

Development of simulation tools to realize an active Thomson Parabola

ARNAUD HUBER

Mehdi TARISIEN (LP2IB), Didier RAFFESTIN (CELIA)



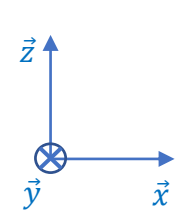
I. Thomson Parabola ? Active ?

II. Simulation tools

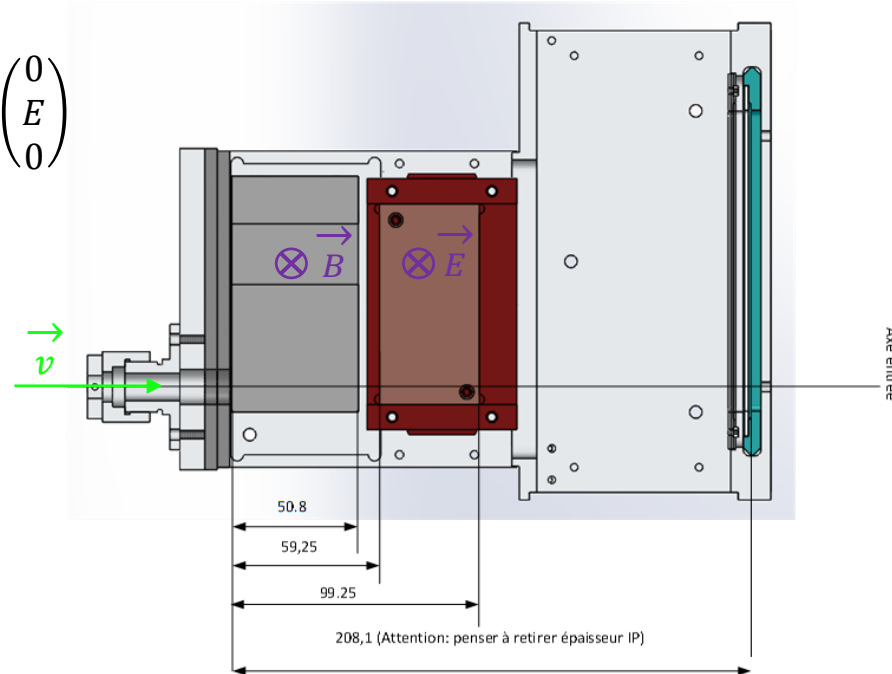
1. EM simulation
2. Optical simulation
3. Fibers simulation

III. New design of TP

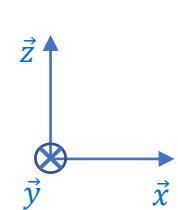
- **Thomson Parabola (TP)** = Parallel magnetic & electrical field with **Imaging Plates (IPs)** for the detection
- Used for **qualitative & quantitative detection** of particules created in a plasma by a laser shot
- Very efficient to **discriminate ions but ...**



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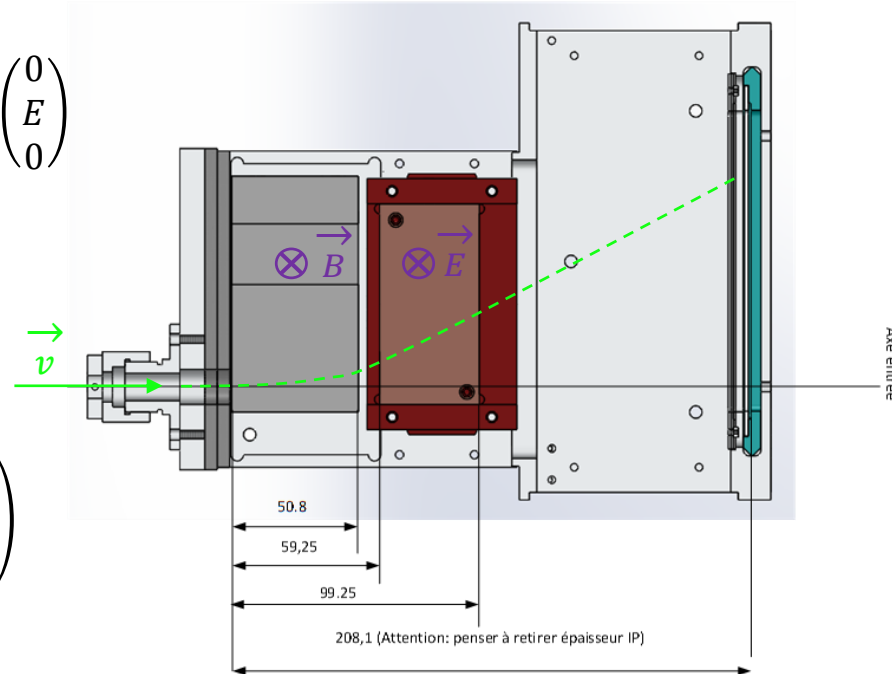
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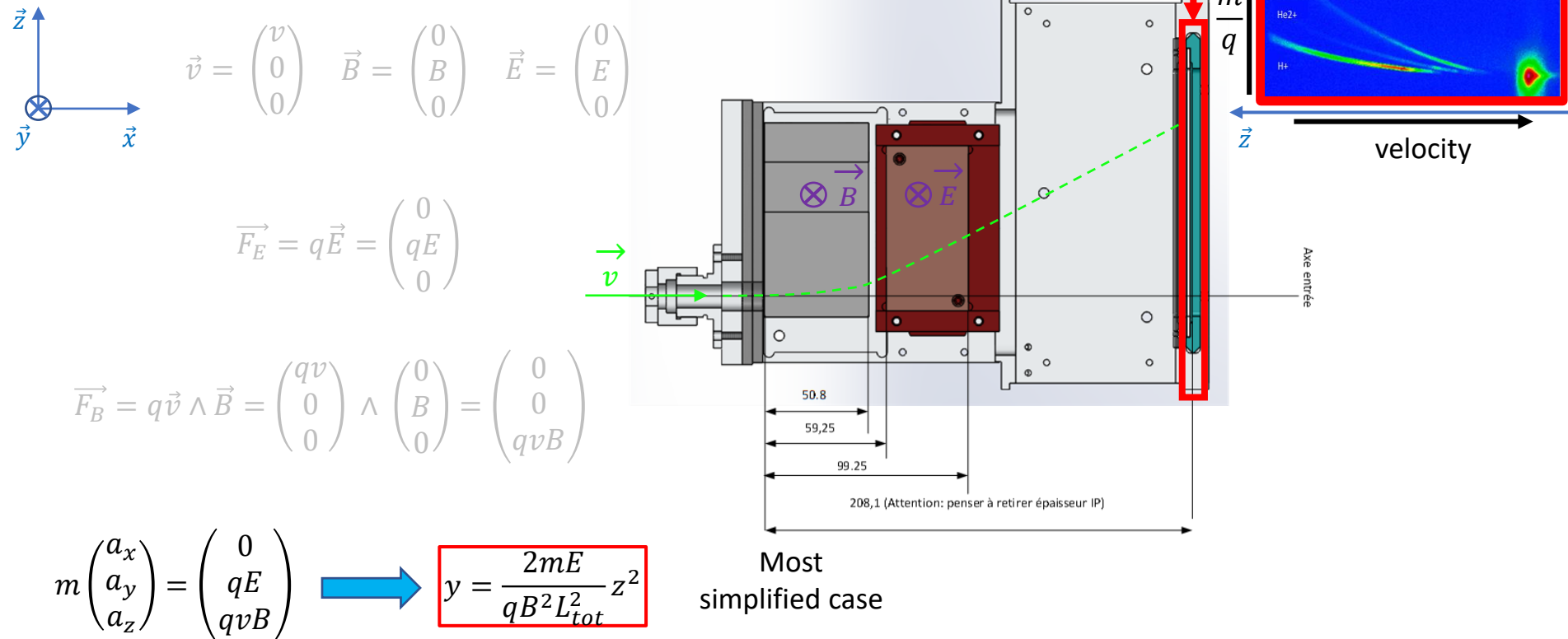
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$$\vec{F}_E = q\vec{E} = \begin{pmatrix} 0 \\ qE \\ 0 \end{pmatrix}$$

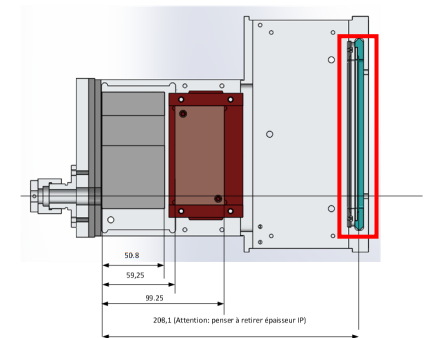
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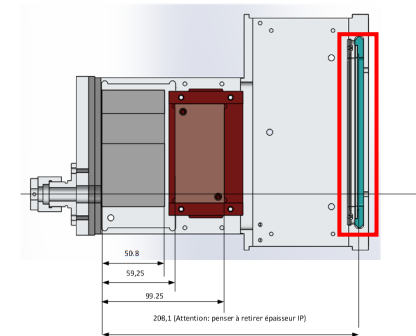
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- ... must be **read after the shot**
- Not possible to use IPs at **high laser repetition rates**
- **Realization of an Active Thomson Parabola** (RATP project with GPR Light)
- 2 detection scenarii to be tested :
 - Combination of **scintillators** imaged with **cameras (CCD, CMOS)**
 - **CMOS detector** directly in focal plan of TP

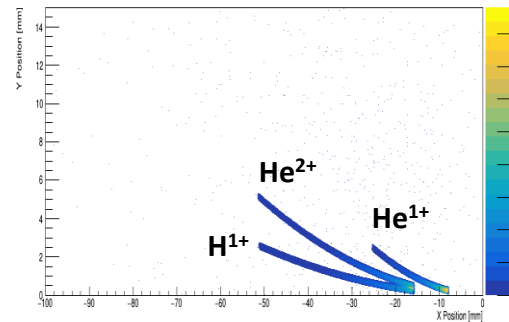


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- Some questions to answer :
 - **What is the « perfect configuration » for a given experiment ?**
 - **What is the impact of the differents TP parameters ?**
 - **Is the light produced in the scintillator sufficient to be detected ?**
 - **Can we use the system in the experimental chamber (EMP, X flash) ?**



- Simulation of TP with GEANT4 software
 - EM part for tracking and energy deposition in detector
 - Optical part for tracking and detection of the scintillation (choice to activate or not)
 - Simulation of p^+ , He^{1+} & He^{2+}

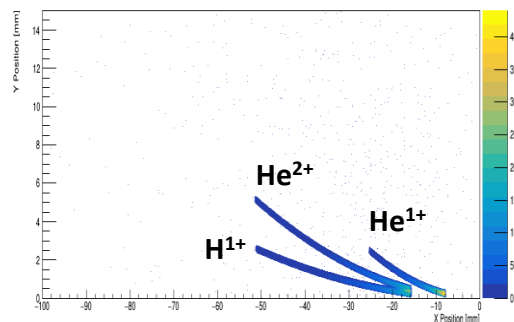
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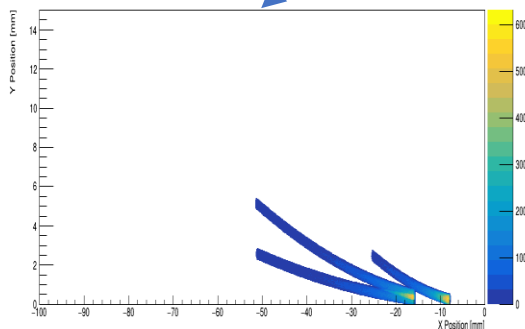
$r_{pinhole} = 0.1$ mm
 B value = 0.6 T
 E value = 630000 V/m
Magnet Length = 50 mm
Ecart plates $D = 0$ mm
Electric length = 40 mm
Distance plate/detector = 175 mm
 $L_{tot} = 265$ mm
Sc length = 200 mm
Sc thickness = 0 mm
ZnS thickness = 0 mm
Optique ? : No

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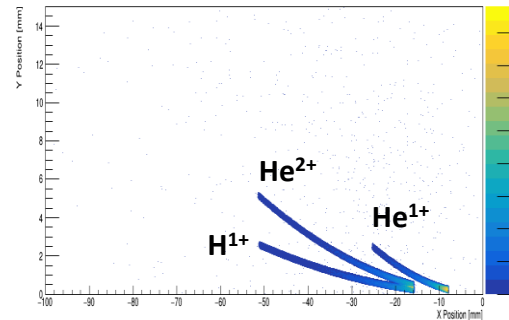
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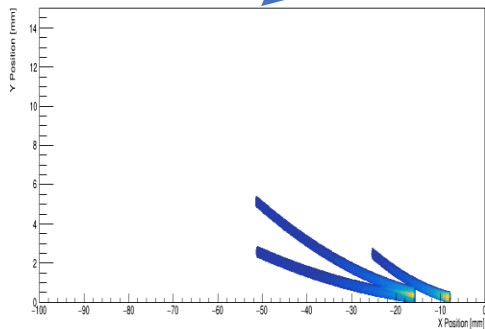


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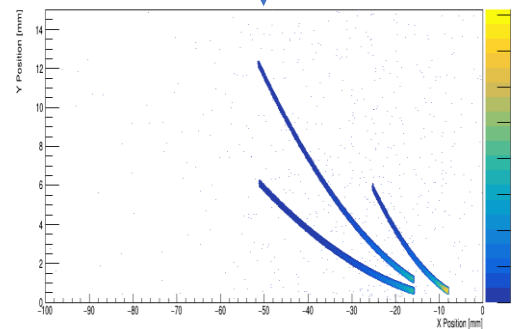
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Entrance pinhole variation

E field variation

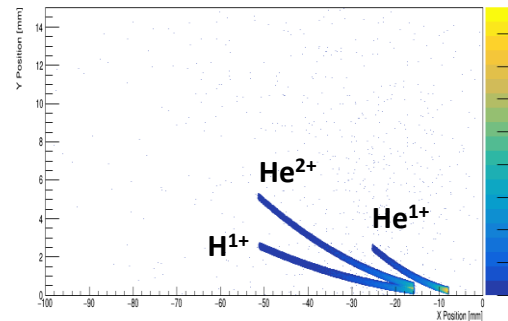


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$E \text{ field} = 1500 \text{ kV/m}$

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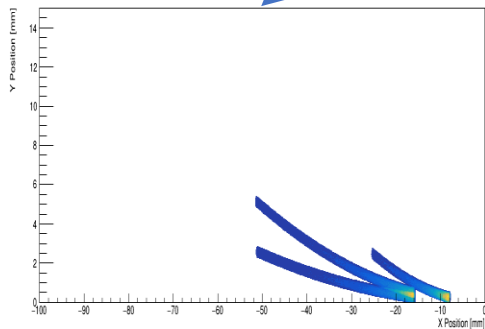
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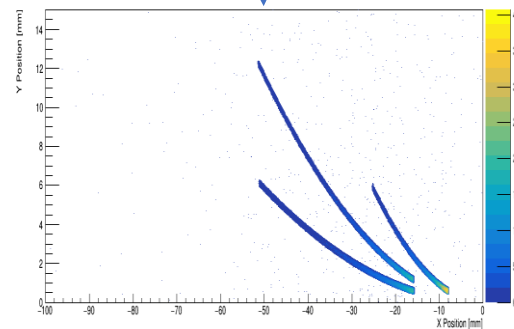
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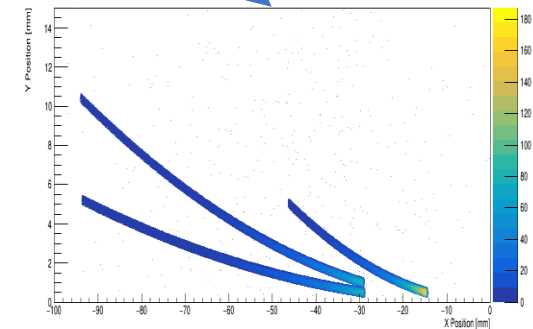
E Field/focal plan distance variation



$r_{\text{pinhole}} = 1.0 \text{ mm}$



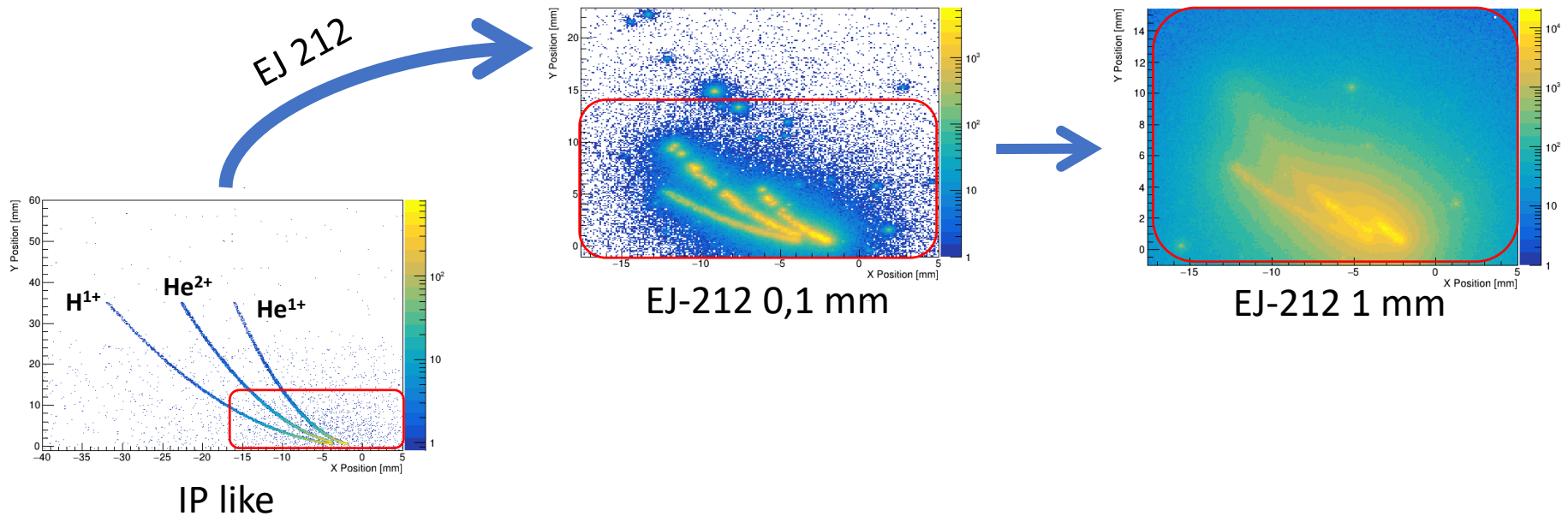
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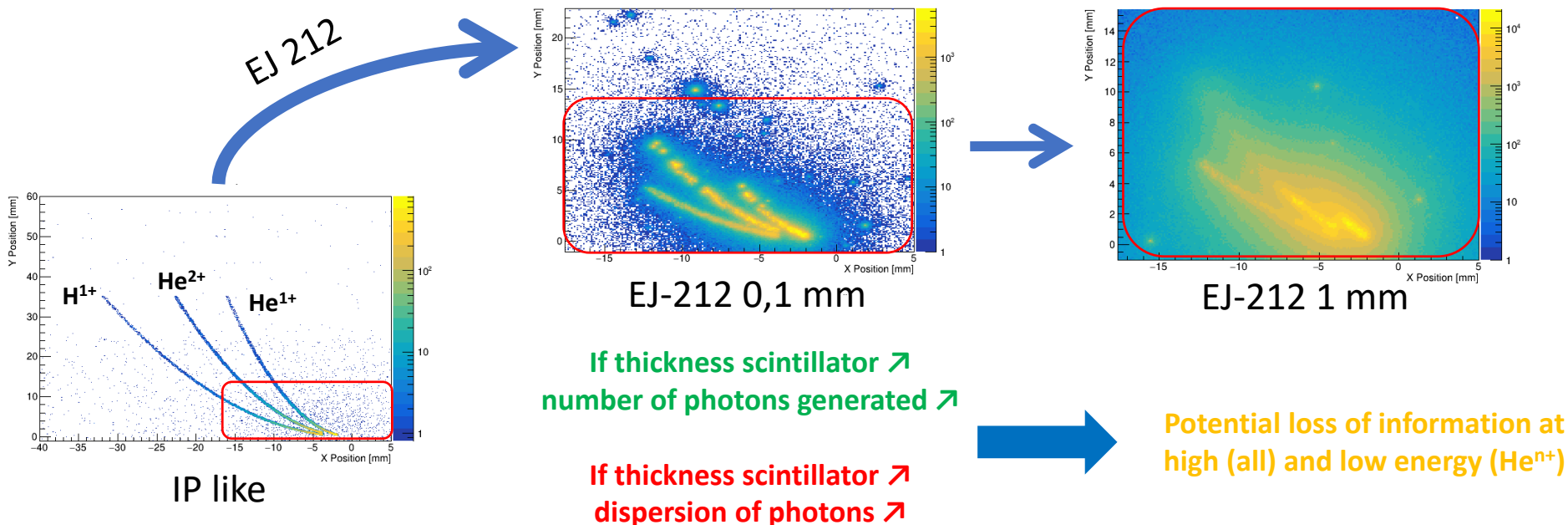
$\text{Distance } E_f/\text{det} = 140 \text{ cm}$

- First study (Jan 22 -> May 22) with a scintillator in focal plan :
 - **Estimate if a CCD/CMOS camera directly in contact is possible**

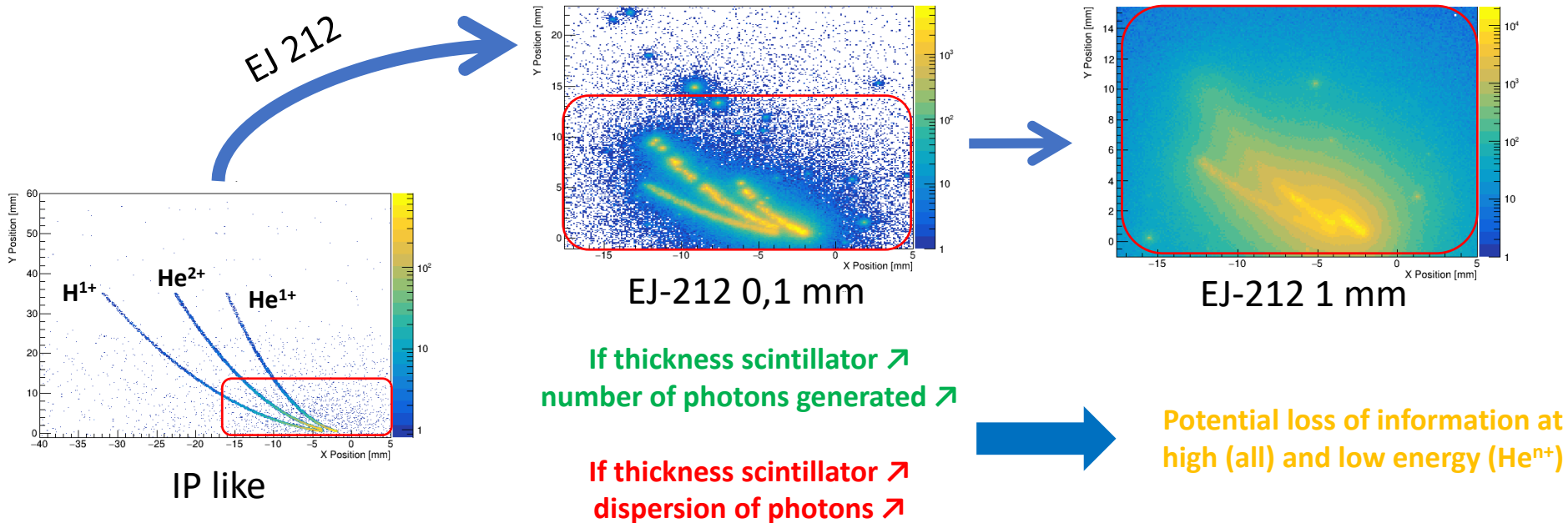
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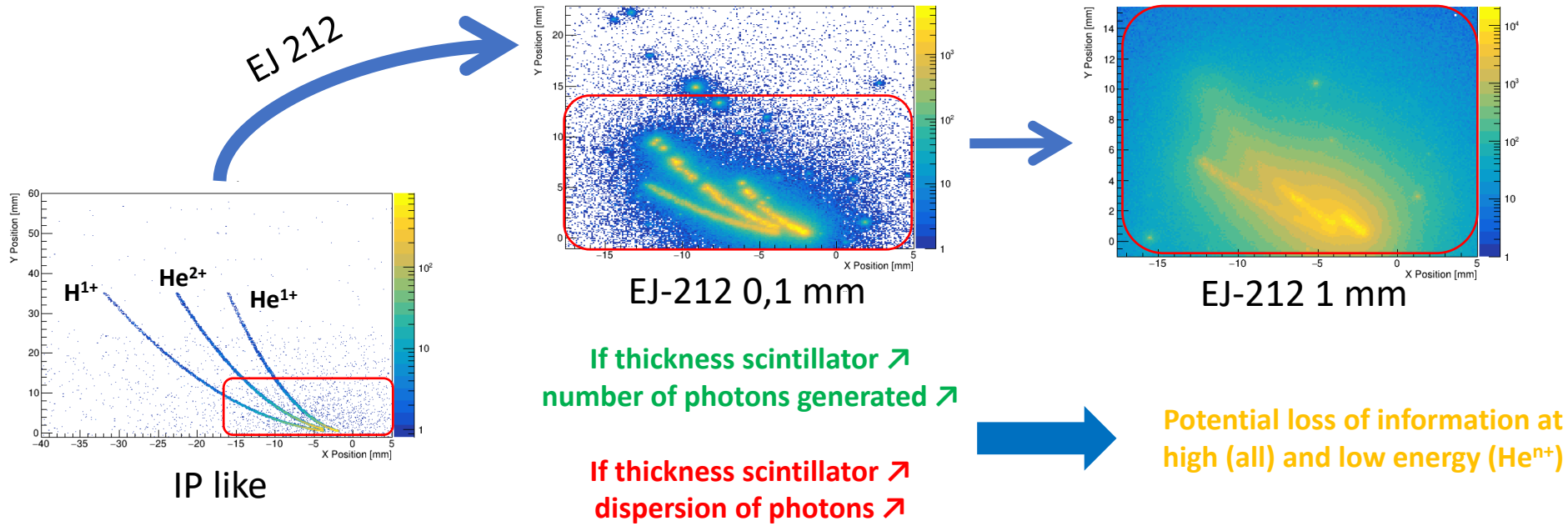


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 - ⚠ Needs more investigations for optimization (additional energy from primary particle)
 - ⚠ Difficult to have a CCD/CMOS Camera with a large Field Of View (FOV)
 - ⚠ Potential problem with EMP

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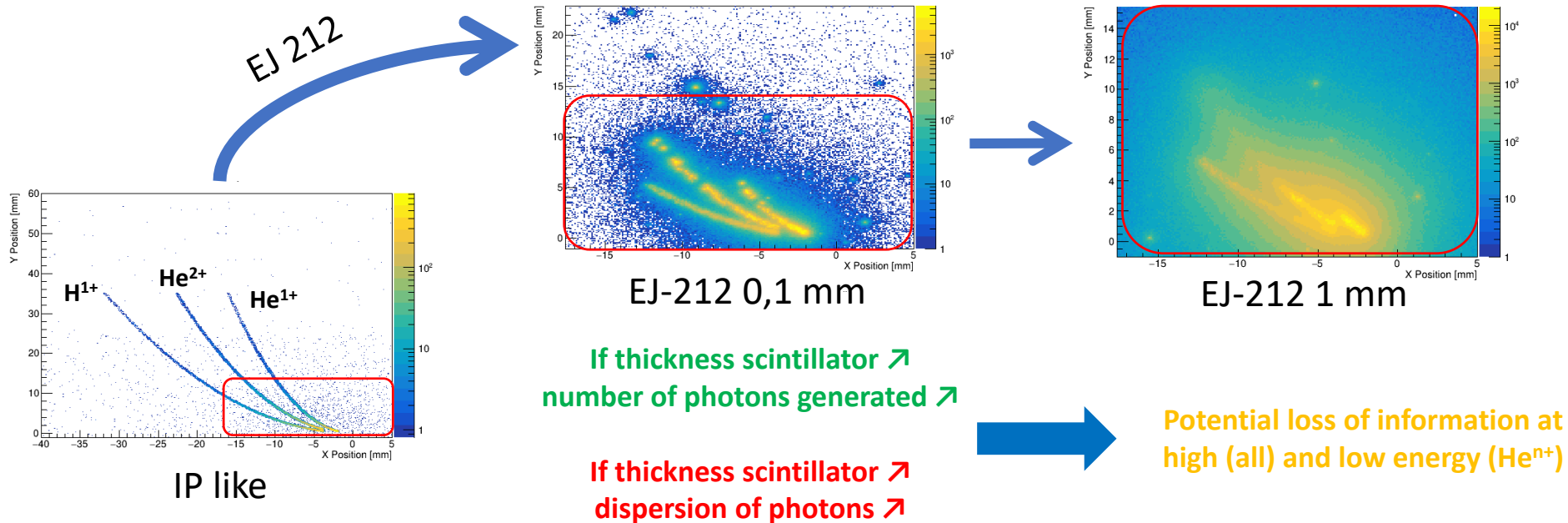


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Simulation of optical device (lenses combination) -> To Do

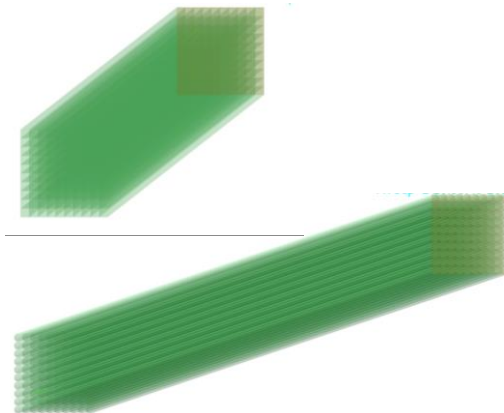
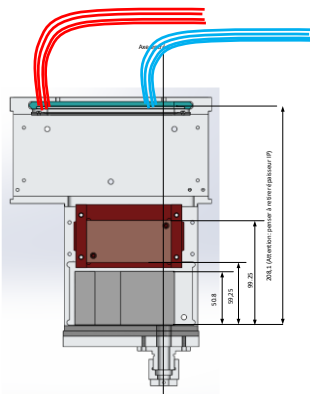
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 - 💡 *Simulation of optical device (lenses combination) -> To Do*
 - 💡 *Simulation of fibers bunch*

Simulation tools-Fibers

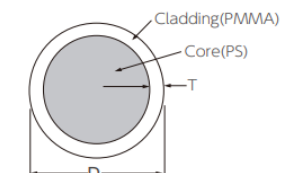
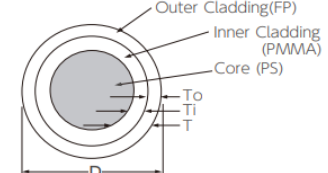
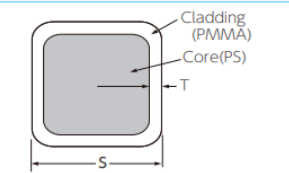
- Optical fiber simulation based on **Kuraray geometries** (LIQUIDO's fibers manufacturer)
- Try with **parameterization** for the bunch generation on the code
- Not conclusive -> loop generation**
- Detector at the end of bunch
- Code automation with a config file
- Very long time of simulation !!!**
 - 3,5 MeV proton on TP with optical photon tracking on fibers = **704s/event**
 - Necessary to improve !!!**



Materials

	Materials	Refractive index	Density (g/cm ³)	No. of atom per cm ³
Core	Polystyrene(PS)	$n_0=1.59$	1.05	C: 4.9×10^{22} H: 4.9×10^{22}
Cladding	for single cladding inner for multi-cladding	Polymethylmethacrylate (PMMA)	$n_0=1.49$	C: 3.6×10^{22} H: 5.7×10^{22} O: 1.4×10^{22}
	outer for multi-cladding	Fluorinated polymer (FP)	$n_0=1.42$	

Cross-section and Cladding Thickness

	Single Cladding	Multi-Cladding (M)
Round Fiber (D)	 Cladding Thickness¹⁾: $T=2\%$ of D Numerical Aperture: $NA=0.55$ Trapping Efficiency : 3.1%	 Cladding Thickness²⁾: $T=2\%(To)+2\%(Ti)$ $=4\%$ of D Numerical Aperture : $NA=0.72$ Trapping Efficiency : 5.4%
Square Fiber (SQ)	 Cladding Thickness : $T=2\%$ of S Numerical Aperture : $NA=0.55$ Trapping Efficiency : 4.2%	Not available

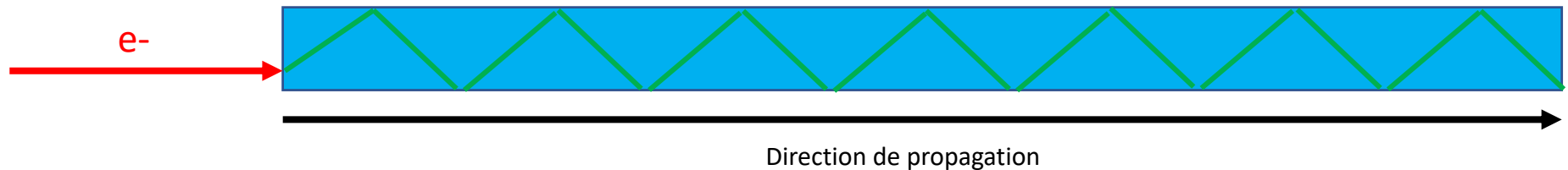
1) In some cases cladding thickness T is 3% of D 2) In some cases cladding thickness T is 6% of D To and Ti are both 3% of D

```

37
38 #Fibers
39 Fiber_geometry 0 #0=round & 1=square
40 Fiber_multi_cladding 0 #0 or 1 to activate
41 Fiber_number_per_line 5
42 Fiber_space 0.001 mm
43 Fiber_width 1 mm
44 Fiber_cladding_ratio 0.02
45 Fiber_length 1. m
46
    
```

Assumptions for a fast optical transport simulation

- Best way is to let **GEANT4** doing all the calculations
- **Most CPU consumption** is coming from the **optical photon tracking**
- Need to take care of several aspects : generation, reflections and absorption.

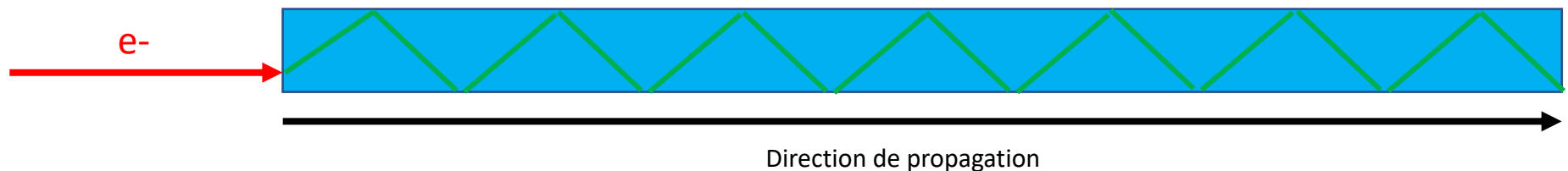


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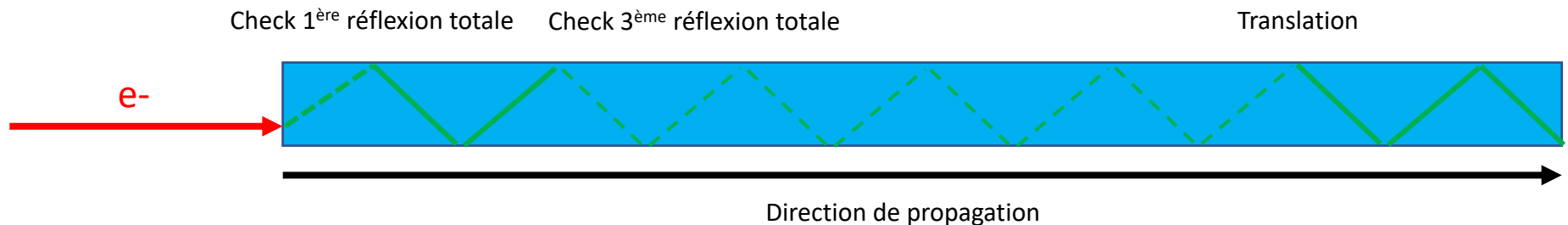
Assumptions from fiber characteristics

- An optical photon trapped inside the fiber will do multiple internal reflections up to be detected or absorbed.
- The angle of a photon at the interface of the fiber will remain the same during all the transport.
- Surface of core and cladding are perfectly polished.



Idea of an algorithm for a fast optical photon transportation

- All the intermediates steps are not necessary for the simulation
- It's sufficient to know that an optical photon made some total internal reflections
- Probability of absorption can be calculated separately for each photon
- Possible to go to a fast photon transportation according to :
 - 1. FastSim algorithm activation if we have 2 internal total reflections
 - 2. Estimation of the final position according to the tracking
 - 3. Absorption check after translation
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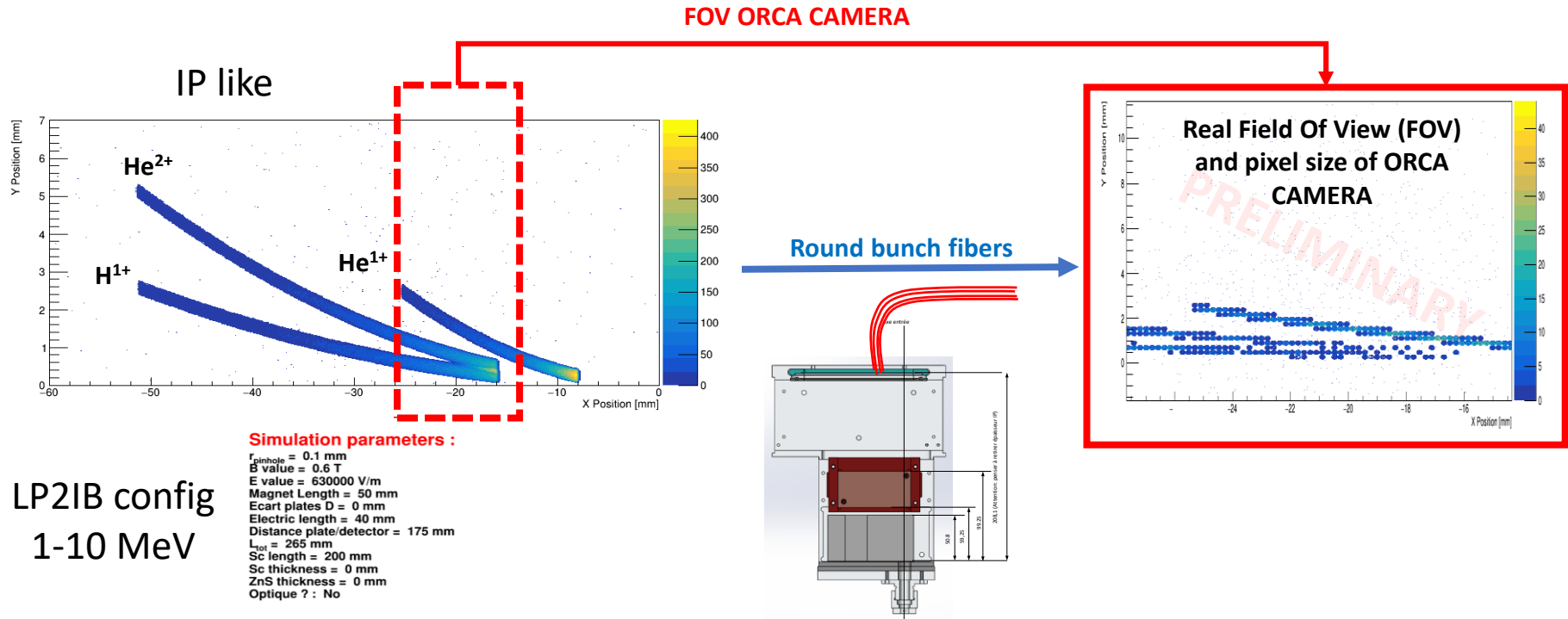
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Time of simulation (proton 3,5 MeV):

- Without G4FAST : 704 s/event
- With G4FAST : 298 s/event

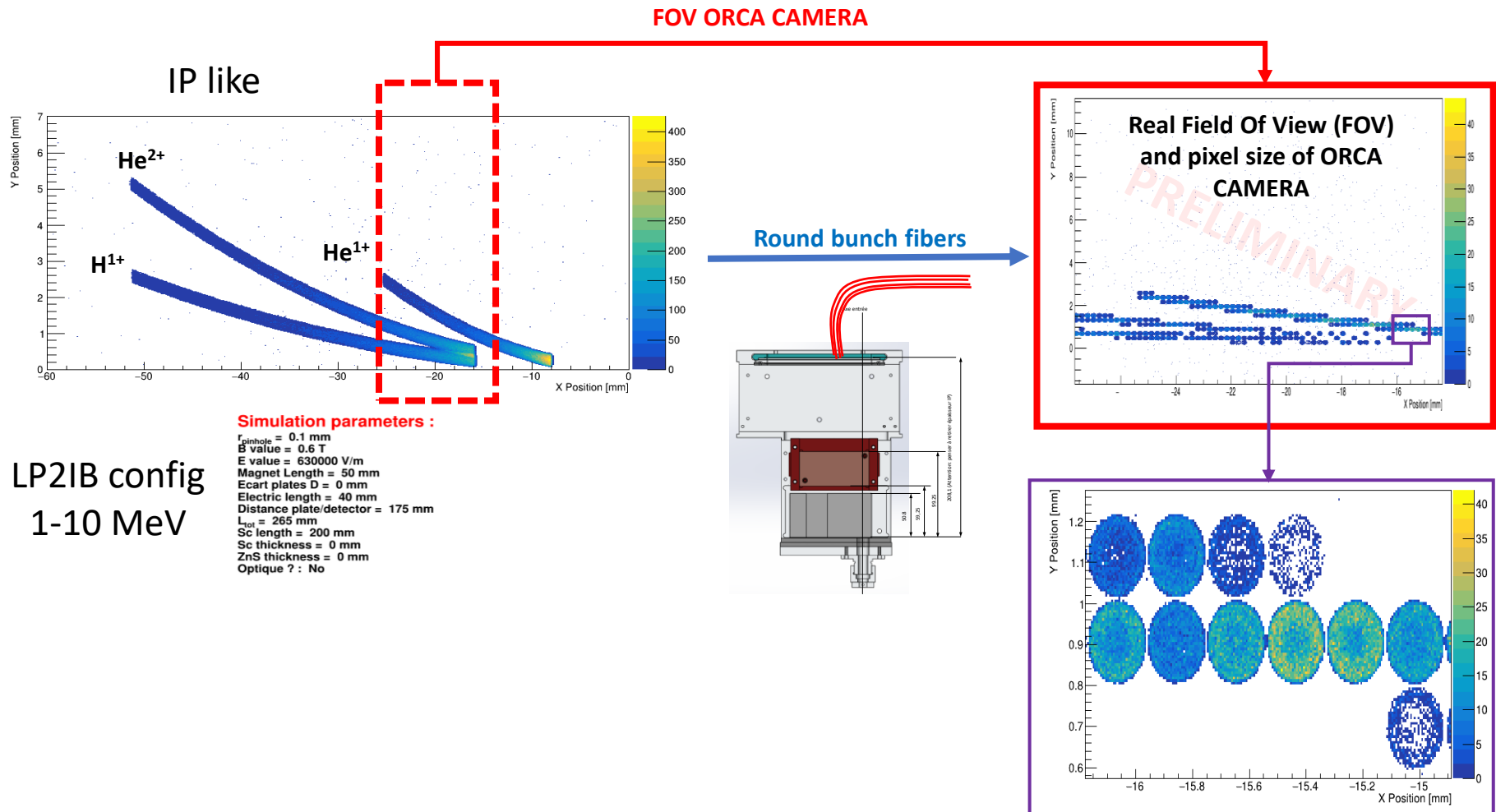
New design of TP

- Second study (May 22 -> ongoing) with a bunch of fibers in focal plan :
 - Remote the detection of light outside the chamber



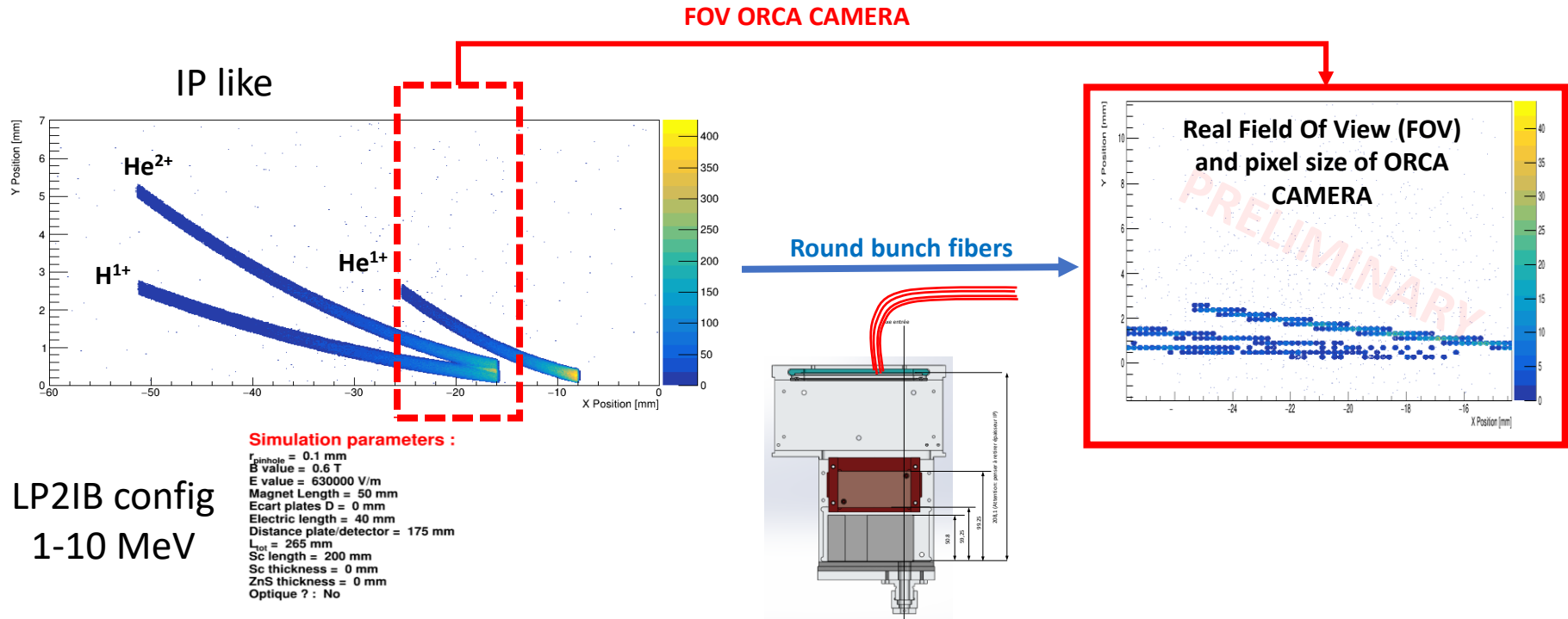
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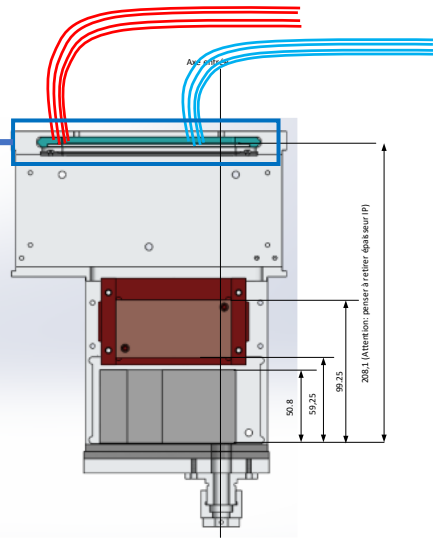
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Potential good solution solution to :

- Maximise Nph/Edep without smearing due to $\nearrow$ scintillator thickness
- Avoid Flash X & EMP problem
- Be adaptative for multiple experiments
- Fiber pixel dependant on the fiber dimensions

New design of TP



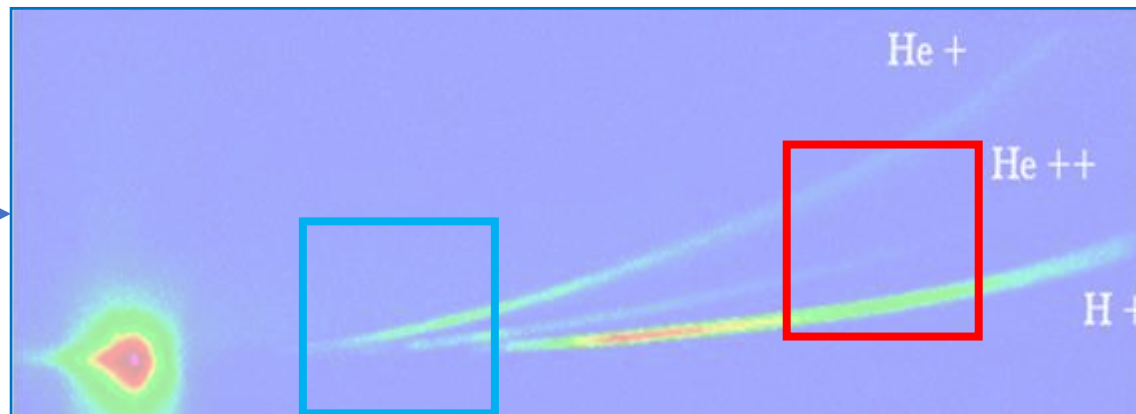
!!! If this configuration is the best solution !!!

- **Mechanical point of view :**

- Adjustable for each TP configuration & type of experiments (plug and play solution)
- Multizones with multiple cameras
- Potential light shielding to take care and so on...

- **Instrumentation point of view :**

- Custom-made CMOS detector (collaboration with IPHC Strasbourg)



- Creation of a **simulation tool** for the **study of Thomson Parabola**
 - **Already in contact** with GSI and CLPU (LaserLAB collaboration)
 - **Feedback are really important** (especially for the optical simulation)
- **Feasibility of TP with scintillator possible**
 - Needs **optimization** and **complete characterization**
- Test also configuration with **CMOS directly in focal plan**
- Decide what is the **best configuration**
- **Tests** of this configuration **to follow**
- **TP production & validation** in 2023-2024

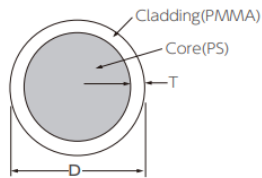
THANK YOU FOR YOUR ATTENTION

This study has received financial support from the French State in the framework of the Investments for the Future programme IdEx université de Bordeaux / GPR LIGHT

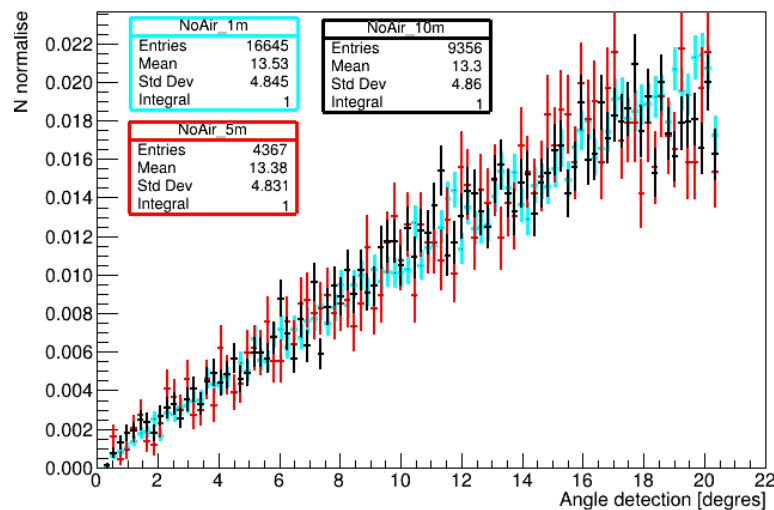
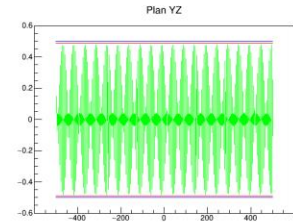
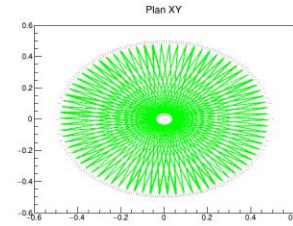
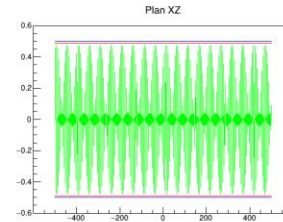
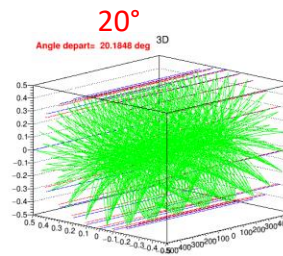
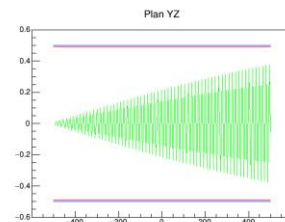
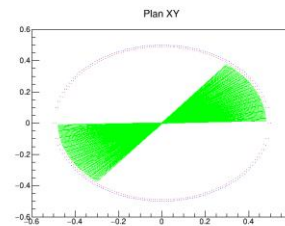
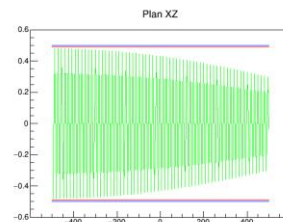
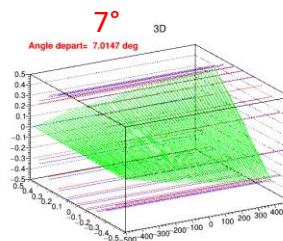
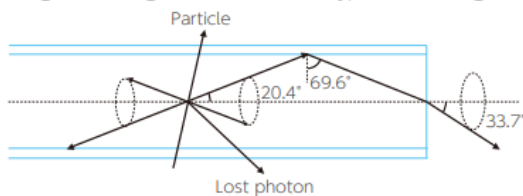
BACKUP

Rond single cladding

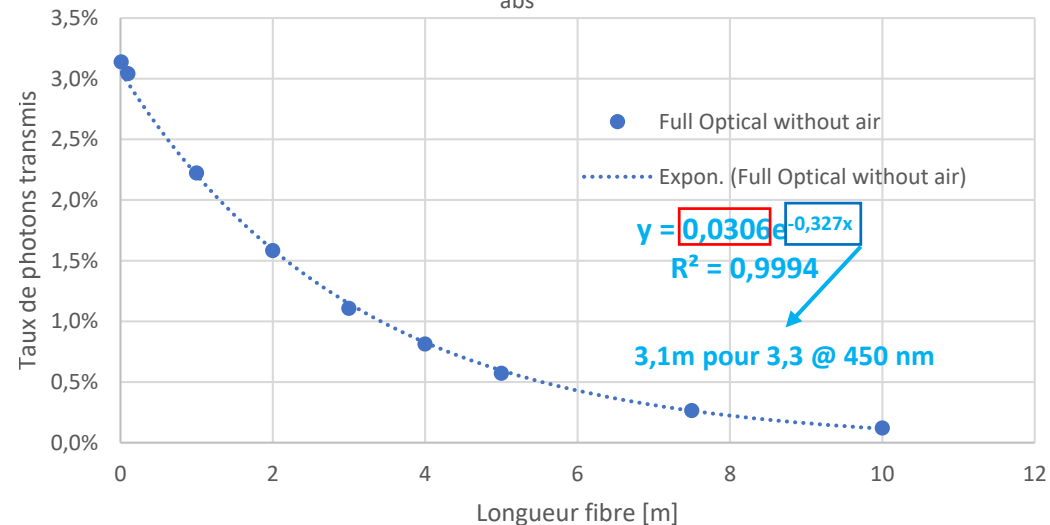
Single Cladding



Cladding Thickness: $T=2\%$ of D
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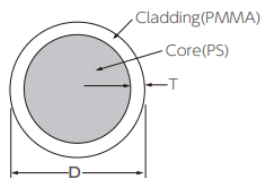


Estimation L_{abs} scintillateur

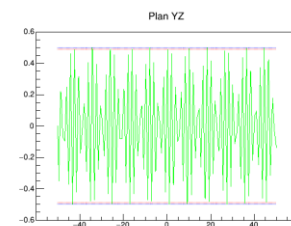
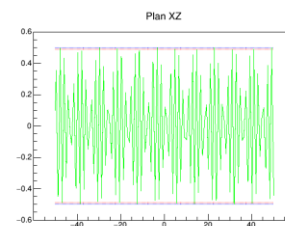
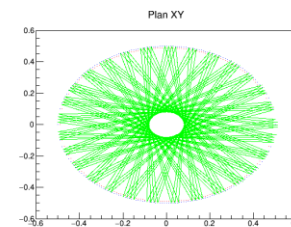
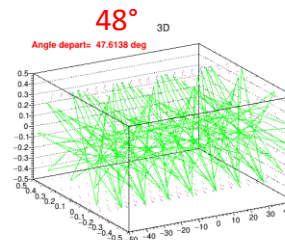
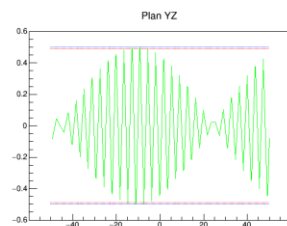
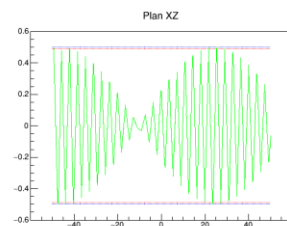
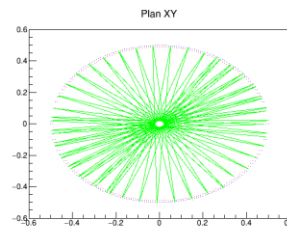
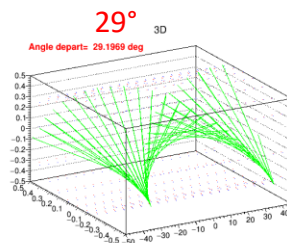


Rond single cladding

Single Cladding



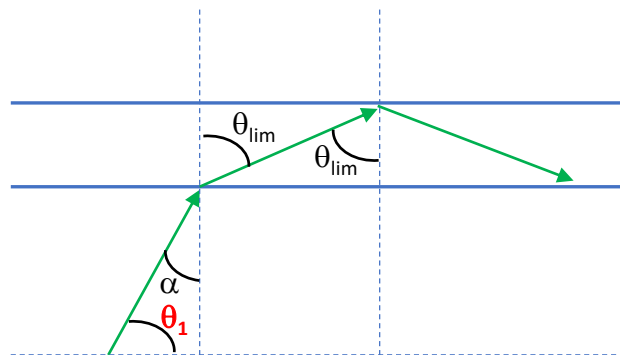
Cladding Thickness: $T=2\%$ of D
Numerical Aperture: $NA=0.55$
Trapping Efficiency : 3.1%



$n=1$

$n=1,49$

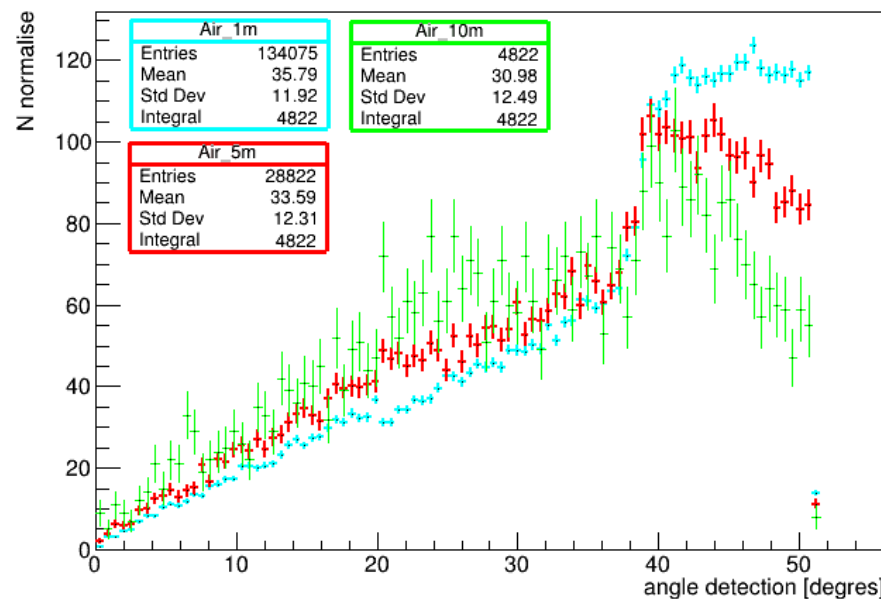
$n=1,59$



$$\theta_{lim} = \sin^{-1}\left(\frac{1}{1,49}\right) = 42,2^\circ$$

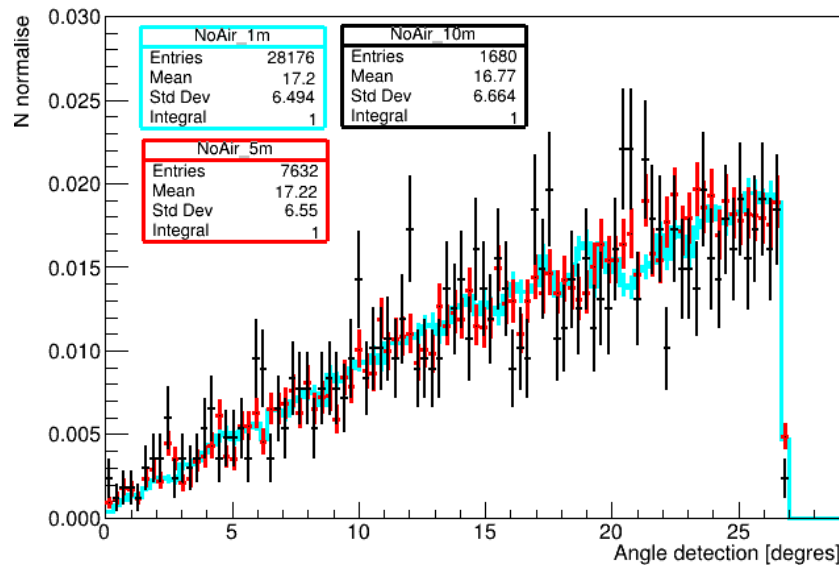
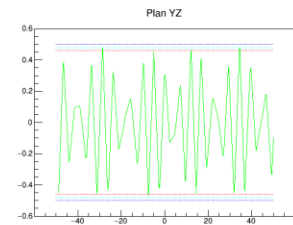
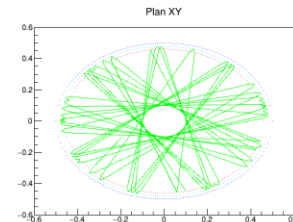
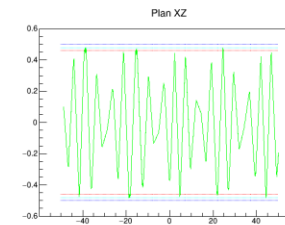
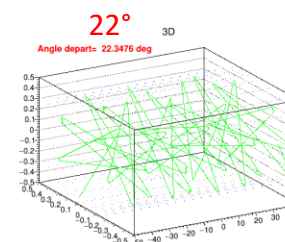
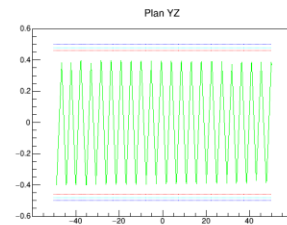
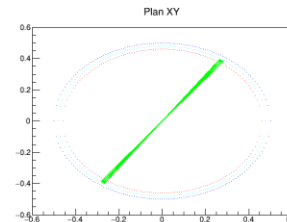
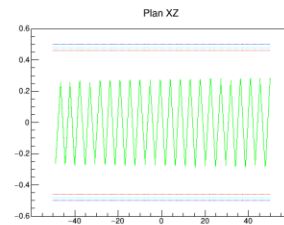
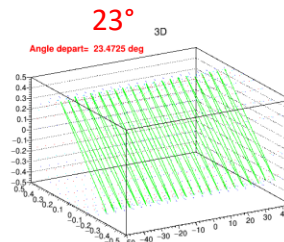
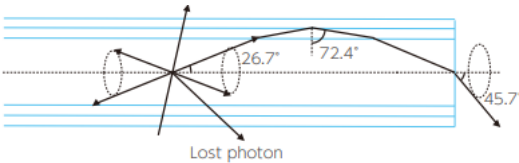
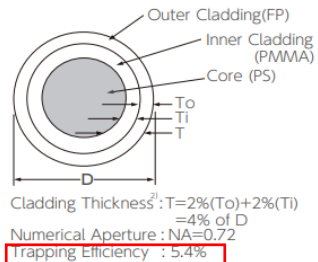
$$\alpha > \sin^{-1}\left(\frac{1,49}{1,59} \times \sin \theta_{lim}\right) = 39,0^\circ$$

$$\theta_1 < 90 - \alpha = 51^\circ$$

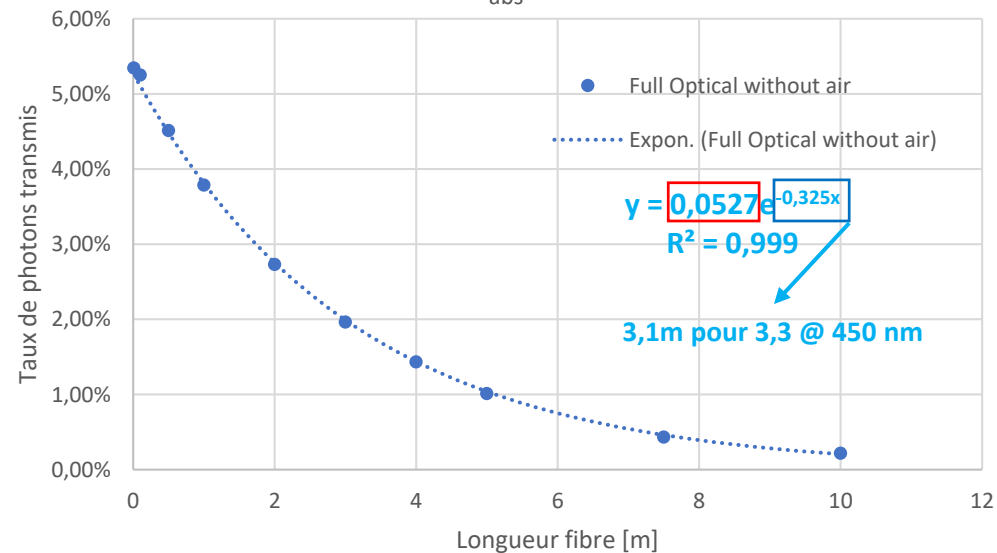


Rond multicladding

Multi-Cladding (M)

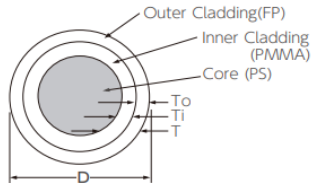


Estimation L_{abs} scintillateur

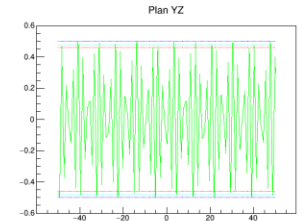
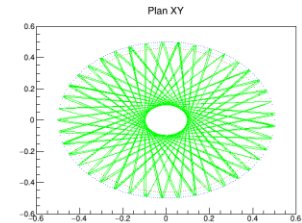
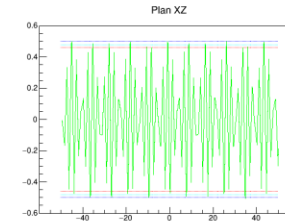
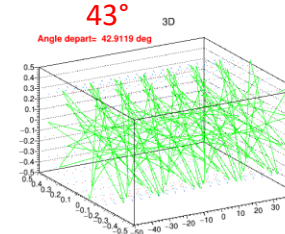
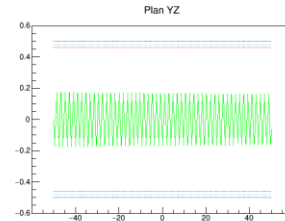
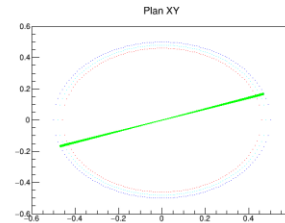
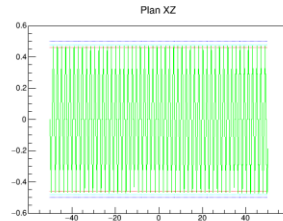
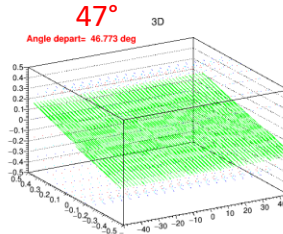


Rond multicladding

Multi-Cladding (M)



Cladding Thickness²⁾: $T = 2\%(T_o) + 2\%(T_i)$
 $\approx 4\%$ of D
 Numerical Aperture : $NA = 0.72$
 Trapping Efficiency : 5.4%

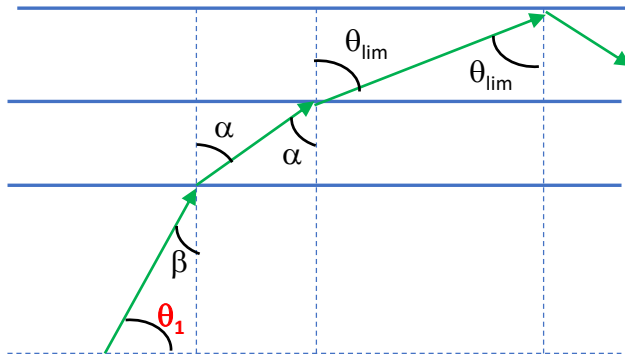


$n=1$

$n=1,42$

$n=1,49$

$n=1,59$

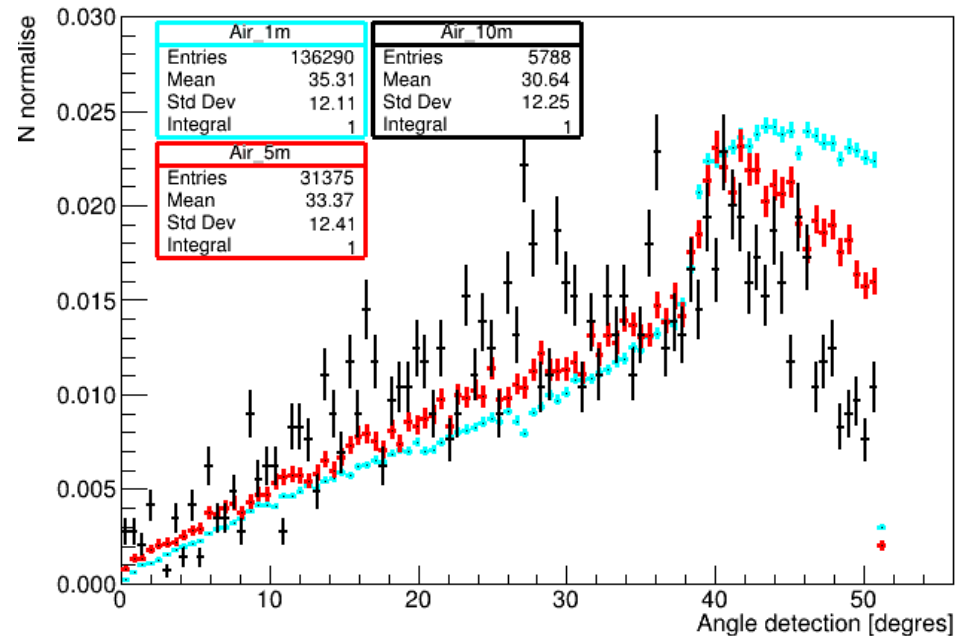


$$\theta_{lim} = \sin^{-1}\left(\frac{1}{1,42}\right) = 44,8^\circ$$

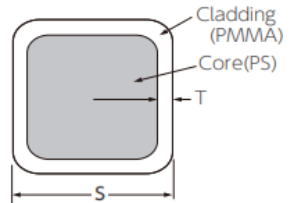
$$\alpha > \sin^{-1}\left(\frac{1,42}{1,49} \times \sin \theta_{lim}\right) = 42,2^\circ$$

$$\beta > \sin^{-1}\left(\frac{1,49}{1,59} \times \sin \alpha\right) = 39,0^\circ$$

$$\theta_1 < 90 - \alpha = 51^\circ$$

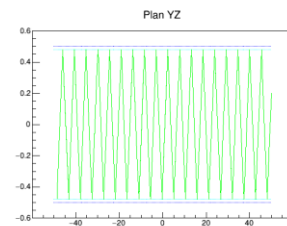
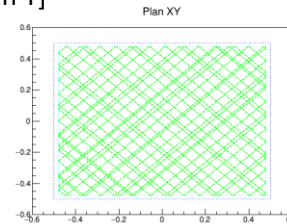
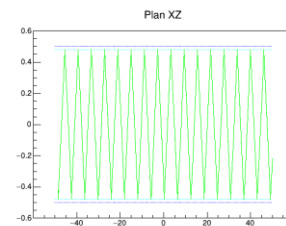
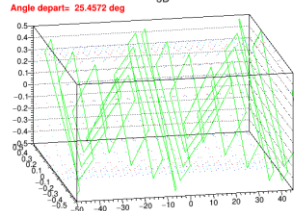


Carré single cladding

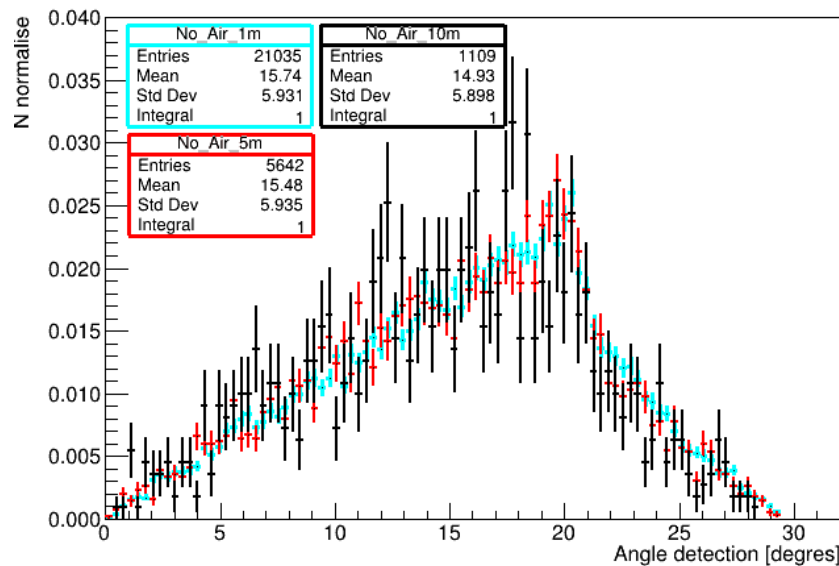
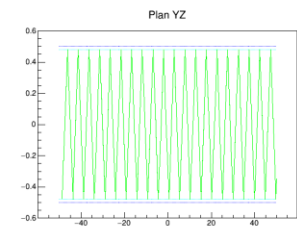
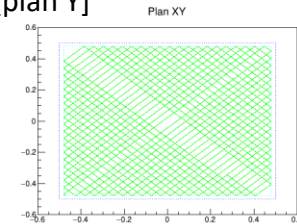
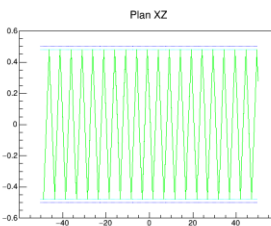
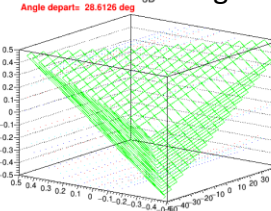


Cladding Thickness : $T=2\%$ of S
Numerical Aperture : $NA=0.55$
Trapping Efficiency : 4.2%

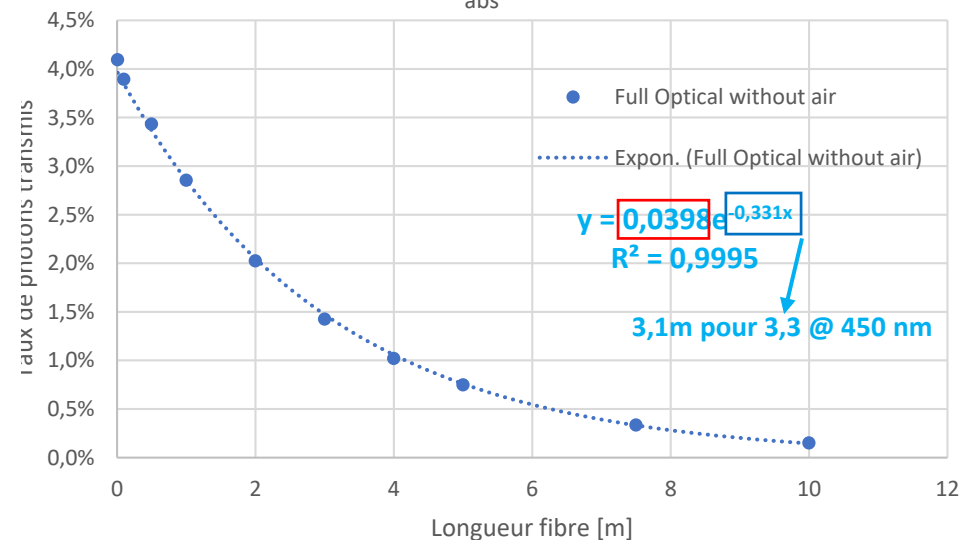
Angle 16° [plan X]
Angle 19° [plan Y]



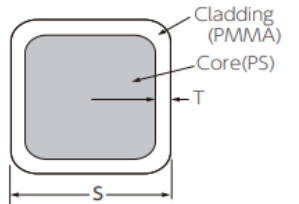
Angle 20° [plan X]
Angle 20° [plan Y]



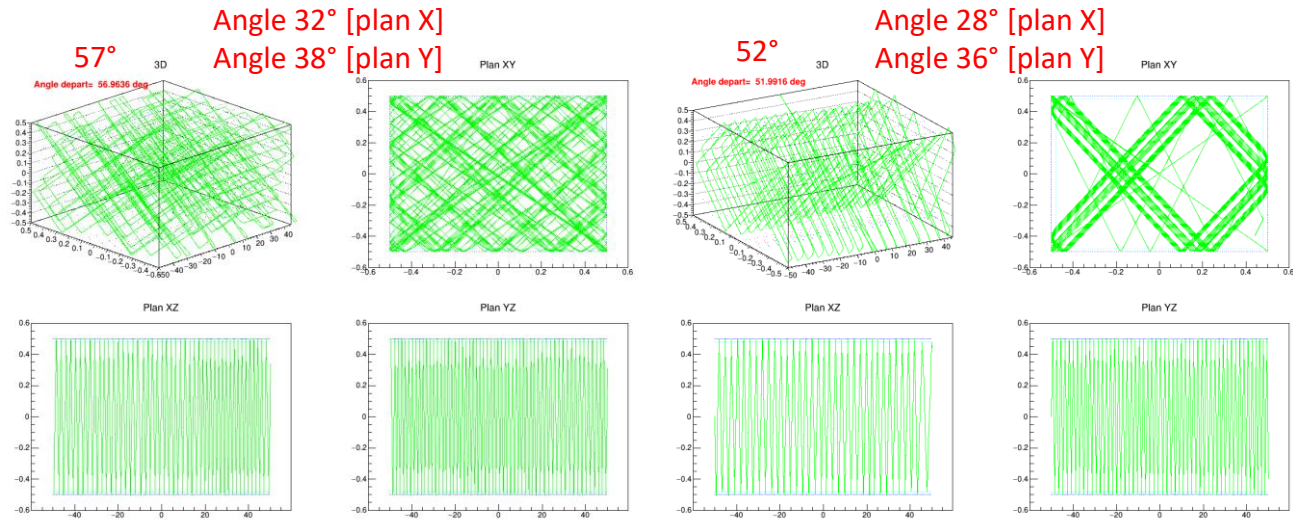
Estimation L_{abs} scintillateur



Carré single cladding



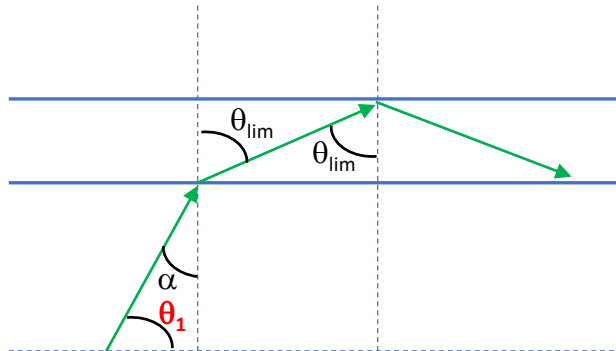
Cladding Thickness : $T=2\%$ of S
Numerical Aperture : $NA=0.55$
Trapping Efficiency : 4.2%



$n=1$

$n=1,49$

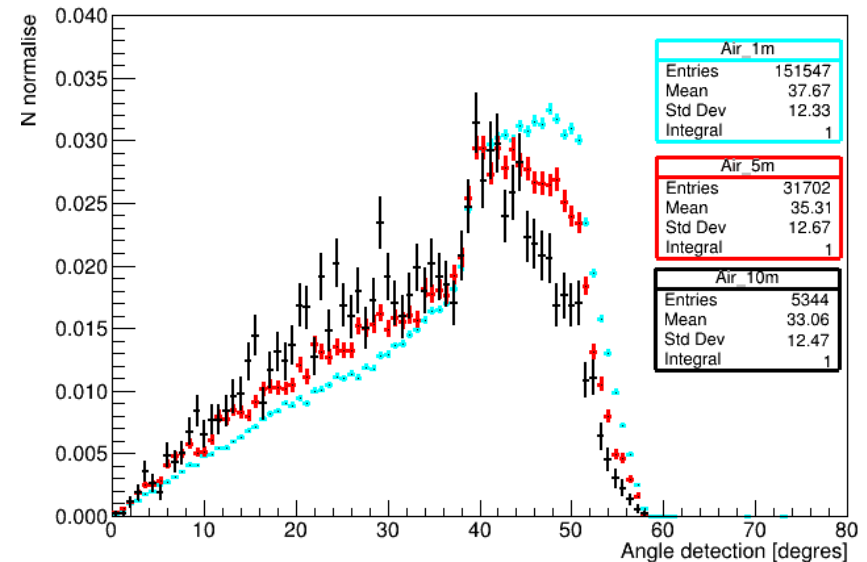
$n=1,59$



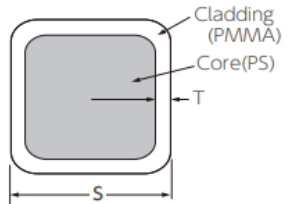
$$\theta_{lim} = \sin^{-1}\left(\frac{1}{1,49}\right) = 42,2^\circ$$

$$\alpha > \sin^{-1}\left(\frac{1,49}{1,59} \times \sin \theta_{lim}\right) = 39,0^\circ$$

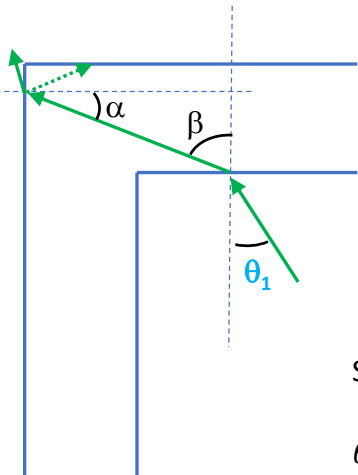
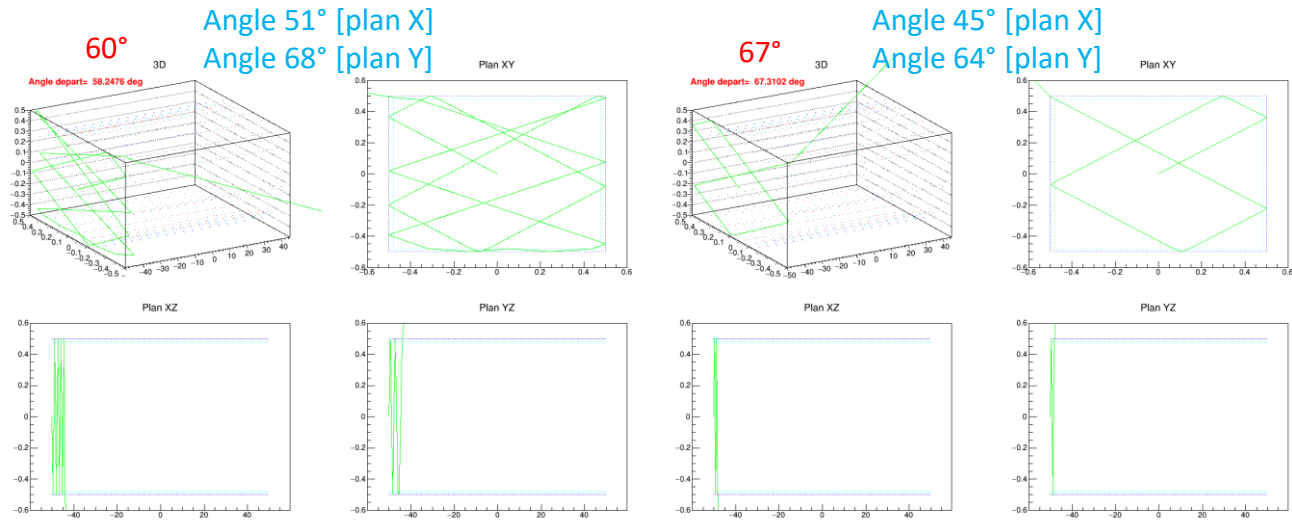
$$\theta_1 < 90 - \alpha = 51^\circ$$



Carré single cladding



Cladding Thickness : $T=2\%$ of S
Numerical Aperture : $NA=0.55$
Trapping Efficiency : 4.2%

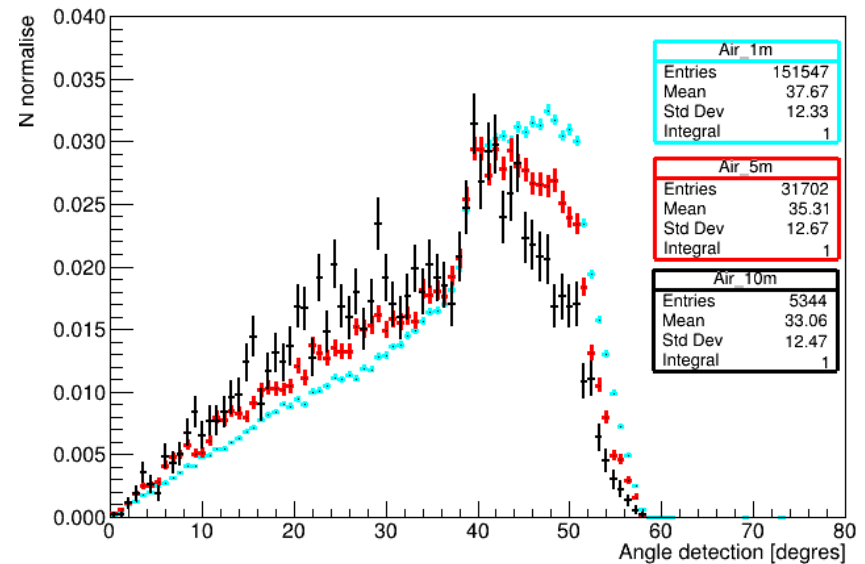


$$\theta_{lim} = \sin^{-1}\left(\frac{1}{1,49}\right) = 42,2^\circ$$

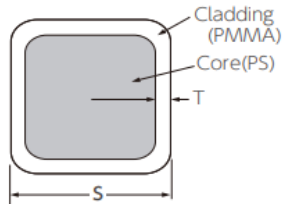
$$\text{Si } \alpha > \theta_{lim} \quad \beta < (90 - \alpha = 47,8^\circ)$$

$$\theta_1 < \left(\sin^{-1}\left(\frac{1,49}{1,59} \times \sin \beta\right)\right) = 44,0^\circ$$

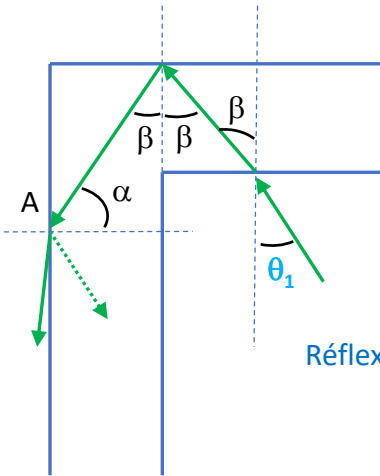
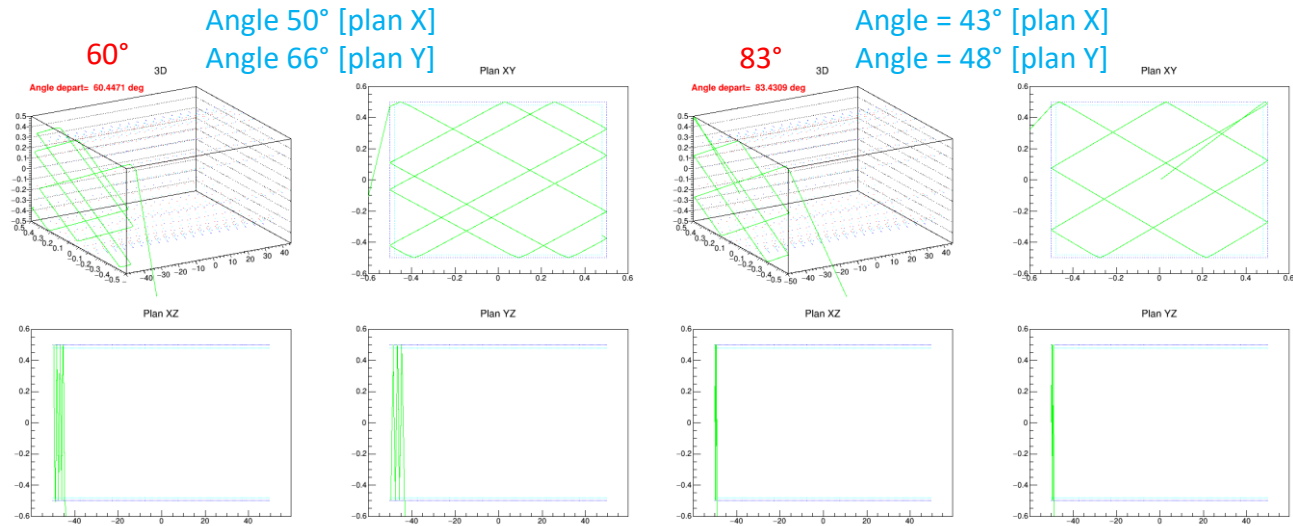
Réflexion totale au point A si et seulement si $\theta_1 < 44^\circ$



Carré single cladding



Cladding Thickness : $T=2\%$ of S
Numerical Aperture : $NA=0.55$
Trapping Efficiency : 4.2%



$$\theta_{lim} = \sin^{-1}\left(\frac{1}{1,49}\right) = 42,2^\circ$$

$$\text{Si } \alpha > \theta_{lim} \quad \beta < (90 - \alpha = 47,8^\circ)$$

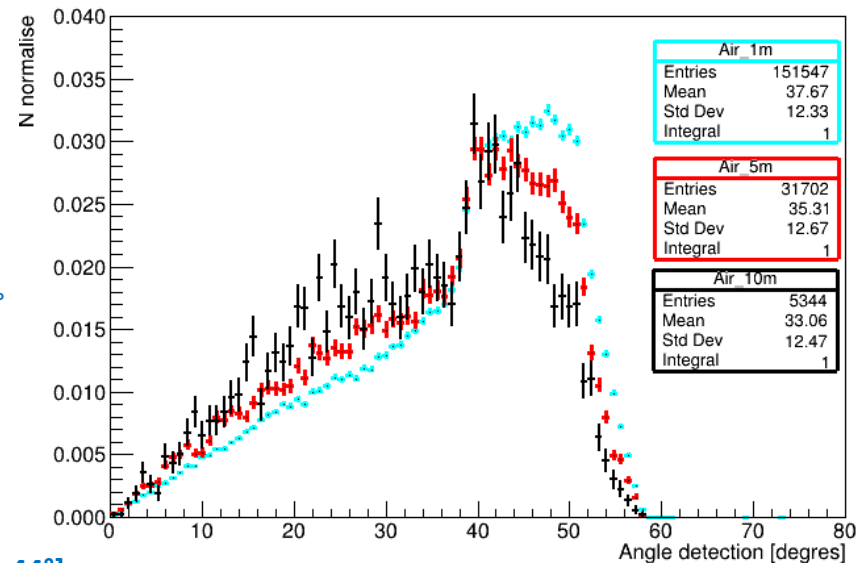
$$\theta_1 < \left(\sin^{-1}\left(\frac{1,49}{1,59} \times \sin \beta\right)\right) = 44,0^\circ$$

R flexion totale au point A si et seulement si $\theta_1 < 44^\circ$

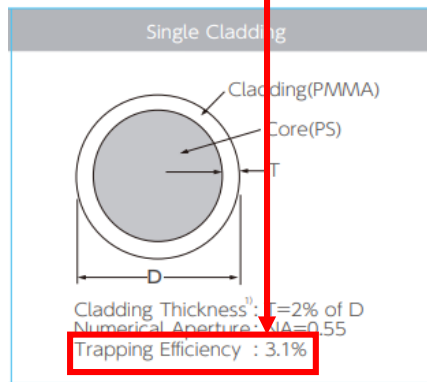
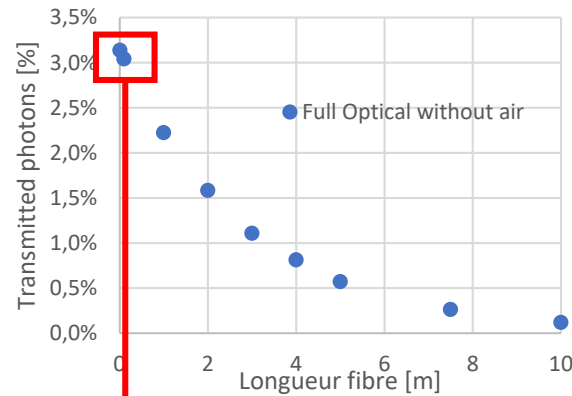
On doit  galement avoir $\beta > \theta_{lim}$

$$\theta_1 > \left(\sin^{-1}\left(\frac{1,49}{1,59} \times \sin \beta\right)\right) = 39,0^\circ$$

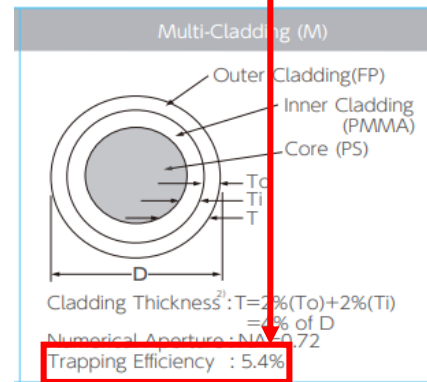
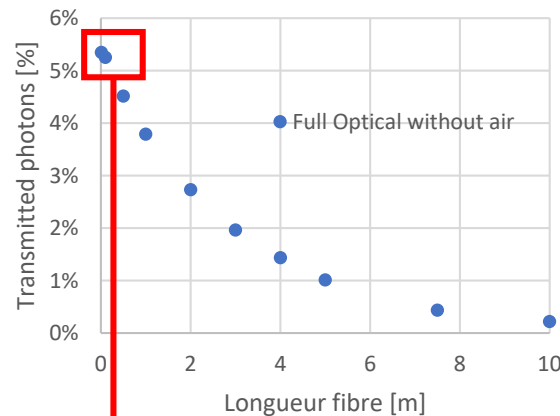
R flexion totale au point A si et seulement si $\theta_1 \in [39^\circ ; 44^\circ]$



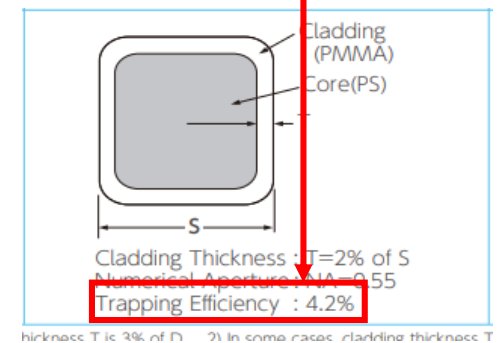
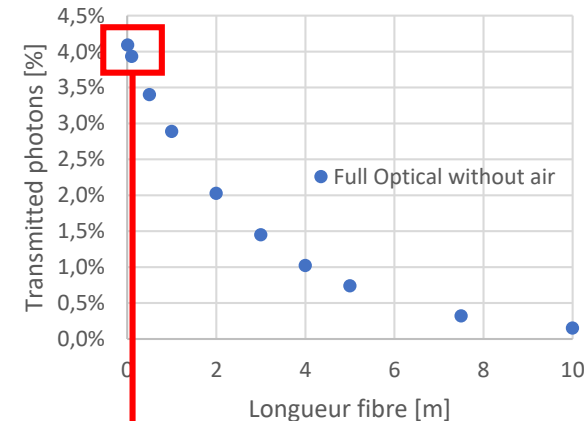
Round single cladding



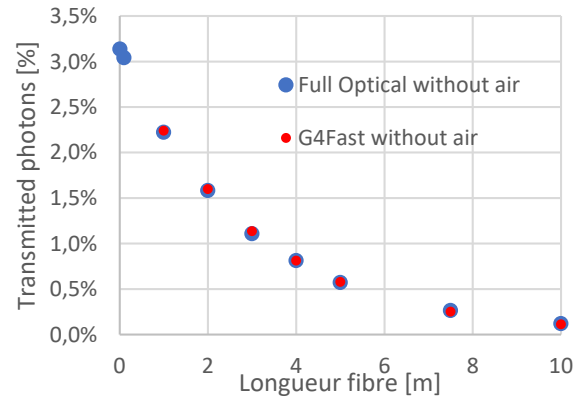
Round multi-cladding



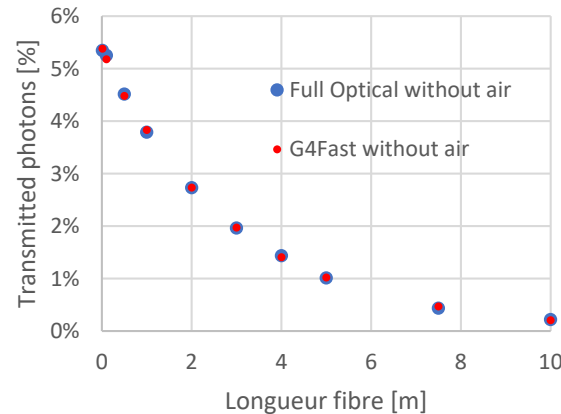
Square single cladding



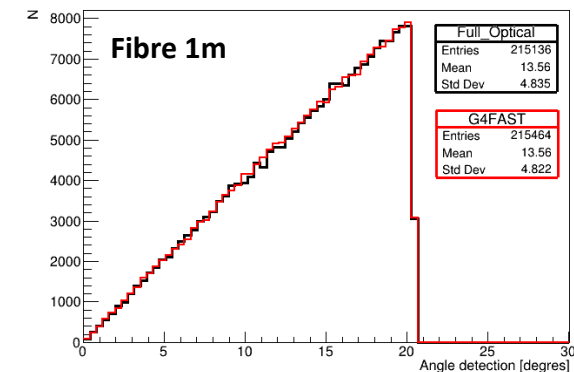
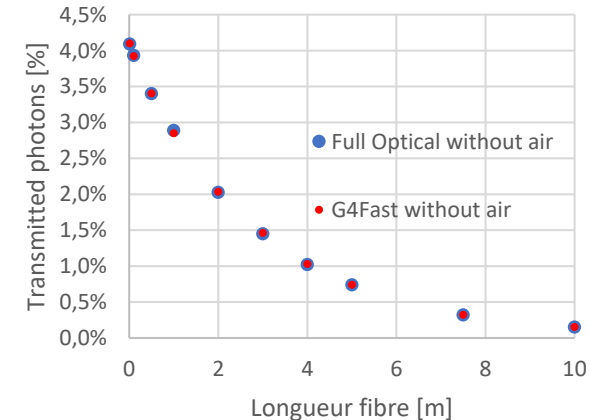
Round single cladding



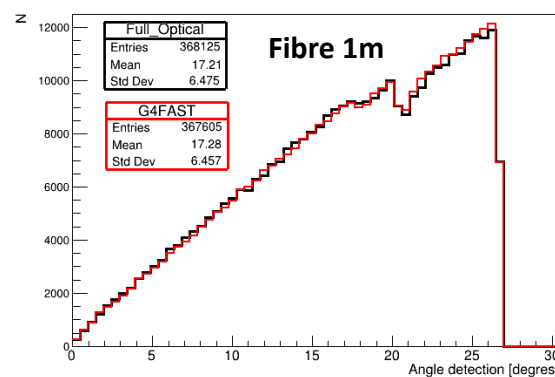
Round multi-cladding



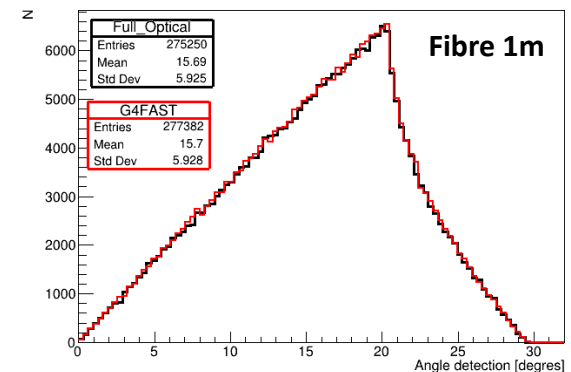
Square single cladding



Full Optical : 358 events/s
G4FAST : 735 events/s

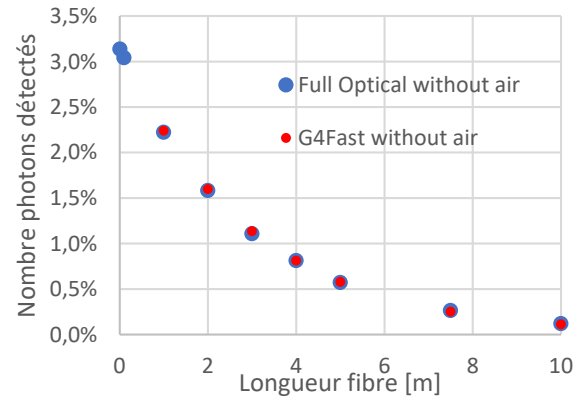


Full Optical : 145 events/s
G4FAST : 602 events/s

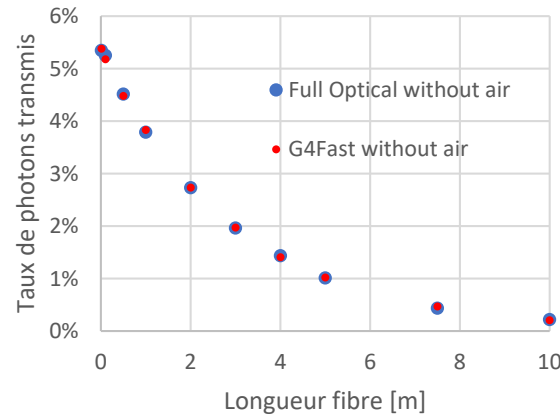


Full Optical : 244 events/s
G4FAST : 781 events/s

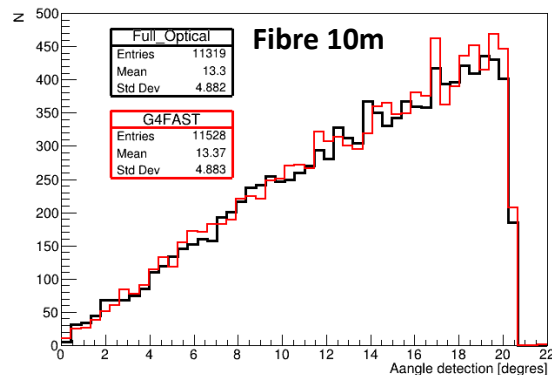
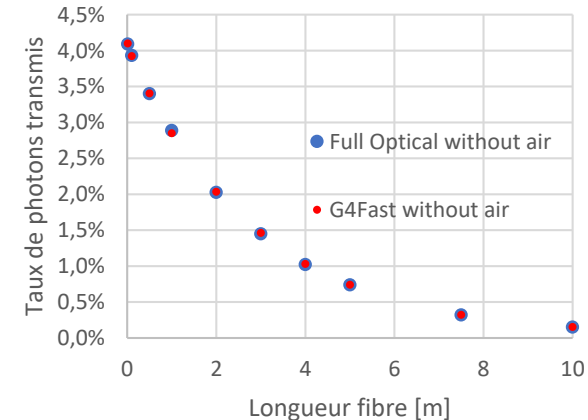
Round single cladding



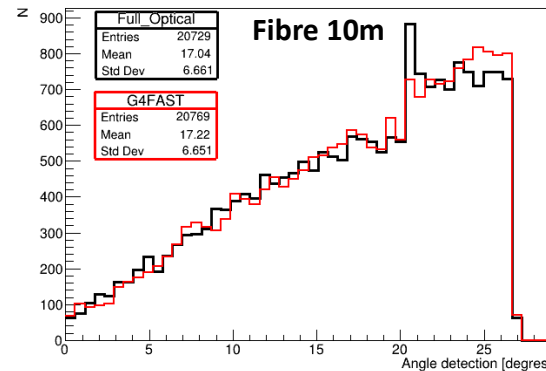
Round multi-cladding



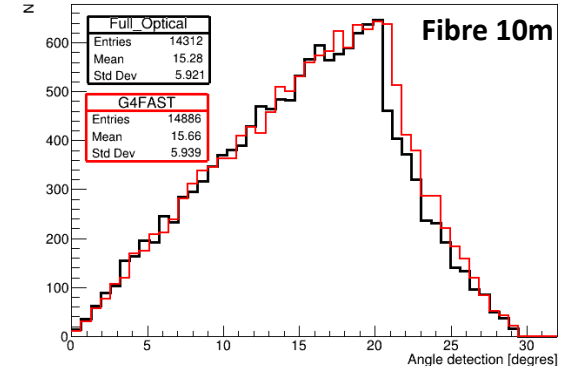
Square single cladding



Full Optical : 78 events/s
G4FAST : 730 events/s

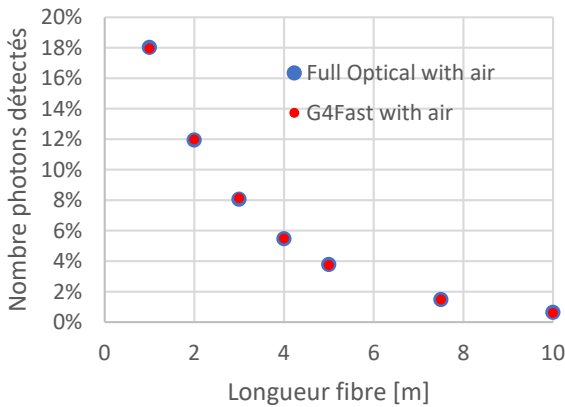


Full Optical : 48 events/s
G4FAST : 549 events/s

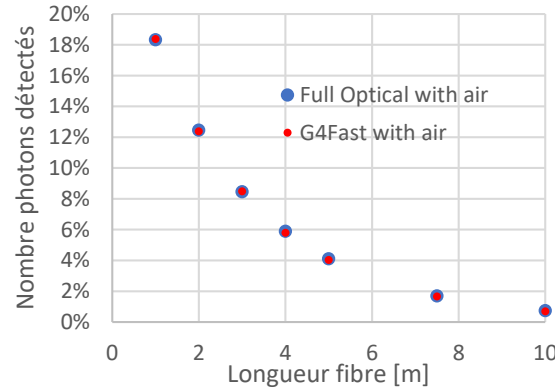


Full Optical : 93 events/s
G4FAST : 840 events/s

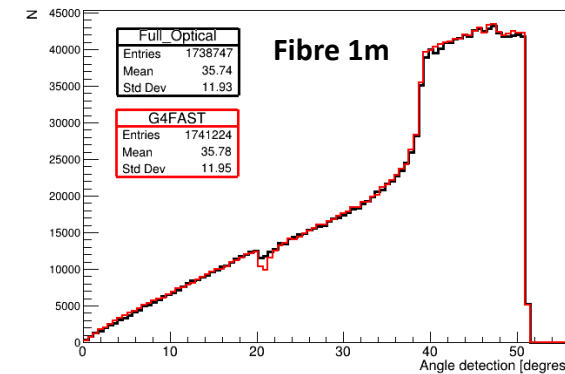
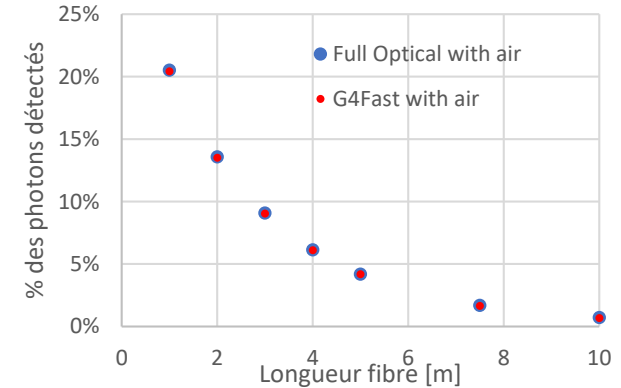
Round single cladding



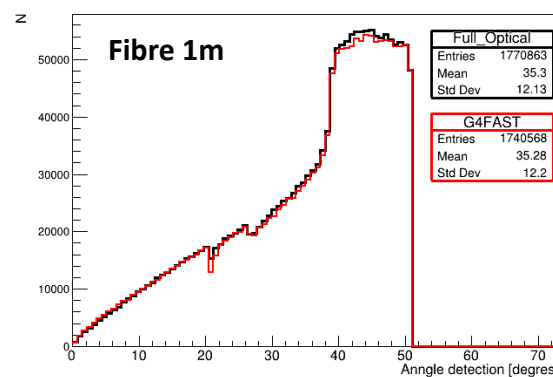
Round multi-cladding



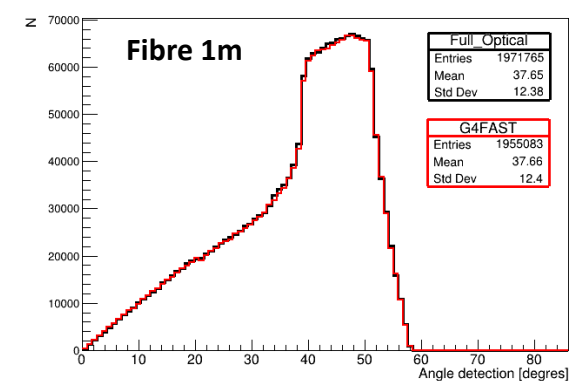
Square single cladding



Full Optical : 12 events/s
G4FAST : 111 events/s

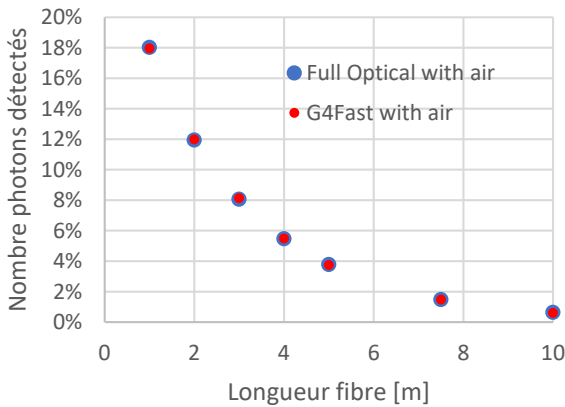


Full Optical : 8 events/s
G4FAST : 75 events/s

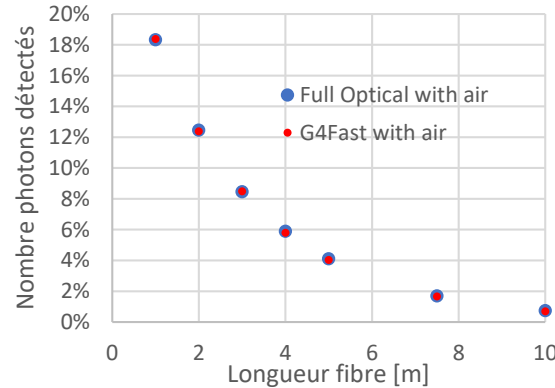


Full Optical : 8 events/s
G4FAST : 22 events/s

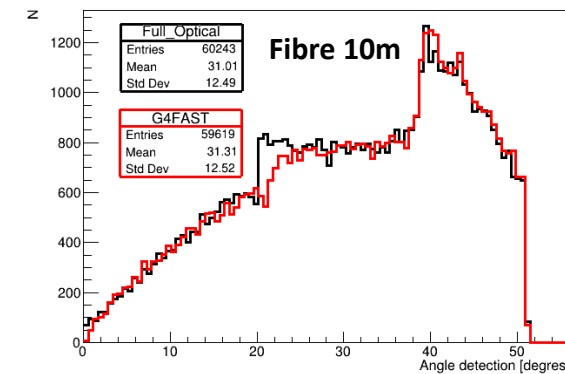
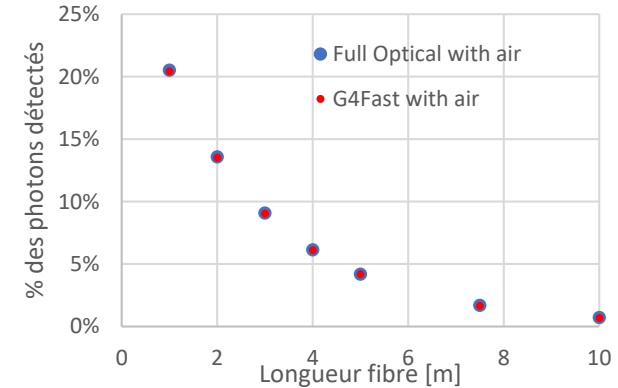
Round single cladding



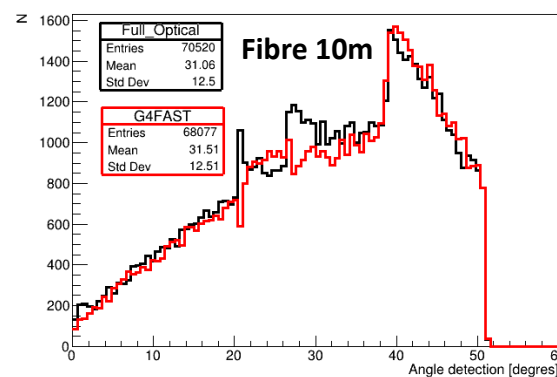
Round multi-cladding



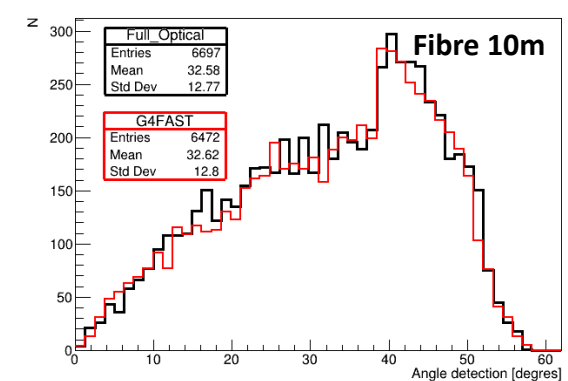
Square single cladding



Full Optical : 4 events/s
G4FAST : 48 events/s



Full Optical : 3 events/s
G4FAST : 32 events/s



Full Optical : 3 events/s
G4FAST : 10 events/s