{12}\nu_2(t) - \nu_1(t)\end{aligned}$$

- Neglecting Doppler shifts causes large residuals
- Solution: replace all  $D_{12} \rightarrow \dot{D}_{12}$

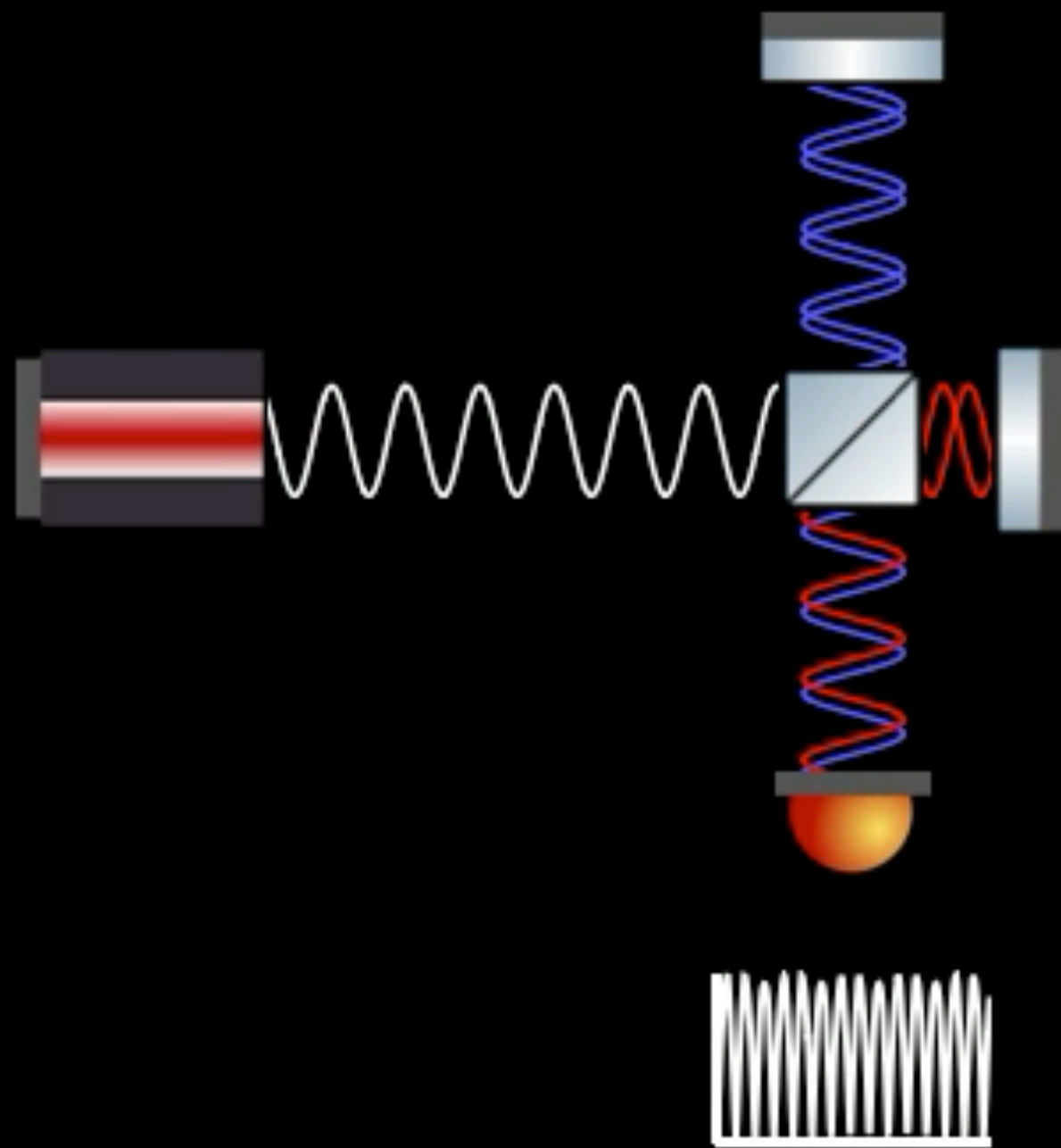


[Bayle,Hartwig,Staab 2021]

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## Clock noise: technical details

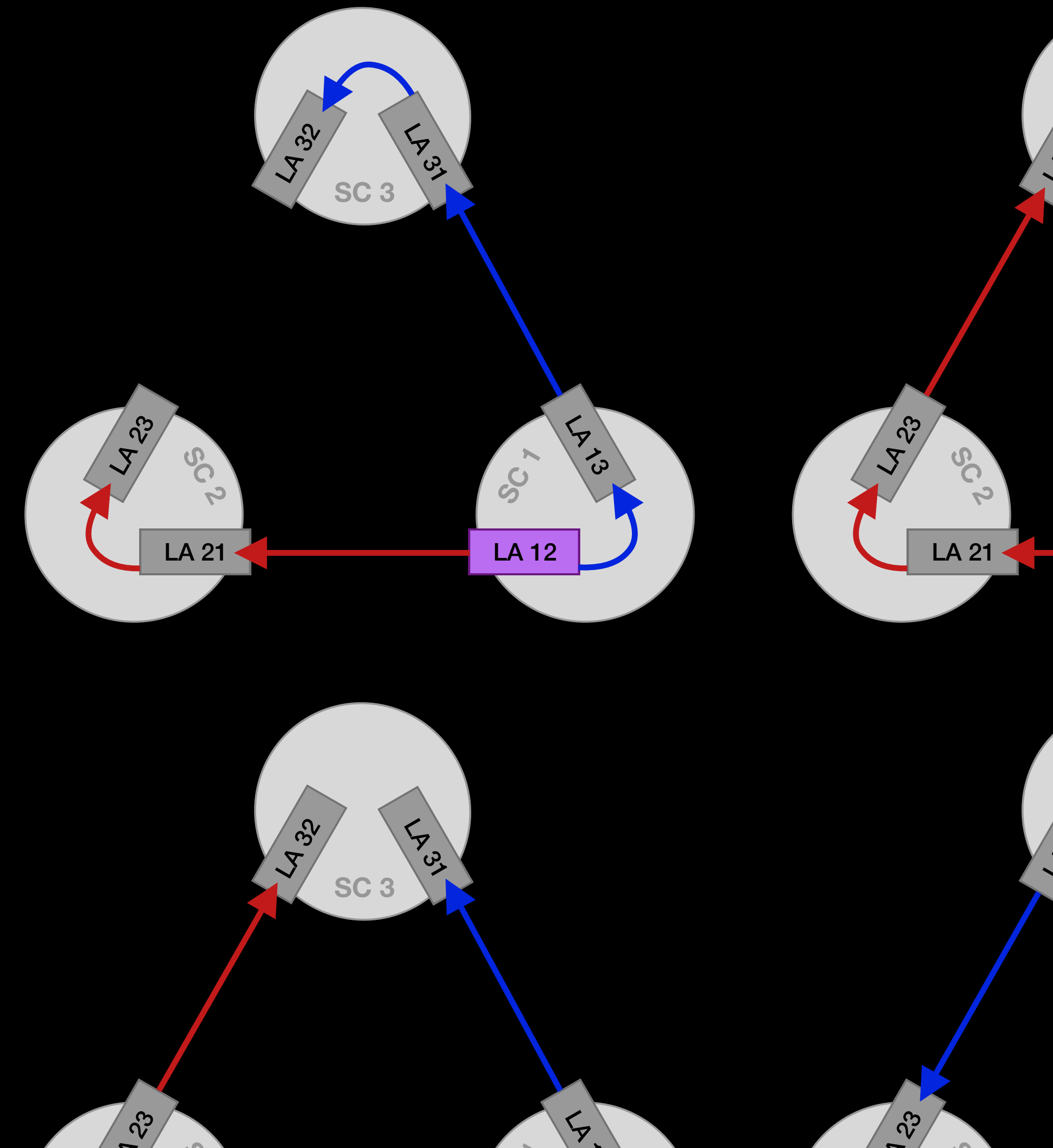
# Further complications: beyond laser noise suppression



- Spacecraft are moving!
- Heterodyne interferometry:
  - Signals are up to 25 MHz beatnotes
  - pm distance fluctuations with  $\lambda = 1064 \text{ nm}$   
 $\Rightarrow$   $\mu$ cycle phase shifts

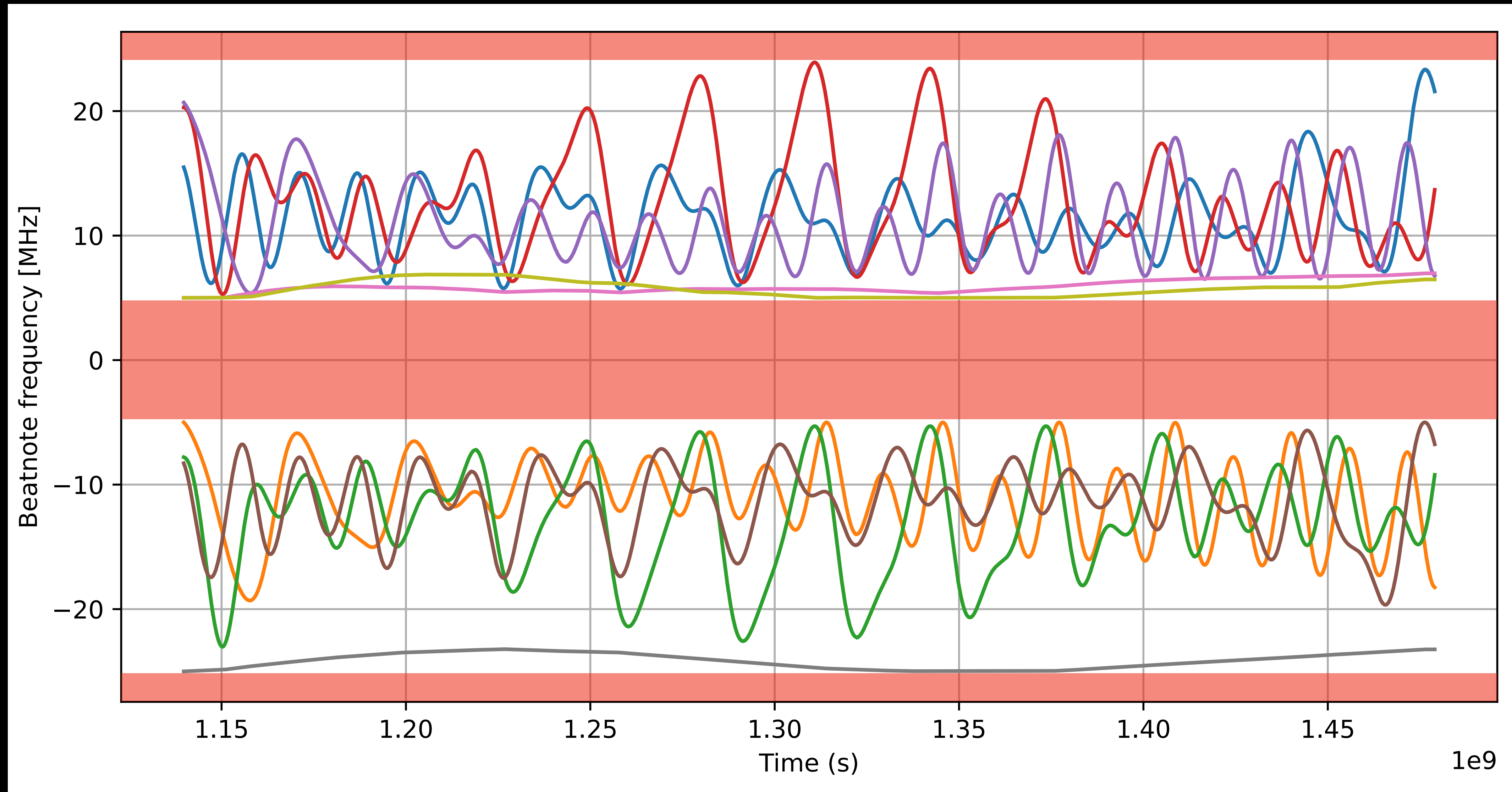
# Laser Locking & Frequency Plan

- Due to time-varying Dopplers, beatnotes are not guaranteed to fall in phasemeter validity frequency range (5 to 25 MHz)
- Doppler shifts: 10s of MHz
- Solution: lock lasers with precomputed frequency plan
- Interesting problem in computational geometry (many configurations possible), see [Heinzel et al.]





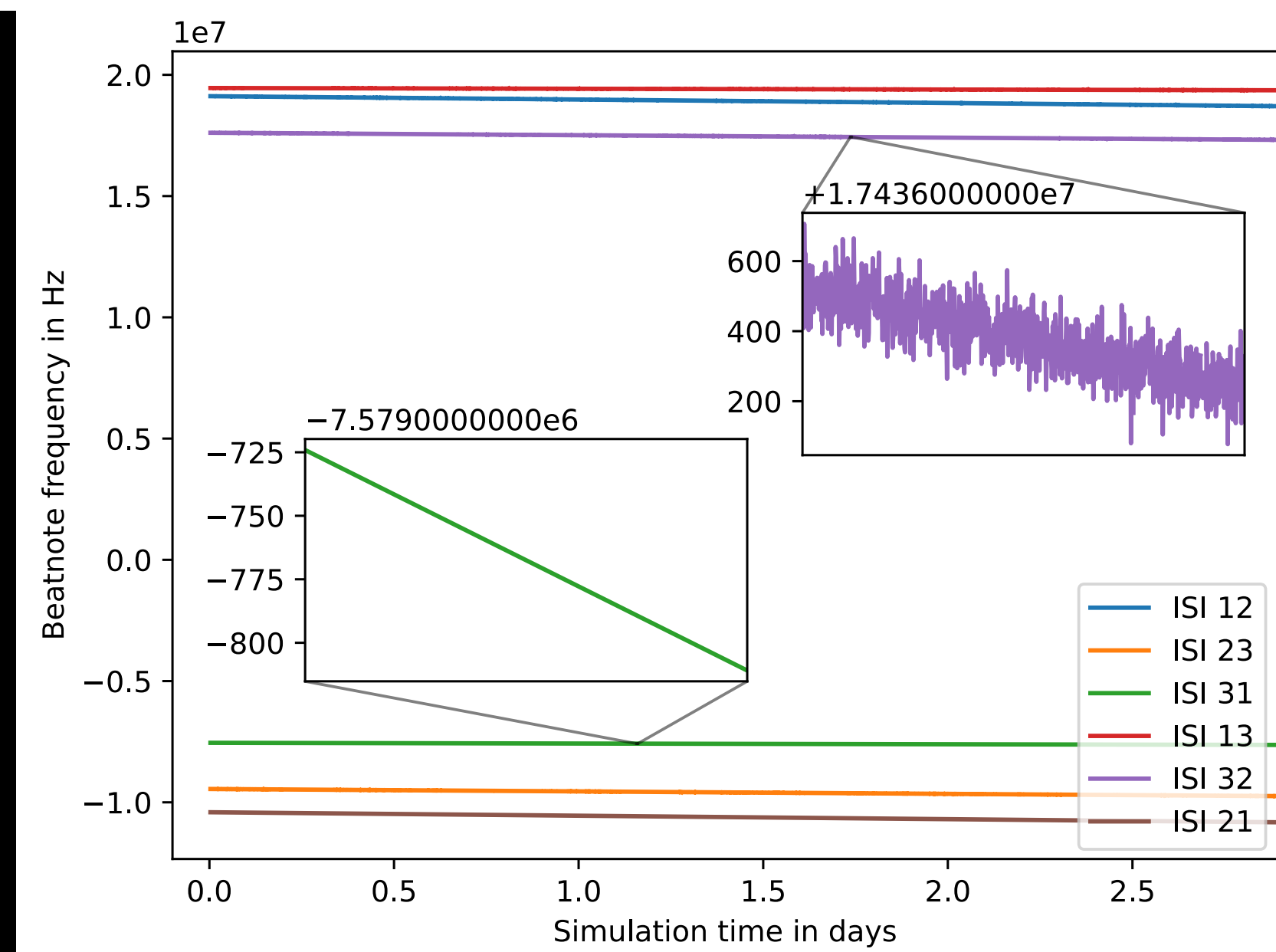
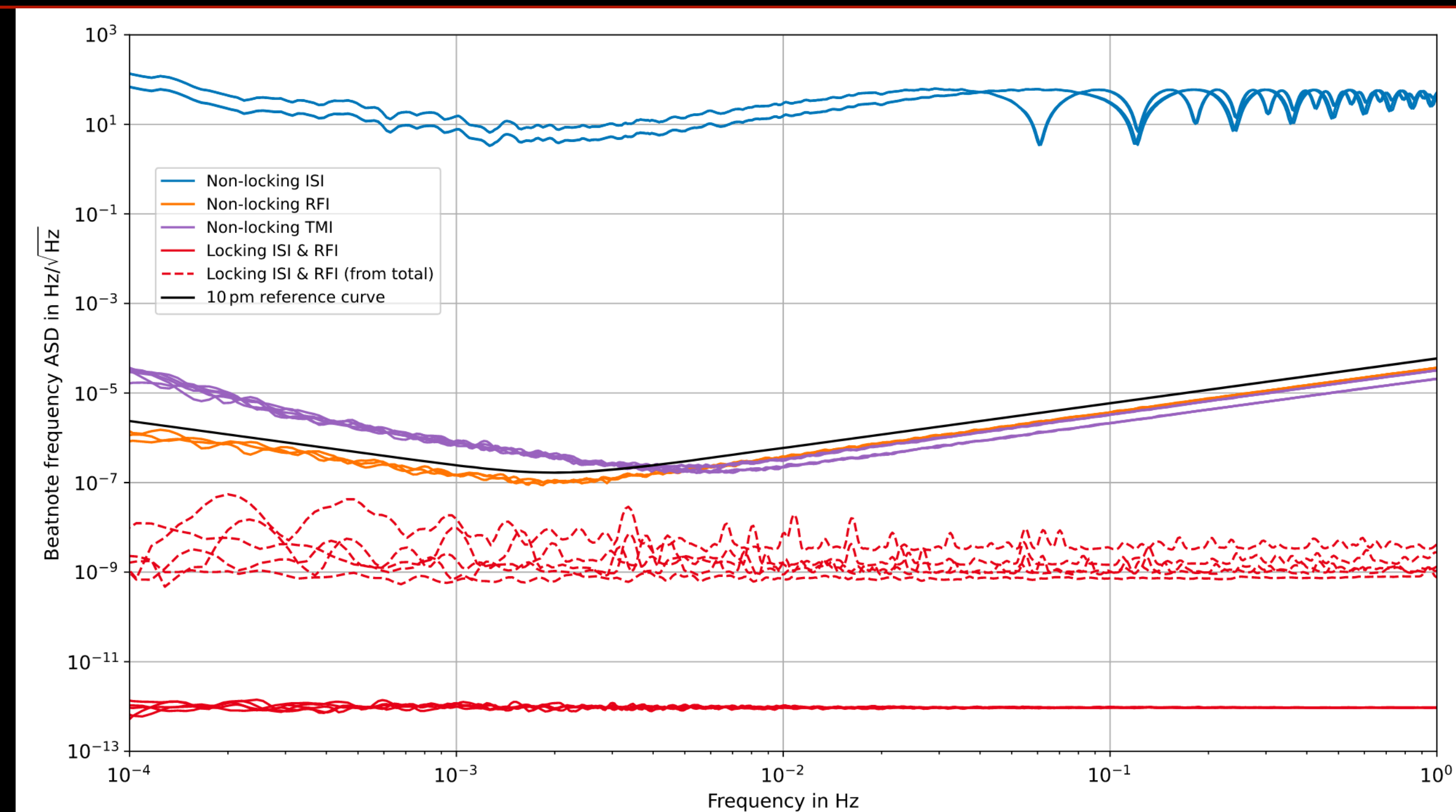
# Laser Locking & Frequency Plan



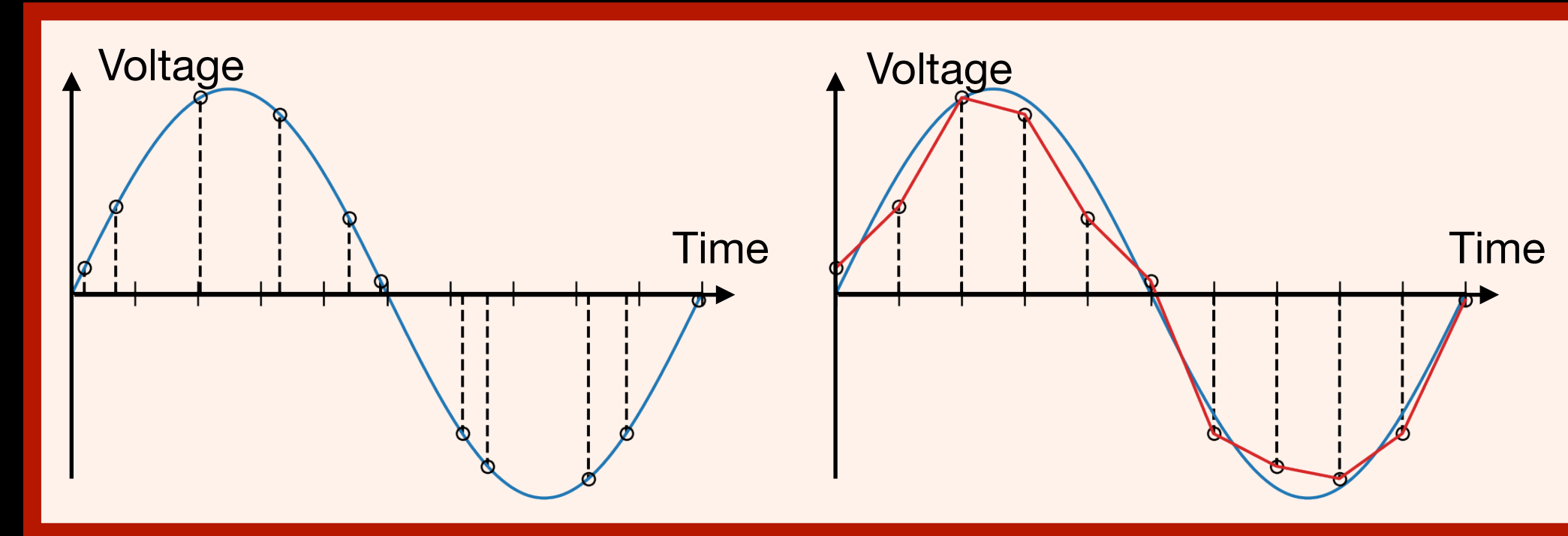
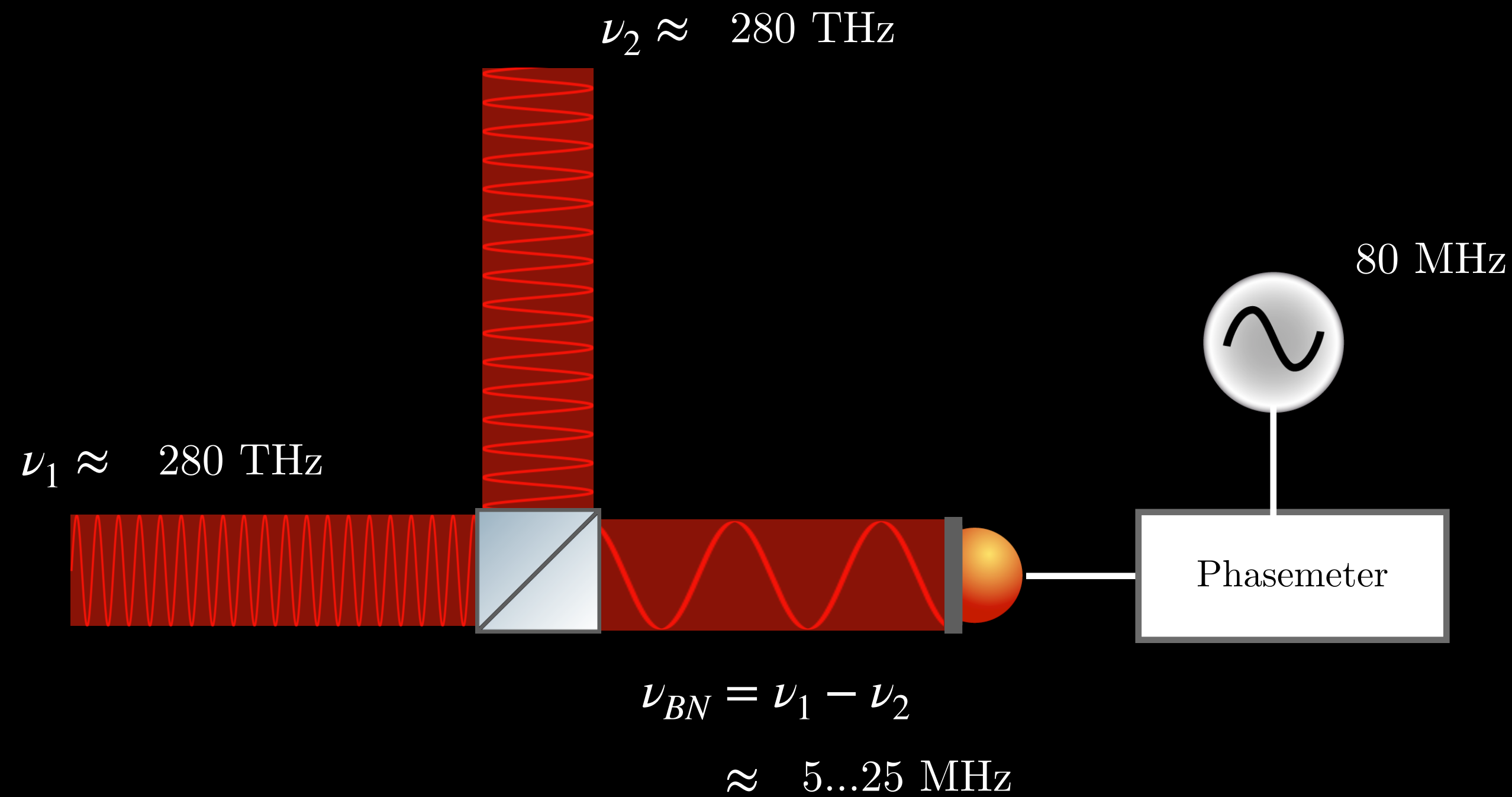


# Laser locking side effects

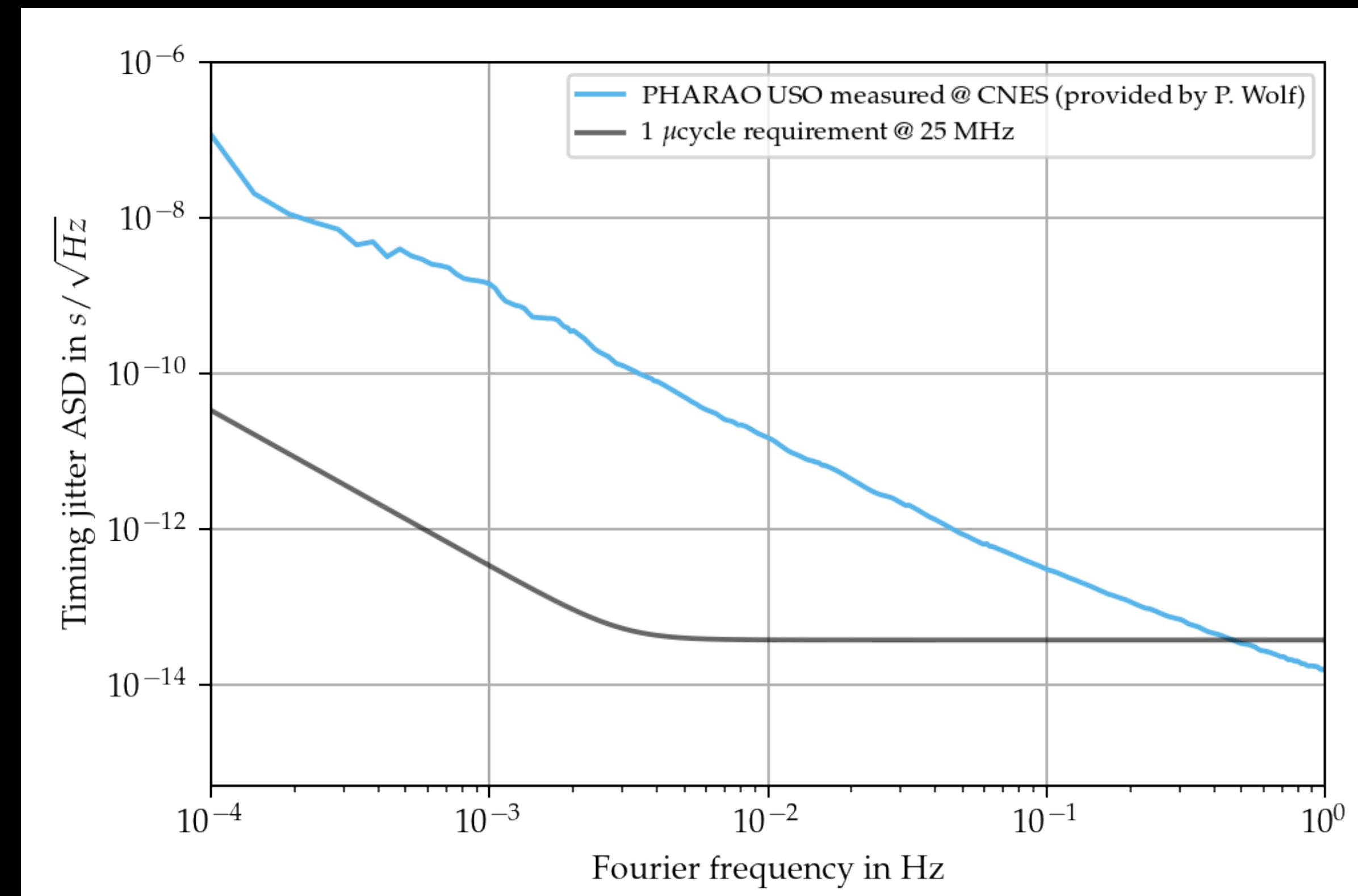
- Locking control loop: adjust local laser frequency based on measured beatnote to drive it to desired value
- Side effect: information is ‘moved around’ between beatnotes
- Drastically changes raw measurements: GW (and secondary noises) only visible in non-locking beatnotes, locking ones follow nominal values
- Interestingly: this (almost) completely disappears on TDI level!
- Simple argument: TDI suppresses whatever comes out of the laser - laser locking simply makes that more complex



# Clock and time-related issues



- Phase tracking requires comparison to local reference clock
- 25 MHz beatnotes require  $40 \text{ fs}/\sqrt{\text{Hz}}$  timing precision for  $\mu\text{cycle}$  phase readout
- Existing space-qualified clocks fall short by a few orders of magnitude!



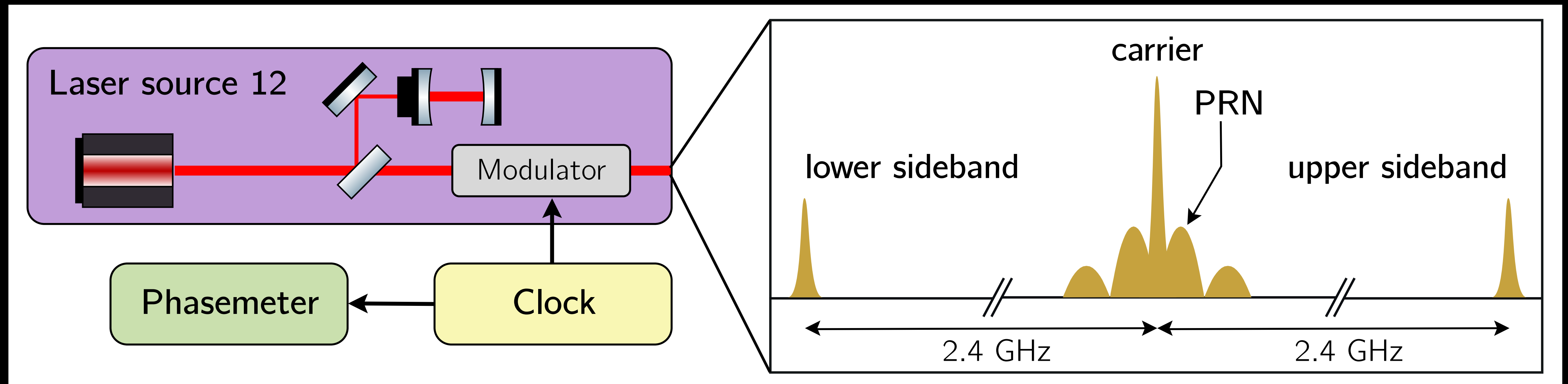
Note: Illustrative, numbers to be seen as placeholders

# Beam Modulation: GHz Sidebands

- Phase modulation used to measure the in-band part of this clock noise

$$E(\tau) \approx E_0(\tau)e^{i\Phi_c(\tau)}e^{im\cos(\Phi_m(\tau))}$$

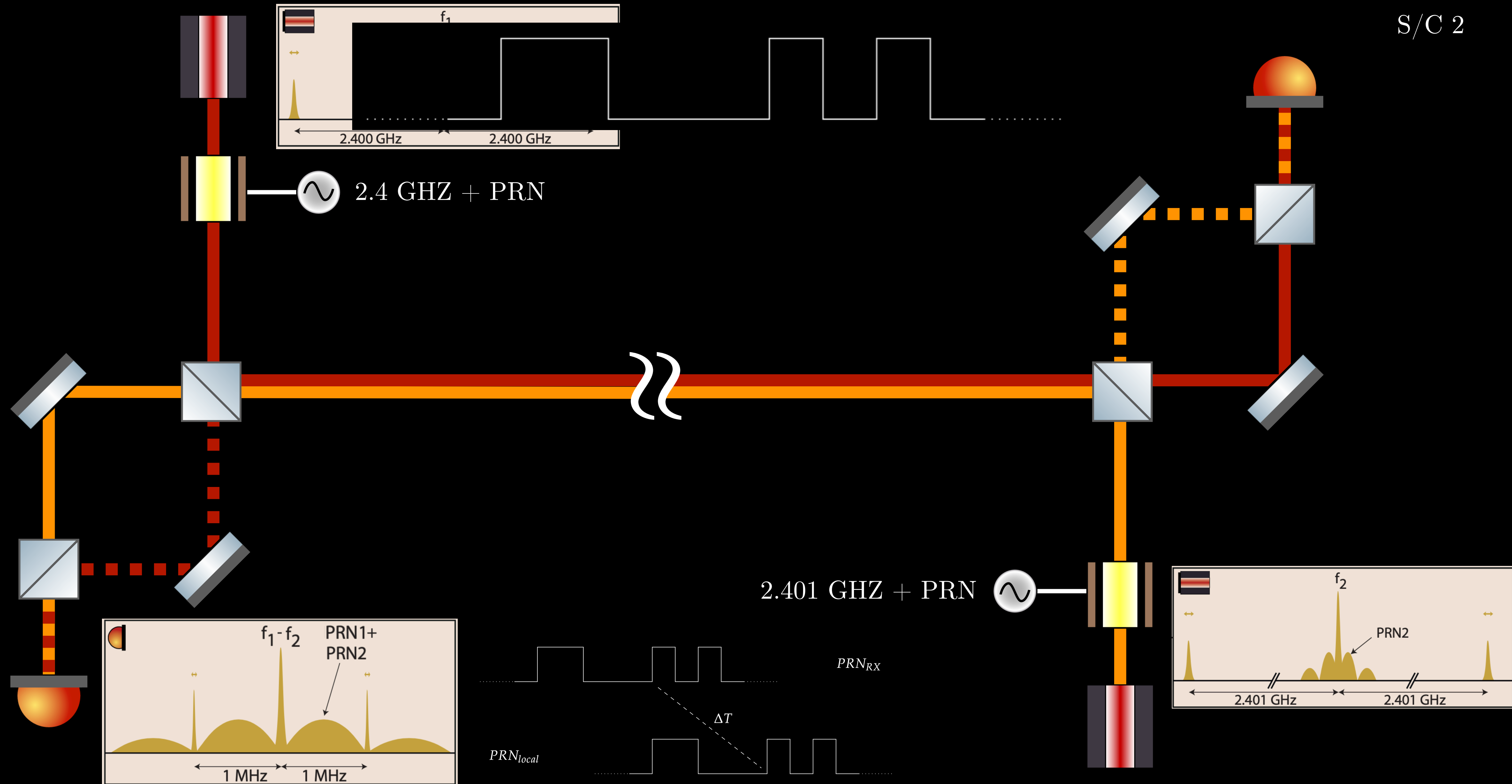
- Modeled as “independent” sideband beams (expansion with Bessel functions)  $e^{im\cos(\Phi_m(\tau))} \approx 1 + \frac{im}{2}e^{i\Phi_m(\tau)} + \frac{im}{2}e^{-i\Phi_m(\tau)}$



# Clock and time-related issues

S/C 1

S/C 2

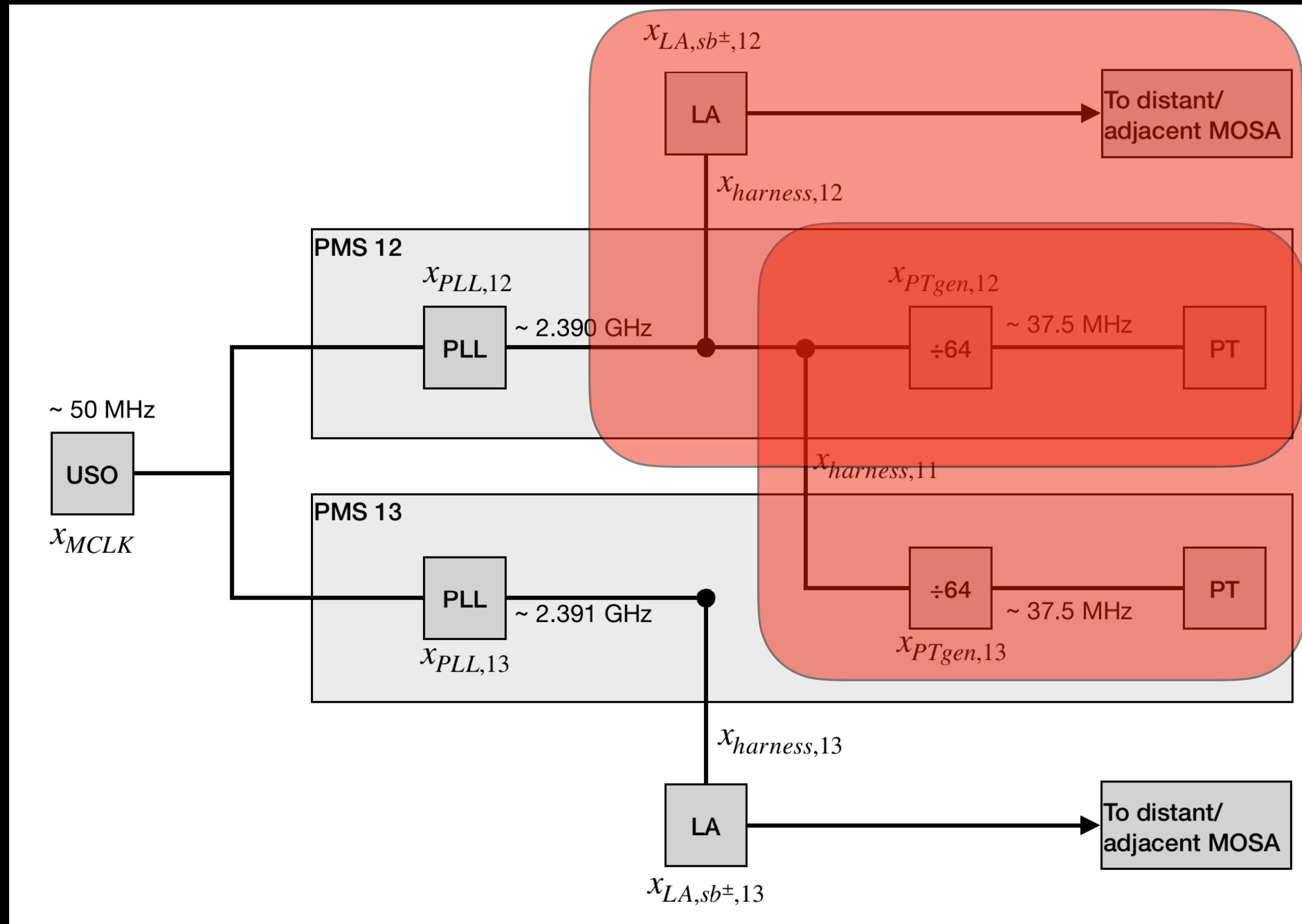


Note: Illustrative, numbers to be seen as placeholders



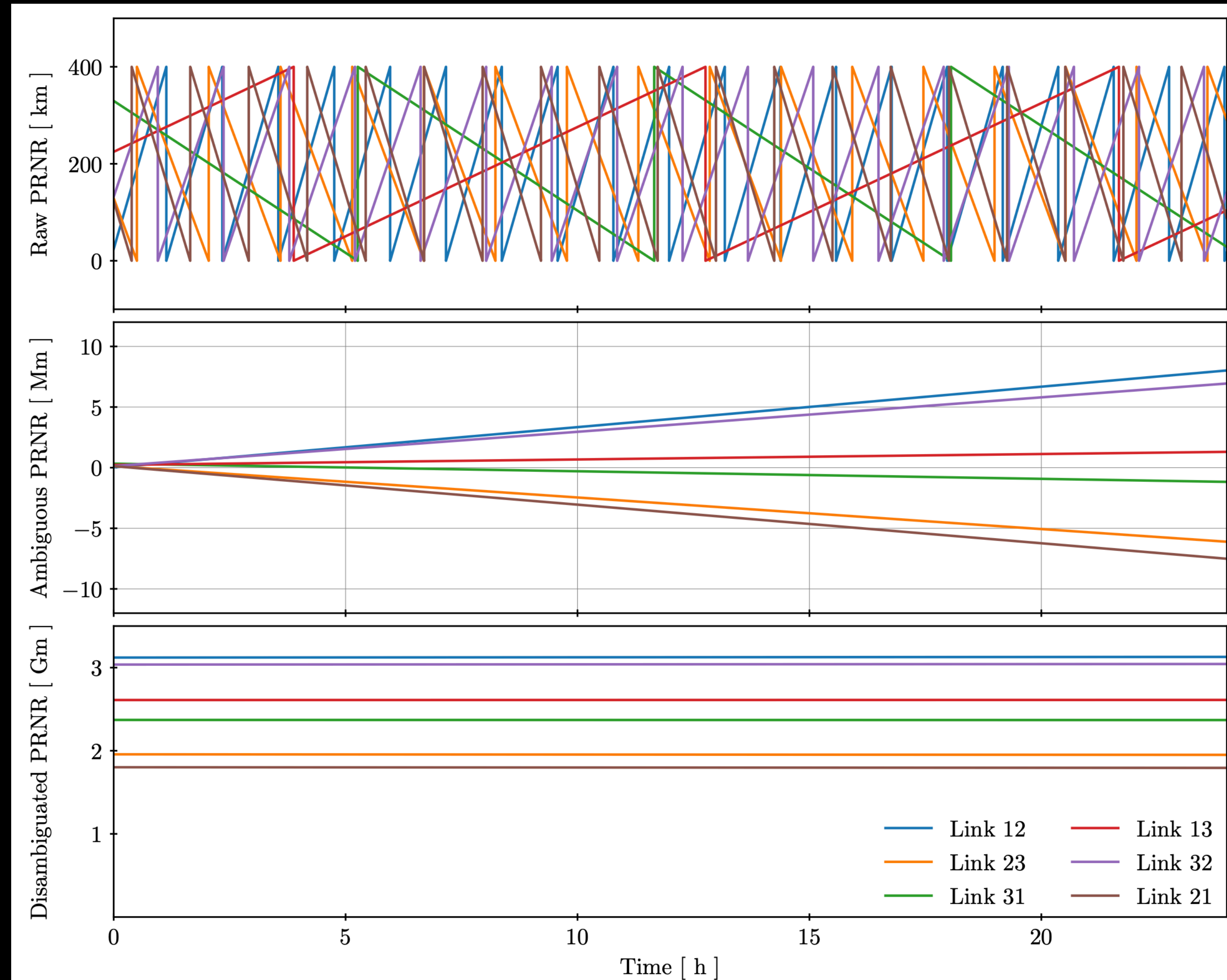
# Frequency distribution system details

- Critical paths (electric):
  - Pilot tone vs. pilot tone
  - Pilot tone vs. **left** laser assembly
- Critical paths must perform (around) the  $40 \text{ fs}/\sqrt{\text{Hz}}$  timing precision mark
- Right handed modulation: Can be corrected using sideband beatnote in RFI



# PRN: processing details

- PRN codes have finite length ( $\approx 400$  km)
- Absolute value and dynamic range of pseudo-range much larger  $\rightarrow$  signal 'wraps' to code length
- First step: un-wrap raw codes, jumps can be detected automatically
- Second step: use ground-based observations (or TDI-R) to find ambiguity/offsets

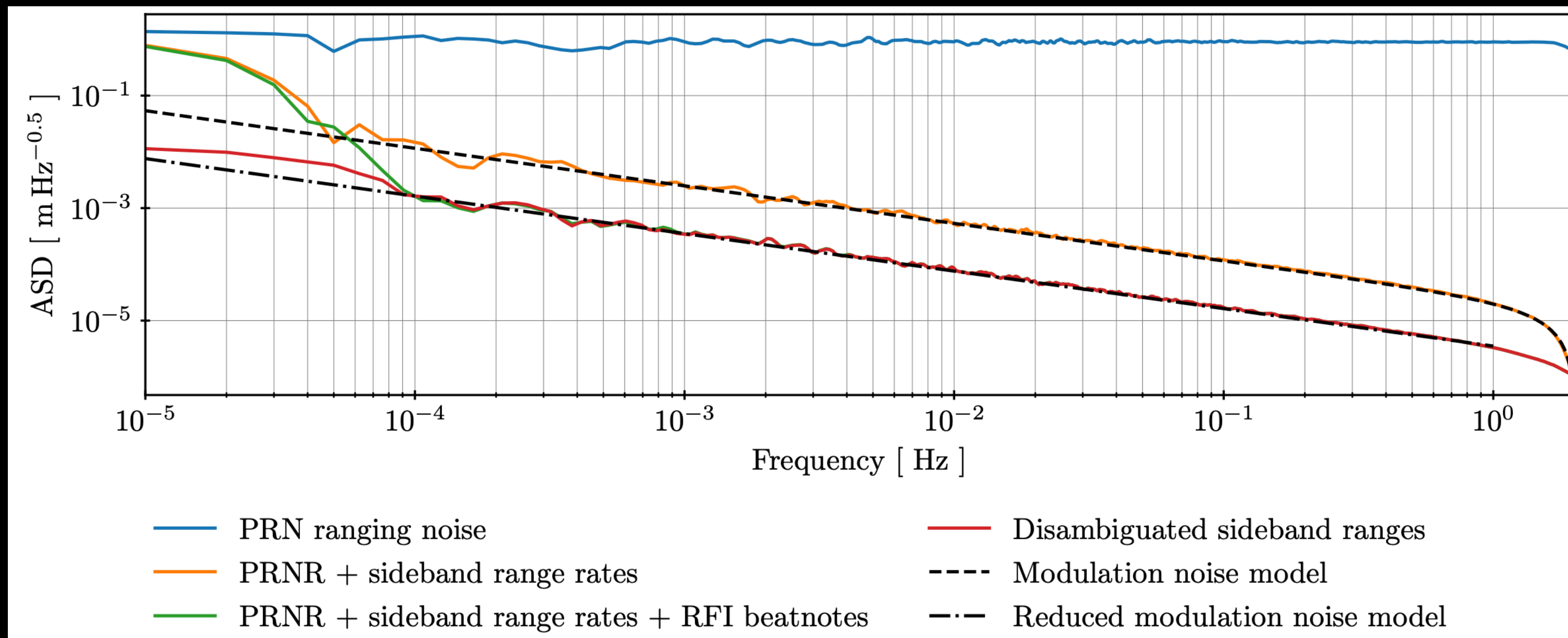


[Reinhard, 2025]



# PRN: processing details

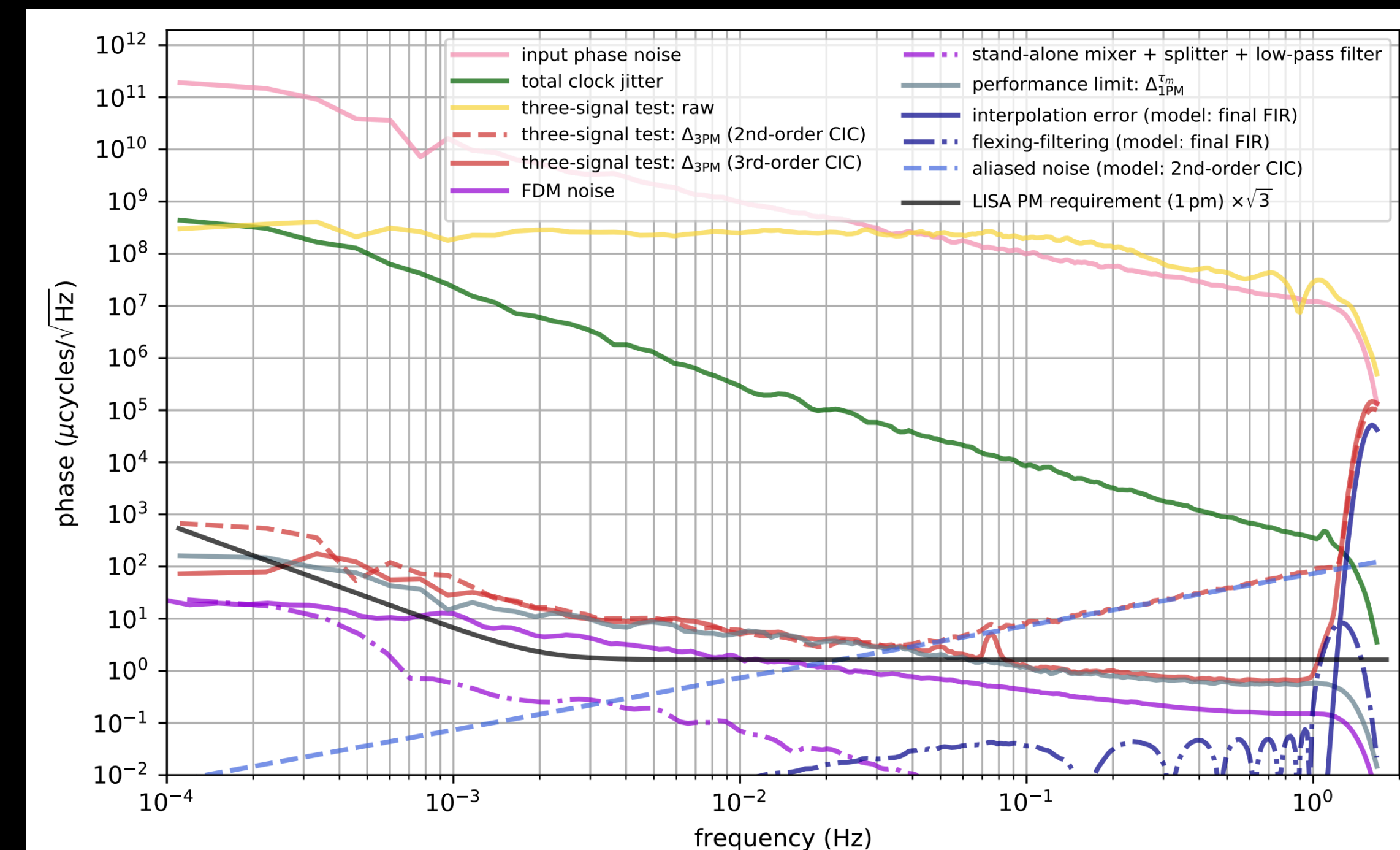
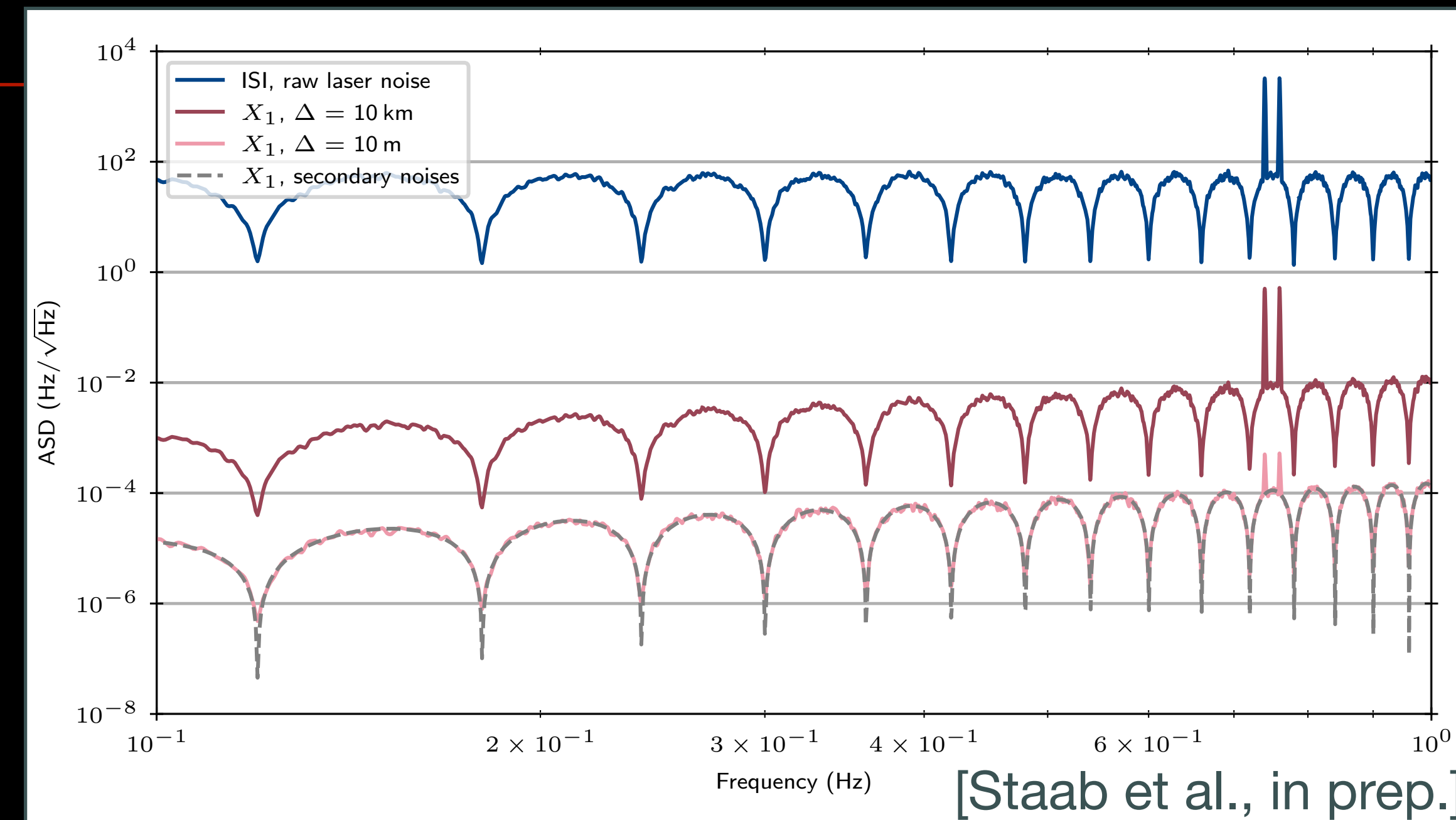
- PRN and sideband fundamentally measure the same quantity: pseudo range
- PRN is absolute, but noisy
- Sideband is precise, but ambiguity even more challenging: 12 cm instead of 400km
- Combined: low-noise, high accuracy pseudo-range measurement



[Reinhard, 2025]

# Alternative/backup to PRN: TDIR

- TDI-ranging (TDI-R): Fit ranging bias by minimizing noise in TDI combination [Tinto et al., 2004]
- Relative clock noise measurements, absolute ranging via PRN and TDI ranging have been demonstrated in hardware demonstrators, e.g., Hexagon experiment [Yamamoto et al., 2022, 2024]

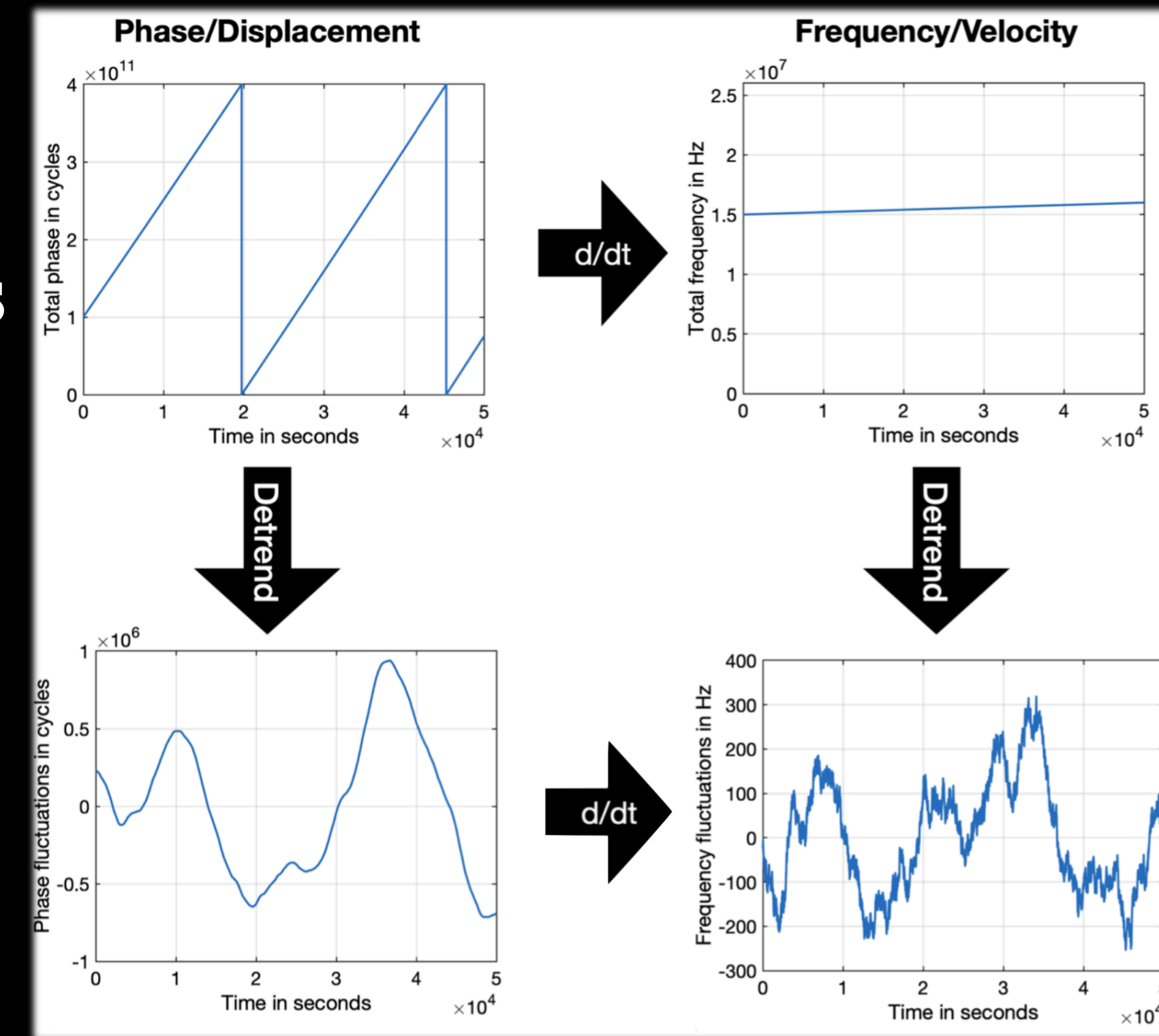


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# Clock noise algorithm

# TDI with or without detrending

- For signals expressed in total phase (or total frequency):
  - Each time shift (Doppler shift) applied in TDI couples to MHz beatnote
  - Previous logic on TDI with unsynchronised clocks directly applies
  - Clock noise correction included in main laser noise reduction step!
- If data is detrended: time shifts applied to residuals
$$\phi(t) \approx -\omega\delta t + \varphi(t - \delta t)$$
  - Time shifts applied to  $\phi$  don't couple to  $\omega$   
 $\implies$  relaxed requirements for laser noise reduction, but time shifts cannot correct for  $\omega\delta t$



# Clock noise with detrending

- With detrending:

$$\eta_{12} = D_{12}\phi_2 - \phi_1 + D_{12}b_{23}q_2 - a_{12}q_1$$

$$\eta_{13} = D_{13}\phi_3 - \phi_1 - (b_{12} + a_{13})q_1$$

- After TDI:

$$\text{TDI} = \sum_{i,j \in I_2} P_{ij} \eta_{ij} \approx \sum_{i,j,k \in I_3^+} [P_{ki} D_{ki} - P_{ik}] b_{ij} q_i - \sum_{i,j \in I_2} P_{ij} a_{ij} q_i$$

- Clock noise terms remain, and need to be removed in an extra processing step, using sideband measurements

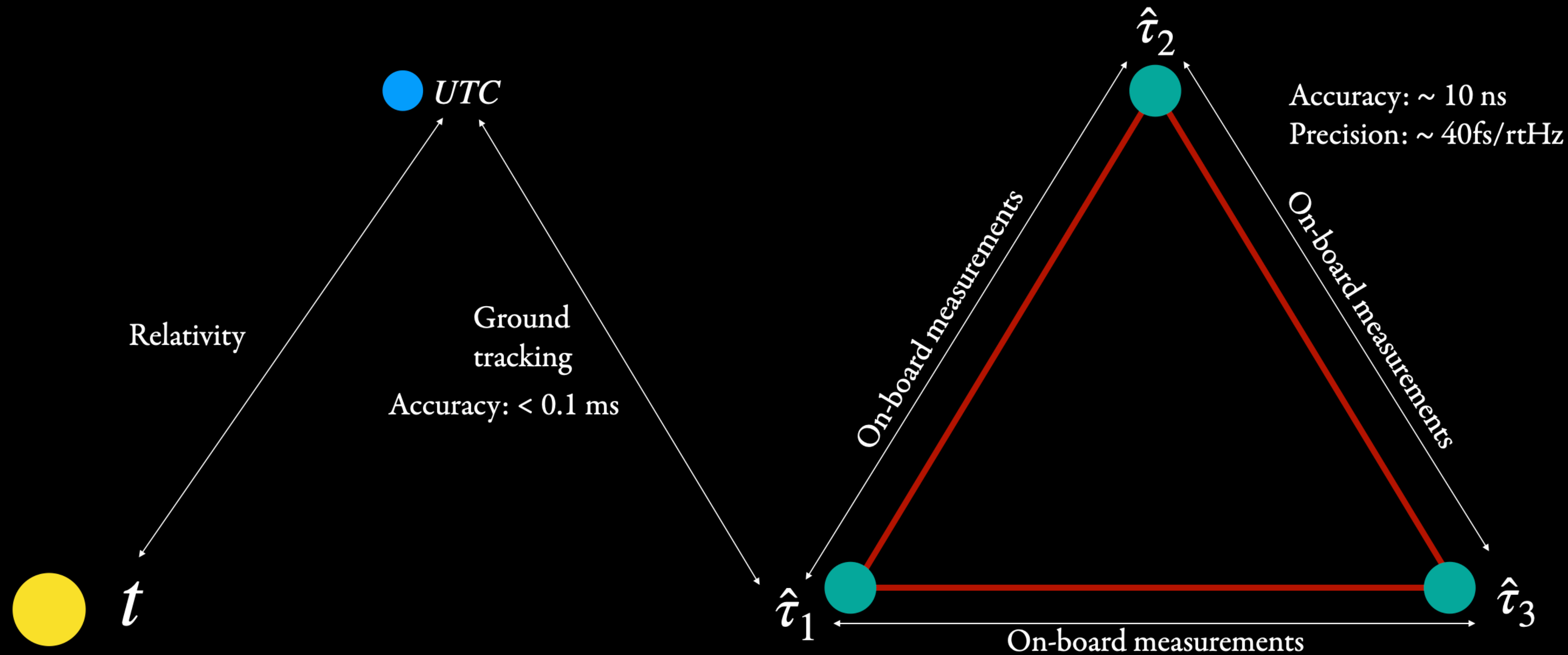
$$r_{ij} = D_{12}q_2 - q_1$$

- Correction non-trivial data combination of  $r_{ij}$ , but can be constructed for any geometric TDI combination



# Clock and time-related issues: summary

Note: Illustrative, numbers to be seen as placeholders



- Inter-SC accuracy: needed for laser noise reduction
- Inter-SC precision: needed for clock noise reduction
- Absolute accuracy wrt. TCB: mostly needed for astrophysical DA

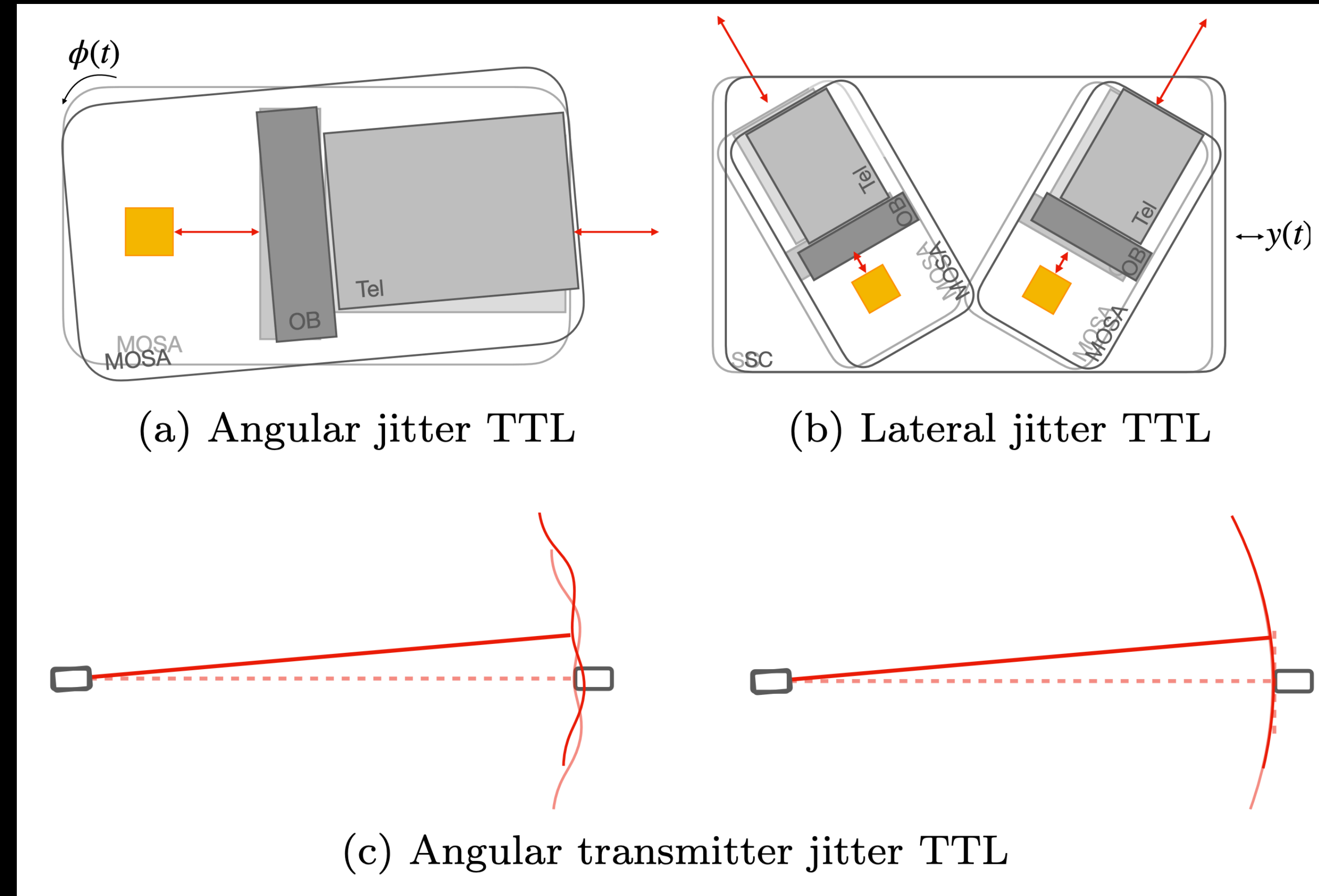


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Angular jitters: Tilt-to-length (TTL) couplings

# TTL coupling

- Tilt-to-length:
- Coupling of other degrees of freedom into desired longitudinal TM-TM measurement
- Typical origins:
  - Optical element misalignment
  - Wavefront errors
- Some compensation in hardware, but expected impact of TTL exceeds requirements

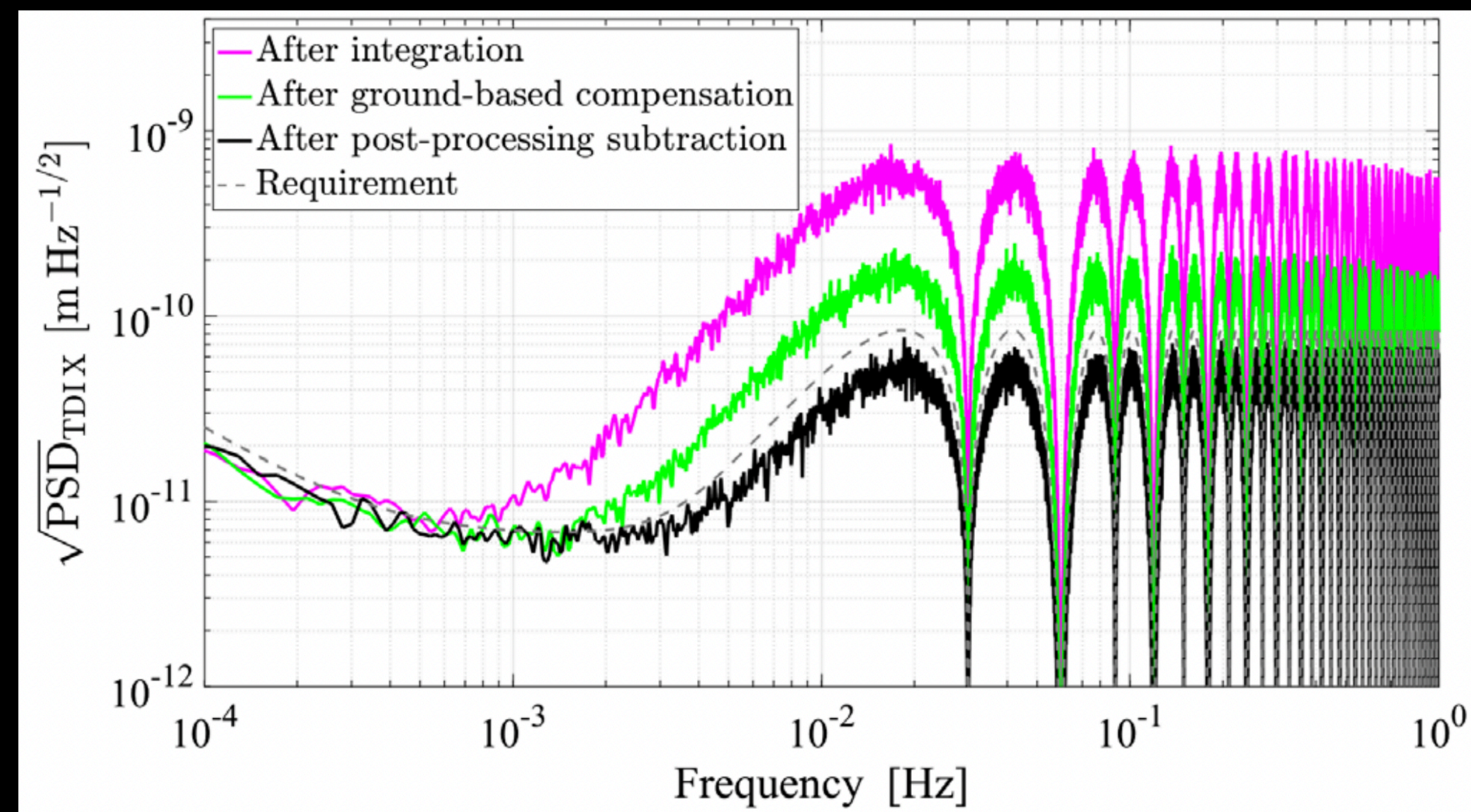
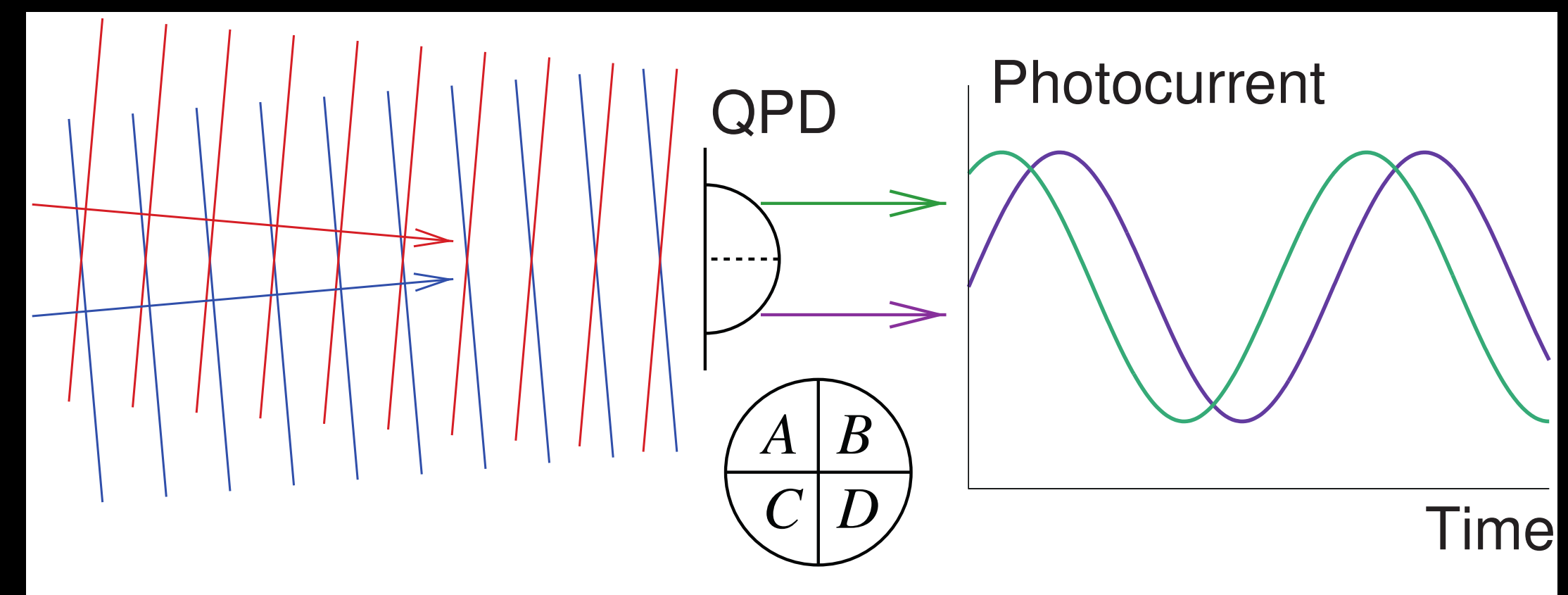




# TTL compensation

Details: Paczkowski et al. 10.1103/PhysRevD.106.042005

- Differential wavefront sensing (DWS) allows to measure angular tilts of 2 beams by combining outputs of a quadrant photodiode
- TTL subtraction:
  - Assume linear model with a set of 24 coefficients relating tilt angles to pathlength changes
  - TTL coefficients are not known sufficiently well a-priori to subtract jitters
  - Fit DWS measurement coupling factors by minimizing the noise



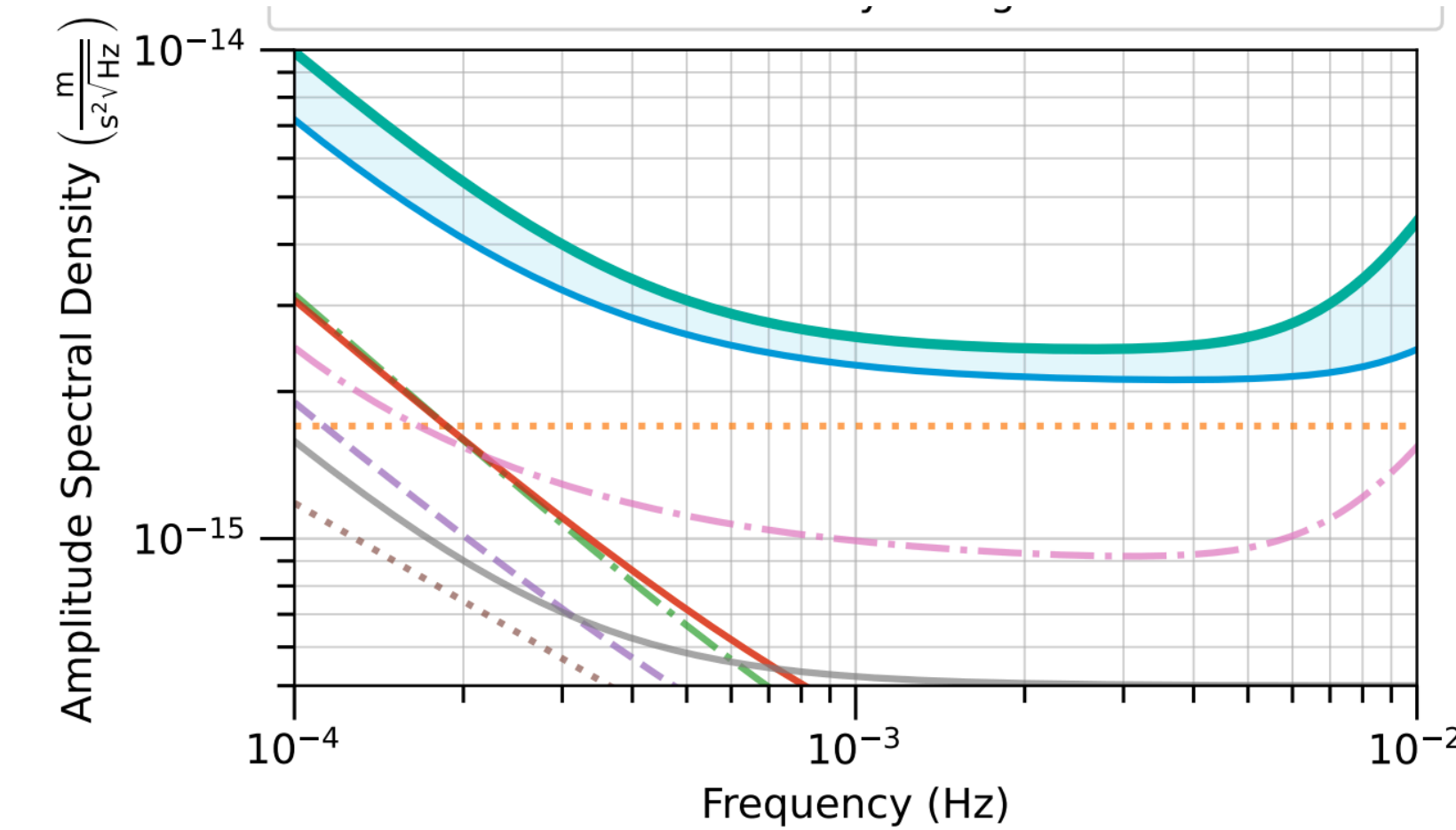
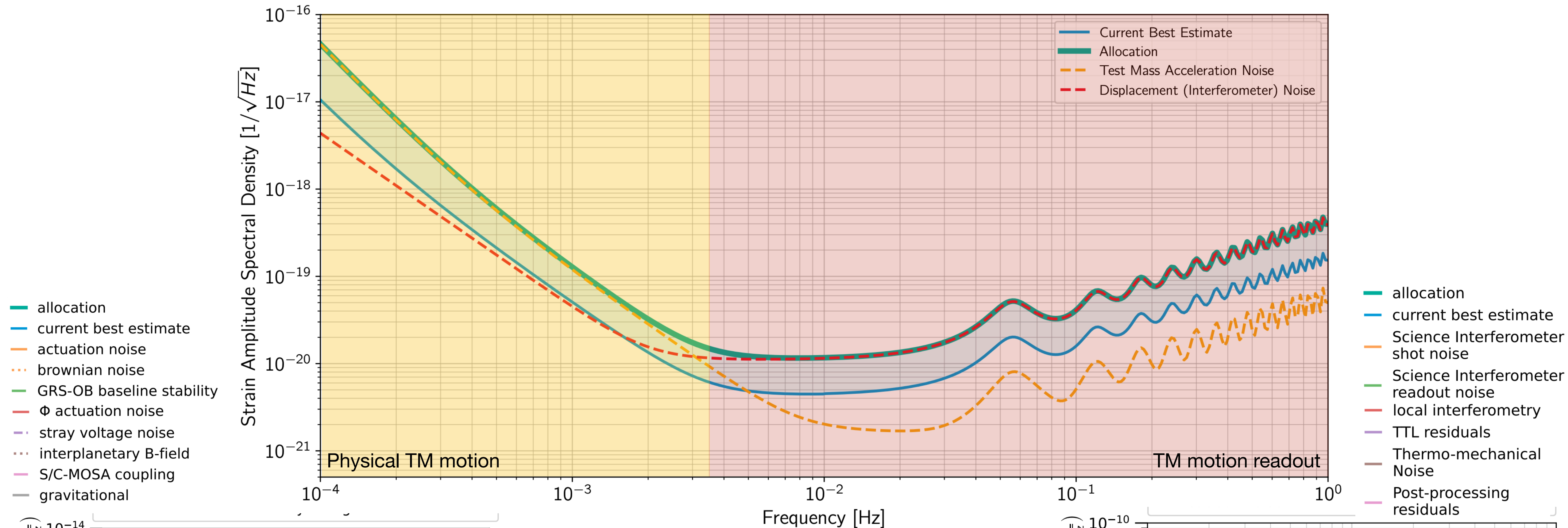
▸ Assumes requirement noise level (flat at high frequency)

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# LISA Performance and Sensitivity

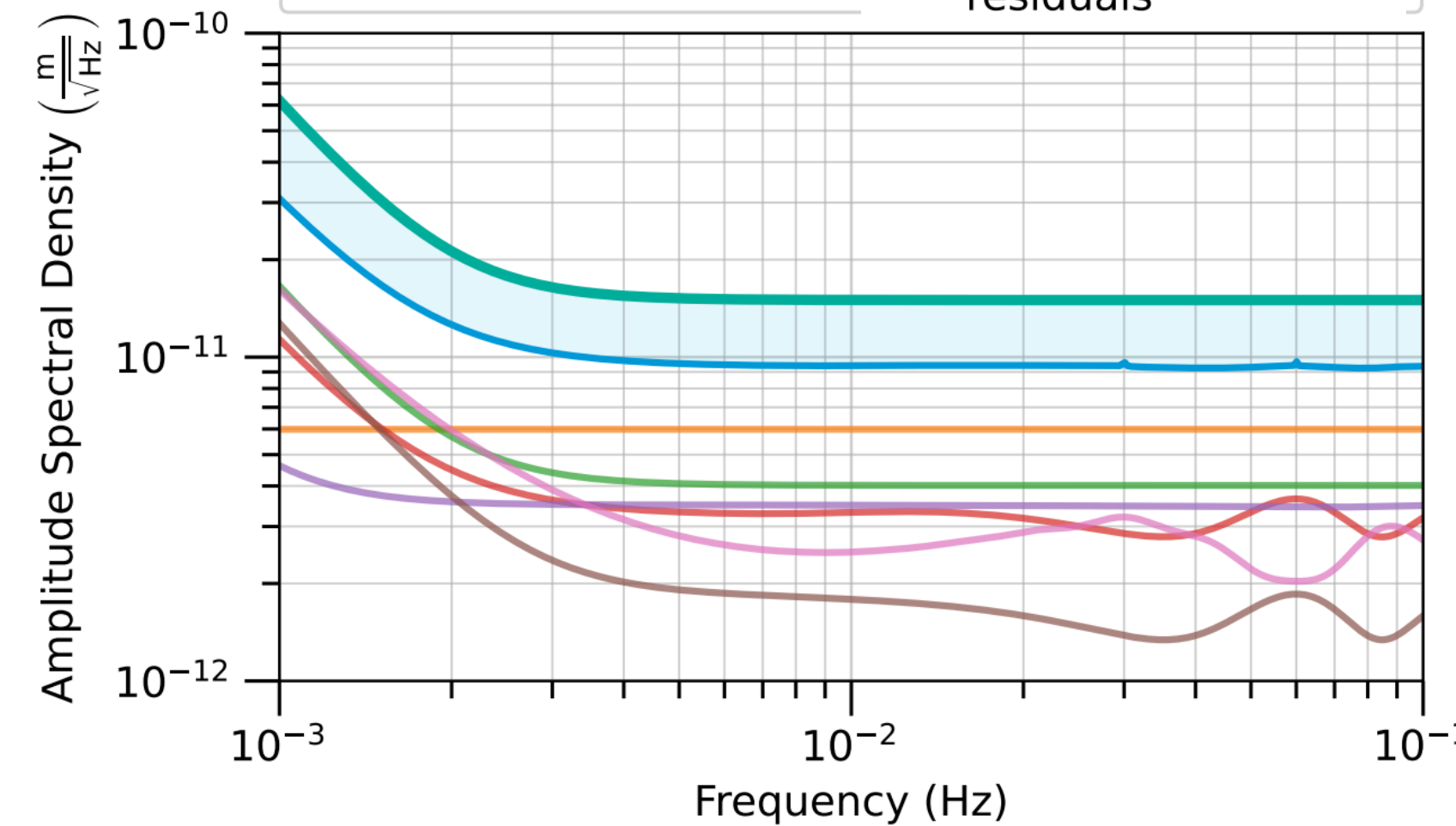


# Main limiting noise sources left after TDI



$$S_h(f) \approx \frac{T_{acc}^X S_{acc}^X + T_{oms}^X S_{oms}^X}{2 R_{GW}^X}$$

!!!



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Thank you for your attention!