Inter-run stability 13590 / 13535

Runs characteristics

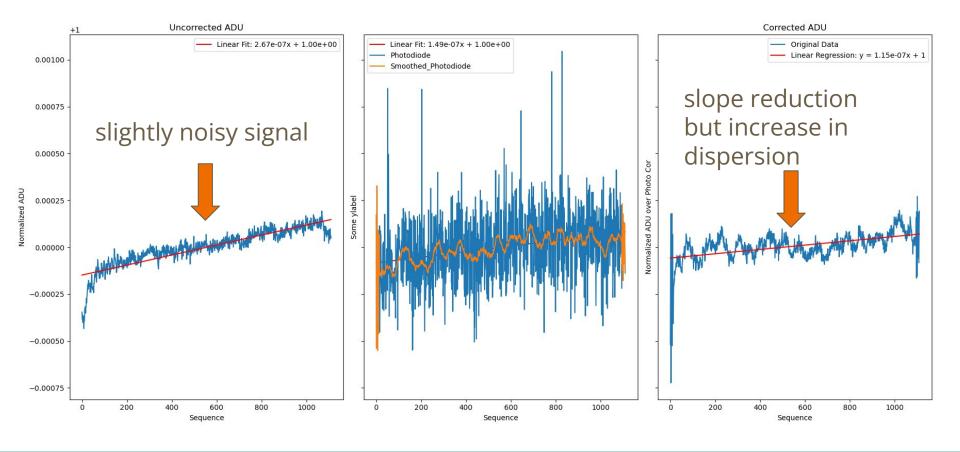
Similarities:

- Stability flat
- CCOB LED: 750 nm
- ~ a day of observations
- more than 1000 obs
- ADU ~ 15000
- ilt configuration

Differences:

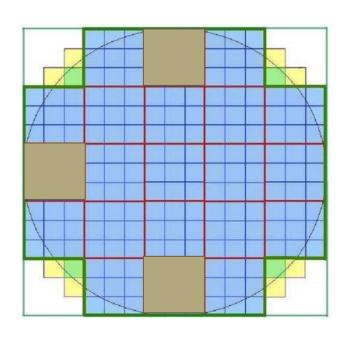
- separated by ~ 2 weeks
- e2v configuration

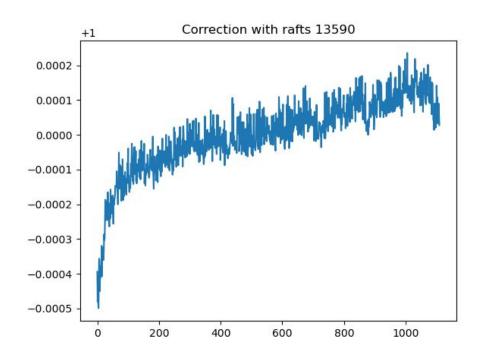
First ADU correction: exemple 13590



Correction 2 : correction by itl

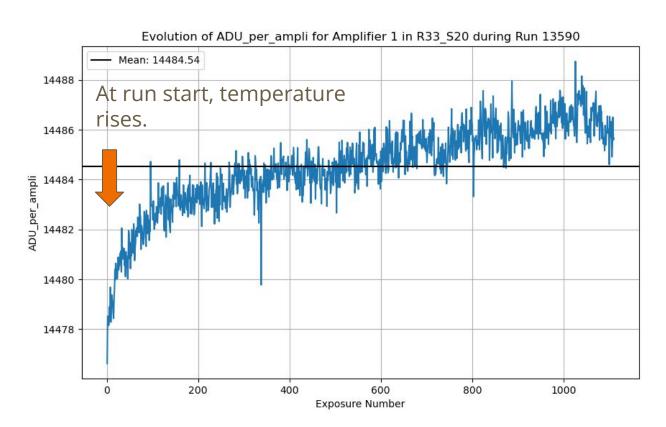
correction rafts = ['R02', 'R20', 'R42'] removing common temp/flux modes





Median ADU across the run for an ampli

This study ignores start/end run effects, focusing on in-run stability.

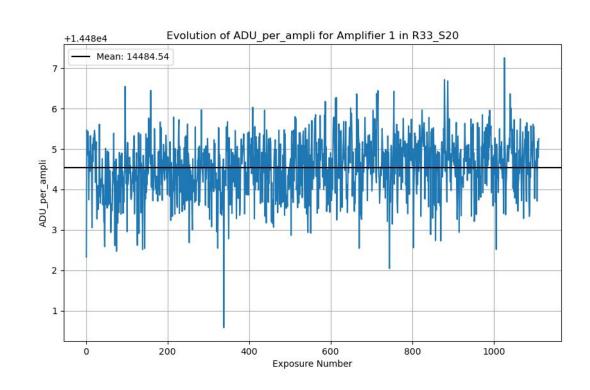


Median ADU corrected by itl rafts

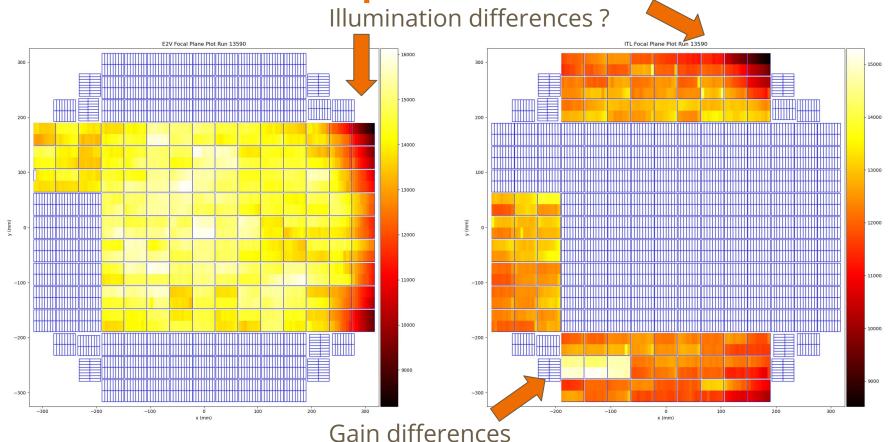
After ITL raft correction:

Deviation ~ 2*10-4 during the run

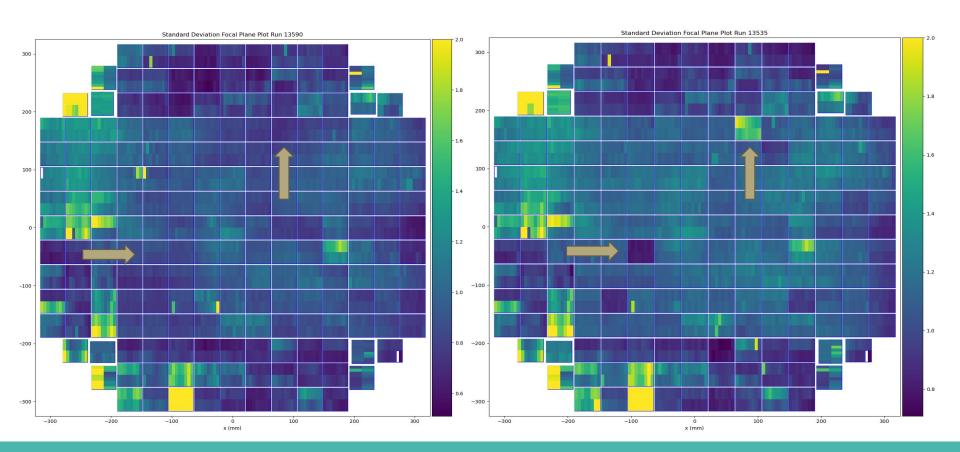
The slope is no longer visible



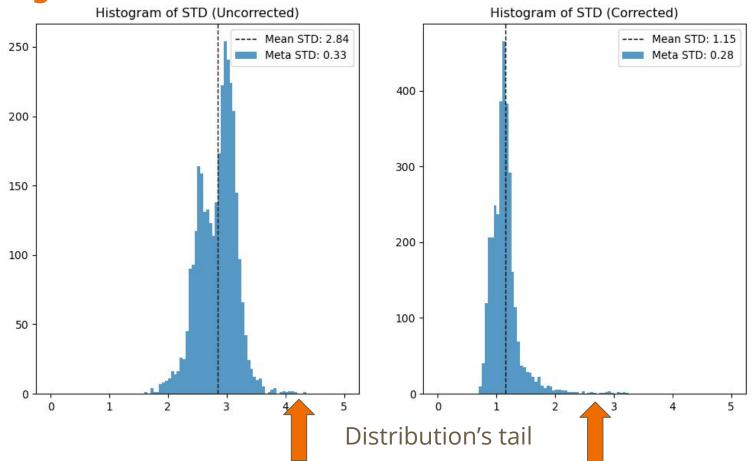
Corrected ADU on focal plane



Focal plane std: 13590 and 13535

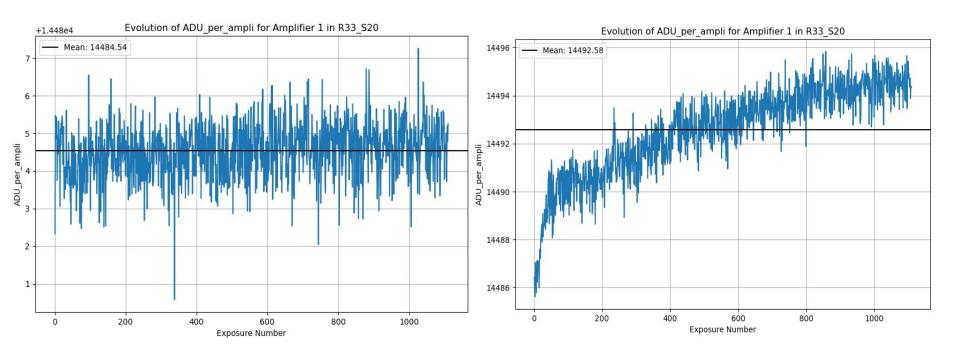


Histogram of standard deviations



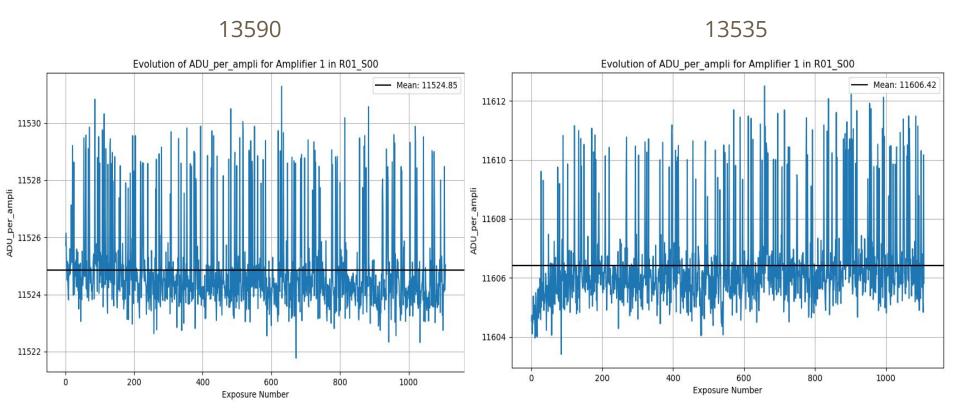
R33_S02

13590 13535



			C	orre	lation	With	in CCD	R33	S20	for R	lun: 1	13590					- 1.0					C	Correl	ation \	Within	CCD	R33_S	20 for	Run:	1353	5				10
1.00	0.70	0.56						0.4								0.52	2.0	-	1.00	0.96	0.94													0.91	1.0
0.70	1.00	0.70						0.4		15 0.						0.53		7	- 0.96	1.00	0.95													0.91	
0.56	0.70	1.00	0.71	0.59						18 0.		0.52	0.57			0.54	- 0.9	m	- 0.94		1.00	0.95												0.91	- 0.9
		0.71	1.00	0.73	0.56	0.5						0.54	0.58			0.48		4	- 0.93			1.00	0.94	0.90										0.90	
		0.59	0.73	1.00	0.72	0.5	7 0.50									0.51		10	- 0.92			0.94	1.00	0.93	0.90									0.91	
				0.72	1.00	0.7	0.53	0.5								0.50	- 0.8	9	- 0.90					1.00	0.92									0.89	- 0.8
							0.68																		_										
							8 1.00											ampli 8																	
																	- 0.7	mn 6																	- 0.7
								_					-					10																	
																		=======================================																	
										-				_	_		- 0.6	12																	- 0.6
											10000							12																	
							1 0.49 9 0.47										- 0.5															_	_	0.92	- 0.5
0.53																1.00		51																1.00	
i	2	3	4	5	6	7		9			,	12		-	-			H	i 0.91		3	4	5	6	7	8	9					14			
				orre	lation	Betv	num veen Co	_ampl		ift: R3	33 &	Run:	1359	0									orrel	ation I	Betwe	num_ en CC		Raft:	R33 8	€ Run	: 135	35			
200			0.49		0.57		0.44	0.4		0.38		0.48		0.41		.45	1.0		005			0.75			0.7		0.51			0.5				0.73	1.0
R33_S00	1.0	,,,	0.49		0.57		3.44	0.4	2	0.50	•	0.48				.45			R33 S00		00	0.75		0.78	0.7	3	0.51		.67	0.5	55	0.73		0.73	
R33_S01	0.4	19	1.00	ı	0.48						0					.33	- 0.9		R33 S01	- 0.	75		3	0.74	0.6	5		c	.61	0.5	50	0.67		0.67	- 0.9
R33_S02	0.5	57	0.48								1					.44	- 0.8		R33 S02	- 0.	78	0.74		1.00	0.7	0	0.48	c	.64	0.5	54	0.71		0.72	- 0.8
									_								0.0																		0.0
R33_S10		14					1.00	0.6	2	0.57	7				0	.46			R33 510	- 0.	73	0.65		0.70	1.0	0	0.68	C	.75	0.5	52	0.72		0.71	
																	- 0.7																		- 0.7
ccd R33_S11		12				(0.62	1.0	0	0.54	4	0.47				.41			ccd R33 511	'ı - 0.	51			0.48	0.6	8	1.00	C	.60	0.4	2	0.55		0.54	
R33_S12	0.3	88	0.30			(0.57	0.5	4	1.00	0				0	.43	- 0.6		R33 512		67	0.61		0.64	0.7	5	0.60	1	00	0.4	17	0.66		0.65	- 0.6
R33_S20	0.4	18					0.46	0.4	7	0.4	1	1.00		0.57	0	.54	- 0.5		R33 520		55	0.50		0.54	0.5	2	0.42	C	.47	1.0	00	0.62		0.70	- 0.5
_S21 R3																																			
R33		1				(0.36				9	0.57		1.00	0	.52	- 0.4		R33 521	0.	73	0.67		0.71	0.7	2	0.55	C	.66	0.6	52	1.00		0.80	- 0.4
R33_S22		15									3	0.54		0.52	1.	.00			R33 522	- 0.	73	0.67		0.72	0.7	1	0.54	C	.65	0.7	0	0.80		1.00	
	022	500	933 50	1 B	33 502	83	3_510	R33 9	11	B33 S	:12	B33 53	20 B	33 521	B33	522				B22	coo	B33 60	1 83	22 502	R33	510 5	222 61	1 023	612	D22	520	P22 6	01 B	22 522	

R01_S00



			Co	rrelation '	Within CCI	0 R01_S0	0 for Run:	13590			1.0			Co	rrelation \	Within CCE	R01_50	0 for Run:	13535			1.0
	rd - 1.00					2 0.80				0.90 0.91	1.0	ed = 1.00					0.51	0.54 0.90				1.0
	∾ - 0.95	1.00 0.95				2 0.80				0.91 0.90		∾ - 0.95	1.00 0.9				0.53	0.53 0.90				
	m = 0.93	0.95 1.00	0.95			2 0.79				0.90 0.89	- 0.8	m = 0.92	0.96 1.0	0 0.95			0.53	0.52 0.89				- 0.8
	4 - 0.91		5 1.00	0.93 0.92		1 0.81				0.88 0.89		4 - 0.91	0.92 0.9	5 1.00	0.94 0.92		0.53	0.52 0.90				
The component of the	in - 0.90		0.93	1.00 0.93	0.90 0.9					0.88 0.88	- 0.6	in - 0.90		1 0.94	1.00 0.93		0.54	0.50 0.89				- 0.6
	φ - 0.93			0.93 1.00		3 0.80				0.89 0.89		ω - 0.93			0.93 1.00		0.53	0.52 0.91				
Section Process Proc	r - 0.93				1.00 0.9	6 0.82				0.89 0.90		► - 0.93				1.00 0.96	0.51	0.55 0.91				
9 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	E.					_					- 0.4	ild ω - 0.92	0.93 0.9	2 0.91	0.90 0.93	0.96 1.00	0.50	0.56 0.90	0.87 0.8	7 0.88	0.90 0.89	- 0.4
## 0.89 0.89 0.89 0.89 0.80 0.80 0.80 0.80	-					_	_					g 6 - 0.51	0.53 0.5	3 0.53	0.54 0.53	0.51 0.50	1.00	0.31 0.51	0.49 0.5	1 0.48	0.49 0.47	
Part						_					- 0.2							_		_		- 0.2
## Correlation Between CCDs for Raft: R01 & Run: 13590 **Correlat						_	_											_				
## - 0.85									_		-00							_		-		- 0.0
27 - 050 031 030 038 038 038 038 038 039 030 030 031 032 032 031 030 032 032 031 030 039 030 030 03 047 050 033 031 02 033 100 033 038 039 030 030 030 030 030 030 030 030 030	ന്ന - 0.86							0.90 1.0	0 0.91	0.85 0.85	-0.0	g - 0.87					0.51	0.52 0.87	0.90 1.0	0.91		- 0.0
9 011 050 050 050 050 050 050 050 050 050																				_		
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 Correlation Between CCDs for Art. RO1 & Run: 13590 10 0 002 0.11 0.01 0.05 0.00 0.00 0.09 0.04 10 0 007 0.14 0.02 0.00 0.08 0.04 0.04 0.01 10 0 007 0.14 0.02 0.00 0.08 0.04 0.04 0.01 10 0 007 0.14 0.02 0.00 0.08 0.04 0.04 0.01 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0									_		0.2	ध्र - 0.90					0.49	0.57 0.89		7 0.92	1.00 0.93	0.2
Correlation Between CCDs for Raft: R01 & Run: 13590																						
1.0	1	2 3			nur	n_ampli				15 16		1	2 3			num	n_ampli				15 16	
Color Colo	8		Со	rrelation l	Between C	CDs for F	Raft: R01 8	k Run: 13!	590		1.0	8		Co	rrelation E	Between C	CDs for F	Raft: R01 8	Run: 135	35		1.0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		1.00	0.02	0.11	0.01	0.05	0.00	0.00	0.09	0.04					0.14	0.02	-0.00	0.08			0.01	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	R01_S01	0.02										5										- 0.8
B G P 0.05 0.13 0.07 0.29 1.00 0.35 0.10 0.64 0.19					0.68		0.50	0.57		0.38	- 0.8			1.00	-0.18	0.73	0.30	0.55		0.33	0.59	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	R01_S02	0.11										S02 R01										- 0.6
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	R01		-0.21	1.00	-0.10	0.07	0.24	-0.23	0.18	0.24	- 0.6	S10 R01_S02 R01_	0.14	-0.18	1.00	0.01	0.15	0.29		0.23	0.32	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R01_S10 R01	0.01	-0.21	1.00	-0.10	0.07	0.24	-0.23	0.18	0.24	- 0.6	cd - 511 R01_510 R01_502 R01_	0.14	-0.18	0.01	0.01	0.15	0.29	-0.05	0.23	0.32	
$ \begin{bmatrix} \frac{1}{2} \\ \frac{1}{2} \end{bmatrix} = 0.09 0.07 0.18 0.25 0.64 0.31 0.04 1.00 0.29 $ $ \begin{bmatrix} \frac{1}{2} \\ \frac{1}{2} \end{bmatrix} = 0.04 0.38 0.24 0.40 0.19 0.38 0.35 0.29 1.00 $ $ \begin{bmatrix} \frac{1}{2} \\ \frac{1}{2} \end{bmatrix} = 0.01 0.59 0.32 0.60 0.45 0.59 0.67 0.58 1.00 $ $ \begin{bmatrix} \frac{1}{2} \\ \frac{1}{2} \end{bmatrix} = 0.04 0.38 0.24 0.40 0.19 0.38 0.35 0.29 1.00 $	ccd S12 R01_S11 R01_S10 R01.	0.01	-0.21 0.68	1.00 -0.10 0.07	-0.10 1.00 -0.29	-0.29	0.24	-0.23 0.60 -0.10	0.18 -0.25 0.64	0.24	- 0.6 - 0.4	ccd ccd R01_S10 R01_S02 R01	0.14	-0.18 0.73	0.01	0.01	0.15	0.29	-0.05 0.71	0.23	0.32 0.60 0.45	- 0.4
$\frac{\widetilde{S}}{2}$ 0.04 0.38 0.24 0.40 0.19 0.38 0.35 0.29 1.00 $\frac{\widetilde{S}}{2}$ 0.01 0.59 0.32 0.60 0.45 0.59 0.67 0.58 1.00	ccd ccd siz RO1_S10 RO1	0.01	-0.21 0.68 -0.13	1.00 -0.10 0.07	-0.10 1.00 -0.29	0.07	0.24	-0.23 0.60 -0.10	0.18 -0.25 0.64 -0.31	0.24	- 0.6 - 0.4 - 0.2	ccd cc3. 101 510 F01.502 F01.	0.14	0.73 0.30	0.01 0.15	0.01	0.15	0.29	0.71 0.28	0.23 0.13 0.73	0.32 0.60 0.45	- 0.4 - 0.2
	ccd CCd 1520 R01_512 R01_510 R01	0.01	-0.21 0.68 -0.13 0.50	1.00 -0.10 0.07 0.24	-0.10 1.00 -0.29 0.79	0.07 -0.29 1.00 -0.35	0.24 0.79 -0.35 1.00	-0.23 0.60 -0.10 0.46	0.18 -0.25 0.64 -0.31	0.24 0.40 0.19 0.38	- 0.6 - 0.4 - 0.2	221 RO1,502 RO1,021 RO1,021 RO1,022 RO1,031 RO	0.14 0.02 -0.00 0.08	0.73 0.30 0.55	0.01 0.15 0.29	0.01 1.00 0.06 0.83	0.15 0.06 1.00 -0.03	0.29 0.83 -0.03	0.71 0.28 0.63	0.23 0.13 0.73 0.04	0.32 0.60 0.45 0.59	- 0.4 - 0.2 - 0.0
ccd ccd	ccd Szz ROJ _S ZS ROJ _S ZS ROJ _S SIZ ROJ _S SIO ROJ	0.01	-0.21 0.68 -0.13 0.50 0.57	1.00 -0.10 0.07 0.24 -0.23	-0.10 1.00 -0.29 0.79 0.60	0.07 -0.29 1.00 -0.35 -0.10	0.24 0.79 -0.35 1.00 0.46	-0.23 0.60 -0.10 0.46 1.00	0.18 -0.25 0.64 -0.31 -0.04	0.24 0.40 0.19 0.38 0.35	- 0.6 - 0.4 - 0.2	000 205,100 012,100 112,100 212,100 052,100 112,100 212,	0.14 0.02 -0.00 0.08 -0.04	0.73 0.30 0.55 0.69	0.01 0.15 0.29 -0.05	0.01 1.00 0.06 0.83 0.71	0.15 0.06 1.00 -0.03 0.28	0.29 0.83 -0.03 1.00 0.63	0.71 0.28 0.63 1.00	0.23 0.13 0.73 0.04 0.37	0.32 0.60 0.45 0.59 0.67	- 0.4 - 0.2 - 0.0

13590 on 13535

13590 appears more stable than **13535**

There are several points remaining to be studied

