



Beta Beams,
EUROnu WP4



Beta Beam's Collective Effect Study

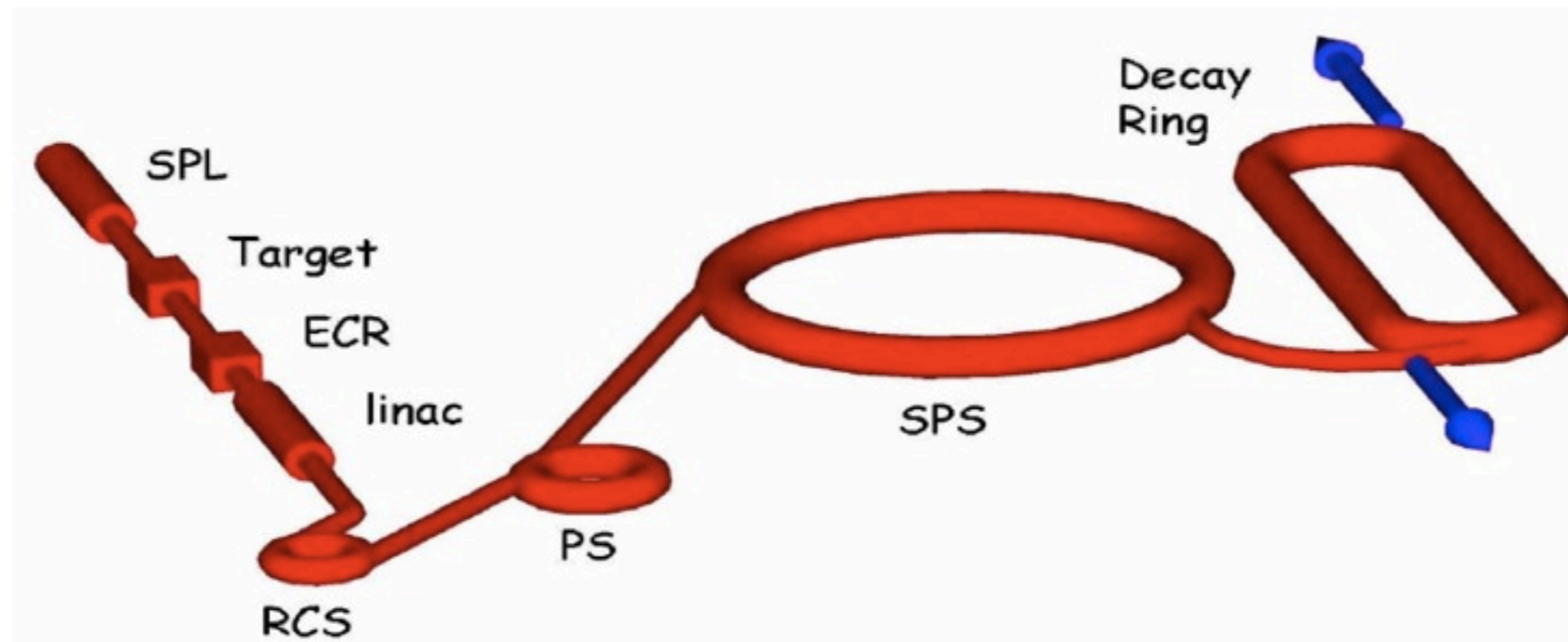


Christian Hansen
EUROν MEETING 2010/06/02

Many thanks to: E. Benedetto, A. Chancé, E. Metral, G. Rumolo & B. Salvant

Introduction

- Beta Beam's physics reach is optimized for high intensity ions beams with short bunch length
- Collective Effects will limit the final performance of accelerators
- Collective Effects has not yet been studied in detail for the CERN Beta Beam complex
- Plan to study all machines for all ions (FP6: ${}^6\text{He}$ & ${}^{18}\text{Ne}$, FP7: ${}^8\text{B}$ & ${}^8\text{Li}$)
 - So far focused on the Decay Ring for ${}^6\text{He}$ and ${}^{18}\text{Ne}$
 - Results shown are based on FP6 design (FP6 database) with some edited values



Outline

- Direct Space Charge & Laslett's Tune Shift
- Transverse Broad Band Resonance:
 - Transverse Mode Coupling Instabilities (TMCI) Limit
 - HeadTail Results
- Longitudinal Broad Band Resonance:
 - Longitudinal Parameters
 - Microwave Instabilities Limits
 - HeadTail Results

Laslett's Tune Shifts



- Laslett's Tune Shifts take into account both DSC and Image Fields:
 - A particle in a bunch feels the collective Coulomb forces due to fields generated by the charge of other particles in the bunch → Direct Space Charge (DSC) → tune shift
 - Also Image Fields due to the surrounding vacuum pipe cause tune shift
- Grouped into Incoherent and Coherent (DSC only Incoherent) where the coherent tune shifts are due to either Penetrating or Non-Penetrating Fields

- **Incoherent Tune Shift**

$$\Delta Q_{x,y}^{incoh} = -\frac{Nr_0R}{\pi\gamma\beta^2Q_{x,y}} \left[\left(\frac{1-\beta^2}{B} + \beta^2 \right) \frac{\epsilon_{x,y}^{incoh}}{h^2} + \frac{1-\beta^2}{2B} \frac{\epsilon_{x,y}^{dsc}}{a_y^2} \right]$$

Here added 1/2B myself, see backup slides

- **Coherent Tune Shift using Penetrating Magnetic Fields**

$$\Delta Q_{x,y}^{coh} = -\frac{Nr_0R}{\pi\gamma\beta^2Q_{x,y}} \left(\frac{1-\beta^2}{B} + \beta^2 \right) \frac{\epsilon_{x,y}^{coh}}{h^2}$$

Here, neglected χ_e and \mathcal{F} (see Ng.)

- **Coherent Tune Shift using Non-Penetrating Magnetic Fields**

$$\Delta Q_{x,y}^{coh} = -\frac{Nr_0R}{\pi\gamma\beta^2Q_{x,y}} \left[\frac{1-\beta^2}{B} \frac{\epsilon_{x,y}^{coh}}{h^2} + \beta^2 \frac{\epsilon_{x,y}^{incoh}}{h^2} \right]$$

K. Y. Ng
Physics of Intensity
Dependent Instabilities
USPAS 2002

Laslett's Tune Shifts

- The absolute value of the tune shifts should be < 0.2

SC	DR ^{18}Ne	DR ^6He
ΔQ_{dsc_x}	-0.0409	-0.0083
ΔQ_{dsc_y}	-0.0946	-0.0192
$\Delta Q_x^{\text{incoh}}$	-0.0409	-0.0083
$\Delta Q_y^{\text{incoh}}$	-0.0946	-0.0192
$\Delta Q_x^{\text{coh p}}$	-1.7470e-04	-3.5564e-05
$\Delta Q_y^{\text{coh p}}$	-3.1937e-04	-6.5016e-05
$\Delta Q_x^{\text{coh np}}$	-6.2768e-05	-1.2765e-05
$\Delta Q_y^{\text{coh np}}$	-1.1475e-04	-2.3337e-05

- We see that the effect of the image forces are negligible relatively to DSC
- DSC is more crucial for low energy so SPS and PS might have a big DSC problem in Beta Beams ... to be studied in the future ...

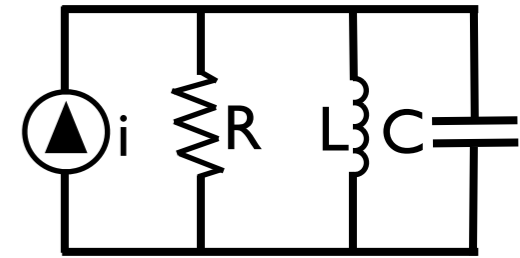
Impedances

Y.H. Chin,
Impedance and Wake
Fields

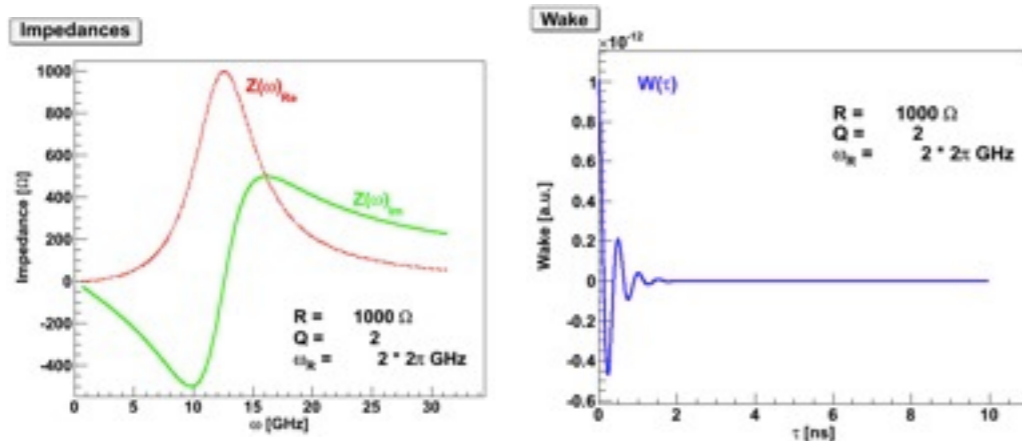
Resonance Impedance

- Wake fields can be trapped in discontinuities (e.g. cavities) in the vacuum chamber
→ resonance impedances → can be modeled with an RLC circuit:

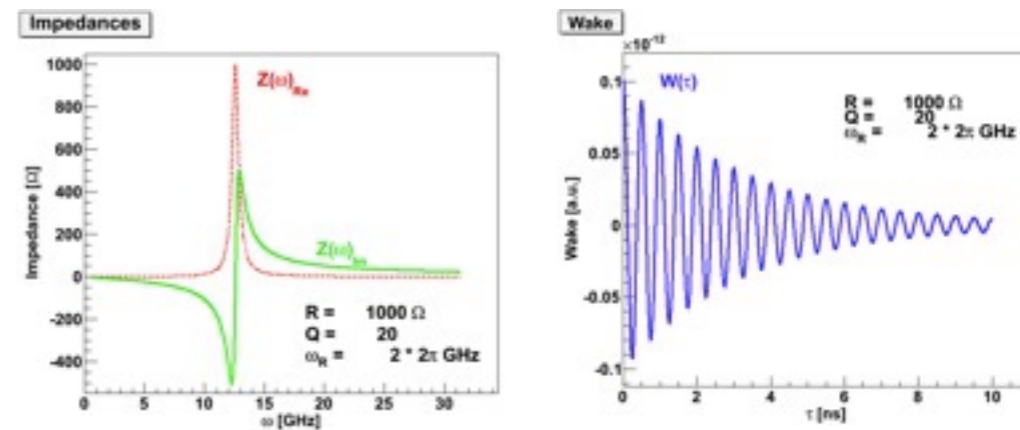
$$Z_{||}(\omega) = \frac{R_{||}}{1 + iQ \left(\frac{\omega_r}{\omega} - \frac{\omega}{\omega_r} \right)} \quad Z_{\perp}(\omega) = \frac{R_{\perp} \frac{\omega_r}{\omega}}{1 + iQ \left(\frac{\omega_r}{\omega} - \frac{\omega}{\omega_r} \right)}$$



Broad Band (low Q)



Narrow Band (high Q)

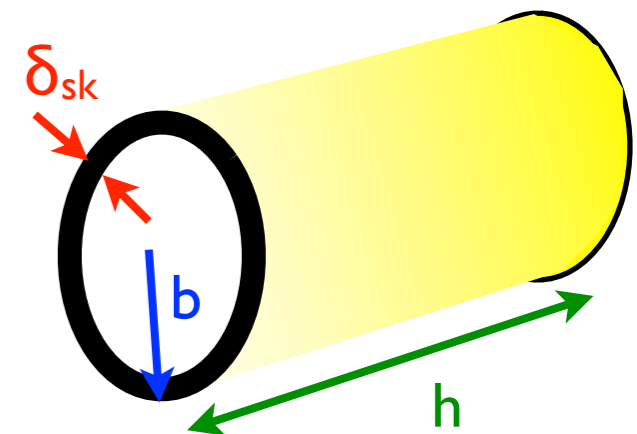


Resistive Wall Impedance

- Due to resistive beam pipe the image current is slowed down → wake field → impedance

$$Z_{||,rw}(\omega) = \frac{\omega}{2} (1 - i) \frac{Z_0 \delta_{sk}(\omega) h}{2\pi b c} \approx (1 - i) \frac{\omega R}{2bc} \sqrt{\frac{2\rho}{\epsilon_0 |\omega|}}$$

$$Z_{\perp, rw}(\omega) = (\text{sgn}(\omega) - i) \frac{Z_0 \delta_{sk}(\omega) h}{2\pi b^3} \approx (\text{sgn}(\omega) - i) \frac{R}{b^3} \sqrt{\frac{2\rho}{\epsilon_0 |\omega|}}$$

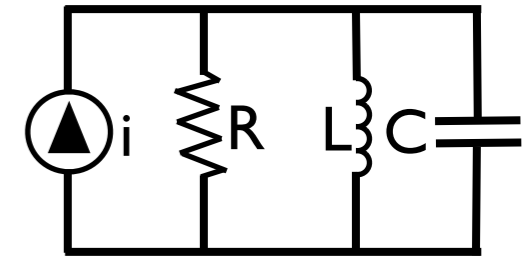


Impedances

Y.H. Chin,
Impedance and Wake
Fields

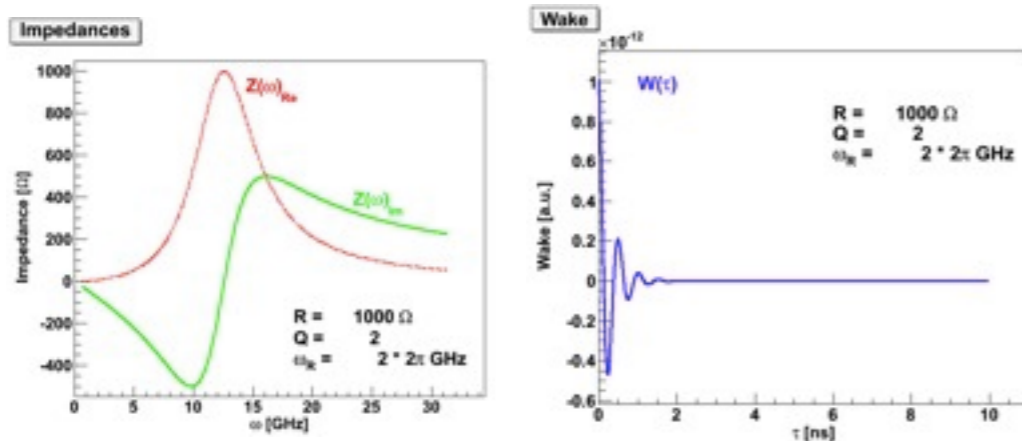
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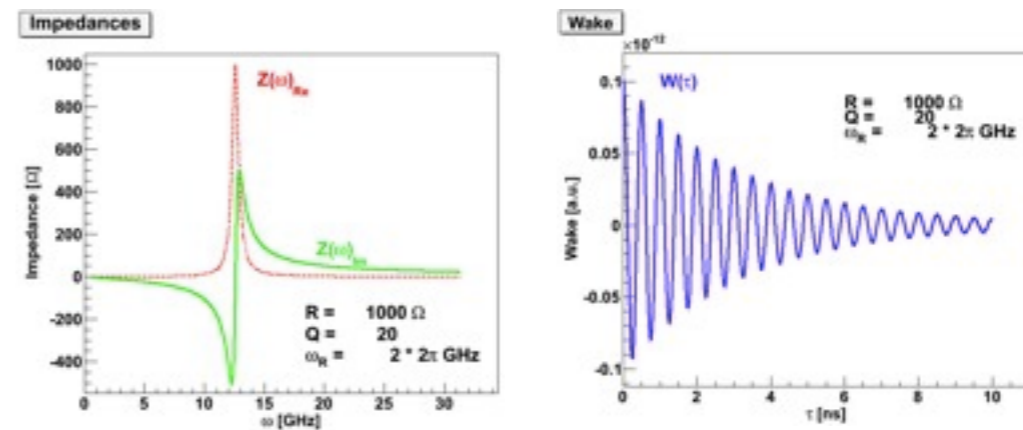


$$Z_{||}(\omega) = \frac{R_{||}}{1 + iQ \left(\frac{\omega_r}{\omega} - \frac{\omega}{\omega_r} \right)} \quad Z_{\perp}(\omega) = \frac{R_{\perp} \frac{\omega_r}{\omega}}{1 + iQ \left(\frac{\omega_r}{\omega} - \frac{\omega}{\omega_r} \right)}$$

Broad Band (low Q)



Narrow Band (high Q)

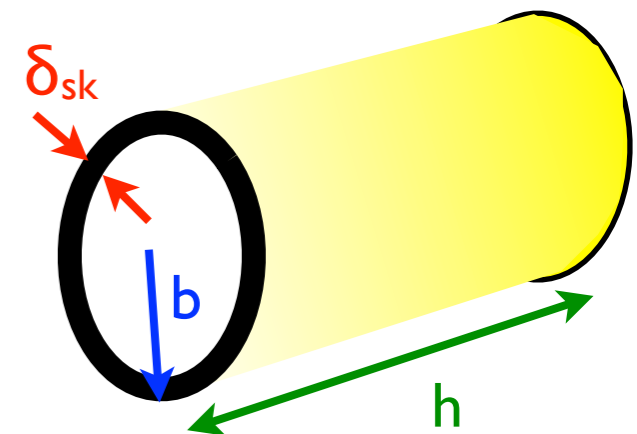


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$$Z_{\perp, rw}(\omega) = (\text{sgn}(\omega) - i) \frac{Z_0 \delta_{sk}(\omega) h}{2\pi b^3} \approx (\text{sgn}(\omega) - i) \frac{R}{b^3} \sqrt{\frac{2\rho}{\epsilon_0 |\omega|}}$$



Inputs for Broad Band Resonance Impedance

- Have assumed same values for the DR as for SPS to know how much better the DR need to be

Parameters	DR ¹⁸ Ne	DR ⁶ He
Q_{\parallel}	1.00	1.00
$\omega_{r,\parallel}$ [GHz]	6.28	6.28
$ Z_{\parallel}/n $ [Ω]	10.00	10.00
$R_{s,\parallel}$ [M Ω]	0.221	0.221
Q_{\perp}	1.00	1.00
$\omega_{r,\perp}$ [GHz]	6.28	6.28
$R_{s,\perp}$ [M Ω /m]	20.00	20.00

Inputs for Chromaticity

- Used

$$\xi_x = 0.05 \text{ and } \xi_y = 0.1 \text{ for DR where } \eta > 0$$

⊥

Transverse

TMCI Limit

- With high bunch intensity the wake fields couple the modes together so the different head-tail modes can **not** be treated separately as is done in Sacherer's Formula
- Instead a Transverse Mode Coupling Instability (TMCI) appears above a threshold for number of particles per bunch:

$$N_{b_{x,y}}^{th} = \frac{32}{3\sqrt{2}\pi} \frac{Q_{x,y} |\eta| \varepsilon_l^{2\sigma} \omega_r}{Z^2 \beta^2 c} \left(\Re \left[Z_{\perp x,y}^{BB} \right]_{max} \right)^{-1} \left(1 + \frac{\omega_{\xi_{x,y}}}{\omega_r} \right)$$

- Where $\varepsilon_l^{2\sigma} = \frac{\pi}{2} \beta^2 E_{tot} \tau_b \delta_{max}$ in eVs (for dimension analysis: Js/C)

	DR ¹⁸ Ne	DR ⁶ He
$\varepsilon_l (2\sigma)$ [eVs]	43.200	14.464
$\rho[Z_{\perp y}^{BB}]_{max}$ [$\frac{M\Omega}{m}$]	21.327	21.327
$N_B/N_{b_x}^{th}$	<u>22.859</u>	<u>4.635</u>
$N_B/N_{b_y}^{th}$	<u>41.646</u>	<u>8.445</u>

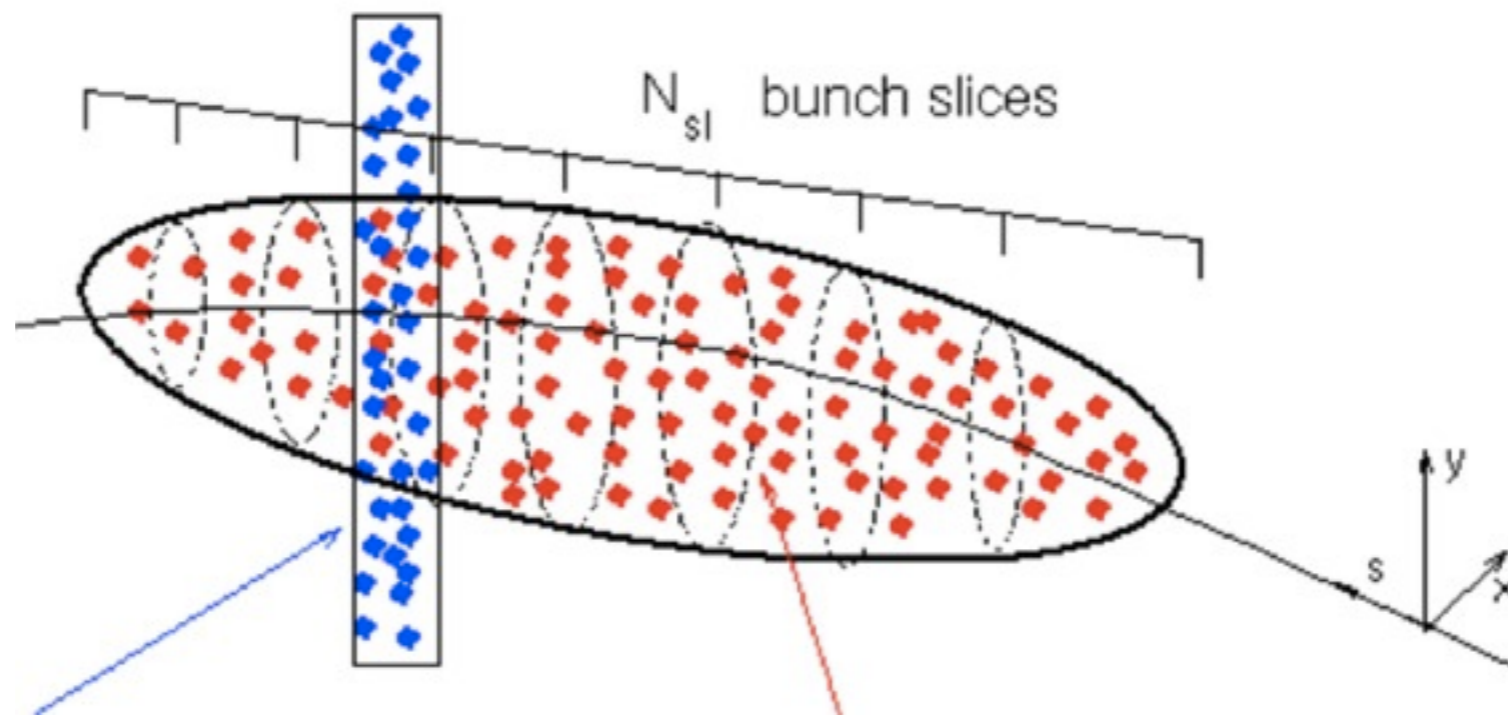
- Worst for ¹⁸Ne in DR: N_B needs to be reduced by a factor 42 OR $R_{\perp}^{DR} = R_{\perp}^{SPS}/42$
- Tried to improve N^{th}/N_B by tuning chromaticity, but didn't help (Here $|\xi_x| = 0.05$ & $|\xi_y| = 0.1$)

HEADTAIL

By Giovanni Rumolo

E. Benedetto, CERN,
Beam stability in the SPL-
Proton Driver accumulator for
a Neutrino Factory at CERN

- HEADTAIL is a multiparticle tracking code
- The bunch is sliced longitudinally
- The impedance is assumed to be localized at a few positions around the ring
- At each impedance location, each slice leaves a wake-field behind and gets a kick by the field generated by the preceding slices
- The bunch is then transferred to the next impedance location via a transport matrix



- For the Beta Beam Studies the possibility of bunches with ^{18}Ne and ^6He was added to the code

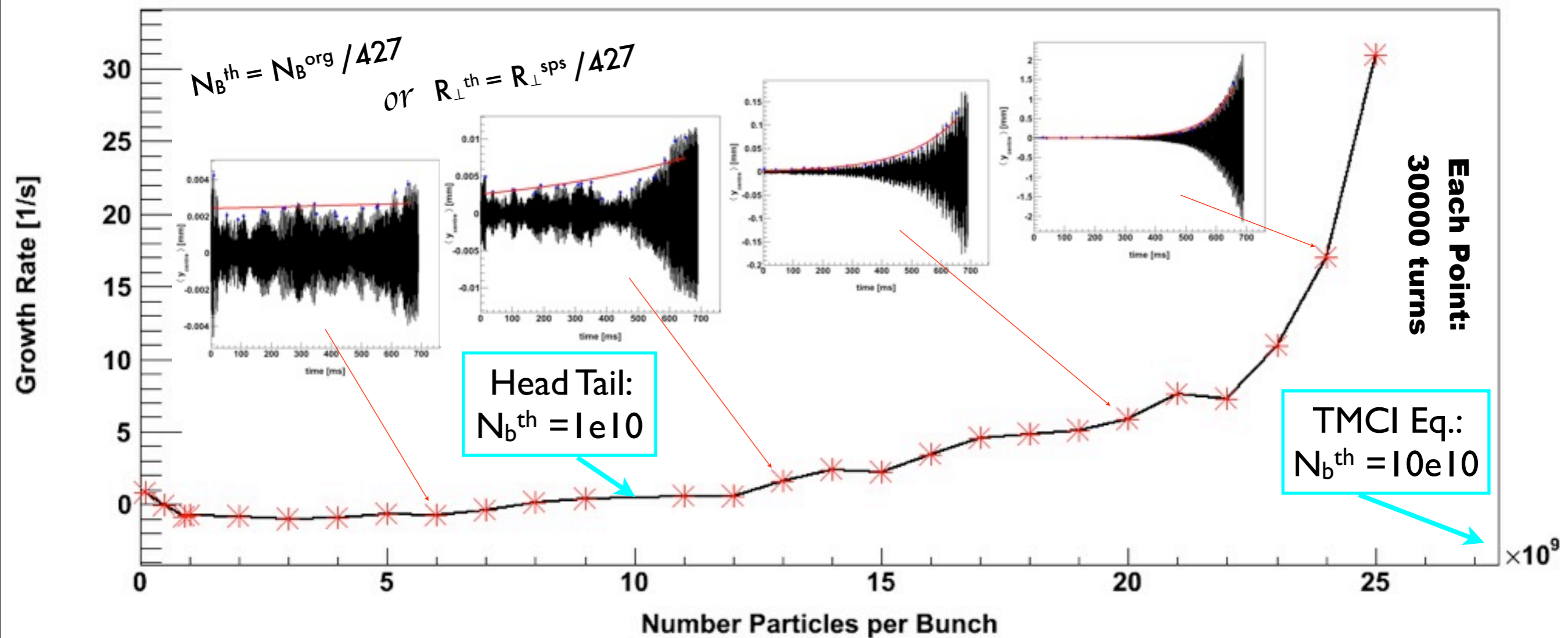
DR ^{18}Ne - Transversal Broad Band

- A Least Square Fit to the exponential gives $\langle y_c \rangle_0$ and the Growth Rate, $1/\tau$

$$\langle y_c \rangle = \langle y_c \rangle_0 e^{t/\tau}$$

- Growth Rate as a function of ion bunch intensity in the Decay Ring:

DR ^{18}Ne
 Transv. Broad Band Res.
 $N_B^{\text{org}} = 4.27\text{e}12$
 $R_{\perp}^{\text{org}} = 20 \text{ M}\Omega/\text{m}$
 $\xi_x^{\text{org}} = 0.05, \xi_y^{\text{org}} = 0.1$
 ($\eta > 0$ for DR)



- HeadTail indicates that for the current anticipated bunch intensity a 427 times smaller shunt impedance than SPS is needed for the DR

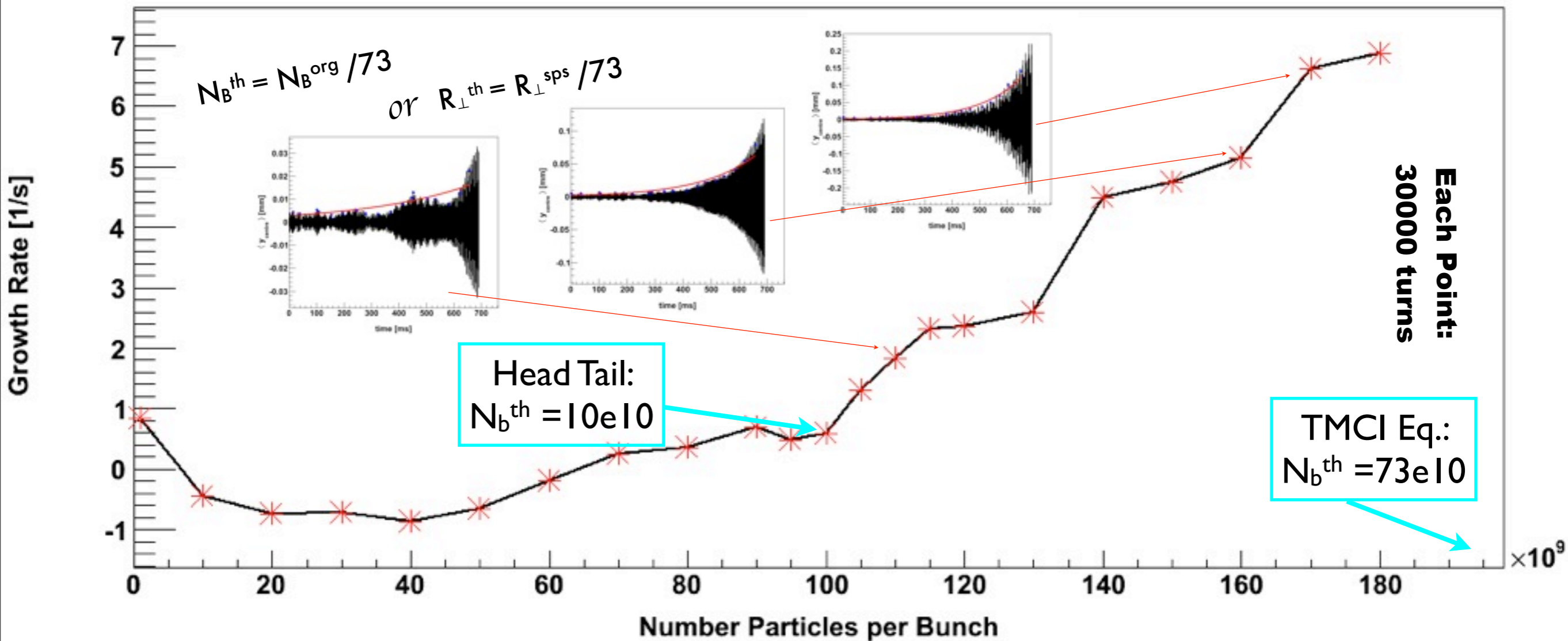
DR ${}^6\text{He}$ - Transversal Broad Band

- A Least Square Fit to the exponential gives $\langle y_c \rangle_0$ and the Growth Rate, $1/\tau$

$$\langle y_c \rangle = \langle y_c \rangle_0 e^{t/\tau}$$

- Growth Rate as a function of ion bunch intensity in the Decay Ring:

DR ${}^6\text{He}$
 Transv. Broad Band Res.
 $N_B^{\text{org}} = 7.24e12$
 $R_{\perp}^{\text{org}} = 20 \text{ M}\Omega/\text{m}$
 $\xi_x^{\text{org}} = 0.05, \xi_y^{\text{org}} = 0.1$
 ($\eta > 0$ for DR)



- HeadTail indicates that for the current anticipated bunch intensity a 73 times smaller shunt impedance than SPS is needed for the DR

||

Longitudinal

Longitudinal Parameters

- The longitudinal parameters are not clear and/or incorrect in our “FP6 database”
- Sorting things out together with Antoine Chancé
- We have succeeded quit well for the DR
- Still working on SPS; Antoine has recently done an RF simulation (with the ESME 2D program) to achieve the longitudinal parameters from SPS

Longitudinal Parameters - DR

- In the DR the reference values are the maximum momentum spread, δ_m , (due to a collimator) and the voltage, V , so we want to solve for bunch length, L_b , and emittance, ϵ_l

- In the phase-space with coordinates (Φ, δ) the synchrotron Hamiltonian is

$$H = \frac{1}{2} h \omega_{rev} \eta \delta^2 + \frac{\omega_{rev} Z e V}{2\pi \beta^2 E_{tot}} [\cos \phi - \cos \phi_s + (\phi - \phi_s) \sin \phi_s]$$

S.Y. Lee,
Accelerator Physics

- The DR is a Storage Ring so $\Phi_s = 0$ ☺

A. Chancé

- If θ_b is the maximum phase advance for a particle then that particle will pass two points: $(0, \delta_m)$ and (θ_b, δ) , and since Hamiltonian is a constant of motion $H(\Phi=0, \delta=\delta_m) = H(\Phi=\theta_b, \delta=0)$

$$-\frac{1}{2} h \omega_{rev} \eta \delta_m^2 = \frac{\omega_{rev} Z e V}{2\pi \beta^2 E_{tot}} [\cos \theta_b - 1] \quad \Rightarrow \quad \theta_b = \arccos \left[1 - \frac{\pi h \eta E_{tot} \beta^2}{Z e V} \delta_m^2 \right]$$

- Since $L_b = (2\theta_b / 2\pi) (2\pi\rho / h) = 2\rho\theta_b/h$

$$L_b = \frac{2\rho}{h} \arccos \left[1 - \frac{\pi h \eta E_{tot} \beta^2}{Z e V} \delta_m^2 \right]$$

Longitudinal Parameters - DR

- The phase space trajectory of the separatrix, that separates the phase space into inside and outside the bunch, we get by using the point $(\Phi=0, \delta=\delta_m)$ and the fact that the hamiltonian is a constant of motion, so $H(\Phi, \delta) = H(\Phi=\theta_b, \delta=0)$

$$\frac{1}{2}h\omega_{rev}\eta\delta^2 + \frac{\omega_{rev}ZeV}{2\pi\beta^2 E_{tot}} [\cos \phi - 1] = \frac{1}{2}h\omega_{rev}\eta\delta_m^2 \quad \Rightarrow \quad \delta(\phi) = \sqrt{\delta_m^2 - \frac{\omega_{rev}ZeV}{2\pi\beta^2 E_{tot}} [\cos \phi - 1]}$$

- The phase-space area of this bunch we get by

$$A = \int_0^{\theta_b} \delta(\phi) d\phi = \dots = \delta_m G \left(\frac{\theta_b}{2} \right) \quad \text{where} \quad G(\phi) = \frac{8}{\sin \phi} [E(\sin \phi) - \cos^2 \phi K(\sin \phi)]$$

A. Chancé

- To get the area in $(\Delta t, \Delta E)$ phase space, ϵ_l , from the area in (Φ, δ) phase space, A , we convert:
 $\epsilon_l = \rho/(\beta hc) \cdot \beta^2 E_{tot} A = \beta \rho E_{tot}/(hc) A$

$$\epsilon_l = \frac{\beta \rho E_{tot}}{hc} \delta_m G \left(\frac{\theta_b}{2} \right)$$

Longitudinal Parameters - DR

- For small amplitude oscillations the phase space ellipse (in the phase space (Φ, δ)) of a particle is defined by its maximum values (θ_b, δ_m) that follows the relation

$$\frac{\delta_m}{\theta_b} = \frac{Q_s}{h|\eta|}$$

S.Y.Lee,
Accelerator Physics

- Using $\theta_b = hL_b/(2\rho)$ we get the test relation that *should* be fulfilled for a matched bunch

$$\frac{\rho|\eta|\delta_m}{Q_s L_b/2} = 1$$

Longitudinal Parameters - DR

	DR ¹⁸ Ne	DR ⁶ He
δ_{\max}	2.500e-03	2.500e-03
eV [MeV]	1.196e+01	2.000e+01
$L_b^* [m] = \frac{2\rho}{h} \arccos\left(1 - \frac{\pi h \eta E_{\text{tot}} (\beta \delta_{\max})^2}{ZeV}\right)$	1.970	1.970
$\epsilon_i^* [eVs] = \frac{\beta \rho E_{\text{tot}} \delta_{\max}}{hc} G\{\theta_b/2\}$	42.947	14.358
$Q_s = \sqrt{\frac{hZeV \eta \cos\phi_s }{2\pi\beta^2 E_{\text{tot}}}}$	3.653e-03	3.653e-03
$\theta_b = \frac{hL_b}{2\rho} [\text{rad}]$	0.827	0.827
$\frac{\rho \eta \delta_{\max}^*}{Q_s L_b/2}$	0.972	0.972

Microwave Instability

- Longitudinal Broad Band Impedance, $Z_{||bb}(\omega)$, can cause internal bunch oscillations which can cause bunch lengthening and increase in energy spread
- The “Keil-Schnell Criterion“ gives an approximate upper allowed limit on number bunch particles

$$N_b^{th} = \frac{2\pi\beta^2|\eta|E_{tot}F}{Z^2e^2\left|\frac{Z_{||}}{n}\right|} \left(\frac{\delta_{max}}{2}\right)^2 \frac{\tau_b}{4}$$

S.Y. Lee,
Accelerator Physics

	DR ¹⁸ Ne	DR ⁶ He
σ_δ	1.250e-03	1.250e-03
τ_b [ns]	6.572	6.572
$\left \frac{Z_{ }}{n}\right $ [Ω]	10.000	10.000
N_b^{th}	2.146e+11	1.794e+12
N_B/N_b^{th}	<u>19.881</u>	<u>4.038</u>

- For ¹⁸Ne in DR: N_B needs to be reduced by a factor 20 OR $R_{||}^{DR} = R_{||}^{SPS}/20$

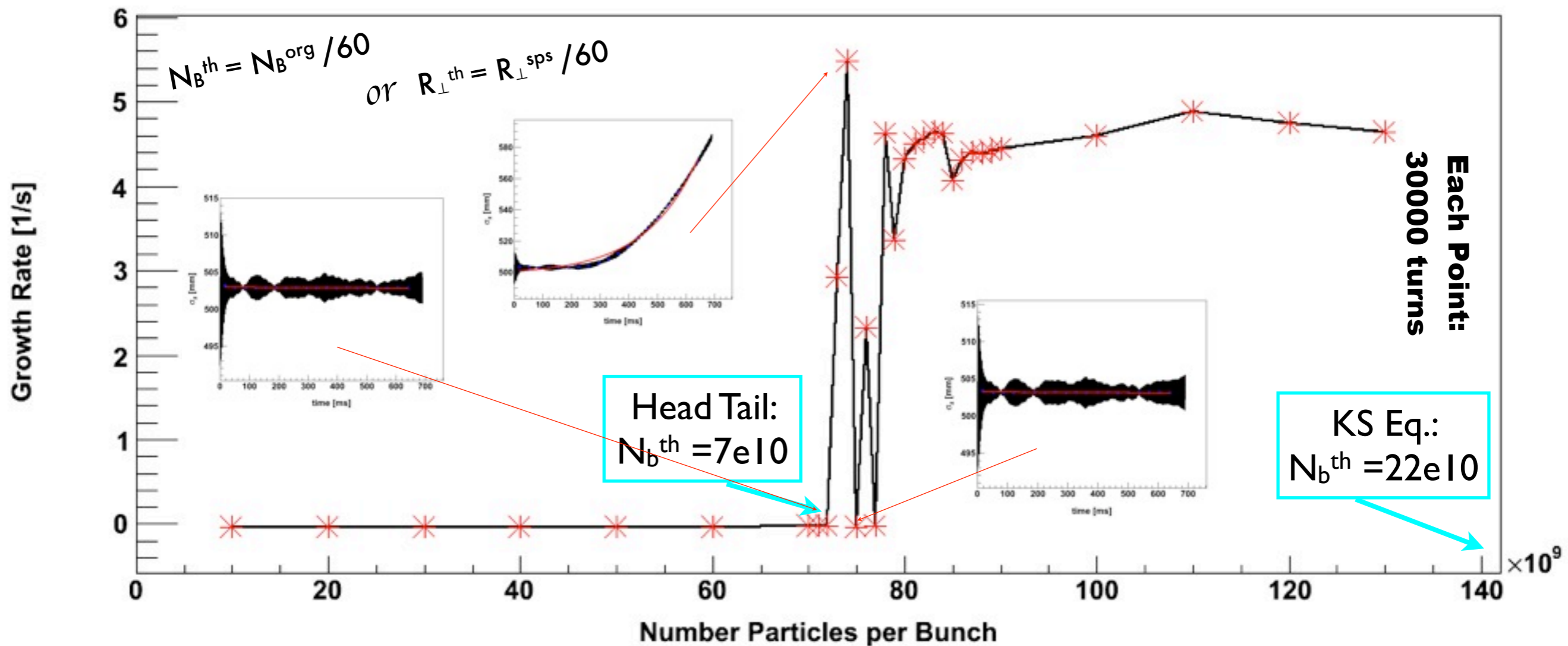
DR ^{18}Ne - Longitudinal Broad Band

- A Least Square Fit to the exponential gives σ_0 and the Growth Rate, $1/\tau$

$$\sigma_z = \sigma_0 e^{t/\tau}$$

- Growth Rate as a function of ion bunch intensity in the Decay Ring:

DR ^{18}Ne
 Long. Broad Band Res.
 $N_B^{\text{org}} = 4.27e12$
 $R_{\parallel}^{\text{org}} = 0.2 \text{ M}\Omega$
 $\xi_x^{\text{org}} = 0.05, \xi_y^{\text{org}} = 0.1$
 ($\eta > 0$ for DR)



- HeadTail indicates that for the current anticipated bunch intensity a 60 times smaller longitudinal shunt impedance than SPS is needed for the DR

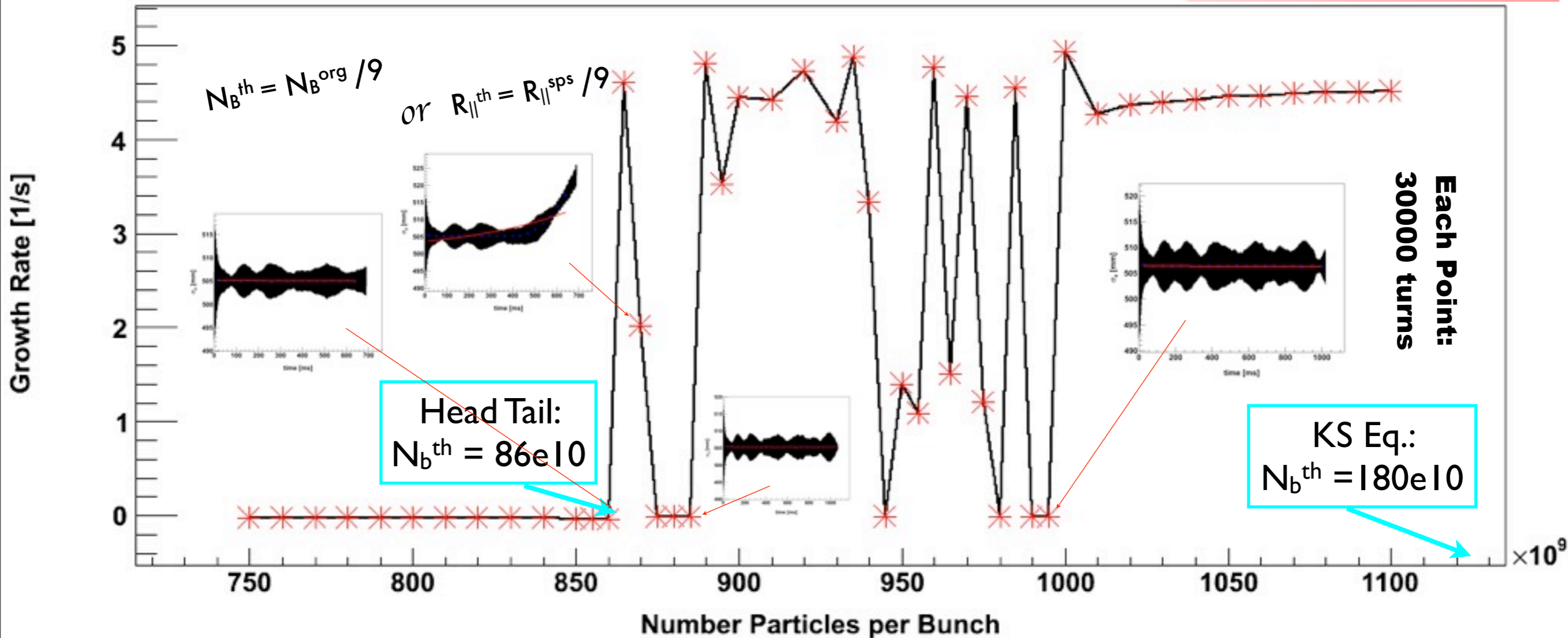
DR ${}^6\text{He}$ - Longitudinal Broad Band

- A Least Square Fit to the exponential gives σ_0 and the Growth Rate, $1/\tau$

$$\sigma_z = \sigma_0 e^{t/\tau}$$

- Growth Rate as a function of ion bunch intensity in the Decay Ring:

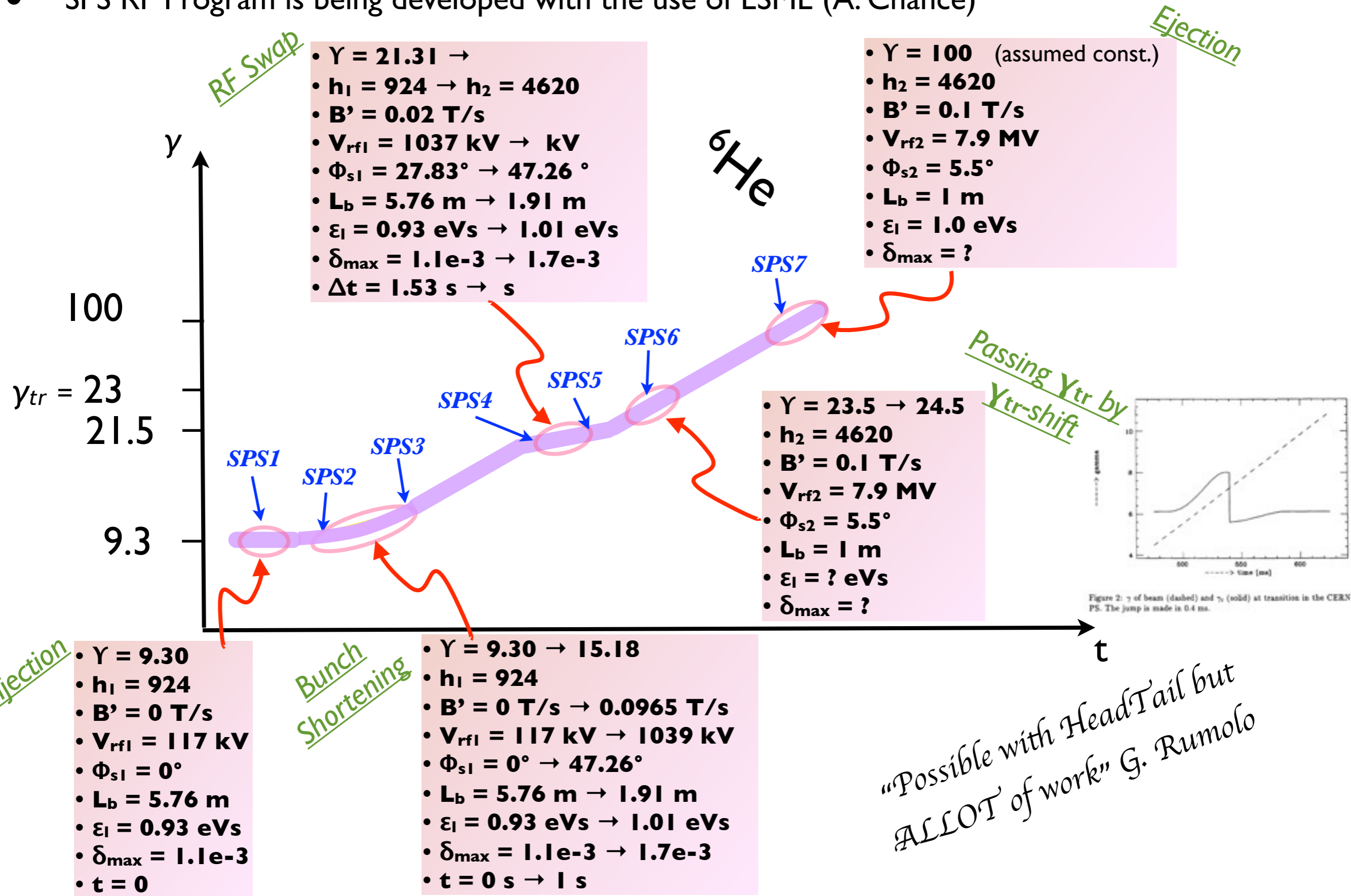
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 Long. Broad Band Res.
 $N_B^{\text{org}} = 7.24e12$
 $R_{||}^{\text{org}} = 0.2 \text{ M}\Omega$
 $\xi_x^{\text{org}} = 0.05, \xi_y^{\text{org}} = 0.1$
 ($\eta > 0$ for DR)



- HeadTail indicates that for the current anticipated bunch intensity a 9 times smaller longitudinal shunt impedance than SPS is needed for the DR
- Will do head-tail mode coupling and decoupling analysis to explain this behavior

Longitudinal Parameters - SPS

- SPS RF Program is being developed with the use of ESME (A. Chancé)



Conclusions

- According to HEADTAIL simulations the DR have to have
 - 430 times better transversal shunt impedance than SPS (^{18}Ne) and
 - 60 times better longitudinal shunt impedance than SPS (^{18}Ne)

To Do

- Finish the SPS RF program with ESME simulations
- Study the instabilities at some crucial parts in the SPS RF cycle
- Include other instabilities like those due to Resistive Wall Impedance
- Try to improve Beta Beam's result by tuning the chromaticity
- If result does not improve allot:
 - Redesign the Beta Beam - N_B , γ_{tr} , ...
 - Study impact on physics reach

Backup Slides

Input Values (I)

Parameters	SPS Inj. ¹⁸ Ne	SPS Inj. ⁶ He	SPS3 ¹⁸ Ne	SPS3 ⁶ He	SPS4 ¹⁸ Ne	SPS4 ⁶ He
Z	10	2	10	2	10	2
A	18	6	18	6	18	6
h	924	924	924	924	924	924
C [m]	6911.6	6911.6	6911.6	6911.6	6911.6	6911.6
γ_{tr}	24.0	24.0	24.0	24.0	24.0	24.0
V_{RF} [MV]	5.646e-03	1.166e-01	1.000e+00	1.000e+00	1.000e+00	1.000e+00
dB/dt [T/s]	0.00	0.00	0.10	0.10	0.02	0.02
γ	15.5	9.3	13.0	13.0	21.5	21.5
δ_{max}	2.37e-04	5.37e-04	1.67e-03	1.67e-03	1.67e-03	1.67e-03
E_{rest} [MeV]	16767.10	5605.54	16767.10	5605.54	16767.10	5605.54
M	20	20	20	20	20	20
L_b [m]	5.984	5.984	1.197	1.197	1.197	1.197
N_b	2.48e+11	7.15e+11	2.45e+11	6.75e+11	2.45e+11	6.75e+11
N_m	1	1	1	1	1	1
t_{1/2} [s]	1.67	0.81	1.67	0.81	1.67	0.81
T_c [s]	3.60	6.00	3.60	6.00	3.60	6.00
Q_x	26.13	26.13	26.13	26.13	26.13	26.13
Q_y	26.18	26.18	26.18	26.18	26.18	26.18
$\langle \beta \rangle_x$ [m]	54.55	54.55	54.55	54.55	54.55	54.55
$\langle \beta \rangle_y$ [m]	54.59	54.59	54.59	54.59	54.59	54.59
$\langle D \rangle_x$ [m]	1.83	1.83	1.83	1.83	1.83	1.83
ξ_x	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05
ξ_y	-0.10	-0.10	-0.10	-0.10	-0.10	-0.10
ϵ_{N_x} (1σ) [πm·rad]	1.23e-05	1.23e-05	1.23e-05	1.23e-05	1.23e-05	1.23e-05
ϵ_{N_y} (1σ) [πm·rad]	6.60e-06	6.60e-06	6.60e-06	6.60e-06	6.60e-06	6.60e-06
ϵ_l (full) [eVs]	1.76	0.80	0.90	0.90	0.90	0.90
b_x [cm]	28.4	28.4	28.4	28.4	28.4	28.4
b_y [cm]	6.9	6.9	6.9	6.9	6.9	6.9
ρ [Ωm]	1.0e-07	1.0e-07	1.0e-07	1.0e-07	1.0e-07	1.0e-07

Input Values (2)

Parameters	SPS5 ¹⁸ Ne	SPS5 ⁶ He	SPS6 ¹⁸ Ne	SPS6 ⁶ He
Z	10	2	10	2
A	18	6	18	6
h	4620	4620	4620	4620
C [m]	6911.6	6911.6	6911.6	6911.6
γ_{tr}	24.0	24.0	24.0	24.0
V_{RF} [MV]	7.900e+00	7.900e+00	7.900e+00	7.900e+00
dB/dt [T/s]	0.02	0.02	0.10	0.10
γ	21.5	21.5	23.5	23.5
δ_{max}	1.67e-03	1.67e-03	1.67e-03	1.67e-03
E_{rest} [MeV]	16767.10	5605.54	16767.10	5605.54
M	20	20	20	20
L_b [m]	1.197	1.197	1.197	1.197
N_b	2.45e+11	6.75e+11	2.45e+11	6.75e+11
N_m	1	1	1	1
$t_{1/2}$ [s]	1.67	0.81	1.67	0.81
T_c [s]	3.60	6.00	3.60	6.00
Q_x	26.13	26.13	26.13	26.13
Q_y	26.18	26.18	26.18	26.18
$\langle \beta \rangle_x$ [m]	54.55	54.55	54.55	54.55
$\langle \beta \rangle_y$ [m]	54.59	54.59	54.59	54.59
$\langle D \rangle_x$ [m]	1.83	1.83	1.83	1.83
ξ_x	-0.05	-0.05	-0.05	-0.05
ξ_y	-0.10	-0.10	-0.10	-0.10
ϵ_{N_x} (1 σ) [π m·rad]	1.23e-05	1.23e-05	1.23e-05	1.23e-05
ϵ_{N_y} (1 σ) [π m·rad]	6.60e-06	6.60e-06	6.60e-06	6.60e-06
ϵ_l (full) [eVs]	0.90	0.90	0.90	0.90
b_x [cm]	28.4	28.4	28.4	28.4
b_y [cm]	6.9	6.9	6.9	6.9
ρ [Ω m]	1.0e-07	1.0e-07	1.0e-07	1.0e-07

Input Values (3)

Parameters	SPS Ej. ^{18}Ne	SPS Ej. ^6He	DR ^{18}Ne	DR ^6He
Z	10	2	10	2
A	18	6	18	6
h	4620	4620	924	924
C [m]	6911.6	6911.6	6911.6	6911.6
γ_{tr}	24.0	24.0	27.0	27.0
V_{RF} [MV]	7.900e+00	7.900e+00	1.196e+01	2.000e+01
dB/dt [T/s]	0.10	0.10	0.00	0.00
γ	100.0	100.0	100.0	100.0
δ_{max}	4.73e-04	1.07e-03	2.50e-03	2.50e-03
E_{rest} [MeV]	16767.10	5605.54	16767.10	5605.54
M	20	20	20	20
L_b [m]	1.197	1.197	1.967	1.970
N_b	2.45e+11	6.75e+11	2.45e+11	6.75e+11
N_m	1	1	20	15
t_{1/2} [s]	1.67	0.81	1.67	0.81
T_c [s]	3.60	6.00	3.60	6.00
Q_x	26.13	26.13	22.23	22.23
Q_y	26.18	26.18	12.16	12.16
$\langle \beta \rangle_x$ [m]	54.55	54.55	148.25	148.25
$\langle \beta \rangle_y$ [m]	54.59	54.59	173.64	173.64
$\langle D \rangle_x$ [m]	1.83	1.83	-0.60	-0.60
ξ_x	1.00	0.05	0.05	0.05
ξ_y	1.00	0.10	0.10	0.10
ϵ_{N_x} (1 σ) [$\pi\text{m}\cdot\text{rad}$]	1.23e-05	1.23e-05	1.48e-05	1.48e-05
ϵ_{N_y} (1 σ) [$\pi\text{m}\cdot\text{rad}$]	6.60e-06	6.60e-06	7.90e-06	7.90e-06
ϵ_i (full) [eVs]	2.20	1.00	42.89	14.36
b_x [cm]	28.4	28.4	16.0	16.0
b_y [cm]	6.9	6.9	16.0	16.0
ρ [Ωm]	1.0e-07	1.0e-07	1.0e-07	1.0e-07

Calculated Values (I)

	SPS Inj. ¹⁸ Ne	SPS Inj. ⁶ He	SPS3 ¹⁸ Ne	SPS3 ⁶ He	SPS4 ¹⁸ Ne	SPS4 ⁶ He
$N_B = N_b \frac{1-2^{-N_m T_c / (\gamma t_{1/2})}}{1-2^{-T_c / (\gamma t_{1/2})}}$	2.48e+11	7.15e+11	2.45e+11	6.75e+11	2.45e+11	6.75e+11
$r_0 [m] = r_p Z^2/A$	8.53e-18	1.02e-18	8.53e-18	1.02e-18	8.53e-18	1.02e-18
$E_{tot} [GeV] = \gamma \cdot E_{rest}$	260.39	52.30	217.97	72.87	360.49	120.52
$\beta = \sqrt{1-1/\gamma^2}$	1.00	0.99	1.00	1.00	1.00	1.00
$\eta = \{1/\gamma_{tr}\}^2 - \{1/\gamma\}^2$	-2.41e-03	-9.75e-03	-4.18e-03	-4.18e-03	-4.27e-04	-4.27e-04
$T_{rev} [ms] = C/(\beta c)$	23.1026	23.1882	23.1231	23.1231	23.0796	23.0796
$\omega_{rev} [MHz] = 2\pi/T_{rev}$	0.27	0.27	0.27	0.27	0.27	0.27
$\sigma_\delta = \delta_{max}/2$	1.19e-04	2.69e-04	8.34e-04	8.34e-04	8.34e-04	8.34e-04
$\tau_b [ns] = L_b / (\beta c)$	20.00	20.08	4.00	4.00	4.00	4.00
$I_b [A] = ZeN_B / \tau_b$	19.87	11.41	98.02	54.01	98.20	54.11
$\varepsilon_1^{2\sigma} [eVs] = \frac{\pi}{2} \beta^2 E_{tot} \tau_b \delta_{max}$	1.93	0.88	2.27	0.76	3.77	1.26
$\omega_s [kHz] = Q_s \cdot \omega_{rev}$	0.08	0.69	1.17	0.90	0.36	0.28
$\omega_x [MHz] = Q_x \cdot \omega_{rev}$	7.11	7.08	7.10	7.10	7.11	7.11
$\omega_y [MHz] = Q_y \cdot \omega_{rev}$	7.12	7.10	7.12	7.12	7.13	7.13
$\omega_c [GHz] = \beta c / b_{\min(x,y)}$	4.34	4.32	4.33	4.33	4.34	4.34
$\Delta Q_{\xi_x} = \xi_x \delta_{max} Q_x$	-3.10e-04	-7.02e-04	-2.18e-03	-2.18e-03	-2.18e-03	-2.18e-03
$\Delta Q_{\xi_y} = \xi_y \delta_{max} Q_y$	-6.21e-04	-1.41e-03	-4.37e-03	-4.37e-03	-4.37e-03	-4.37e-03

Calculated Values (2)

	SPS5 ¹⁸ Ne	SPS5 ⁶ He	SPS6 ¹⁸ Ne	SPS6 ⁶ He
$N_B = N_b \frac{1-2^{-N_m T_c / (\gamma t_{1/2})}}{1-2^{-T_c / (T_{1/2})}}$	2.45e+11	6.75e+11	2.45e+11	6.75e+11
$r_0 \text{ [m]} = r_p Z^2 / A$	8.53e-18	1.02e-18	8.53e-18	1.02e-18
$E_{\text{tot}} \text{ [GeV]} = \gamma \cdot E_{\text{rest}}$	360.49	120.52	394.03	131.73
$\beta = \sqrt{1-1/\gamma^2}$	1.00	1.00	1.00	1.00
$\eta = \{1/\gamma_{tr}\}^2 - \{1/\gamma\}^2$	-4.27e-04	-4.27e-04	-7.47e-05	-7.47e-05
$T_{\text{rev}} \text{ [ms]} = C/(\beta c)$	23.0796	23.0796	23.0755	23.0755
$\omega_{\text{rev}} \text{ [MHz]} = 2 \pi / T_{\text{rev}}$	0.27	0.27	0.27	0.27
$\sigma_\delta = \delta_{\text{max}} / 2$	8.34e-04	8.34e-04	8.34e-04	8.34e-04
$\tau_b \text{ [ns]} = L_b / (\beta c)$	4.00	4.00	4.00	4.00
$I_b \text{ [A]} = Ze N_B / \tau_b$	98.20	54.11	98.22	54.12
$\xi_1^2 \text{ [eVs]} = \frac{\pi}{2} \beta^2 E_{\text{tot}} \tau_b \delta_{\text{max}}$	3.77	1.26	4.12	1.38
$\omega_s \text{ [kHz]} = Q_s \cdot \omega_{\text{rev}}$	2.26	1.75	0.90	0.70
$\omega_x \text{ [MHz]} = Q_x \cdot \omega_{\text{rev}}$	7.11	7.11	7.11	7.11
$\omega_y \text{ [MHz]} = Q_y \cdot \omega_{\text{rev}}$	7.13	7.13	7.13	7.13
$\omega_c \text{ [GHz]} = \beta c / b_{\text{min}(x,y)}$	4.34	4.34	4.34	4.34
$\Delta Q_{\xi_x} = \xi_x \delta_{\text{max}} Q_x$	-2.18e-03	-2.18e-03	-2.18e-03	-2.18e-03
$\Delta Q_{\xi_y} = \xi_y \delta_{\text{max}} Q_y$	-4.37e-03	-4.37e-03	-4.37e-03	-4.37e-03

Calculated Values (3)

	SPS Ej. ^{18}Ne	SPS Ej. ^6He	DR ^{18}Ne	DR ^6He
$N_B = N_b \frac{1-2^{-N_m T_c / (\gamma t_{1/2})}}{1-2^{-T_c / (\gamma t_{1/2})}}$	2.45e+11	6.75e+11	4.27e+12	7.24e+12
$r_0 \text{ [m]} = r_p Z^2 / A$	8.53e-18	1.02e-18	8.53e-18	1.02e-18
$E_{\text{tot}} \text{ [GeV]} = \gamma \cdot E_{\text{rest}}$	1676.71	560.55	1676.71	560.55
$\beta = \sqrt{1-1/\gamma^2}$	1.00	1.00	1.00	1.00
$\eta = \{1/\gamma_{\text{tr}}\}^2 - \{1/\gamma\}^2$	1.64e-03	1.64e-03	1.27e-03	1.27e-03
$T_{\text{rev}} \text{ [ms]} = C/(\beta c)$	23.0558	23.0558	23.0558	23.0558
$\omega_{\text{rev}} \text{ [MHz]} = 2\pi/T_{\text{rev}}$	0.27	0.27	0.27	0.27
$\sigma_\delta = \delta_{\text{max}}/2$	2.37e-04	5.34e-04	1.25e-03	1.25e-03
$\tau_b \text{ [ns]} = L_b / (\beta c)$	3.99	3.99	6.56	6.57
$I_b \text{ [A]} = ZeN_B / \tau_b$	98.31	54.17	1041.99	353.19
$\xi_1^{2\sigma} \text{ [eVs]} = \frac{\pi}{2} \beta^2 E_{\text{tot}} \tau_b \delta_{\text{max}}$	4.98	3.75	43.20	14.46
$\omega_s \text{ [kHz]} = Q_s \cdot \omega_{\text{rev}}$	2.05	1.58	1.00	1.00
$\omega_x \text{ [MHz]} = Q_x \cdot \omega_{\text{rev}}$	7.12	7.12	6.06	6.06
$\omega_y \text{ [MHz]} = Q_y \cdot \omega_{\text{rev}}$	7.14	7.14	3.31	3.31
$\omega_c \text{ [GHz]} = \beta c / b_{\text{min}(x,y)}$	4.34	4.34	1.87	1.87
$\Delta Q_{\xi_x} = \xi_{sx} \delta_{\text{max}} Q_x$	1.24e-02	1.40e-03	2.78e-03	2.78e-03
$\Delta Q_{\xi_y} = \xi_{sy} \delta_{\text{max}} Q_y$	1.24e-02	2.80e-03	3.04e-03	3.04e-03

RF Values - No Acc.

	SPS Inj. ¹⁸ Ne	SPS Inj. ⁶ He	DR ¹⁸ Ne	DR ⁶ He
$(\delta_{\max})^* = \frac{h\epsilon_1 c}{\rho E_{\text{tot}} G\{\theta_b/2\}}$	2.373e-04	5.370e-04	-	-
δ_{\max}	2.373e-04	5.370e-04	2.500e-03	2.500e-03
$eV^* [\text{MeV}] = \frac{\pi h \eta E_{\text{tot}} \{\beta \delta_{\max}\}^2}{Z(1-\cos\theta_b)}$	5.646e-03	1.166e-01	-	-
$eV [\text{MeV}]$	5.646e-03	1.166e-01	1.196e+01	2.000e+01
$L_b^* [\text{m}] = \frac{2\rho}{h} \arccos\left(1 - \frac{\pi h \eta E_{\text{tot}} (\beta \delta_{\max})^2}{ZeV}\right)$	-	-	1.970	1.970
$L_b [\text{m}]$	5.984	5.984	1.967	1.970
$\epsilon_1^* [\text{eVs}] = \frac{\beta \rho E_{\text{tot}} \delta_{\max}}{hc} G\{\theta_b/2\}$	-	-	42.883	14.358
$\epsilon_1 [\text{eVs}]$	1.760	0.800	42.890	14.360
$Q_s = \sqrt{\frac{hZeV \eta \cos\phi_s }{2\pi\beta^2 E_{\text{tot}}}}$	2.778e-04	2.543e-03	3.653e-03	3.653e-03
$\theta_b = \frac{hL_b}{2\rho} [\text{rad}]$	2.513	2.513	0.826	0.827
$\frac{\rho \eta \delta_{\max}^*}{Q_s L_b / 2}$	0.757	0.757	0.973	0.972

RF Values - Acc. (I)

	SPS3 ¹⁸ Ne	SPS3 ⁶ He	SPS4 ¹⁸ Ne	SPS4 ⁶ He
$(\delta_{\max})^* = ?$??	??	??	??
δ_{\max}	1.668e-03	1.668e-03	1.668e-03	1.668e-03
$eV^* [\text{MeV}] = ?$??	??	??	??
$eV [\text{MeV}]$	1.000e+00	1.000e+00	1.000e+00	1.000e+00
$L_b^* [\text{m}] = ?$??	??	??	??
$L_b [\text{m}]$	1.197	1.197	1.197	1.197
$\epsilon_i^* [\text{eVs}] = ?$??	??	??	??
$\epsilon_i [\text{eVs}]$	0.900	0.900	0.900	0.900
$\phi_s [^\circ] = \text{asin}\left(\frac{2\pi\rho^2 B'(t)}{V_{rf}}\right)$	49.49	49.49	8.75	8.75
$Q_s = \sqrt{\frac{hZeV \eta\cos\phi_s }{2\pi\beta^2 E_{\text{tot}}}}$	4.293e-03	3.321e-03	1.314e-03	1.016e-03
$\theta_b = \frac{hL_b}{2\rho} [\text{rad}]$	0.503	0.503	0.503	0.503
$\frac{\rho \eta \delta_{\max}^*}{Q_s L_b/2}$	2.986	3.860	0.997	1.289

RF Values - Acc. (2)

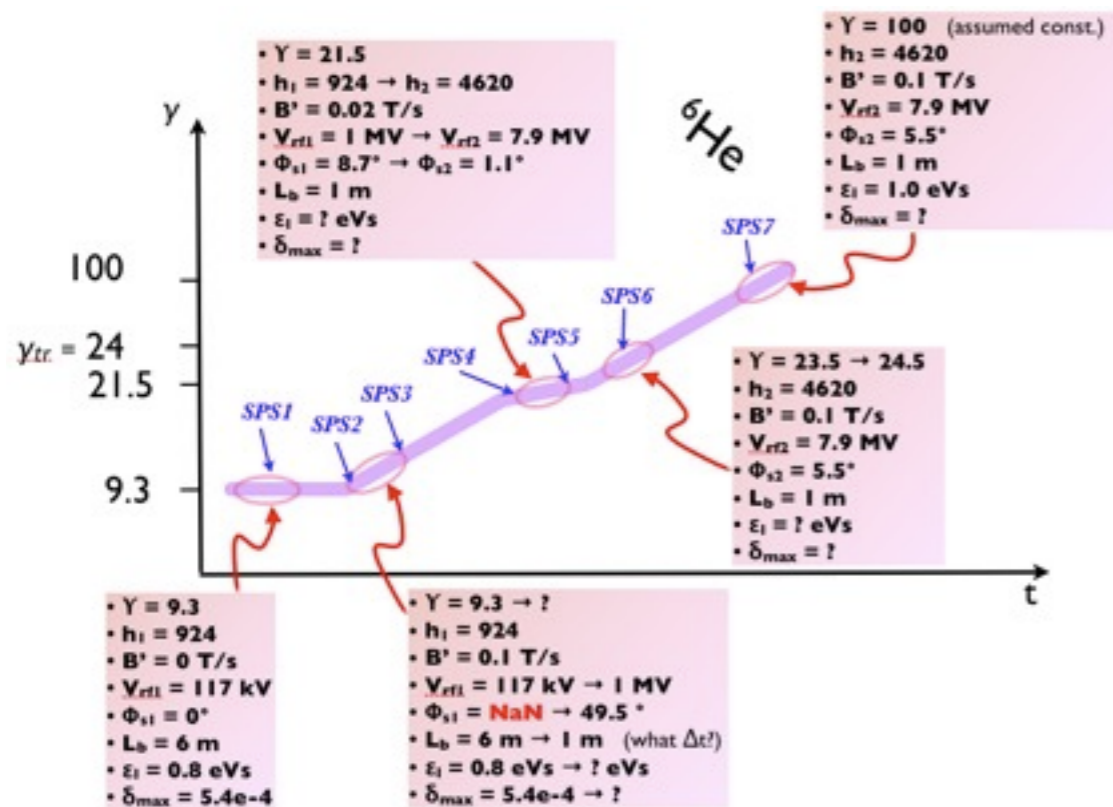
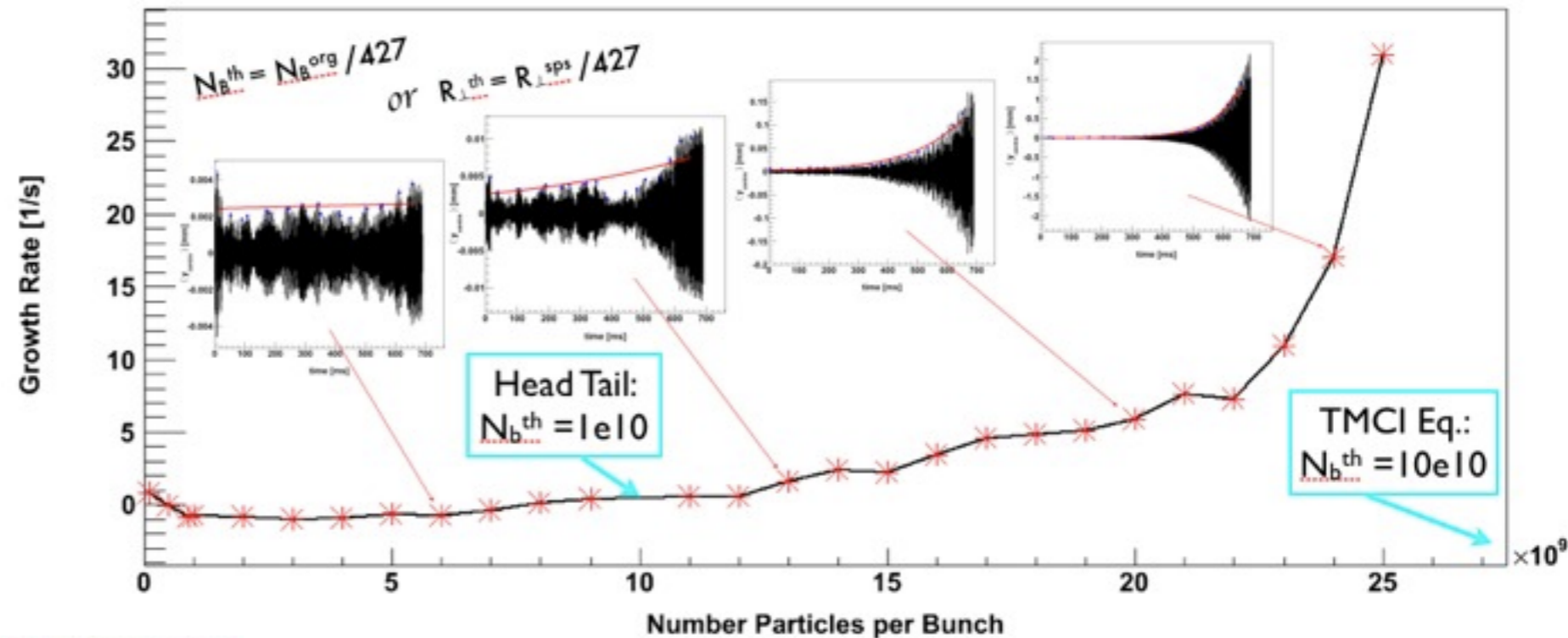
	SPS5 ¹⁸ Ne	SPS5 ⁶ He	SPS6 ¹⁸ Ne	SPS6 ⁶ He	SPS Ej. ¹⁸ Ne	SPS Ej. ⁶ He
$(\delta_{\max})^{\circ} = ?$??	??	??	??	??	??
δ_{\max}	1.668e-03	1.668e-03	1.668e-03	1.668e-03	4.734e-04	1.068e-03
$eV^{\circ} [\text{MeV}] = ?$??	??	??	??	??	??
$eV [\text{MeV}]$	7.900e+00	7.900e+00	7.900e+00	7.900e+00	7.900e+00	7.900e+00
$L_b^{\circ} [\text{m}] = ?$??	??	??	??	??	??
$L_b [\text{m}]$	1.197	1.197	1.197	1.197	1.197	1.197
$\epsilon_i^{\circ} [\text{eVs}] = ?$??	??	??	??	??	??
$\epsilon_i [\text{eVs}]$	0.900	0.900	0.900	0.900	2.200	1.000
$\phi_s [\text{°}] = \text{asin}\left(\frac{2\pi\rho^2 B'(t)}{V_{rf}}\right)$	1.10	1.10	5.52	5.52	5.52	5.52
$Q_s = \sqrt{\frac{hZeV \eta\cos\phi_s }{2\pi\beta^2 E_{\text{tot}}}}$	8.305e-03	6.424e-03	3.313e-03	2.562e-03	7.512e-03	5.810e-03
$\theta_b = \frac{hL_b}{2\rho} [\text{rad}]$	2.514	2.514	2.514	2.514	2.514	2.514
$\frac{\rho \eta \delta_{\max}^{\circ}}{Q_s L_b / 2}$	0.158	0.204	0.069	0.089	0.190	0.553

Beta Beam Instability Studies

C. Hansen

- Collective Effect studies with the “Head Tail” simulation program will be made to study instabilities for all beams in the Beta Beam complex
- Instability dependencies of bunch intensities are being investigated for the Decay Ring

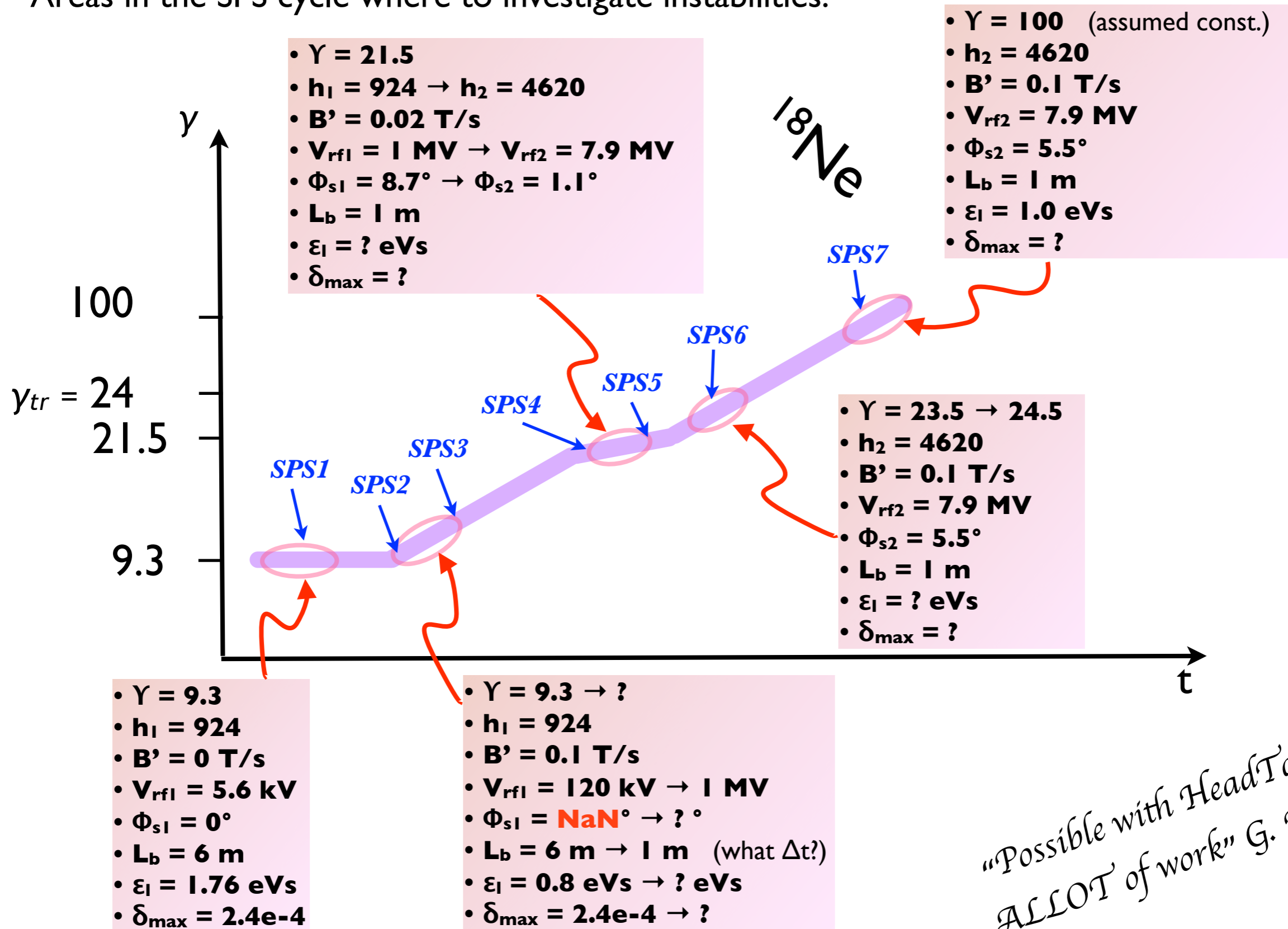
(To the right: Instability growth rate ($1/\tau$) due to transversal broadband impedance for ${}^6\text{He}$ in DR)



- The extra impedance due to beam loading at the special RF cavity in the Decay Ring will have to be taken into account
- The SPS' RF programs for the Beta Beams (left) are currently being developed in detail (A. Chancé) for the Instability Studies

Longitudinal Parameters - SPS

- Areas in the SPS cycle where to investigate instabilities:



Transversal Instability Limits

HeadTail and Formulas

$\xi = \xi^{\text{org}}$	HeadTail	Transverse Mode Coupling (TMCI Eq.)
DR ^{18}Ne ; BB \perp	$R_{\perp} = R_{\perp}^{\text{sps}}/427$	$R_{\perp} = R_{\perp}^{\text{sps}}/42$
DR ^6He ; BB \perp	$R_{\perp} = R_{\perp}^{\text{sps}}/73$	$R_{\perp} = R_{\perp}^{\text{sps}}/9$
SPS Ej. ^{18}Ne ; BB \perp	$N_B = N_B^{\text{org}}/??$	$N_B = N_B^{\text{org}}/10$
SPS Ej. ^6He ; BB \perp		$N_B = N_B^{\text{org}}/4$
SPS Inj. ^{18}Ne ; BB \perp	$N_B = N_B^{\text{org}}/??$	$N_B = N_B^{\text{org}}/14$
SPS Inj. ^6He ; BB \perp		$N_B = N_B^{\text{org}}$

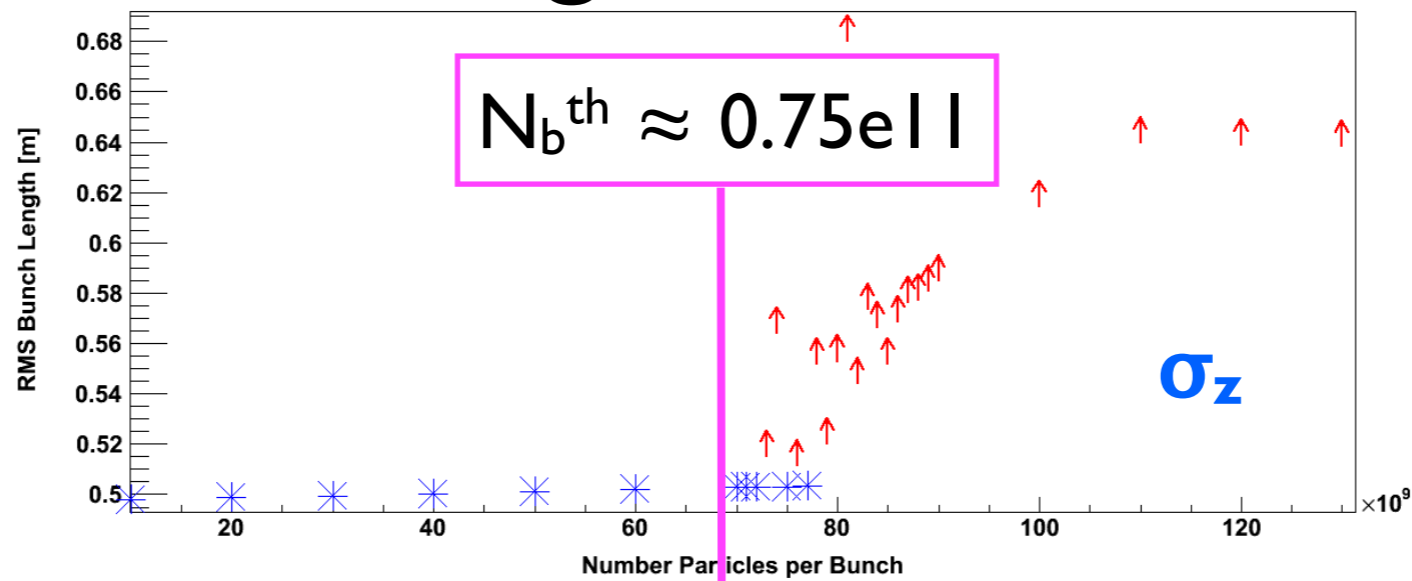
Longitudinal Instability Limits

HeadTail and Formulas

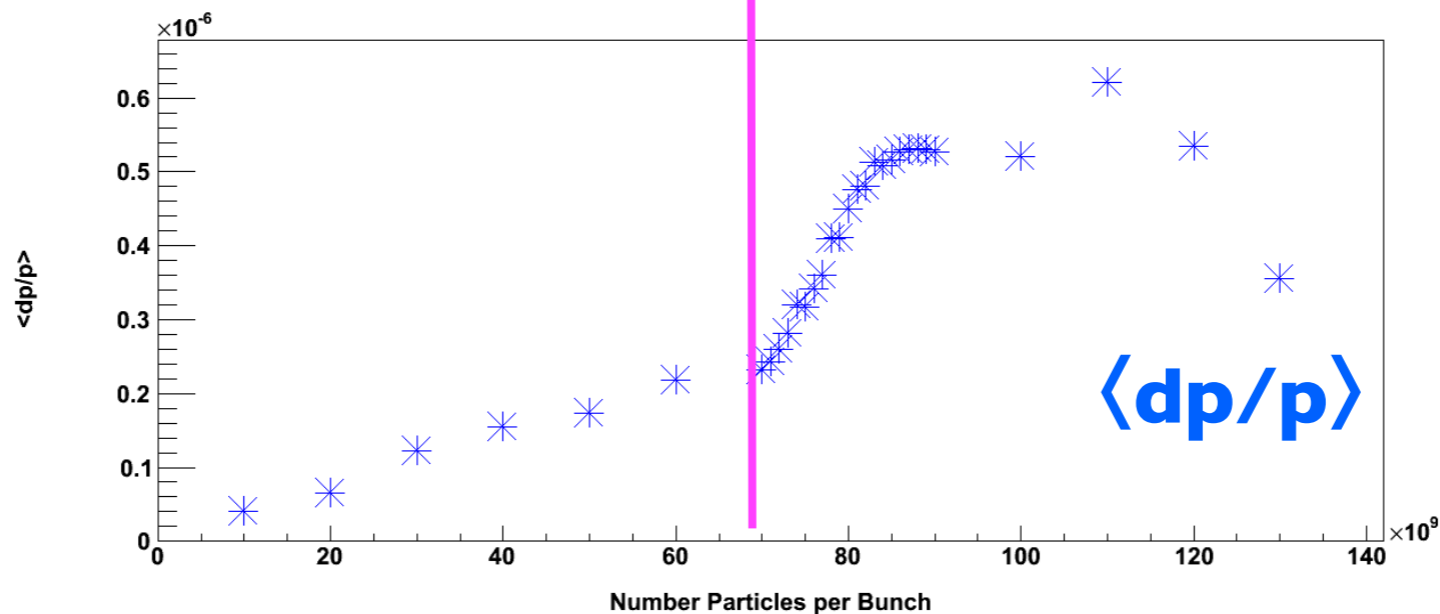
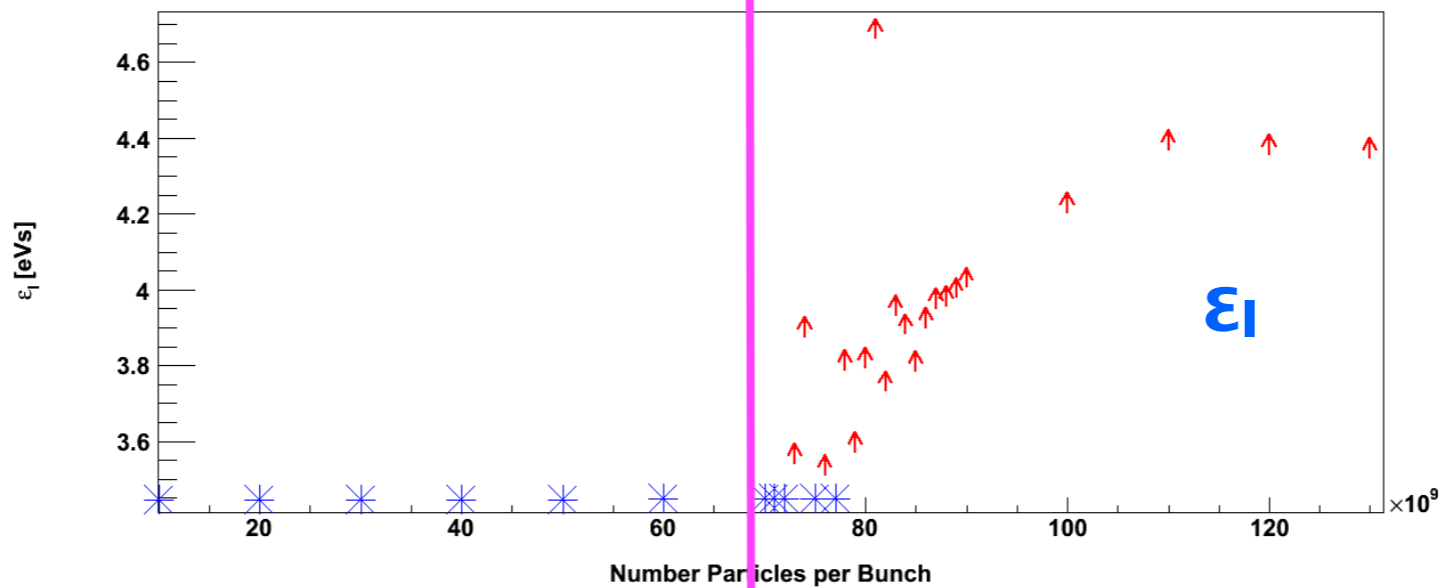
$\xi = \xi^{\text{org}}$	HeadTail	Micro Wave Instabilities (Keil Schnell)
DR ^{18}Ne ; BB	$R_{ } = R_{ }^{\text{SPS}}/60$	$R_{ } = R_{ }^{\text{SPS}}/20$
DR ^6He ; BB	$R_{ } = R_{ }^{\text{SPS}}/9$	$R_{ } = R_{ }^{\text{SPS}}/4$
SPS Ej. ^{18}Ne ; BB		$N_B = N_B^{\text{org}}/44$
SPS Ej. ^6He ; BB		$N_B = N_B^{\text{org}}/8$
SPS Inj. ^{18}Ne ; BB		$N_B = N_B^{\text{org}}/36$
SPS Inj. ^6He ; BB		$N_B = N_B^{\text{org}}$

DR ^{18}Ne - Longitudinal Broad Band

**Each point:
30000 turns**



Stability Limit:



**DR ^{18}Ne
Longitudinal Broad
Band Resonance**

$$N_B^{\text{org}} = 4.27e12$$

$$R_{\parallel}^{\text{org}} = 0.2 \text{ M}\Omega$$

$$\xi_x^{\text{org}} = 0.05, \xi_y^{\text{org}} = 0.1 \text{ for DR } (\eta > 0)$$

$$\text{KS: } N_B = N_B^{\text{org}} / 20$$

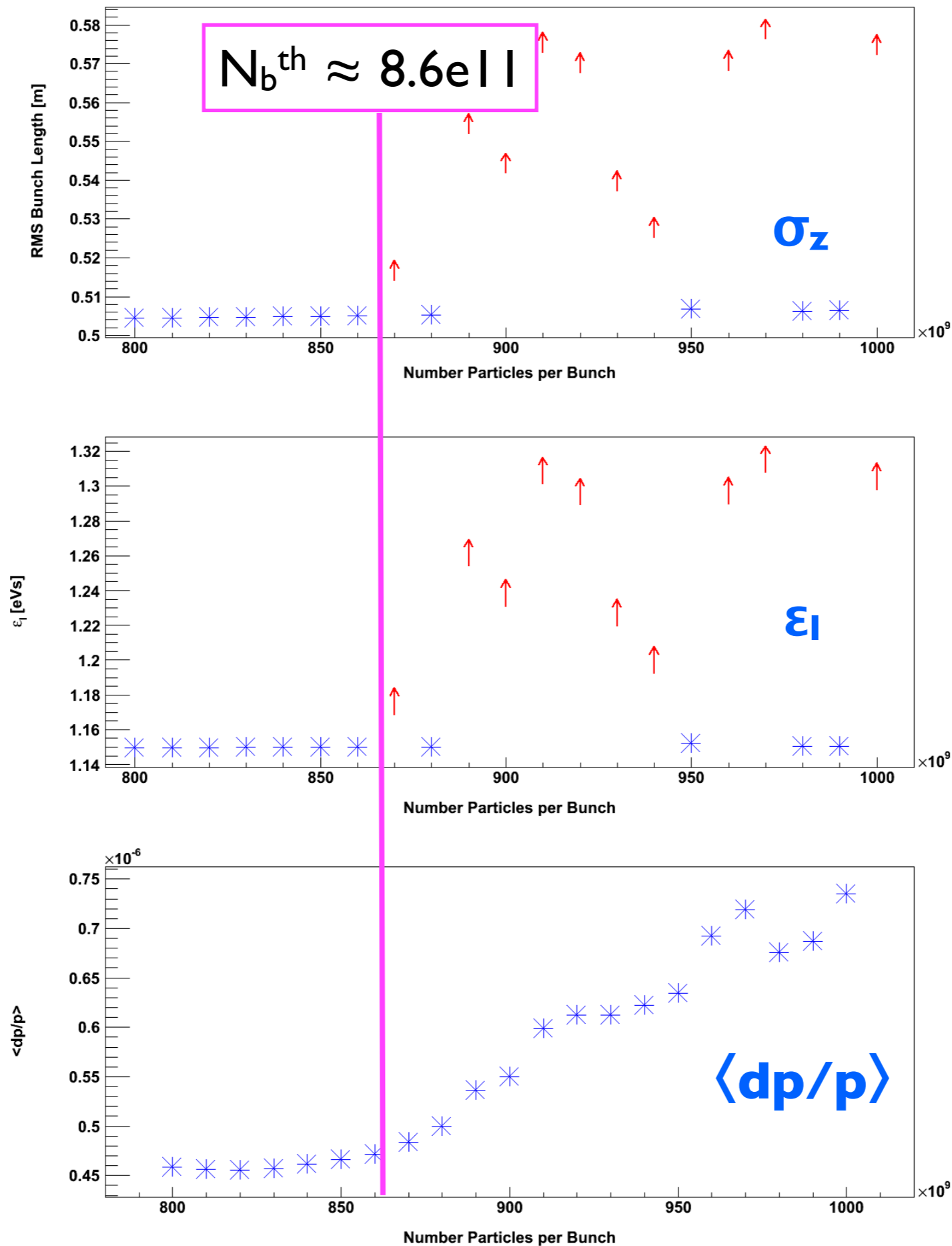
$$\text{BI: } N_B = N_B^{\text{org}} / 10$$

Head Tail:
 $N_B = N_B^{\text{org}} / 57$

Keil Schnell:
 $N_B = N_B^{\text{org}} / 20$

DR ${}^6\text{He}$ - Longitudinal Broad Band

**Each point:
30000 turns**



Stability Limit:

Head Tail:
 $N_B = N_B^{\text{org}} / 8$

Keil Schnell:
 $N_B = N_B^{\text{org}} / 4$

**DR ${}^6\text{He}$
Longitudinal Broad
Band Resonance**

$$N_B^{\text{org}} = 7.24e12$$

$$R_{||}^{\text{org}} = 0.2 \text{ M}\Omega$$

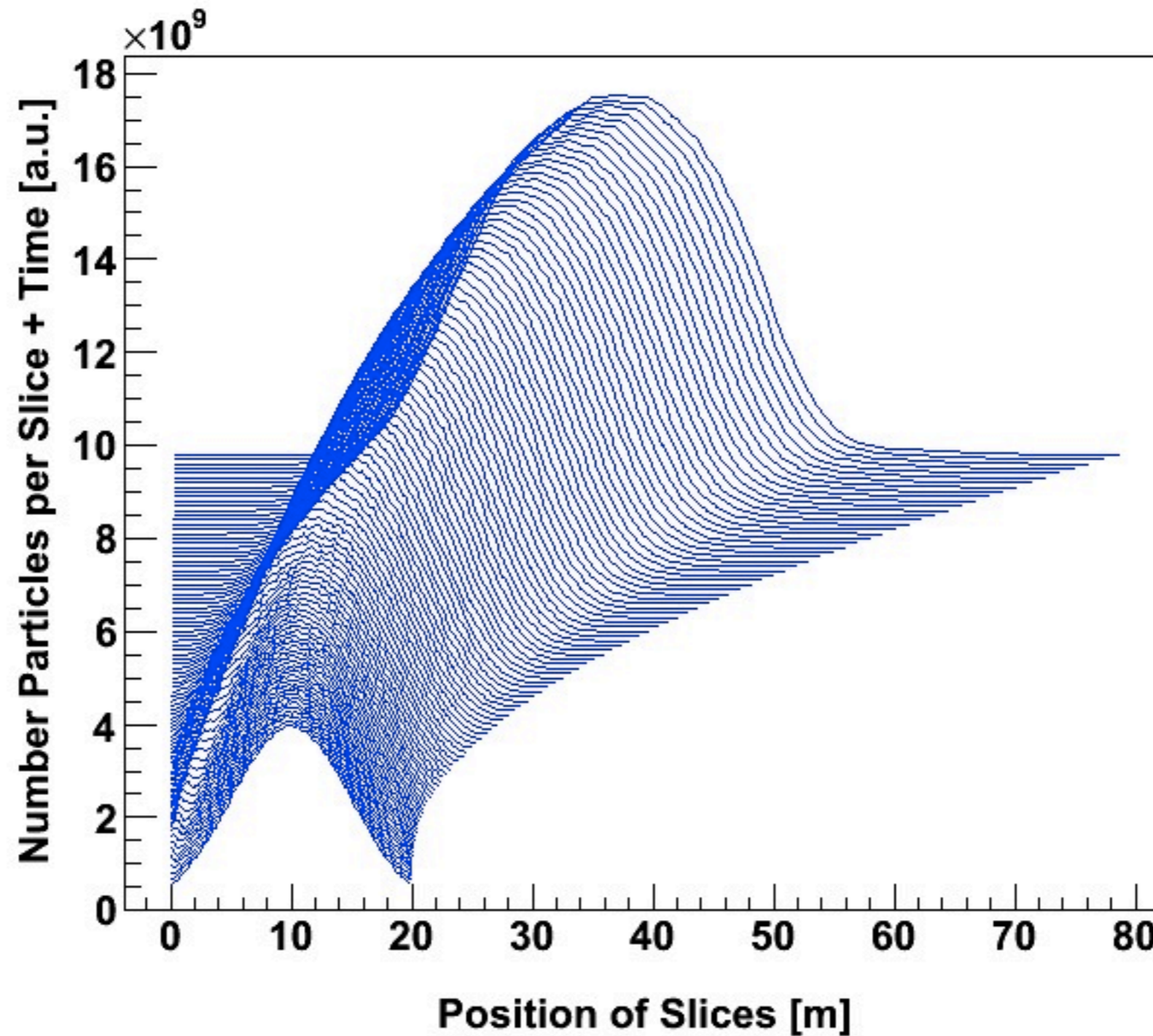
$$\xi_x^{\text{org}} = 0.05, \xi_y^{\text{org}} = 0.1 \text{ for DR } (\eta > 0)$$

$$\text{KS: } N_B = N_B^{\text{org}} / 4$$

$$\text{BI: } N_B = N_B^{\text{org}} / 2$$

SPS ^{18}Ne Injection - Long. Broad Band

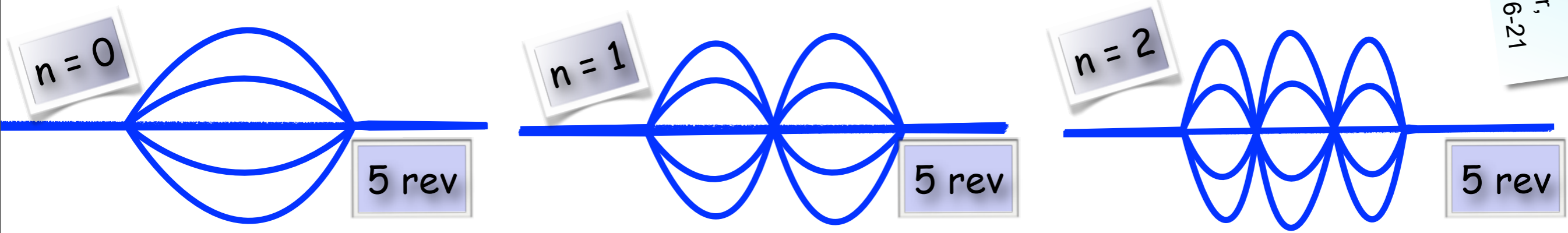
$$N_B = N_B^{\text{org}} \quad \text{and} \quad \xi = \xi^{\text{org}}$$



Head Tail Modes (n)

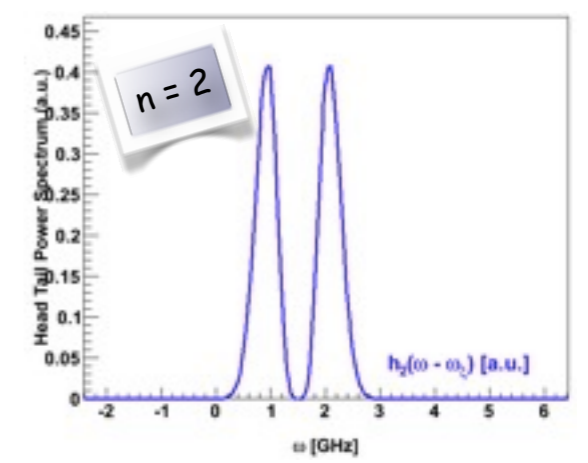
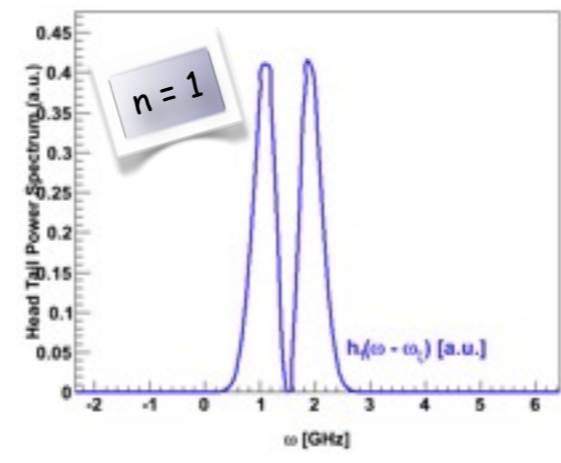
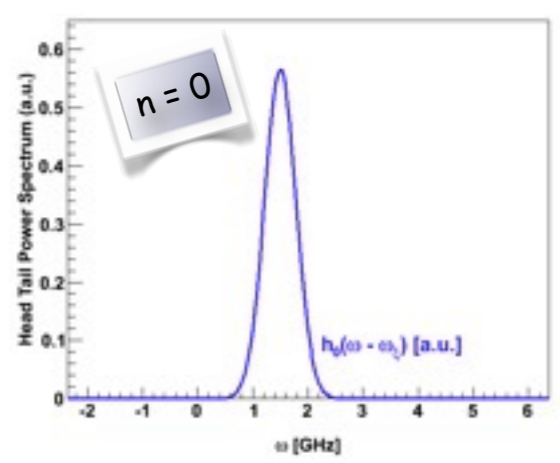
- The different ways particles in the front (head) of the bunch are positioned compared to particles in the back (tail) of the bunch are grouped in different “modes”
- The “head-tail mode number”, n , defines how the head and tail couples in that mode
- The signal of a bunch in a position monitor shows n nodes for mode n :

F.J. Sacherer,
CERN/PS/BR 76-21



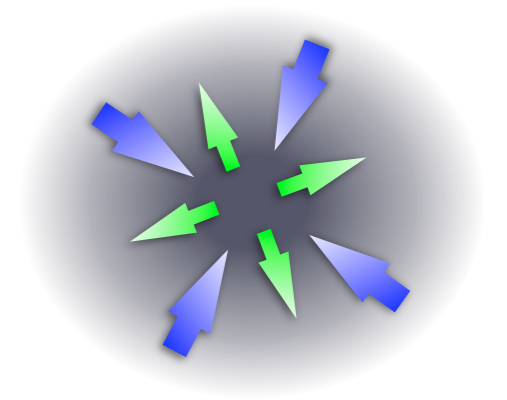
- These *head-tail modes in time domain* can be Fourier transformed and squared to get the “head-tail power spectrum”, $h_n(\omega)$:

$$p_n(t) = \begin{cases} \cos \left[(n+1)\pi \frac{t}{\tau_b} \right] & , n = 0, 2, 4, \dots \\ \sin \left[(n+1)\pi \frac{t}{\tau_b} \right] & , n = 1, 3, 5, \dots \end{cases} \quad \Rightarrow \quad |\mathcal{F}(p_n(t))|^2 = h_n(\omega)$$



Direct Space Charge

- A particle in a bunch feels the collective Coulomb forces due to fields generated by the charge of the other particles in the bunch
- For relativistic beams the repulsive **E forces** are cancelled by the contracting **B forces** → tune shift due to space charge $\propto \gamma^{-2}$



$$\Delta Q_{dsc_{x,y}} = -\frac{\lambda r_0 R}{2\beta\gamma^2 \epsilon_{N_{x,y}}}$$

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Instabilities

- Assuming Gaussian bunches the peak line charge density near the bunch center is

$$\lambda = N / \left(\sqrt{2\pi} \sigma_z \right) \quad \text{and the full bunch length} \quad L_b = 4\sigma_z$$

- For ions $r_0 = r_p Z^2 / A$ so we get the tune shift

$$\Delta Q_{dsc_{x,y}} = -\frac{2N_B r_p Z^2 R}{\sqrt{2\pi} A L_b \beta \gamma^2 \epsilon_{N_{x,y}}}$$

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Instabilities

- If absolute value is more than 0.2 it could cause the tune to cross over the resonance lines

Direct Space Charge

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Dependent Instabilities
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$$\Delta Q_{dsc_{x,y}} = -\frac{1}{B} \frac{N_B r_0 R}{\pi \gamma^3 \beta^2 Q_{x,y}} \frac{\epsilon_{x,y}^{dsc}}{2\sigma_y^2}$$

Exchanged $a_{x,y} \rightarrow \sqrt{2}\sigma_{x,y}$
and $\epsilon \rightarrow \epsilon^{1\sigma}$ to assume
Gaussian instead of Uniform.

where

$$\epsilon_x^{dsc} = \frac{\sigma_y^2}{\sigma_x(\sigma_y + \sigma_x)}$$

$$\sigma_x = \sqrt{\frac{\langle \beta_x \rangle \epsilon_{N_x}^{1\sigma}}{\gamma \beta} + \langle D_x \rangle^2 \left(\frac{dp}{p} \right)_{max}^2}$$

$$\epsilon_y^{dsc} = \frac{\sigma_y}{\sigma_y + \sigma_x}$$

$$\sigma_y = \sqrt{\frac{\langle \beta_y \rangle \epsilon_{N_y}^{1\sigma}}{\gamma \beta}}$$

DSC	DR ¹⁸ Ne	DR ⁶ He	SPS Ej. ¹⁸ Ne	SPS Ej. ⁶ He	SPS Inj. ¹⁸ Ne	SPS Inj. ⁶ He
ΔQ_{dsc_x}	-0.0402	-0.0082	-0.0109	-0.0036	-0.0916	-0.0881
ΔQ_{dsc_y}	-0.0930	-0.0189	-0.0149	-0.0049	-0.1252	-0.1204

(added the factor 1/B myself; B is the bunching factor)

Direct Space Charge

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- For elliptical beam according to Ng

$$\Delta Q_{dsc_{x,y}} = - \frac{8N_B r_0 R}{\sqrt{2\pi} L_b \beta \gamma^2 \sqrt{\epsilon_{N_{x,y}}} \left[\sqrt{\epsilon_{N_{x,y}}} + \sqrt{\epsilon_{N_{y,x}}} \frac{\langle \beta_{y,x} \rangle}{\langle \beta_{x,y} \rangle} \right]}$$

DSC	DR ¹⁸ Ne	DR ⁶ He	SPS Ej. ¹⁸ Ne	SPS Ej. ⁶ He	SPS Inj. ¹⁸ Ne	SPS Inj. ⁶ He
ΔQ_{dsc_x}	<u>-0.2410</u>	-0.0491	-0.0287	-0.0095	<u>-0.2418</u>	<u>-0.2327</u>
ΔQ_{dsc_y}	<u>-0.3570</u>	-0.0727	-0.0393	-0.0130	<u>-0.3303</u>	<u>-0.3177</u>

- But if we assume round beam this becomes a factor 2 bigger than Chao's equation (prev. slide)
- So let's divide Ng's equation by 2

$$\Delta Q_{dsc_{x,y}} = - \frac{4N_B r_0 R}{\sqrt{2\pi} L_b \beta \gamma^2 \epsilon_{N_{x,y}}}$$

$$\Delta Q_{dsc_{x,y}} = - \frac{4N_B r_0 R}{\sqrt{2\pi} L_b \beta \gamma^2 \sqrt{\epsilon_{N_{x,y}}} \left[\sqrt{\epsilon_{N_{x,y}}} + \sqrt{\epsilon_{N_{y,x}}} \frac{\langle \beta_{y,x} \rangle}{\langle \beta_{x,y} \rangle} \right]}$$

DSC	DR ¹⁸ Ne	DR ⁶ He	SPS Ej. ¹⁸ Ne	SPS Ej. ⁶ He	SPS Inj. ¹⁸ Ne	SPS Inj. ⁶ He
ΔQ_{dsc_x}	-0.1205	-0.0245	-0.0144	-0.0048	-0.1209	-0.1163
ΔQ_{dsc_y}	-0.1785	-0.0364	-0.0196	-0.0065	-0.1651	-0.1589

Image Coefficients for Elliptical Vacuum Chambers

- Assume the beam is centered, then

$$\varepsilon_y^{incoh} = -\varepsilon_x^{incoh} = \frac{h^2}{12\epsilon^2} \left[(1 + k'^2) \left(\frac{2K(k)}{\pi} \right)^2 - 2 \right]$$

$$\varepsilon_y^{coh} = \frac{h^2}{4\epsilon^2} \left[\left(\frac{2K(k)}{\pi} \right)^2 - 1 \right]$$

$$\varepsilon_x^{coh} = \frac{h^2}{4\epsilon^2} \left[1 - \left(\frac{2K(k)k'}{\pi} \right)^2 \right]$$

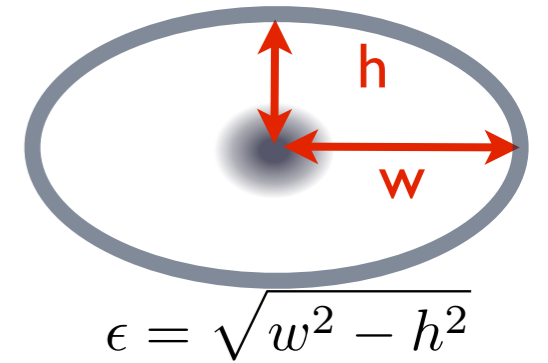
where

$$k' = \left(\frac{1 + 2 \sum_{s=1}^{\infty} (-1)^s q^{s^2}}{1 + 2 \sum_{s=1}^{\infty} q^{s^2}} \right)^2$$

$$q = \frac{w - h}{w + h}$$

$$k = \sqrt{1 - k'^2}$$

$$K(k) = \int_0^{\pi/2} \frac{d\theta}{\sqrt{1 - k^2 \sin^2 \theta}}$$



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When $w = h$ (e.g. for the DR) then

$$\varepsilon_y^{incoh} = \varepsilon_x^{incoh} = 0$$

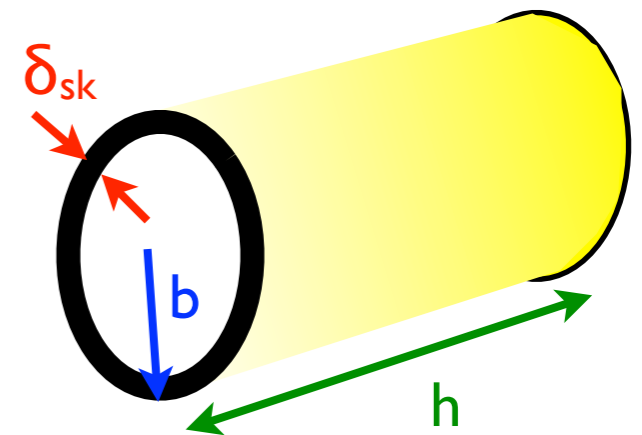
$$\varepsilon_y^{coh} = \varepsilon_x^{coh} = 1/2$$

Resistive Wall Impedance

- Since the conductivity of the beam pipe is not perfect the image current is slowed down, radiates a wake field which gives an impedance
- To get the Resistive Wall Impedance one takes into account that the EM fields penetrate the pipe material to a thickness called “**Skin Depth**”, that equals

Stainless Steel:
 Magnetic Permeability = $\mu = \mu_{ss} \mu_0$
 $= 1.05 \cdot 4\pi \cdot 10^{-7} \text{ Vs/Am}$
 Resistivity = $\rho = 1 \cdot 10^{-7} \Omega\text{m}$

$$\delta_{sk}(\omega) = \sqrt{\frac{2\rho}{|\omega|\mu}}$$



where ρ is the materials “bulk resistance” and then gets the “resistant” (real) and “reactive” (imaginary) parts for the longitudinal and transverse impedances of a cylindrical model with length h (circumference of the ring is used for h), radius b and thickness δ_{sk}

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 Impedance and Wake
 Fields

$$Z_{||,rw}(\omega) = \frac{\omega}{2} (1 - i) \frac{Z_0 \delta_{sk}(\omega) h}{2\pi b c} \approx (1 - i) \frac{\omega R}{2bc} \sqrt{\frac{2\rho}{\epsilon_0 |\omega|}}$$

$$Z_{\perp,rw}(\omega) = (\text{sgn}(\omega) - i) \frac{Z_0 \delta_{sk}(\omega) h}{2\pi b^3} \approx (\text{sgn}(\omega) - i) \frac{R}{b^3} \sqrt{\frac{2\rho}{\epsilon_0 |\omega|}}$$

$$Z_0 = \sqrt{\frac{\mu_0}{\epsilon_0}}$$

$$h = C = 2\pi R$$

$$\mu \approx \mu_0$$

- ... To be “plugged in” in Sacherer’s formulas ... (see coming slides)

Resonance Impedances

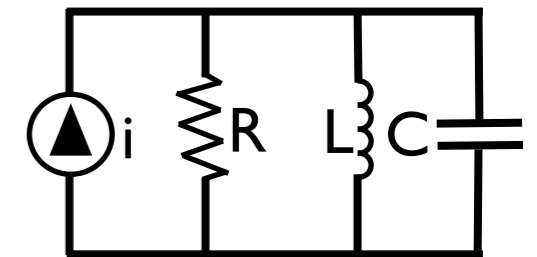
$$\omega < \omega_c$$

- Wake Fields trapped in cavities or discontinuities in the vacuum chamber cause Resonance Impedances
- Resonance Impedances consist of a real (resistive) part and a imaginary (reactive) part:

$$Z = Z_{Re} + iZ_{Im}$$

→ We see an analogy between Resonance Wake Fields and Electronic Circuits

→ The Impedance of “high order modes” Wakes can be modeled with the RLC circuit



$$\rightarrow Z_{||}(\omega) = \frac{R_{||}}{1 + iQ \left(\frac{\omega_r}{\omega} - \frac{\omega}{\omega_r} \right)}, \quad Z_{\perp}(\omega) = \frac{R_{\perp} \frac{\omega_r}{\omega}}{1 + iQ \left(\frac{\omega_r}{\omega} - \frac{\omega}{\omega_r} \right)}$$

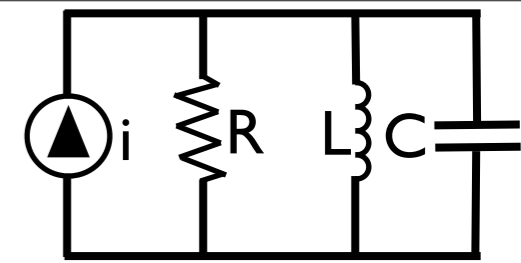
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Impedance and Wake
Fields

where $Q = R\sqrt{C/L}$ is the “Quality Factor” and $\omega_r = 1/\sqrt{LC}$ is the characteristic frequency for the RLC circuit, or for the pipe it is the “Characteristic Frequency” for the structure causing the Wake Field and $R_{||}$ and R_{\perp} are the “Shunt Impedances”

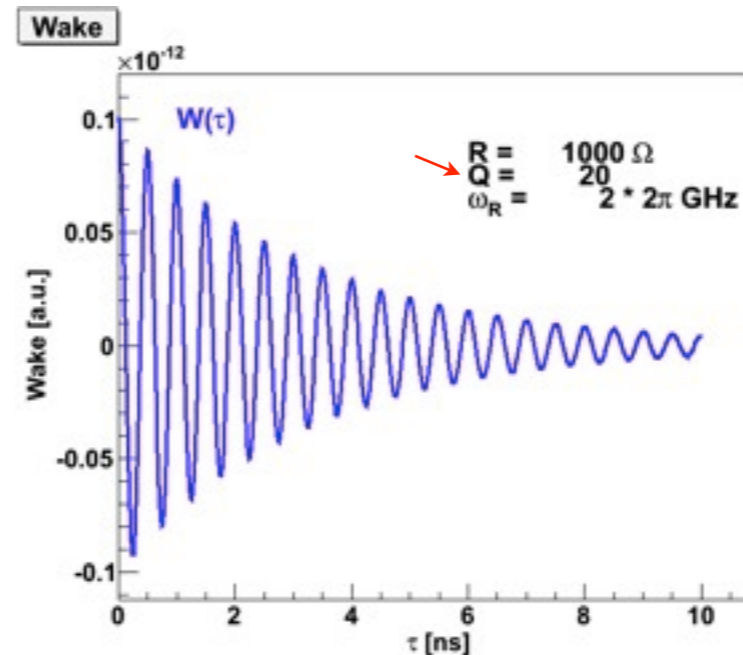
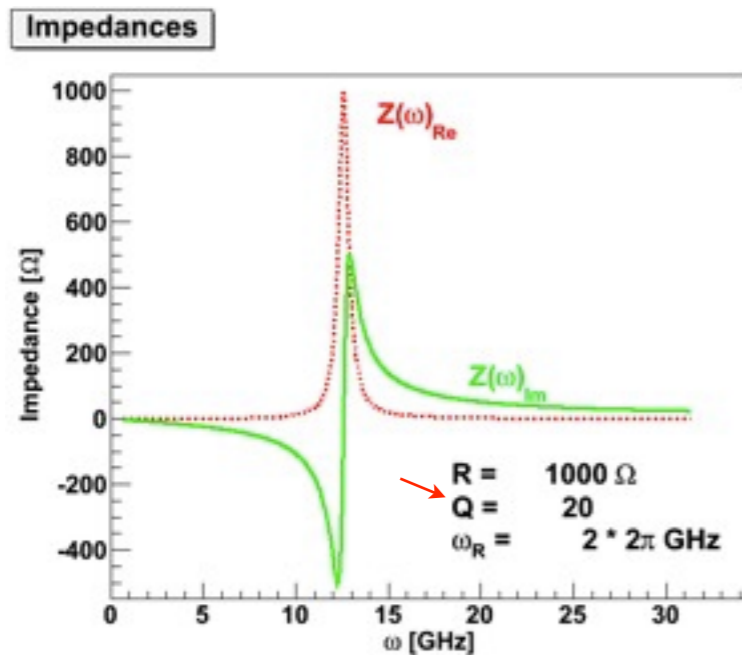
Take the Inverse FT to get the Wake Fields →

$$W_{||}(\tau) = \frac{e^{-\omega_r \tau / 2Q}}{C} \left[\cos \left(\omega_r \tau \sqrt{1 - 1/(4Q^2)} \right) - \frac{1}{\sqrt{4Q^2}} \sin \left(\omega_r \tau \sqrt{1 - 1/(4Q^2)} \right) \right], \quad \tau > 0, \quad = 0 \quad \tau < 0$$

Narrow & Broad Band

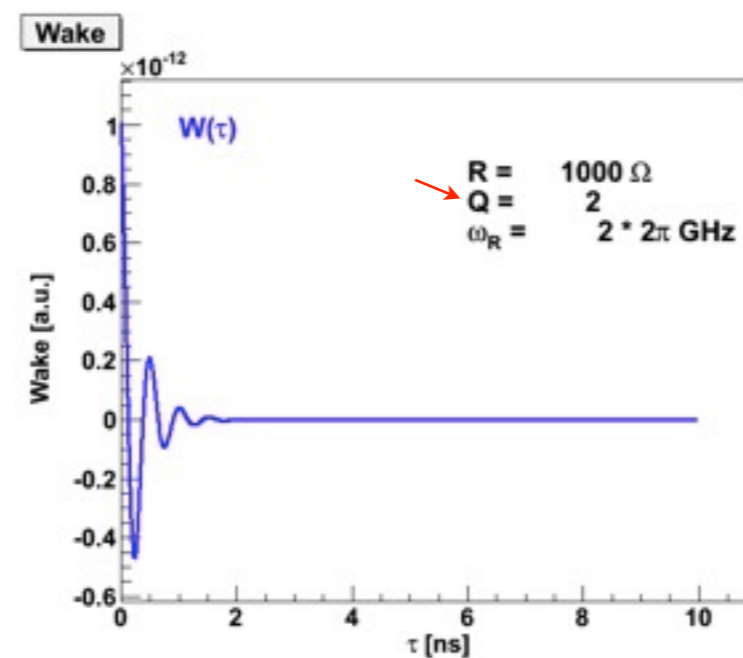
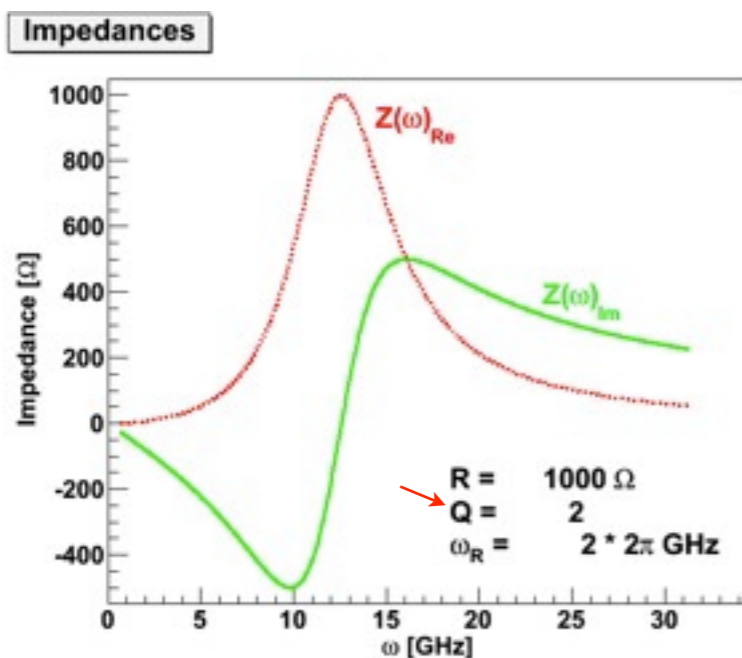


- From the RLC circuit model we see the behavior of the resonant wake fields and the real and imaginary part of the impedance in the case of high quality factor; **Narrow Band**



High Q → Narrow Band → Long Lasting Wake Field → Multi Bunch Instabilities

and in the case of low quality factor; **Broad Band**



Low Q → Broad Band → Short Lasting Wake Field → Single Bunch Instabilities