

GRAAL meeting: MINERVA RF/Cryo modelling for C&C optimization studies



ACCELERATORS AND
CRYOGENIC SYSTEMS



Laboratoire de Physique
des 2 Infinis

ACCELERATORS and CRYOGENIC SYSTEMS

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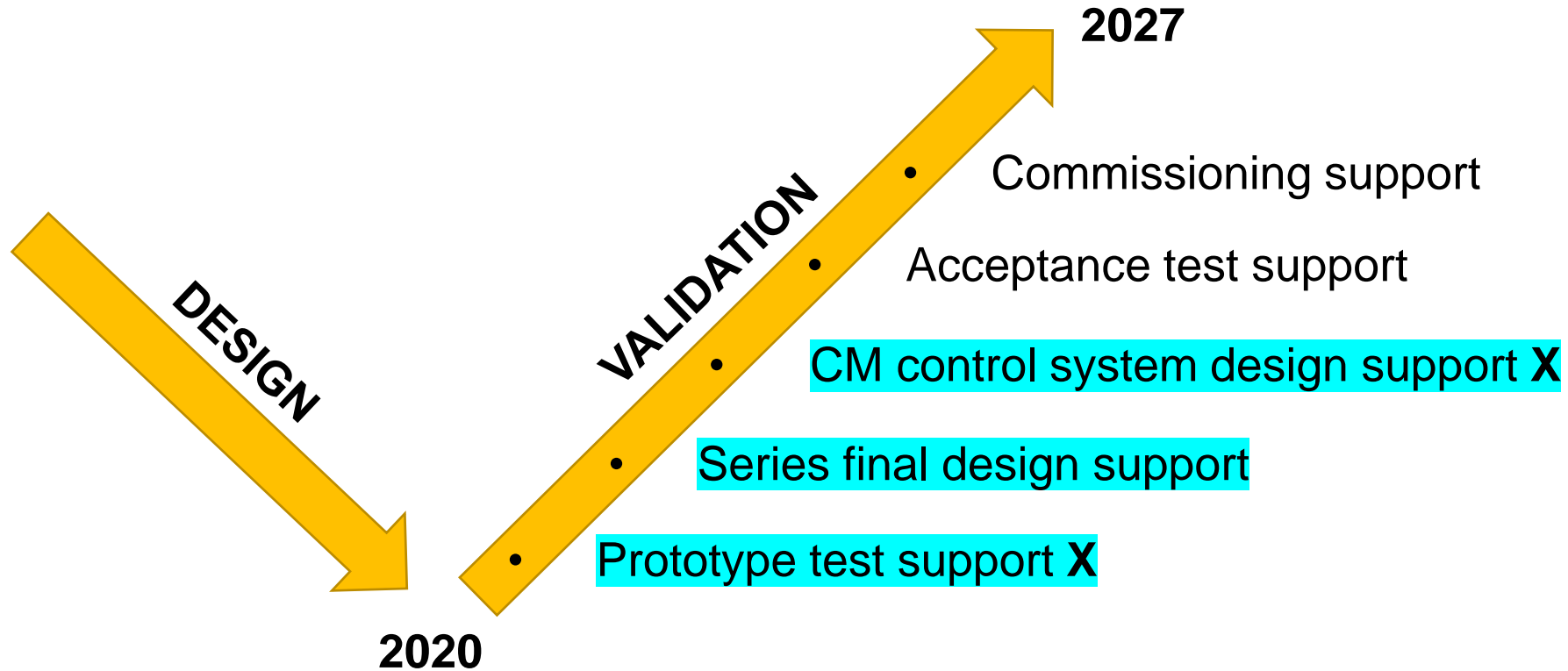


Outline

- Application of the model by project phase
- Brainstorming results
- On-going C&C-oriented studies → 5 illustrations



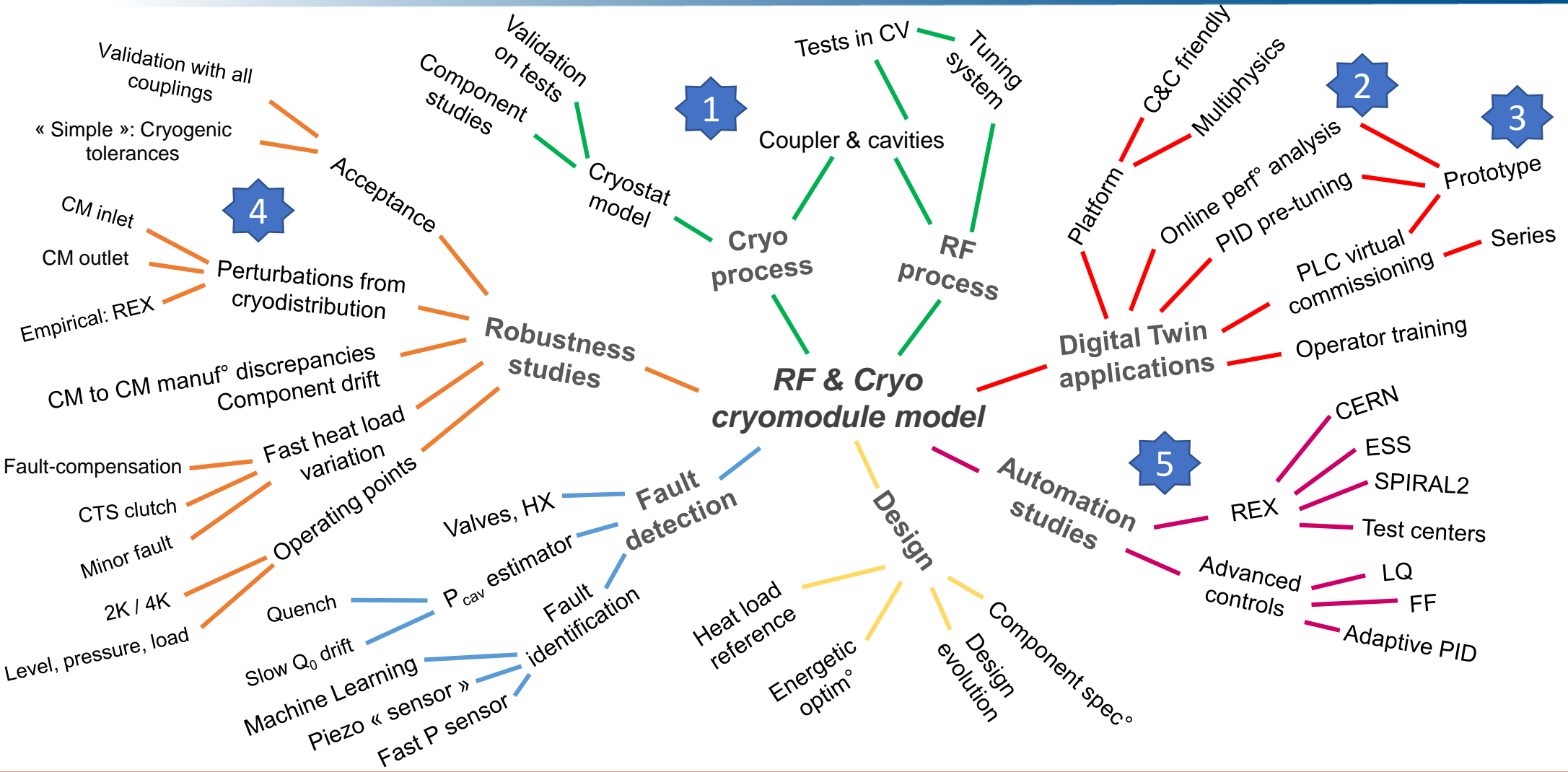
Application by project phase



→ Need for a model which follows the project cycle



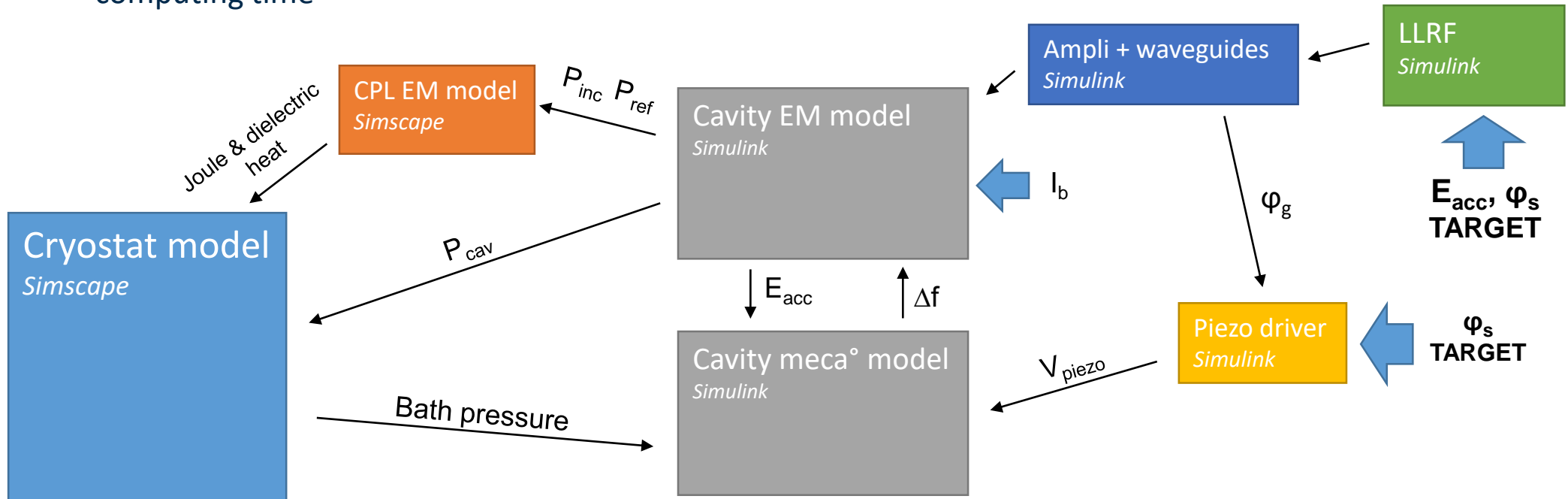
Brainstorming result = an organized mess !





1. Coupling together RF and cryo models

- RF and cryo strongly coupled → **modelling them together is necessary** to check the “cohabitation” !
- But those processes have **much different characteristic times** → find a way to save computing time





1. Implementation of RF models

- Simulink models of the cavity (same than FPGA HIL studies)

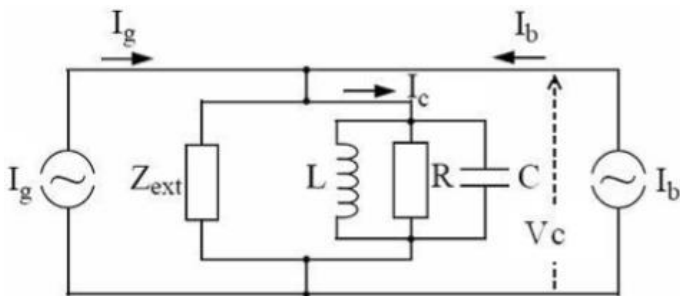
- Cavity envelope equation
- Closed loop on E_{acc} and φ_s
- Outputs P_{cav} / P_{inc} / P_{ref} / φ_g
- As a function of Δf , Q_0 , E_{acc} , φ_s

- Detuning models

- Piezo and motor tuner $\Delta f = f$ (command)
- He bath pressure: $\Delta f = f(P)$
- Lorenz force: $\Delta f = f(E_{acc})$
- Piezo dynamic TF

- As usual, crucial to **model** the feedback loop I/O with the **physical** attenuations and phase shifts

- The transmitted signals from the cavity (V_{ti} , V_{tq})
- The cavity detuning error ($\varphi_g - \varphi_s$)

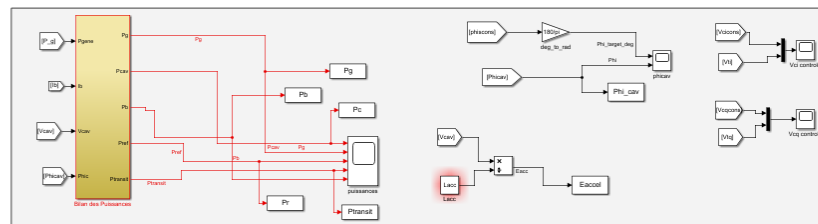
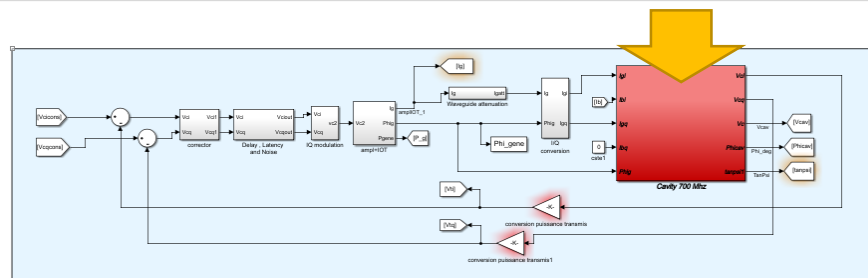
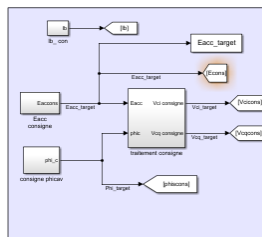


$$\frac{d^2 V_c}{dt^2} + 2\omega_{1/2} \frac{dV_c}{dt} + \omega_0^2 V_c = 2\omega_{1/2} R_L \frac{dI}{dt}$$



Cavity baseband equation:

$$\frac{d\vec{V}_c}{dt} + (\omega_{1/2} - j\Delta\omega)\vec{V}_c = \omega_{1/2} R_L \vec{I}$$



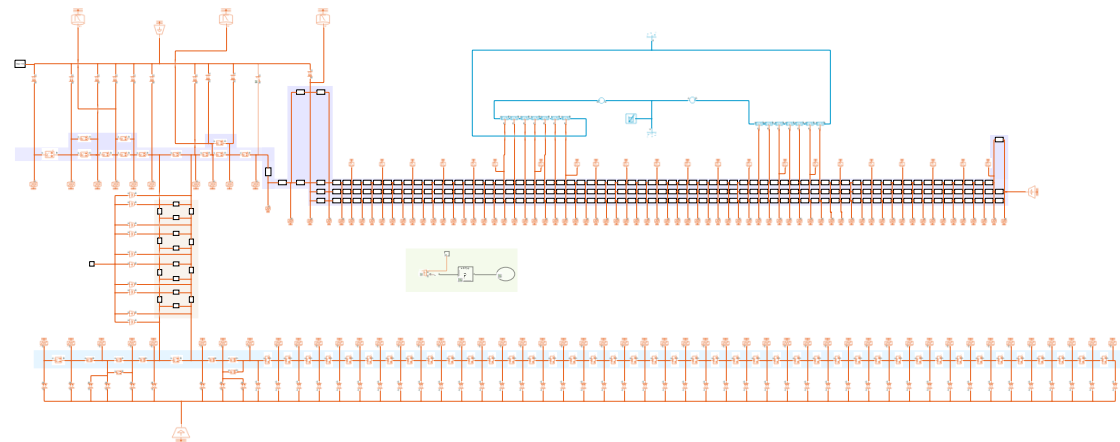
*LLRF Lecture Part 3.1 S. Simrock, Z. Geng - ITER / PSI

** Thesis F. Bouly 2011



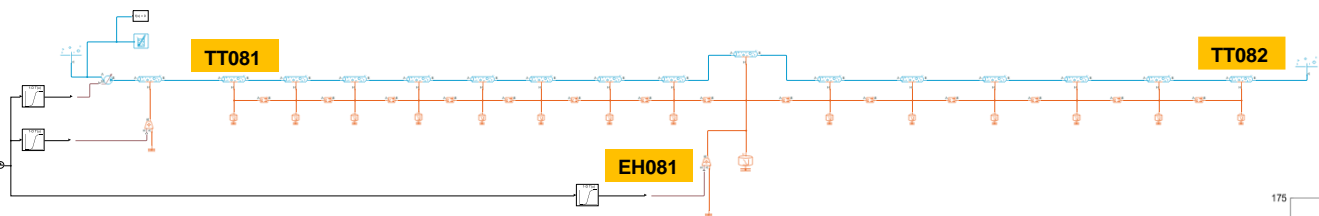
1. Implementation of RF models

- **Joules & dielectric heat loads** calculated from:
 - RF field imported from EM code (CST, HFSS)
 - Material electrical properties = $f(T)$
- **To do**
 - Implement a simple RF field model to cover all cases without an EM code
 - As a function of P_{inc} , P_{ref} from the cavity model



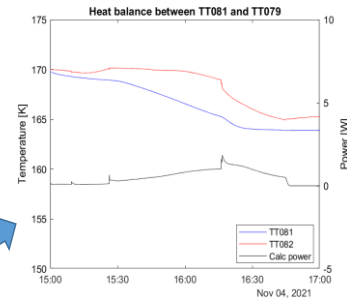
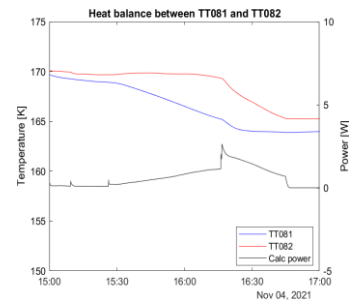


2. Support to prototyping phases

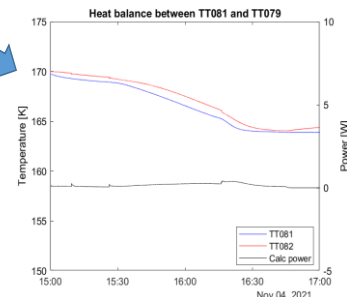


Mock-up coupler heat load measurement calibration
→ *unsteady heat balance analysis*

Experiment



Model
→ heaters ON

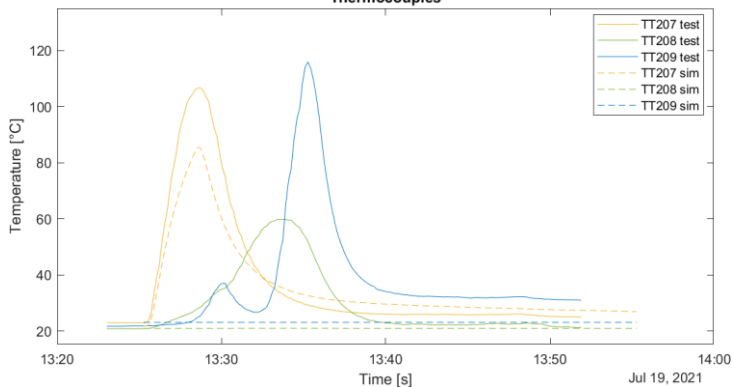


Model
→ heaters OFF

Coupler conditioning
multipacting heat load simulations

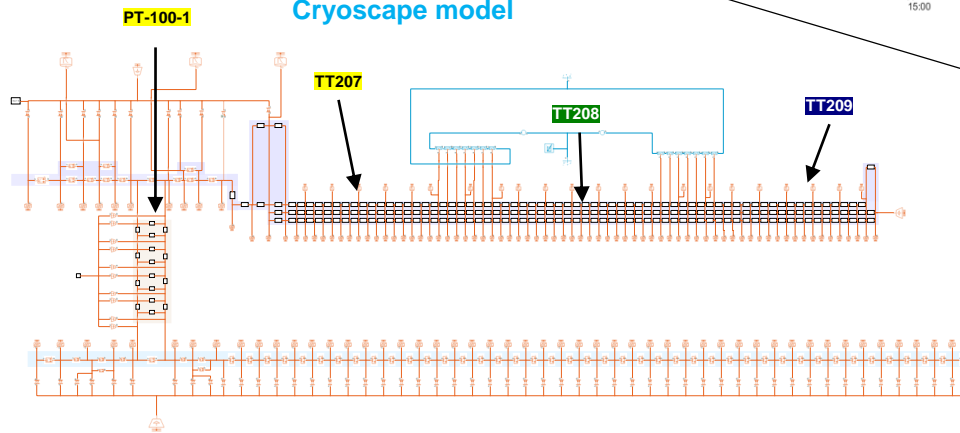
Cross-check with CST / SPARK 3D

Thermocouples



Coupler tube temperatures: test VS Cryospace

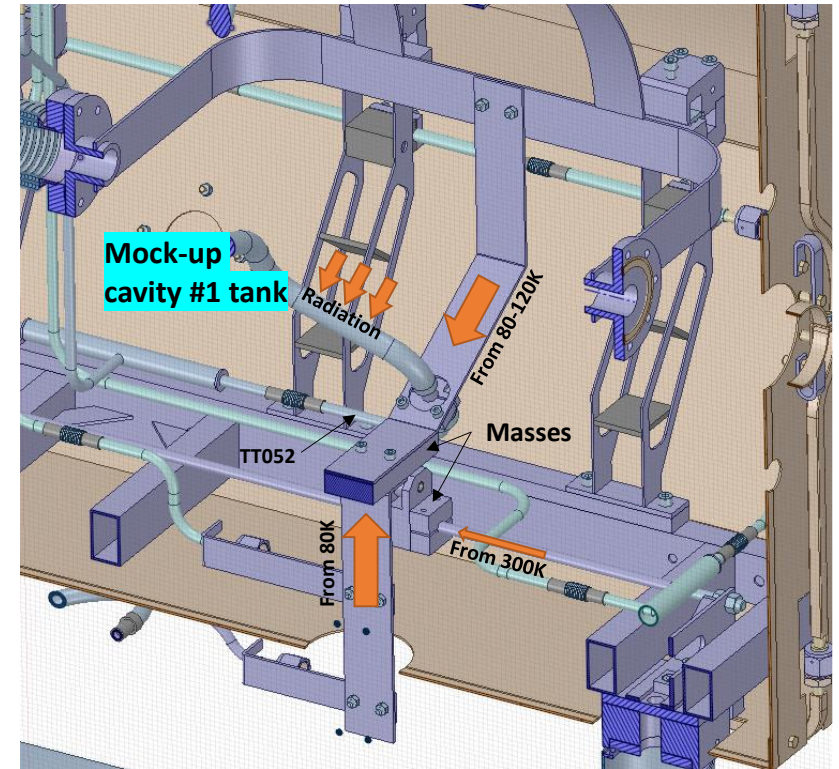
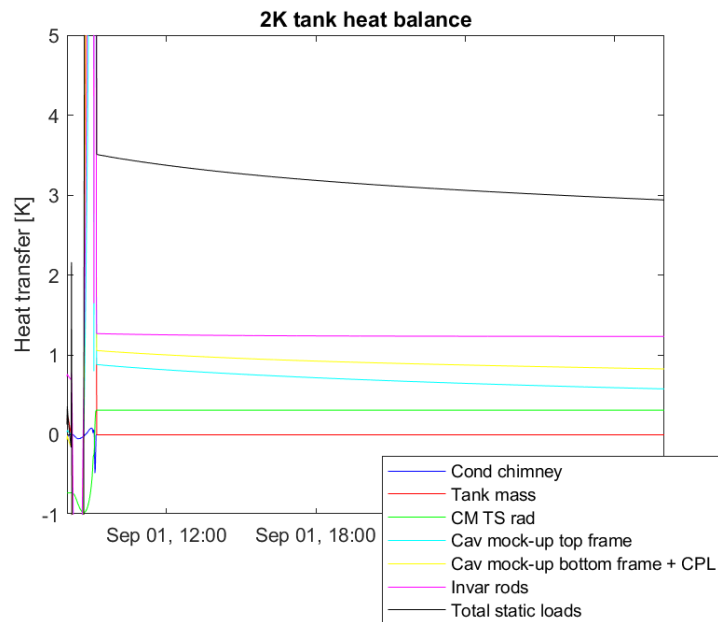
Cryospace model





2. Support to prototyping phases

- *testQVB & QM heat load analysis*
- *Pointing out the need for additional instrumentation*





3. Digital Twin supporting the prototyping PLC code dvpt

Main problem

- The PLC code developer needs the process hardware asap for debugging
 - Sequence virtual commissioning
 - HMI development
 - PID tuning
- Idea: the model is connected to the PLC and mimics the process

Step 1, done on the prototype in CD

- PID gain pre-tuned on Simscape and used as start values in TIA Portal
- Need similar PID controller architecture Model VS TIA Portal

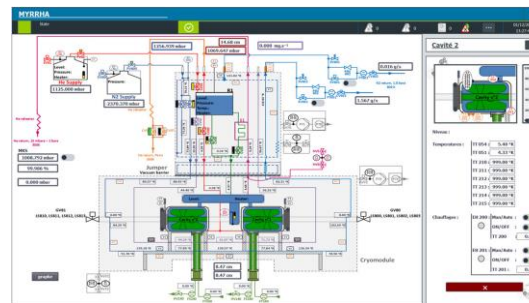
Actuator	Sensor	Simscape pre-tuning		Online tuned	
		P	Ti	P	Ti
CV01	LT01	0,1	50	0,5	1
CV04	LT050	0,1	50	0,5	1
CV601	TT620	-0,5	1666	-0,35	3000
CV651	TT651	-0,5	1666	-0,5	1666
CV06	PT01	-120	60	-200	8
MKS	PT50/51				

From MKS conditioner

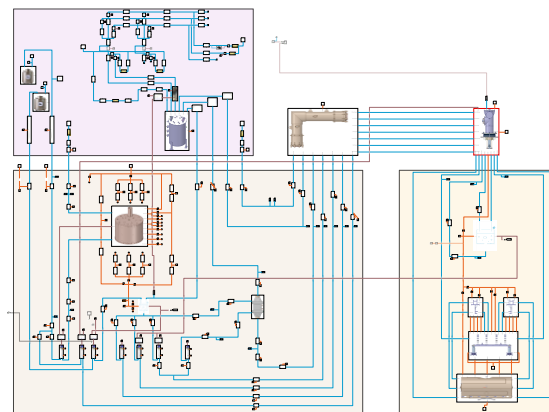
Step 2, on-going

- Originally, Simscape is controlled by Simulink (sequences and feedback loops) → control from PLC instead
- Hardware or Software in the loop approach (Real or simulated PLC)
- Need to run in real time
- Thorough work to connect all I/O

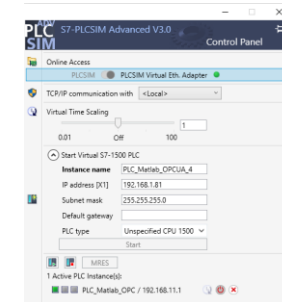
WinCC HMI proto



Simscape model



PLCsim



OPC UA server

MATLAB OPC UA Client

```

uaClient =
OPC UA Client:
Server Information:
  Name: 'SIMATIC_57-1500-OPC-UA-Application:PLC_1'
  Hostname: '192.168.1.01'
  Port: 4840
  EndpointUrl: 'opc.tcp://192.168.1.01:4840'
Connection Information:
  Timeout: 10
  Status: 'Disconnected'
  ServerState: '<Not connected>'
Security Information:
  MessageSecurityMode: None
  ChannelSecurityPolicy: None
  Endpoints: [1]: opc.ua.EndpointDescription
  
```



4. Target for the cryogenic feedback loops

- **Context**

- The bibliographic studies and REX points toward cryogenic pressure regulation tolerances about +/- 5 mbar
- Often **based on what is achievable**, not **what is required**

- **Problematic**

- In principle, on MINERVA, the piezo can compensate for 200 mbar pressure deviation → **no stress at all ?**
- Not safe nor feasible → there should be a tolerance anyway !
- Suppose that the piezo will not compensate for the pressure oscillations

- **Approach**

- Set a criteria on the maximum acceptable cavity detuning
- Translate it into pressure regulation tolerances

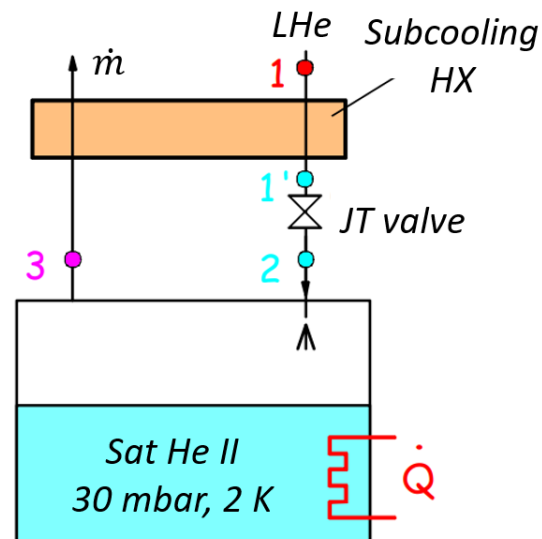


5. Automation studies on pressure and level regulations

- DSBT and GANIL teams demonstrated the advantage of an LQ over a double PID
 - In the context of a 4K LINAC

→ Same conclusion in the case of a 30 mbar bath with an additional process (subcooling + expansion) ?

- Abdelouadoud, preparing the Centrale-Supélec **ATSI Master** is taking the challenge !
- **Good point:** compared to SPIRAL2, these automation studies are starting at an earlier project phase



MOTTO

- Cryogenic availability
- Minimize the calibration work
- Minimize the electrical consumption

