

# Gravitational Waves: The instrumental challenges of the detection

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# Table of Contents

- **How can we detect gravitational waves with laser interferometers?**
- **How do ground-based interferometers work?**
  - The Virgo optical configuration or how to measure  $10^{-20}$  m
  - How to maintain the ITF at its working point?
  - How to measure the GW strain  $h(t)$  from this detector?
  - Noises limiting the ITF sensitivity: how to tackle them?
- **Prospectives for interferometers and other detectors**

# Reminder: effect of a GW on free fall masses

A gravitational wave (GW) modifies the distance between free-fall masses

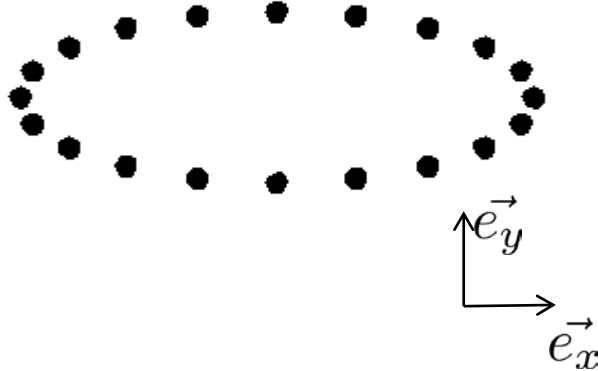


# Reminder: effect of a GW on free fall masses

A gravitational wave (GW) modifies the distance between free-fall masses

$$\delta x(t) = -\delta y(t) = \frac{1}{2} h(t) L_0$$

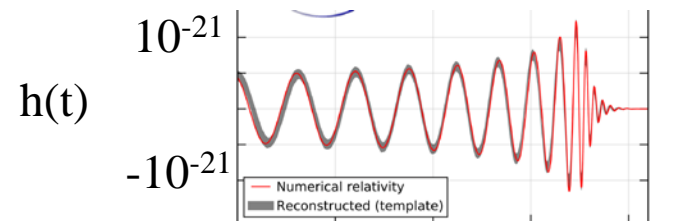
$h(t)$ : amplitude of the GW (= strain)



Typical amplitude of a GW crossing the Earth:  
 $h \sim 10^{-23}$   
( $h$  has no dimension/unit)

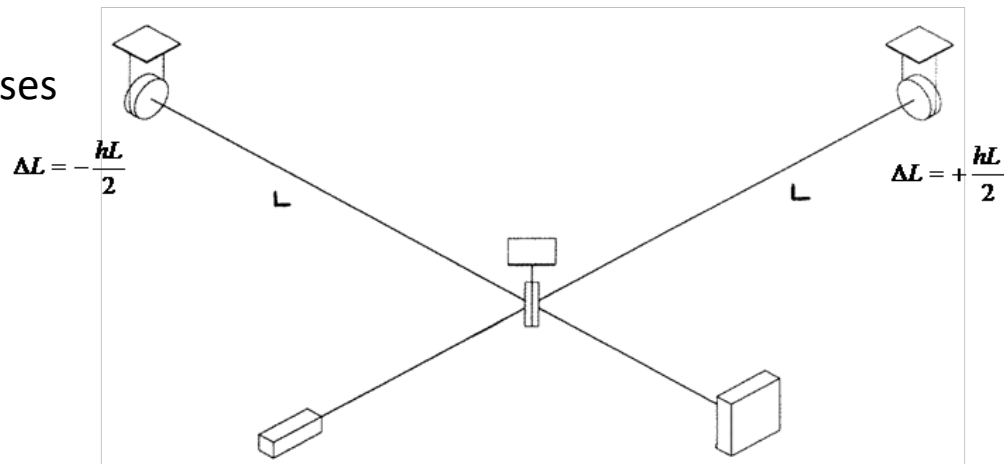
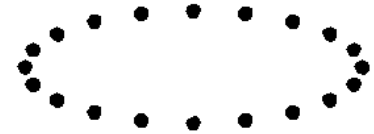
Case of a GW with polarisation + propagating along z

Reconstructed strain of GW150914



# Terrestrial GW Interferometer: basic principle

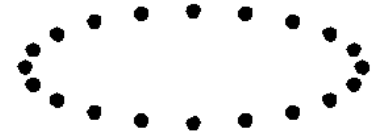
- Measure a variation of distance between masses
  - Measure the light travel time to propagate over this distance
  - Laser interferometry is an appropriate technique
    - Comparative measurement
    - Suspended mirrors = free fall test masses



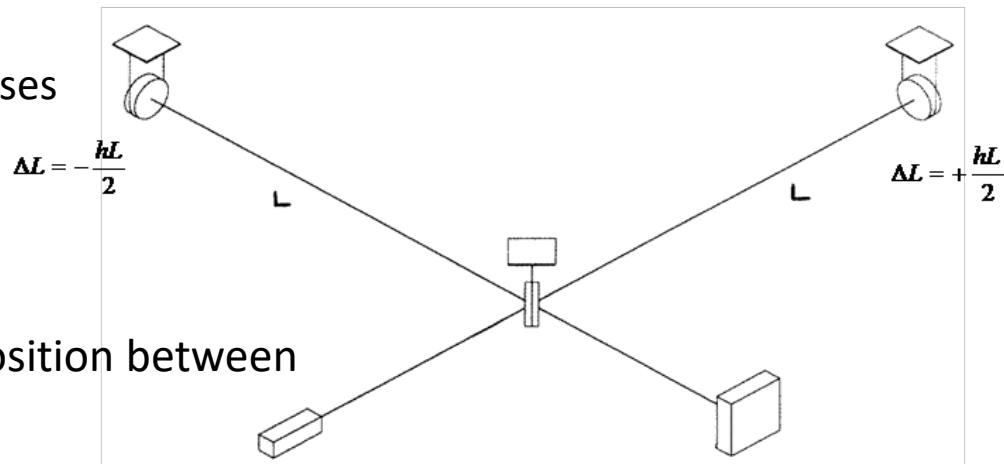
# Terrestrial GW Interferometer: basic principle



# Terrestrial GW Interferometer: basic principle



- Measure a variation of distance between masses
  - Measure the light travel time to propagate over this distance
  - Laser interferometry is an appropriate technique
    - Comparative measurement
    - Suspended mirrors = free fall test masses



- Michelson interferometer well suited:
  - Effect of a gravitational wave is in opposition between 2 perpendicular axes
  - **Light intensity of interfering beams is related to the difference of optical path length in the 2 arms**

**Bandwidth: 10 Hz to few kHz**

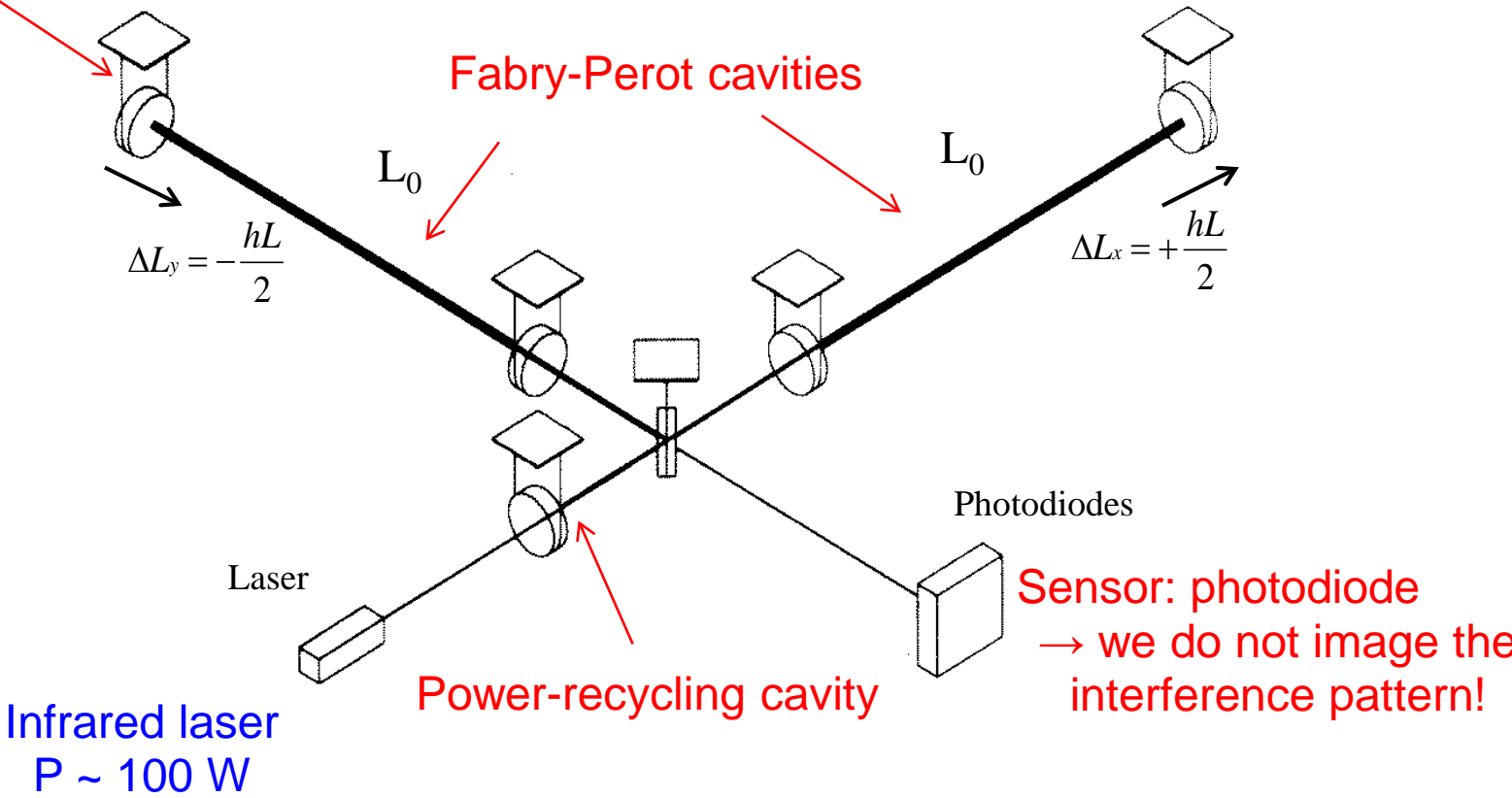
We need a big interferometer:

$\Delta L$  proportional to  $L$

➔ need several km arms!

# Virgo/LIGO: more complicated interferometers

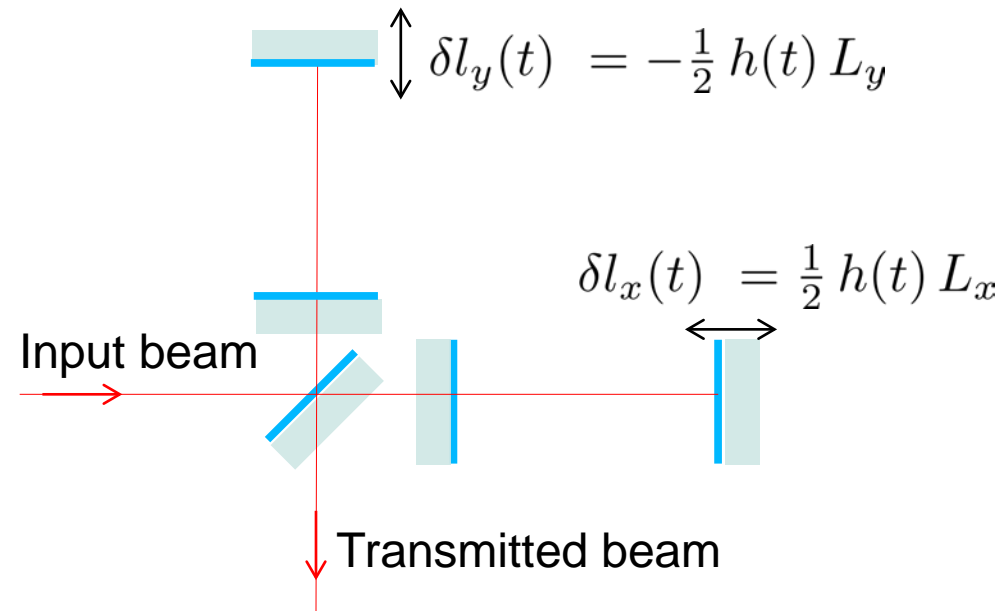
**Suspended mirrors** → Mirrors can be considered as free-falling in the ITF plane for frequencies larger than ~10 Hz



**WARNING: STILL VERY SIMPLIFIED SCHEME!**



# Orders of magnitude



Typical amplitude of differential arm length variations when a GW crosses the Earth:

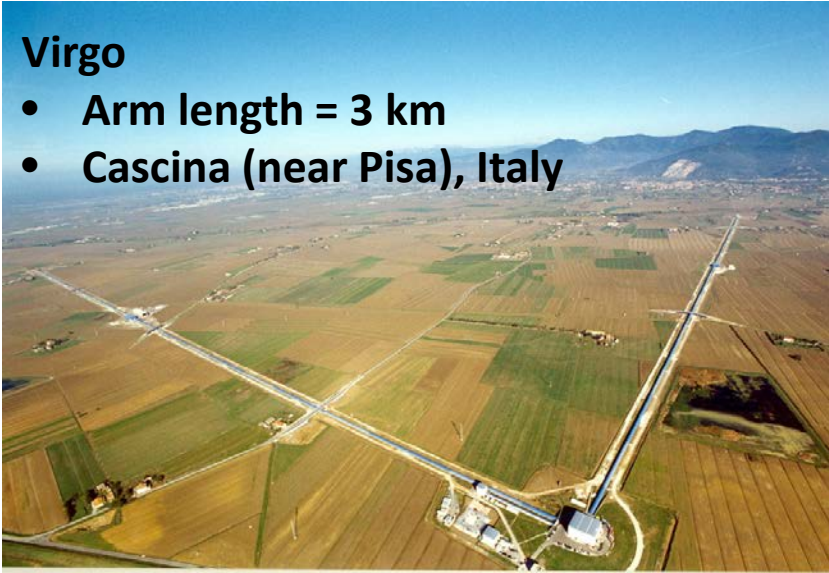
$$\begin{aligned}\delta\Delta L &= \delta l_x(t) - \delta l_y(t) \\ &= h(t) L_0\end{aligned}$$

$$\begin{aligned}h &\sim 10^{-23} & L_0 &= 3 \text{ km} \\ \rightarrow \delta\Delta L &\sim 3 \times 10^{-20} \text{ m} \\ &\sim \frac{\text{size of a proton}}{100000}\end{aligned}$$

# Km scale interferometers

## Virgo

- Arm length = 3 km
- Cascina (near Pisa), Italy



## LIGO Livingston

- Arm length = 4 km
- Louisiana



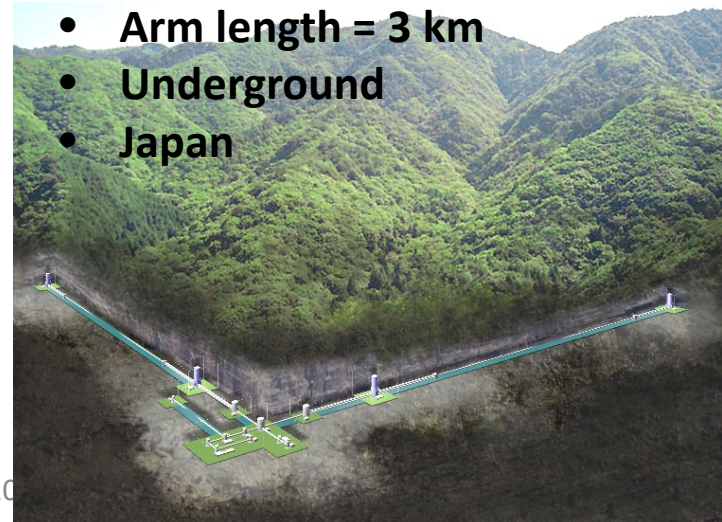
## LIGO Hanford

- Arm length = 4 km
- Washington State



## KAGRA

- Arm length = 3 km
- Underground
- Japan



# The detector network

Advanced LIGO  
Hanford  
2015



GEO600 (HF)  
2011



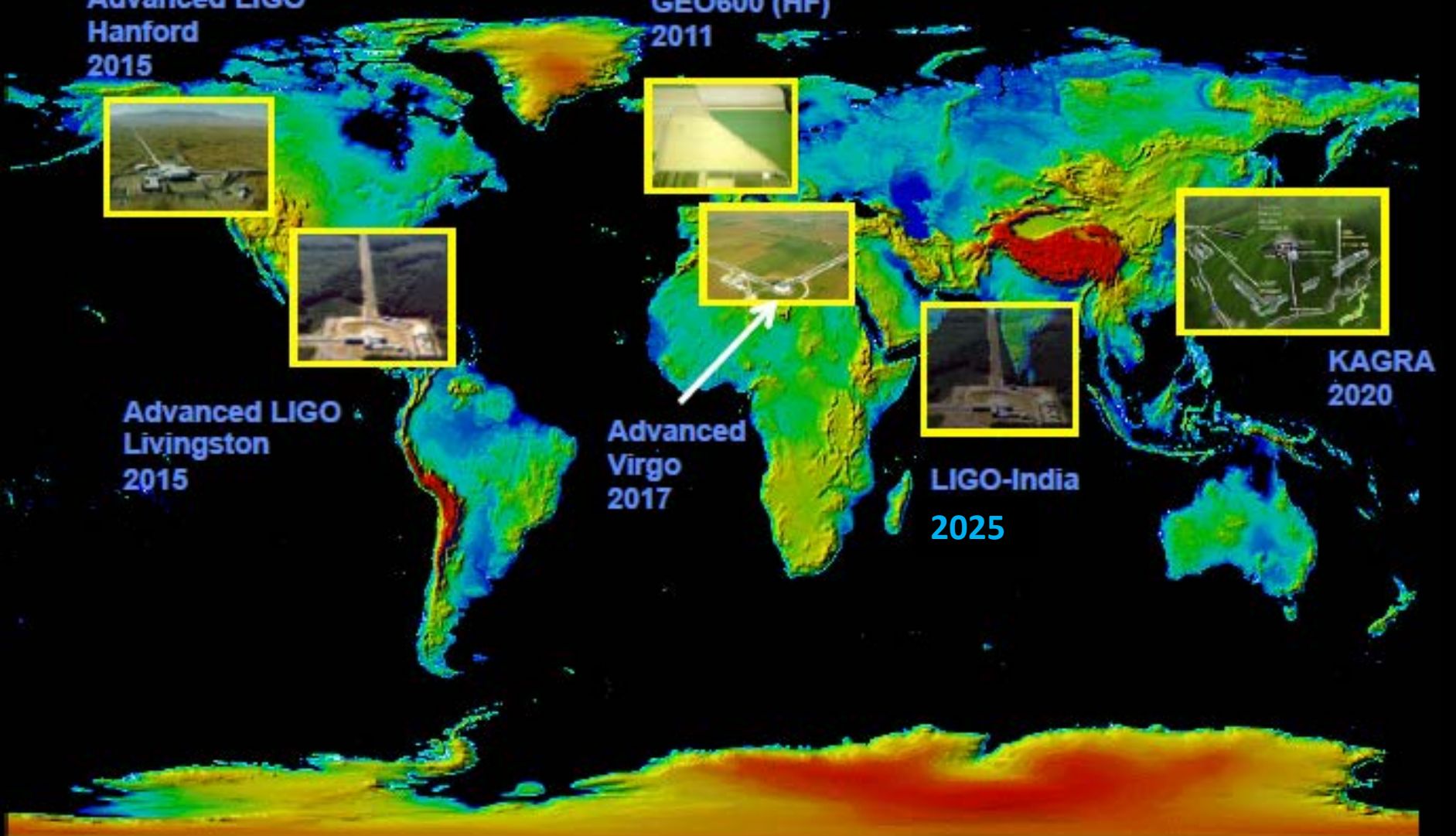
KAGRA  
2020

Advanced LIGO  
Livingston  
2015

Advanced  
Virgo  
2017

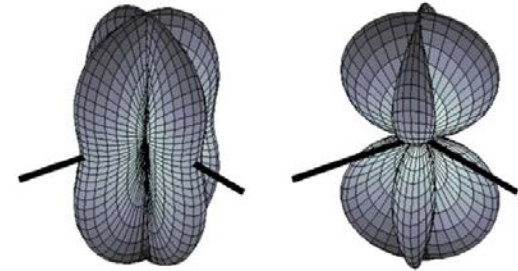


LIGO-India  
2025

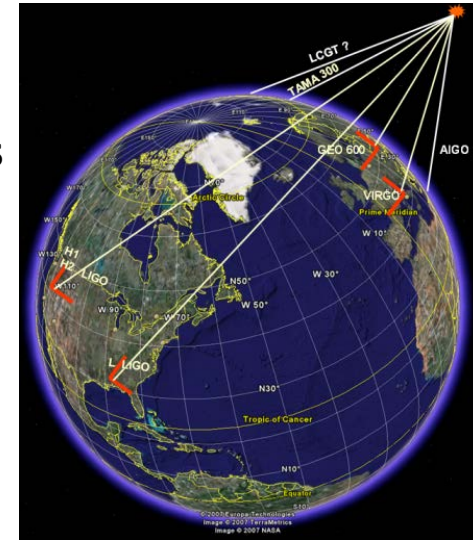
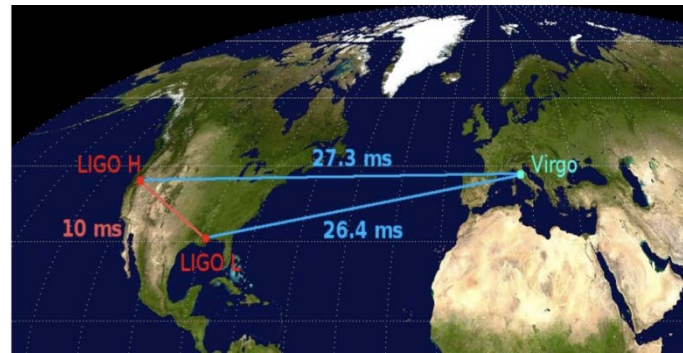


# The benefits of the network

- A GW interferometer acts as a wide beam antenna
  - A single detector cannot localize the source
  - Need to compare the signals found in coincidence between several detectors (triangulation):



- allow to point towards the source position in the sky
- the telescope is obtained by a network of interferometers



- Looking for rare and transient signals: can be hidden in detector noise
  - requires observation in coincidence between at least 2 detectors
- Since 2007, Virgo and LIGO share their data and analyze them jointly

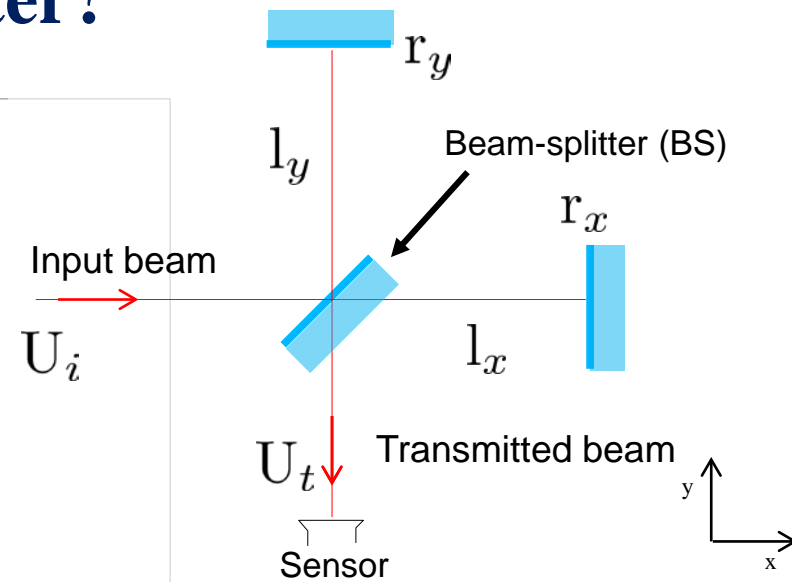
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# How do we « observe » $\Delta L$ with a Michelson interferometer?

- Input wave  $U_i(x, t) = \underline{\mathcal{A}}_i e^{j k x}$   
 $= \underline{\mathcal{A}}_i$  on BS
- BS located at (0,0)
- Sensor located at (0,- $y_s$ )
- Amplitude reflection and transmission coefficients:  $r$  and  $t$

→ We are interested in the beam transmitted by the interferometer: it is the sum of the two beams (fields) that have propagated along each arm



Around the mirrors:

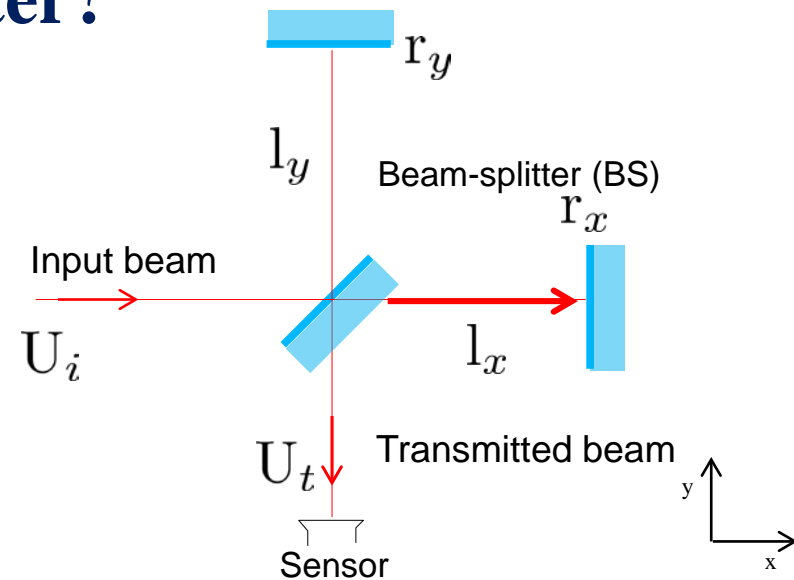
- Radius of curvature of the beam  $\sim 1400$  m
- Size of the beam  $\sim$  few cm

→ The beam can be approximated by plane waves

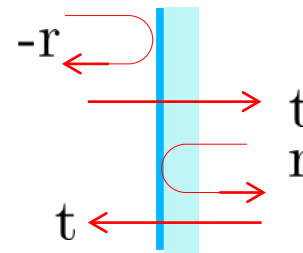
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- Beam propagating along x-arm:

$$U_{tx} = \underline{\mathcal{A}}_i t_{BS} e^{j k l_x} \dots\dots$$



Sign convention for amplitude reflection and transmission coefficients



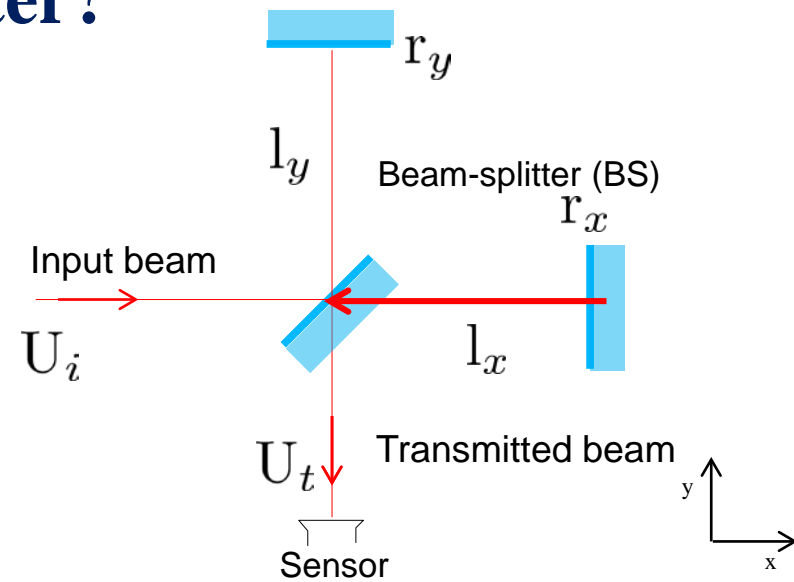
Without losses:  
 $t^2 + r^2 = 1$

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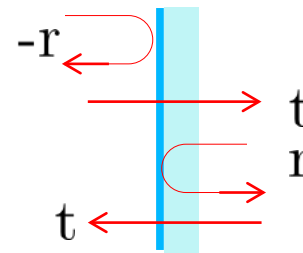
- Beam propagating along x-arm:

$$U_{tx} = \underline{\mathcal{A}}_i t_{BS} e^{j k l_x} \quad (-r_x) e^{j k l_x} \dots\dots$$



Sign convention for amplitude reflection and transmission coefficients

Without losses:  
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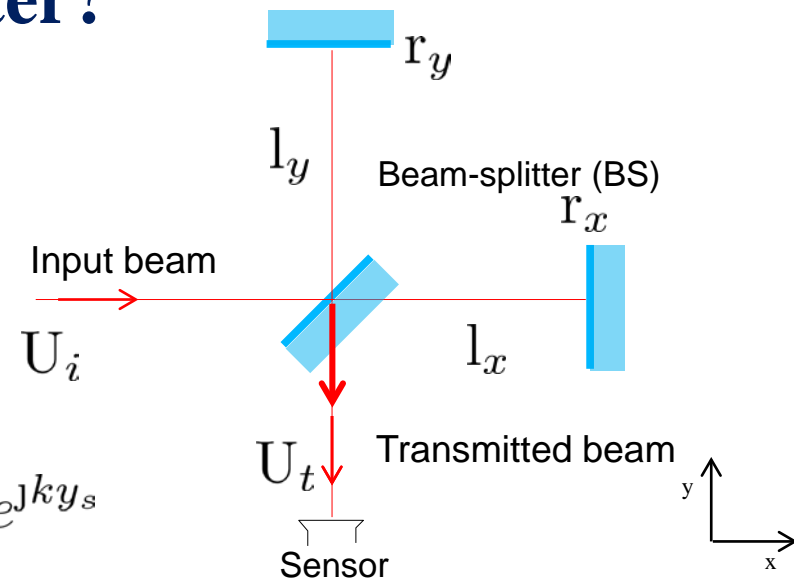


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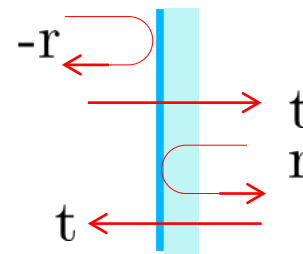
- Beam propagating along x-arm:

$$U_{tx} = \underline{\mathcal{A}}_i t_{BS} e^{j k l_x} \quad (-r_x) e^{j k l_x} \quad r_{BS} e^{j k y_s}$$



Sign convention for amplitude reflection and transmission coefficients

Without losses:  
 $t^2 + r^2 = 1$



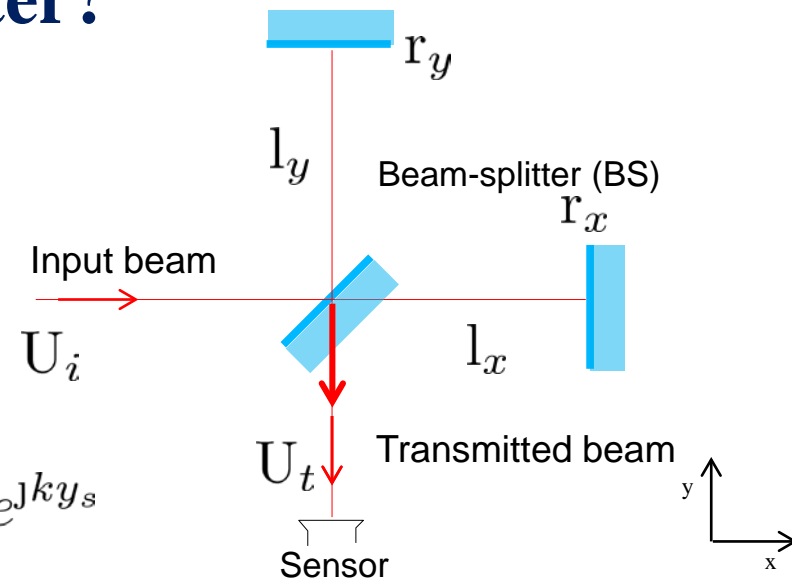
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- Beam propagating along x-arm:

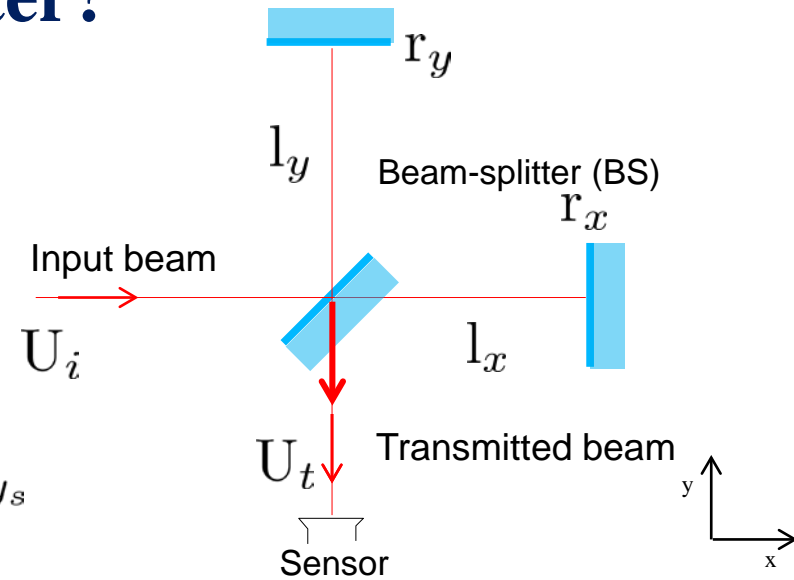
$$\begin{aligned}
 U_{tx} &= \underline{\mathcal{A}}_i t_{BS} e^{j k l_x} \quad (-r_x) e^{j k l_x} \quad r_{BS} e^{j k y_s} \\
 &= \underline{\mathcal{A}}_i t_{BS} r_{BS} (-r_x) e^{2j k l_x} e^{j k y_s} \\
 &= \frac{\underline{\mathcal{A}}_i}{2} \times \underbrace{(-r_x e^{2j k l_x})}_{\text{Complex reflection of the x-arm}} e^{j k y_s} \quad \text{with } t_{BS} = r_{BS} = \frac{1}{\sqrt{2}}
 \end{aligned}$$

Complex reflection of the x-arm



# How do we « observe » $\Delta L$ with a Michelson interferometer?

Input wave  $U_i(x, t) = \underline{\mathcal{A}}_i e^{j k x}$   
 $= \underline{\mathcal{A}}_i$  on BS



Beam propagating along x-arm:

$$U_{tx} = \underline{\mathcal{A}}_i t_{BS} e^{j k l_x} (-r_x) e^{j k l_x} r_{BS} e^{j k y_s}$$

$$= \underline{\mathcal{A}}_i t_{BS} r_{BS} (-r_x) e^{2j k l_x} e^{j k y_s}$$

$$= \frac{\mathcal{A}_i}{2} \times \underbrace{(-r_x e^{2j k l_x})}_{\text{Complex reflection of the x-arm}} e^{j k y_s}$$

Beam propagating along y-arm:

$$U_{ty} = -\frac{\mathcal{A}_i}{2} \times \underbrace{(-r_y e^{2j k l_y})}_{\text{Complex reflection of the y-arm}} e^{j k y_s}$$

Transmitted field:

$$U_t = U_{tx} + U_{ty}$$

$$= \frac{\mathcal{A}_i}{2} e^{j k y_s} (r_y e^{2j k l_y} - r_x e^{2j k l_x})$$

Complex reflection of the y-arm

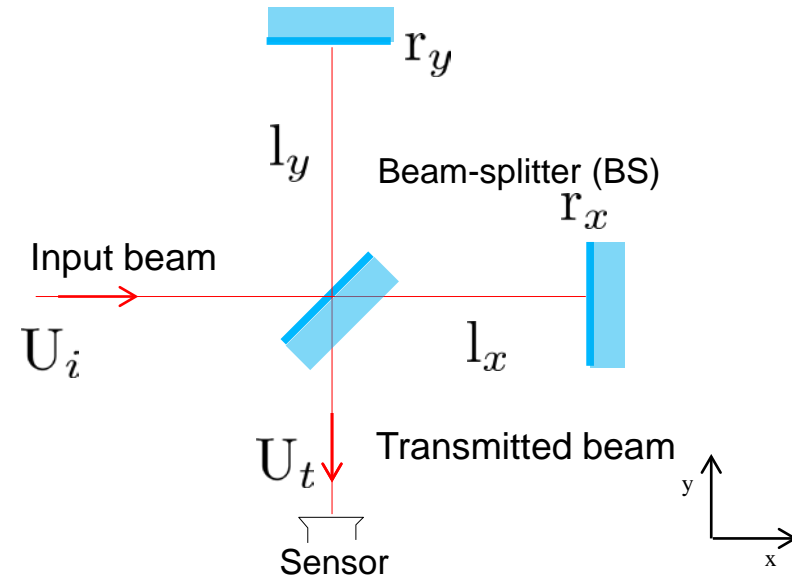
# Simple Michelson interferometer: transmitted power

## Field transmitted by the interferometer

$$U_t = \frac{A_i}{2} (r_y e^{2jkly} - r_x e^{2jklx})$$

$k$  is the wave number,  $k = 2\pi/\lambda$

$\lambda$  is the laser wavelength ( $\lambda=1064$  nm)



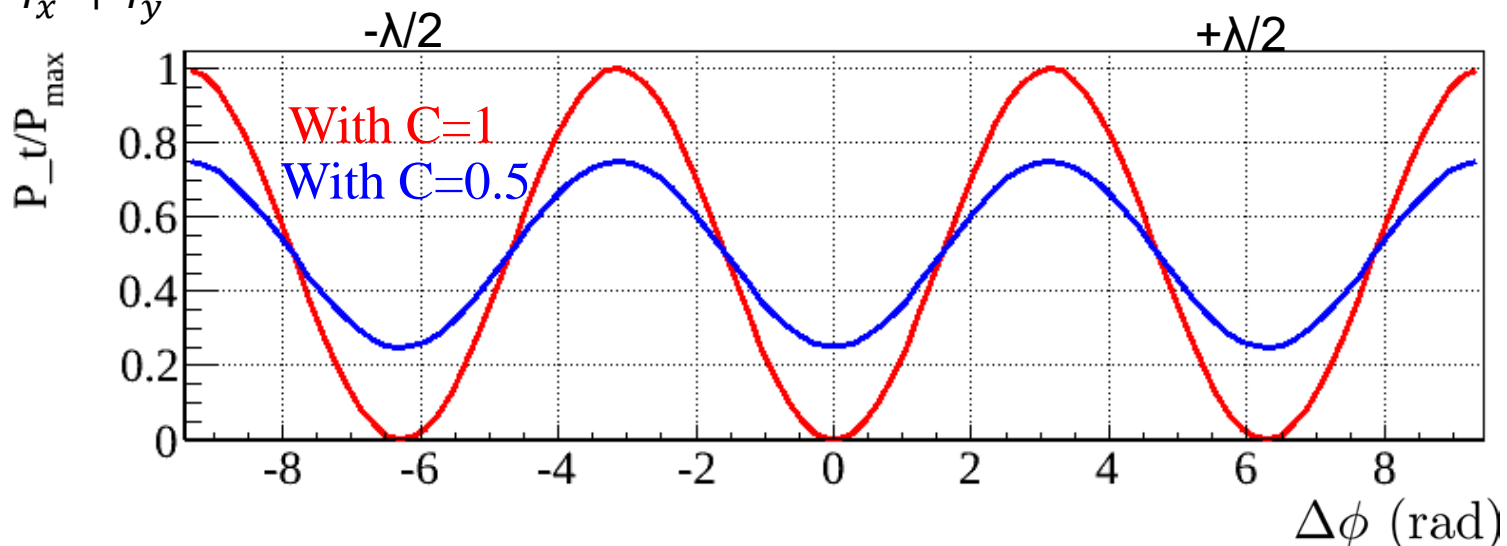
## Transmitted power

$$P_t \propto |U_t|^2 = \frac{P_{max}}{2} (1 - C \cos(\Delta\phi))$$

where  $\Delta\phi = 2k(l_y - l_x)$

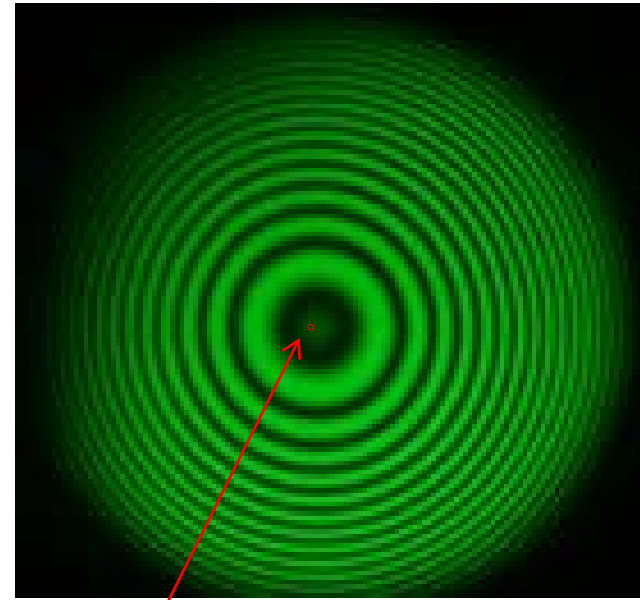
$$\text{ITF contrast: } C = \frac{2r_x r_y}{r_x^2 + r_y^2}$$

$$P_{max} = \frac{P_i}{2} (r_x^2 + r_y^2)$$

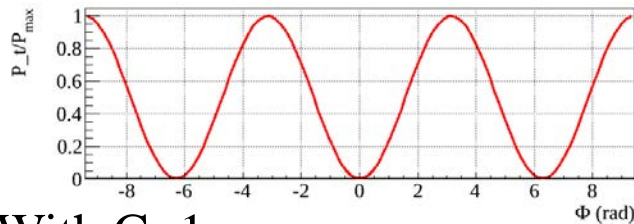


# What power does Virgo measure?

- In general, the beam is not a plane wave but a spherical wave
  - interference pattern  
(and the complementary pattern in reflection)
- Virgo interference pattern much larger than the beam size:
  - ~1 m between two consecutive fringes
  - we do not study the fringes in nice images !



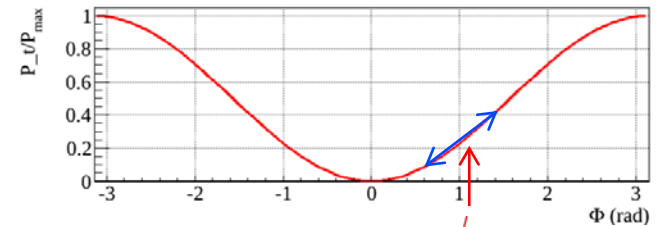
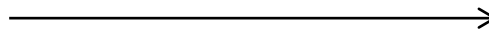
Equivalent size of Virgo beam



With  $C=1$

Freely swinging mirrors

Setting a working point



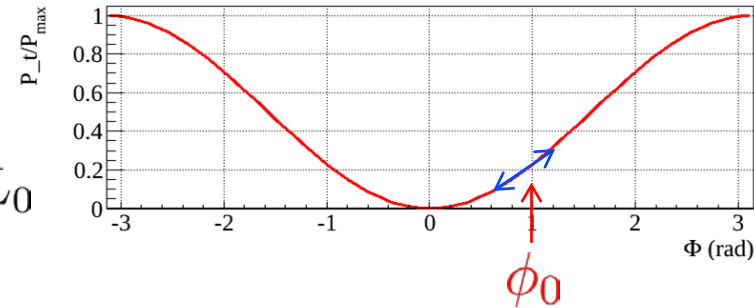
Controlled mirror positions

# From the power to the gravitational wave

$$P_t = \frac{P_i}{2} (1 - C \cos(\phi)) \quad \text{where } \phi = 2\frac{2\pi}{\lambda}(l_y - l_x)$$

- Around the working point:

$$\left. \frac{dP_t}{d\phi} \right|_{\phi_0} = \frac{P_i}{2} C \sin(\phi_0) \quad \text{where } \phi_0 = \frac{4\pi}{\lambda} \Delta L_0$$



- Power variations as function of small differential length variations:

$$\delta P_t = \frac{P_i}{2} C \sin(\phi_0) \delta \phi$$

$$\delta P_t = P_i C \frac{2\pi}{\lambda} \sin\left(\frac{4\pi}{\lambda} \Delta L_0\right) \delta \Delta L$$

$$\delta P_t \propto \delta \Delta L = h L_0 \quad \text{around the working point !}$$

# From the power to the gravitational wave

- Around the working point:

$$\delta P_t = P_i C \frac{2\pi}{\lambda} \sin\left(\frac{4\pi}{\lambda} \Delta L_0\right) \delta \Delta L$$

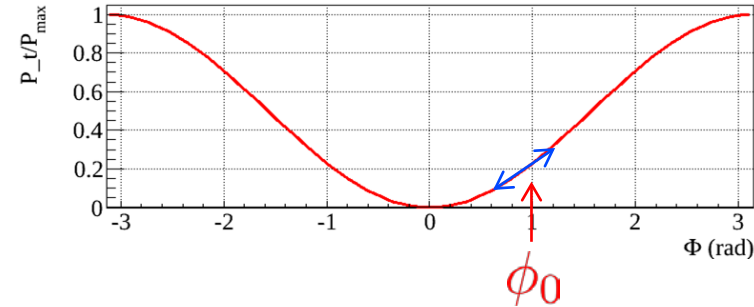
$$\delta P_t = \underbrace{\left(\text{Interferometer response}\right)}_{\text{(W/m)}} \times \delta \Delta L$$



Measurable physical quantity



Physical effect to be detected

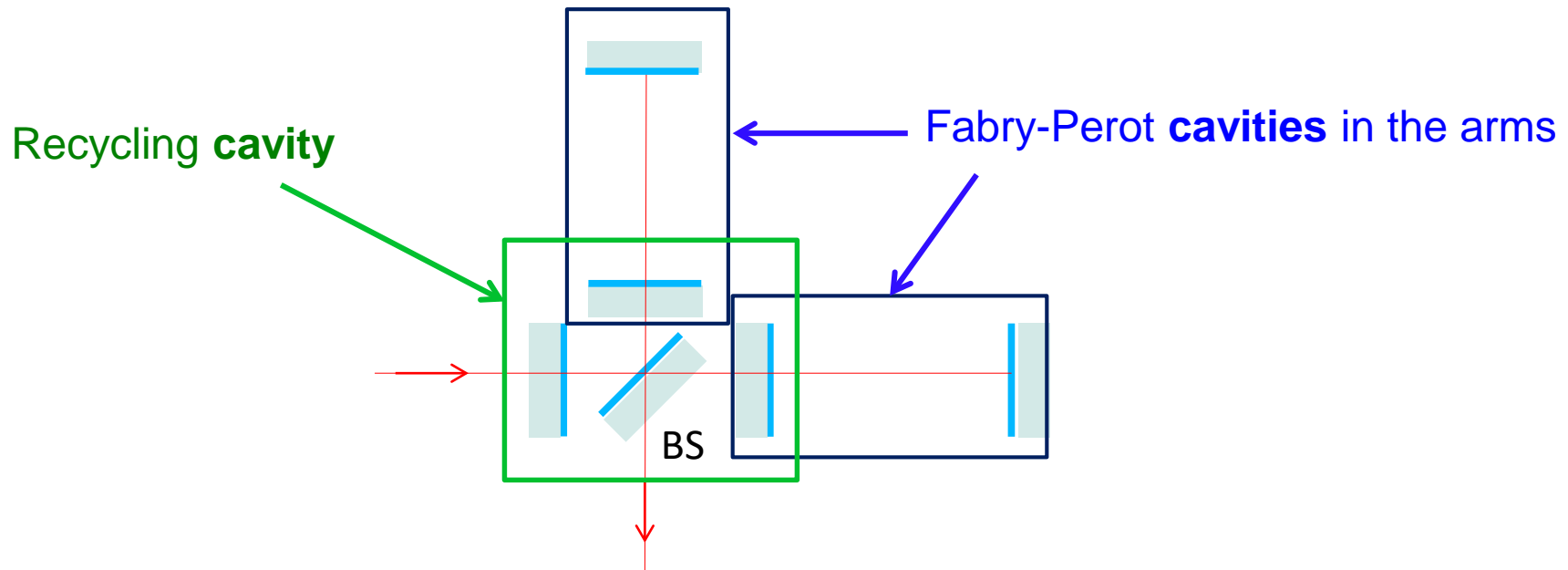


# Improving the interferometer sensitivity

$$\delta P_t = \underbrace{(P_i)}_{\text{Increase the input power on BS}} C \sin\left(\frac{4\pi}{\lambda} \Delta L_0\right) \underbrace{(k \delta \Delta L)}_{\propto \delta \phi}$$

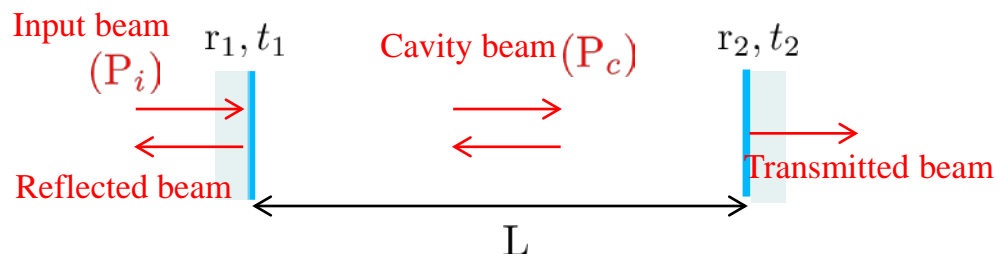
Increase the input power on BS

Increase the phase difference between the arms for a given differential arm length variation





# Beam resonant inside the cavities

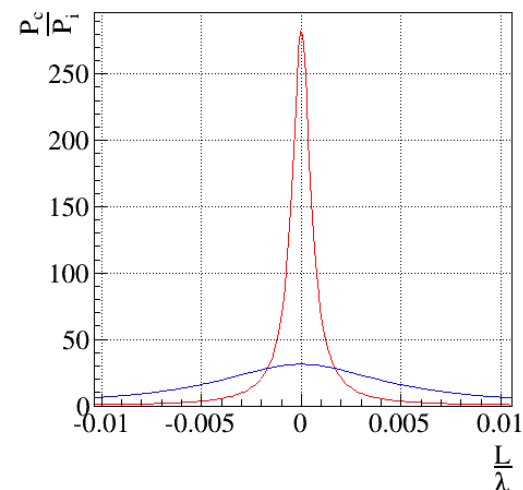
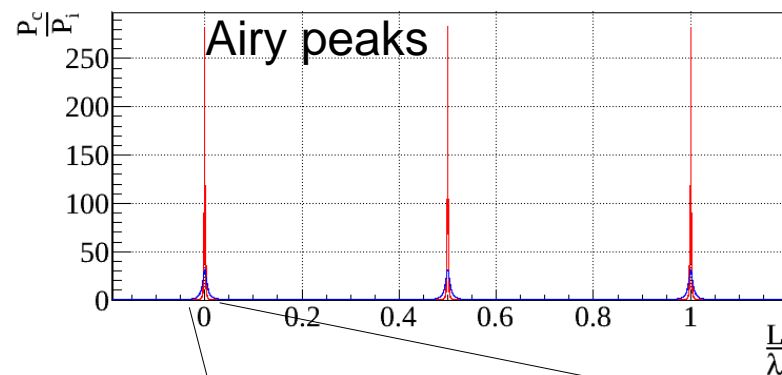


$$P_c = P_i \frac{t_1^2}{(1 - r_1 r_2)^2} \frac{1}{1 + \left(\frac{2\mathcal{F}}{\pi}\right)^2 \sin^2(kL)}$$

$$\text{Finesse } \mathcal{F} = \frac{\pi \sqrt{r_1 r_2}}{1 - r_1 r_2}$$

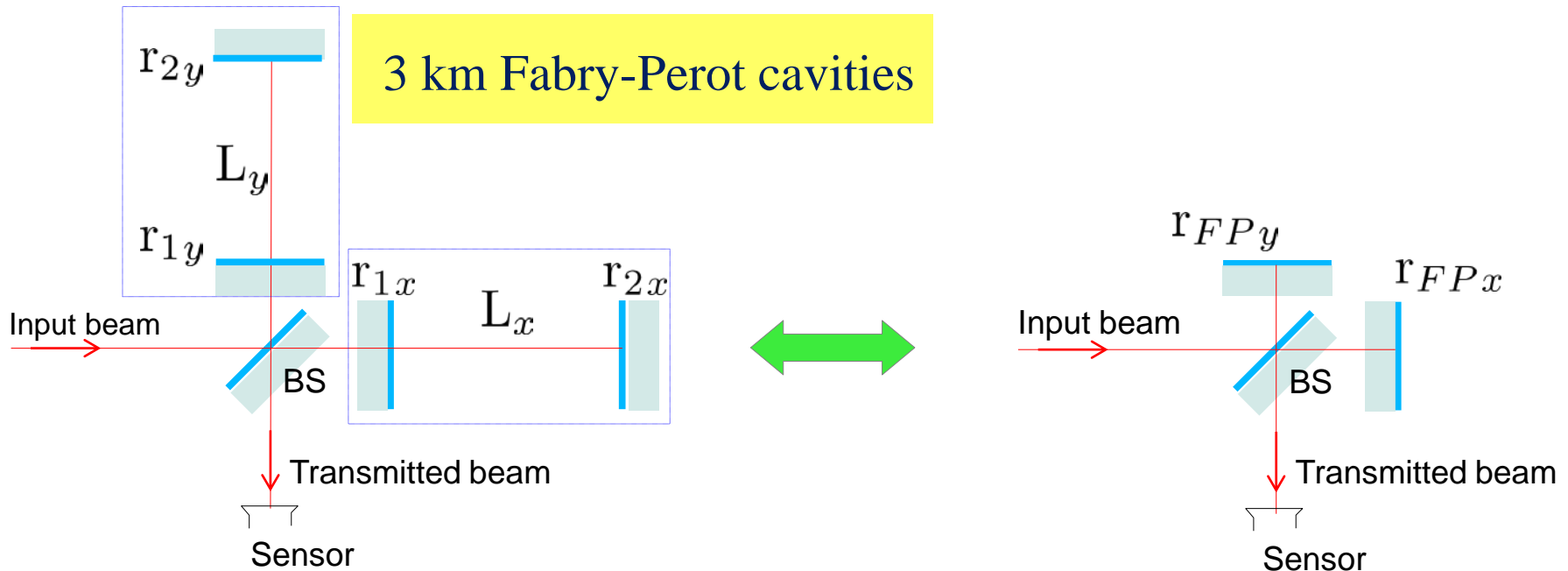
Virgo cavity at resonance:  $L = n \frac{\lambda}{2} \quad (n \in \mathbb{N})$

Virgo  $\mathcal{F} = 50$   
AdVirgo  $\mathcal{F} = 443$



Average number of light round-trips in the cavity:  $N = \frac{2\mathcal{F}}{\pi}$

# How do we amplify the phase offset?



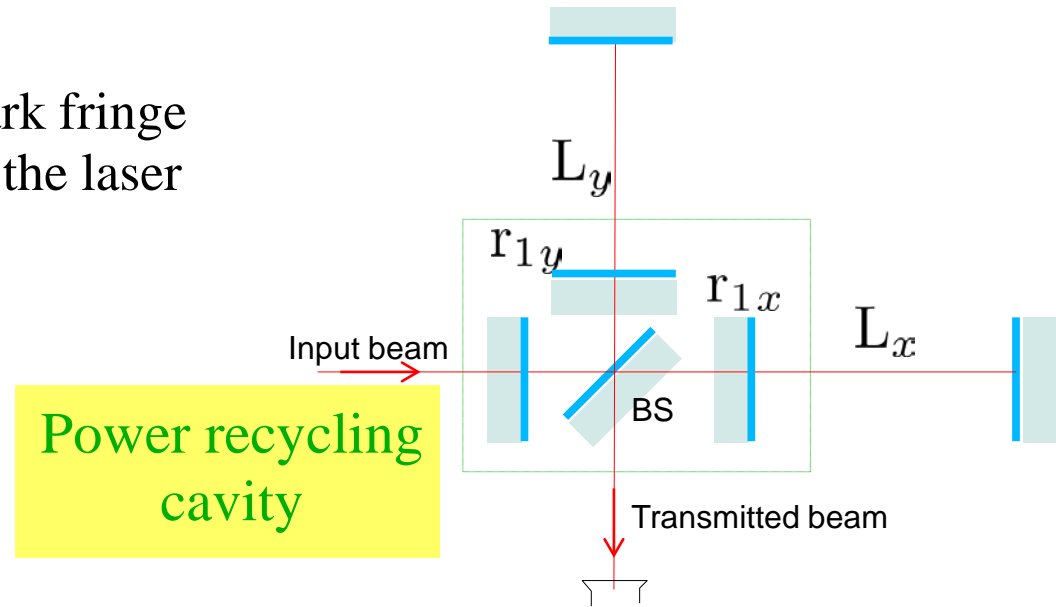
$$r_{FPx} = -1 \times e^{j \frac{2\mathcal{F}}{\pi} 2k \delta L_x}$$

~number of round-trips in the arm  
~300 for AdVirgo

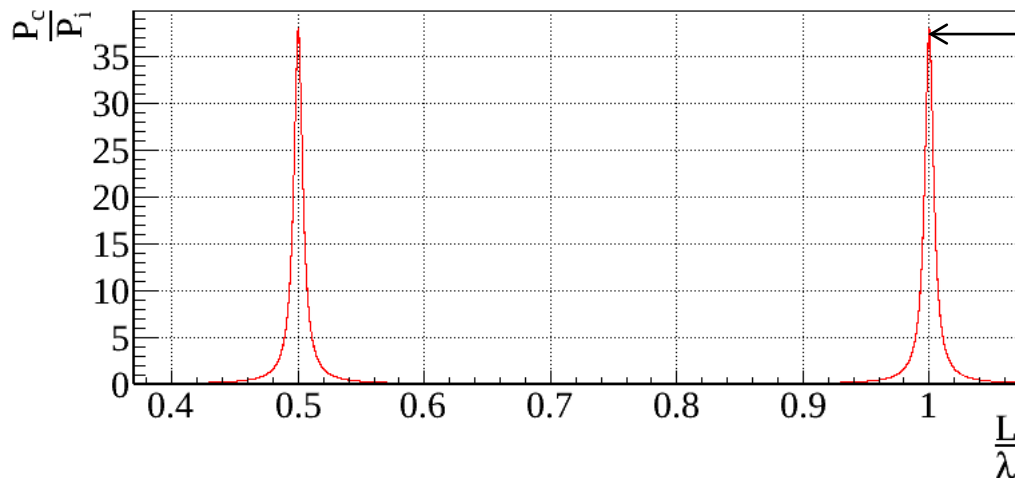
(instead of  $r_{armx} = -1 \times e^{j2k(L_x + \delta L_x)}$  in the arm of a simple Michelson)

# How do we increase the power on BS?

Detector working point close to a dark fringe  
 → most of power go back towards the laser



Resonant power recycling cavity



$$G_{PR} = 38 \quad (r_{PR}^2 = 0.95)$$

→ input power on BS  
 increased by a factor 38!

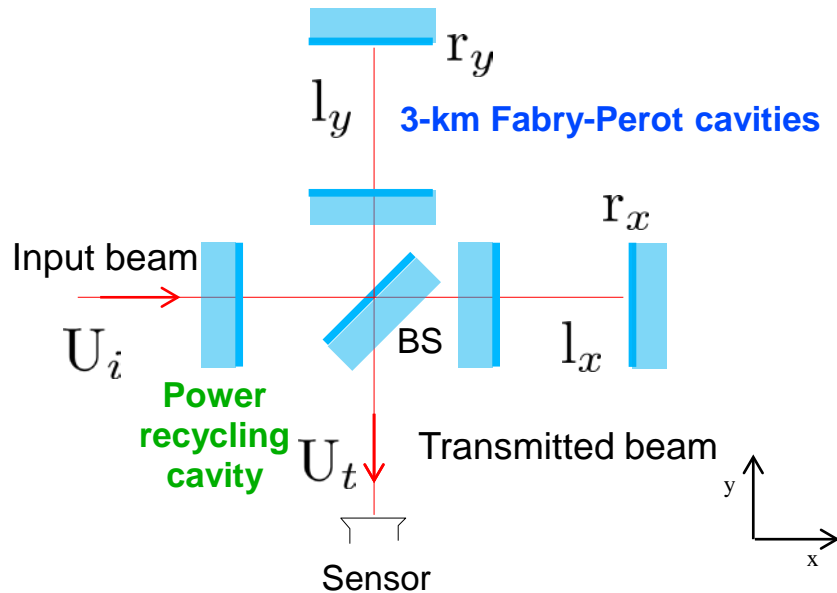
# Improved interferometer response

- Response of simple Michelson:

$$\delta P_t = P_i C \frac{2\pi}{\lambda} \sin\left(\frac{4\pi}{\lambda} \Delta L_0\right) \delta \Delta L$$

$$\delta P_t = (\text{Michelson response}) \times \delta \Delta L \quad (\text{W/m})$$

- Response of recycled Michelson with Fabry-Perot cavities:



$$\delta P_t = G_{PR} P_i C \frac{2\pi}{\lambda} \sin\left(\frac{4\pi}{\lambda} \Delta L_0\right) \frac{2\mathcal{F}}{\pi} \delta \Delta L$$

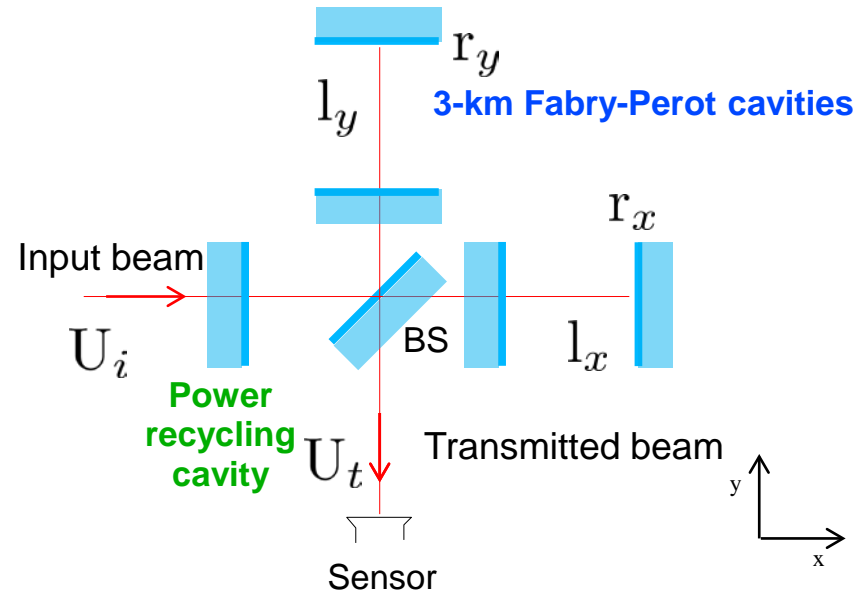
$\sim 38$ 
 $\sim 300$

**For the same  $\delta \Delta L$ ,  $\delta P_t$  has been increased by a factor  $\sim 12000$**

# Order of magnitude of the « sensitivity »

$$\delta P_t = G_{PR} P_i C \frac{2\pi}{\lambda} \sin\left(\frac{4\pi}{\lambda} \Delta L_0\right) \frac{2\mathcal{F}}{\pi} \delta \Delta L$$

Laser wavelength	$\lambda = 1064 \text{ nm}$
Input power	$P_i \sim 100 \text{ W}$
Interferometer contrast	$C \sim 1$
Cavity finesse	$\mathcal{F} \sim 450$
Power recycling gain	$G_{PR} \sim 38$
Working point	$\Delta L_0 \sim 10^{-11} \text{ m}$



Shot noise due to output power of  $\sim 50 \text{ mW}$

$$\rightarrow \delta P_{t,min} \sim 0.1 \text{ nW} \quad \longrightarrow$$

$$\delta \Delta L_{min} \sim 5 \times 10^{-20} \text{ m}$$

$$\rightarrow h_{min} = \frac{\delta \Delta L_{min}}{L} \sim 10^{-23}$$



*In reality, the detector response depends on frequency...*

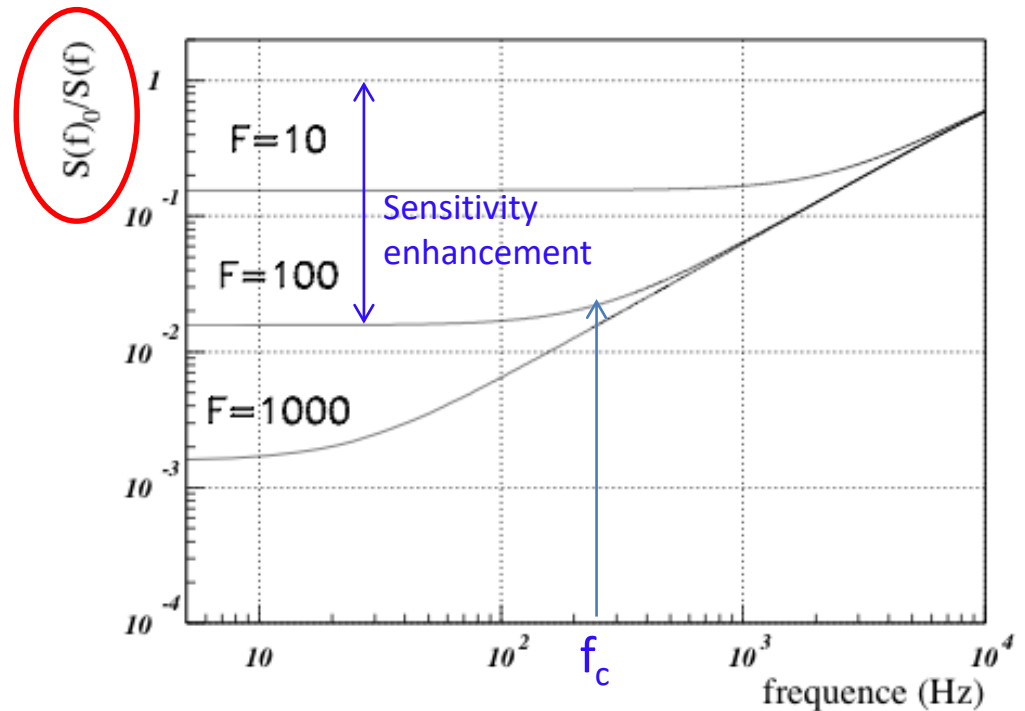


# Example of frequency dependency of the ITF response

- Light travel time in the cavities must be taken into account
- Fabry-Perot cavities behave as a low pass filter
- Frequency cut-off:

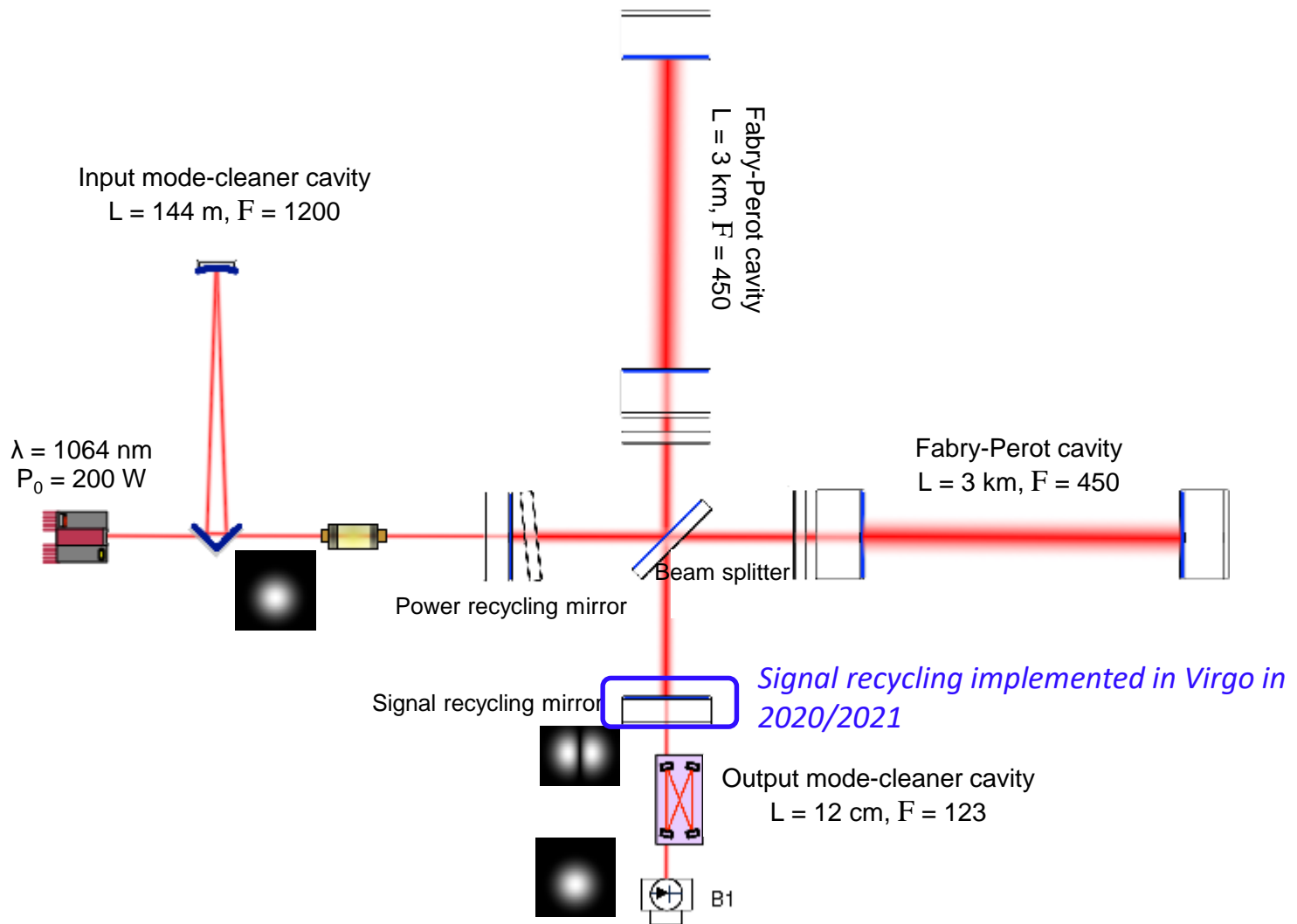
$$f_c = \frac{c}{4FL}$$

Ratio between the sensitivity of an interferometer with Fabry-Perot cavities versus the sensitivity of an interferometer without cavities



- Finesse of Virgo Fabry Perot cavities:  $F = 450$ ,  $L = 3$  km  $\rightarrow$   $f_c = 55$  Hz

# Optical layout of Virgo



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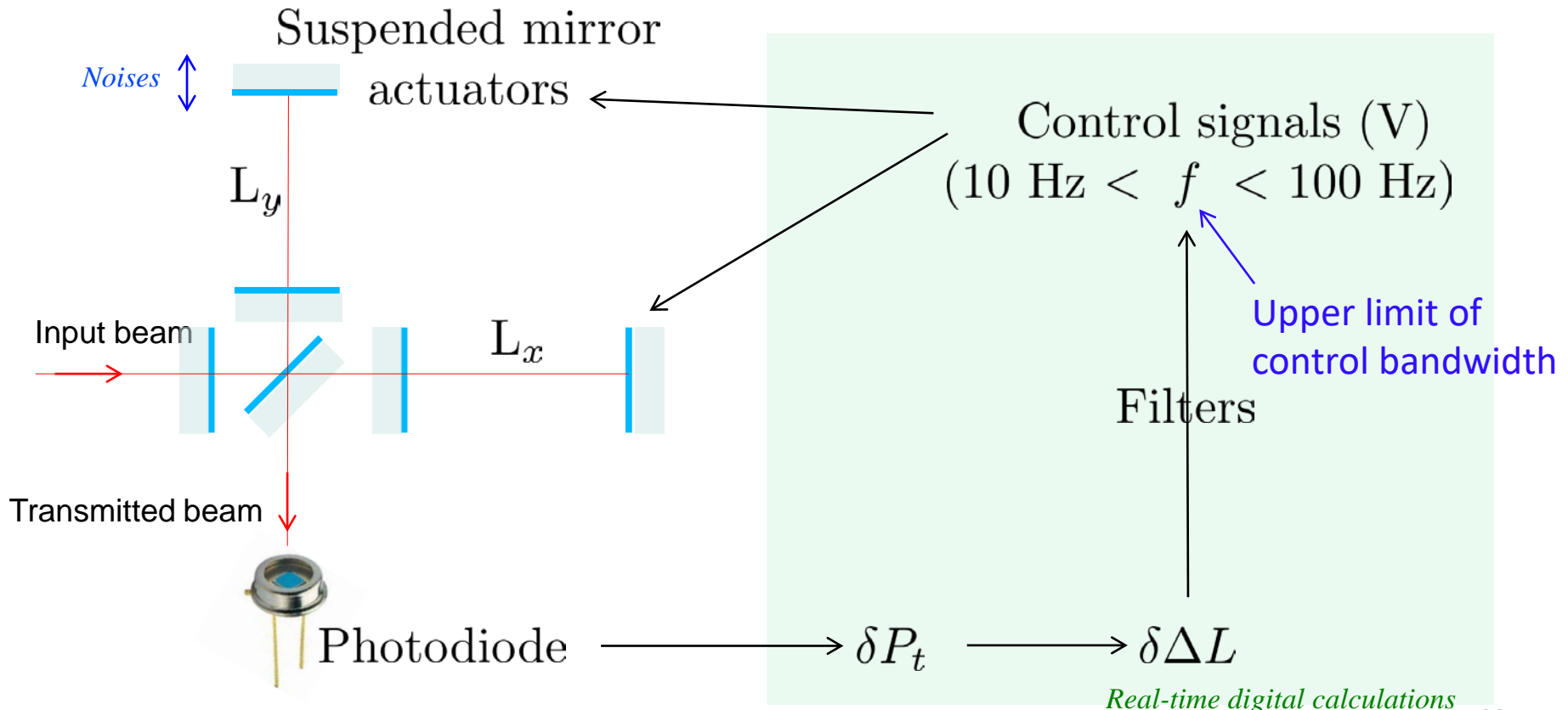


# How do we control the working point?



Small offset from a dark fringe:  $\Delta L_0 = n \frac{\lambda}{2} + 10^{-11} \text{ m}$

- Controls to reduce the motion up to  $\sim 100 \text{ Hz}$
- Precision of the control  $\delta \Delta L_{true} \sim 10^{-15} \text{ m}$

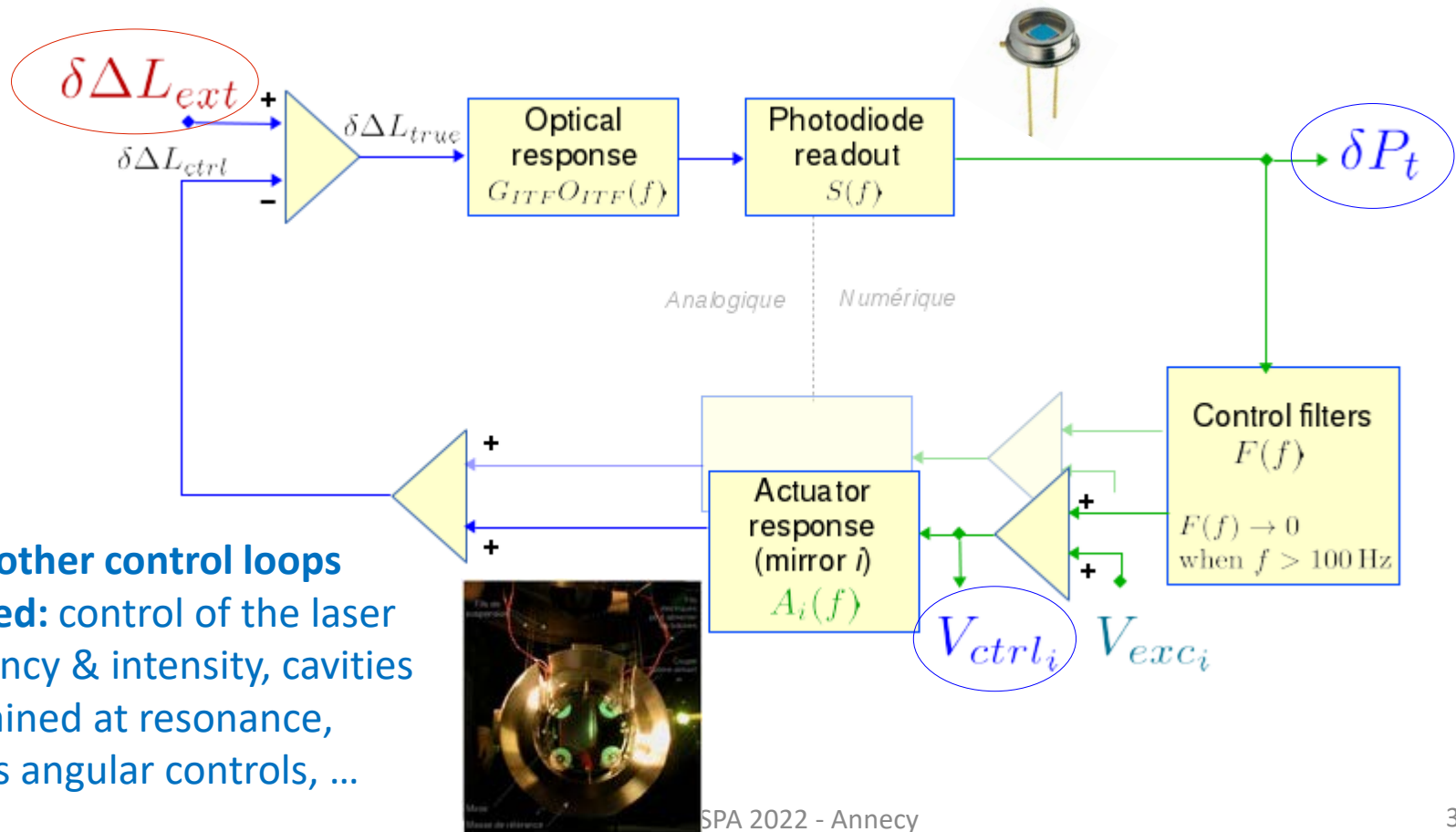


# How do we control the working point?

Small offset from a dark fringe:  $\Delta L_0 = n \frac{\lambda}{2} + 10^{-11} \text{ m}$

- Controls to reduce the motion up to  $\sim 100 \text{ Hz}$
- Precision of the control  $\delta \Delta L_{true} \sim 10^{-15} \text{ m}$

$$\delta \Delta L_{ext} = \delta \Delta L_{noise} + \delta \Delta L_{GW}$$



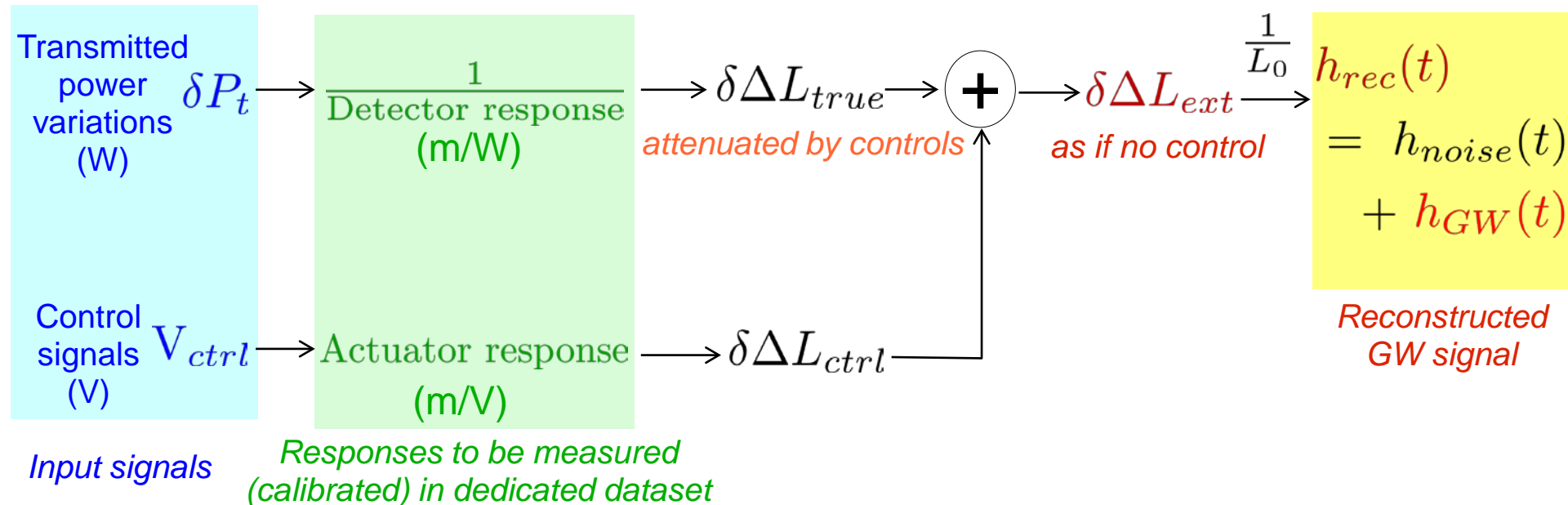
**Many other control loops required:** control of the laser frequency & intensity, cavities maintained at resonance, mirrors angular controls, ...

# From the detector data to the GW strain $h(t)$

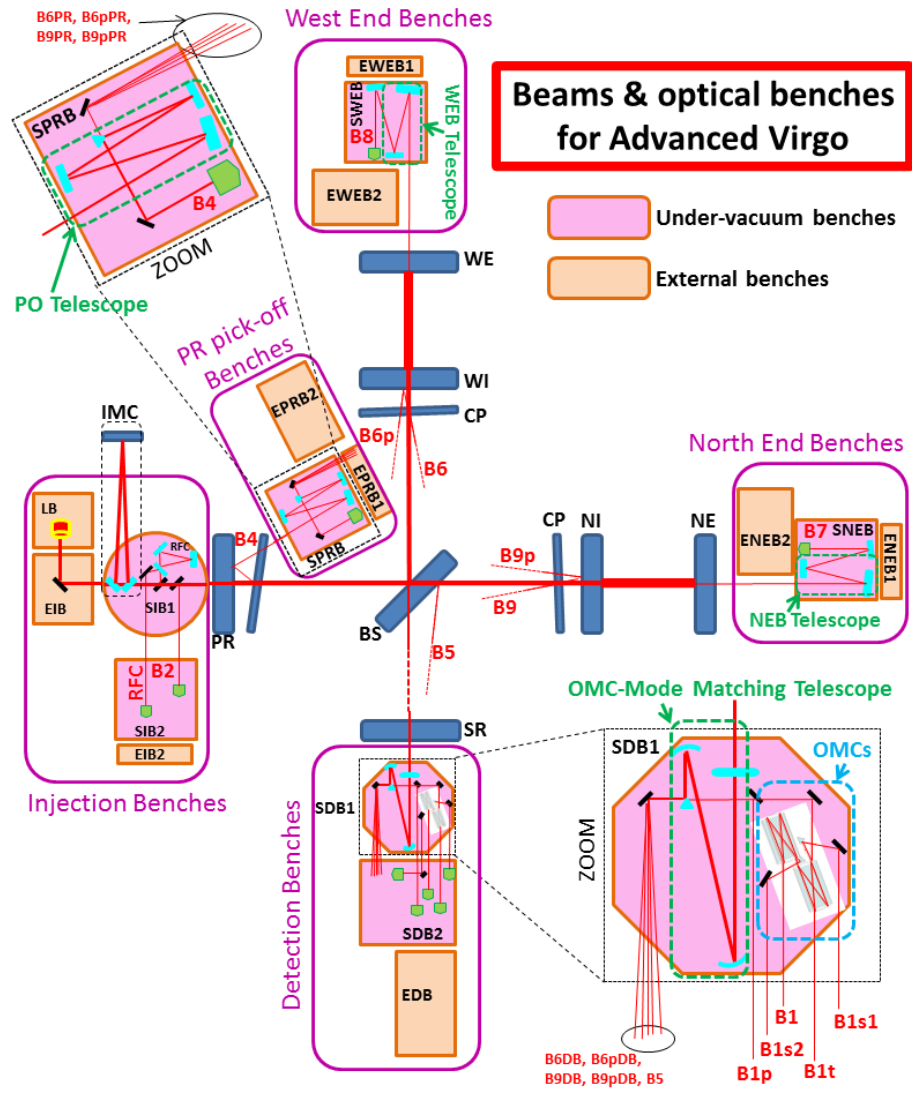
- High frequency ( $>100$  Hz): mirrors behave as free falling masses

$$\rightarrow h(t) = \frac{\delta\Delta L_{true}(t)}{L_0}$$

- Lower frequency: the controls attenuate the noise... but also the GW signal!  
 $\rightarrow$  the control signals contain information on  $h(t)$



# How to extract all error signals? Interferometer optical ports

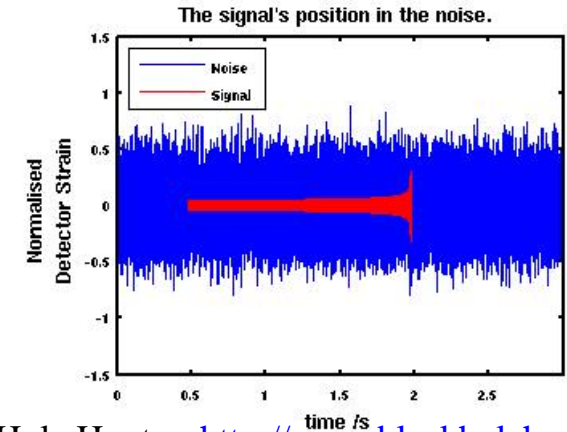
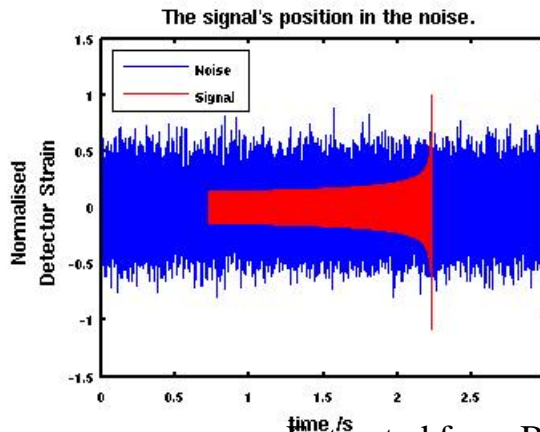
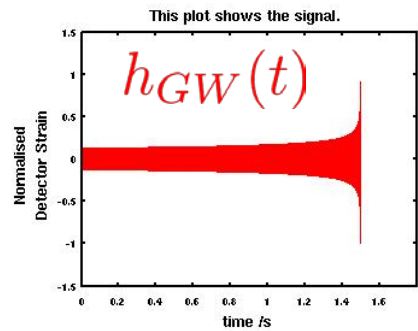
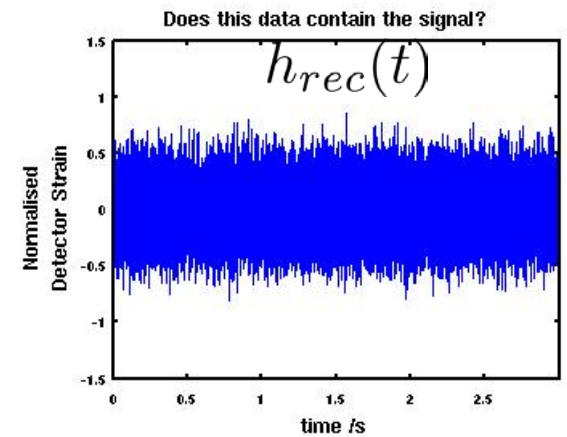
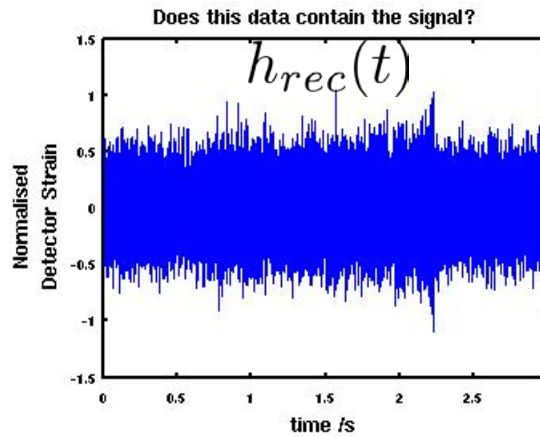
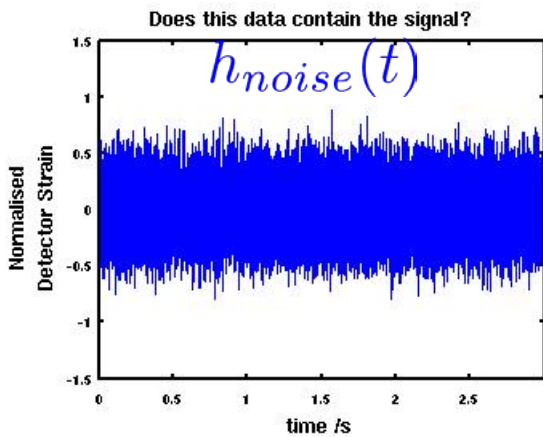


**Noises limiting interferometer  
sensitivity:  
How to tackle them ?**

# What is noise in GW detectors ?

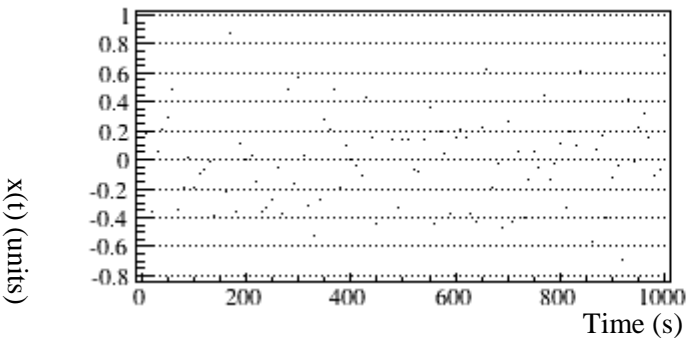
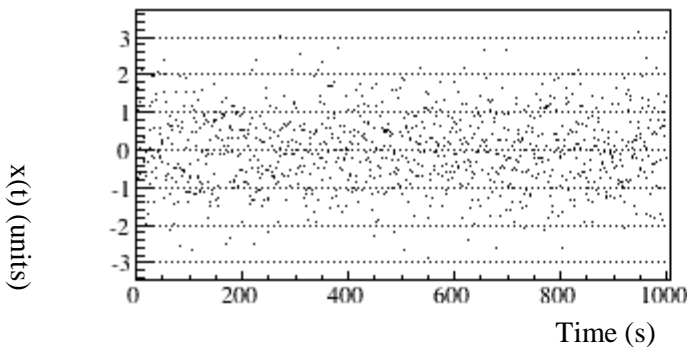
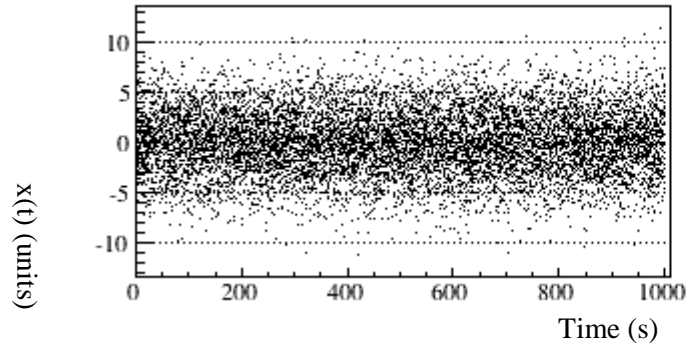
- Stochastic (random) signal that contributes to the signal  $h_{rec}(t)$  but does not contain information on the gravitational wave strain  $h_{GW}(t)$

$$h_{rec}(t) = h_{noise}(t) + h_{GW}(t)$$

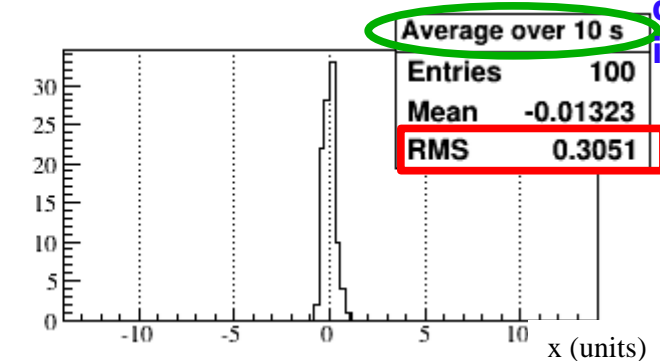
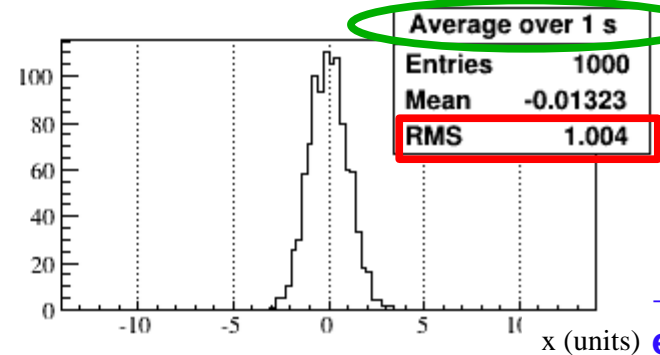
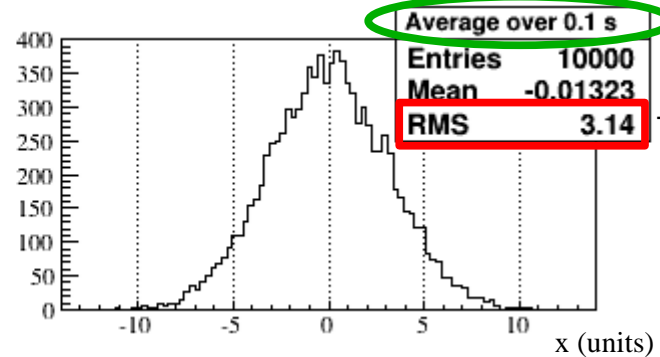


# How do we characterize noise?

## Data points (noise)



## Distribution of the data



→ Noise characterised by its standard deviation  $\sigma_x$

$$\sigma_x = \frac{D}{\sqrt{\text{average duration}}}$$

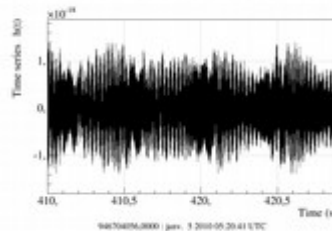
$D$  is in (Data units  $\times \sqrt{s}$ )  
or  $\frac{\text{Data units}}{\sqrt{\text{Hz}}}$

→ its absolute value is equal to the standard deviation of the noise when it is averaged over 1 s

# From hrec(t) to Virgo sensitivity curve

1/ Reconstruction of  $h(t)$

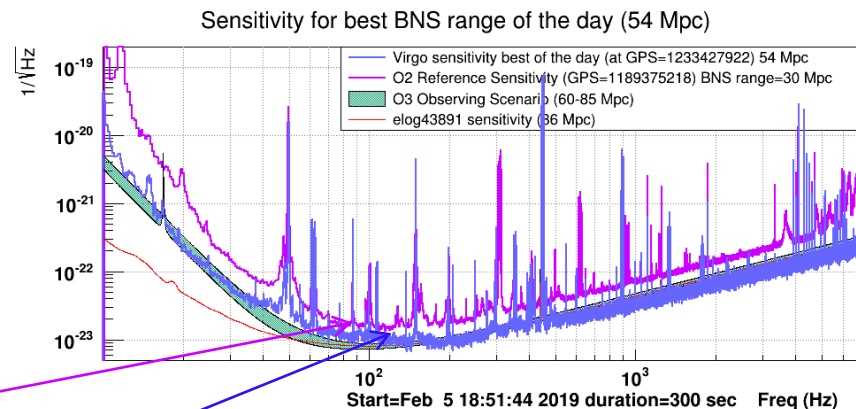
$$h_{rec}(t) = h_{noise}(t) + h_{GW}(t)$$



2/ Amplitude spectral density of  $h(t)$   
(noise standard deviation over 1 s)

$$ASD = \sqrt{PSD} = \sqrt{\frac{|DFT|^2}{T}}$$

Discrete Fourier Transform (DFT)



$\sim 5 \times 10^{-20}$  m/ $\sqrt{\text{Hz}}$  (Advanced Virgo O2, 2017)

$\sim 3 \times 10^{-20}$  m/ $\sqrt{\text{Hz}}$  (Advanced Virgo in Feb 2019)

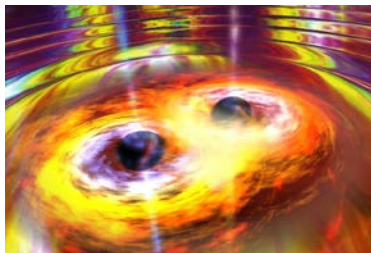


Image: Danna Berry/SkyWorks/NASA

## Compact Binary Coalescences

Signal lasts for a few seconds

→ can detect  $h \sim 10^{-23}$

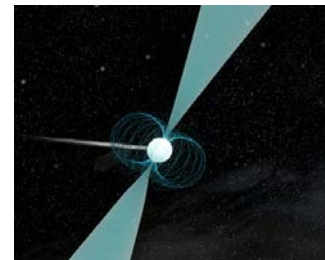


Image: B. Saxton (NRAO/AUI/NSF)

## Rotating neutron stars

Signal averaged over days ( $\sim 10^6$  s)

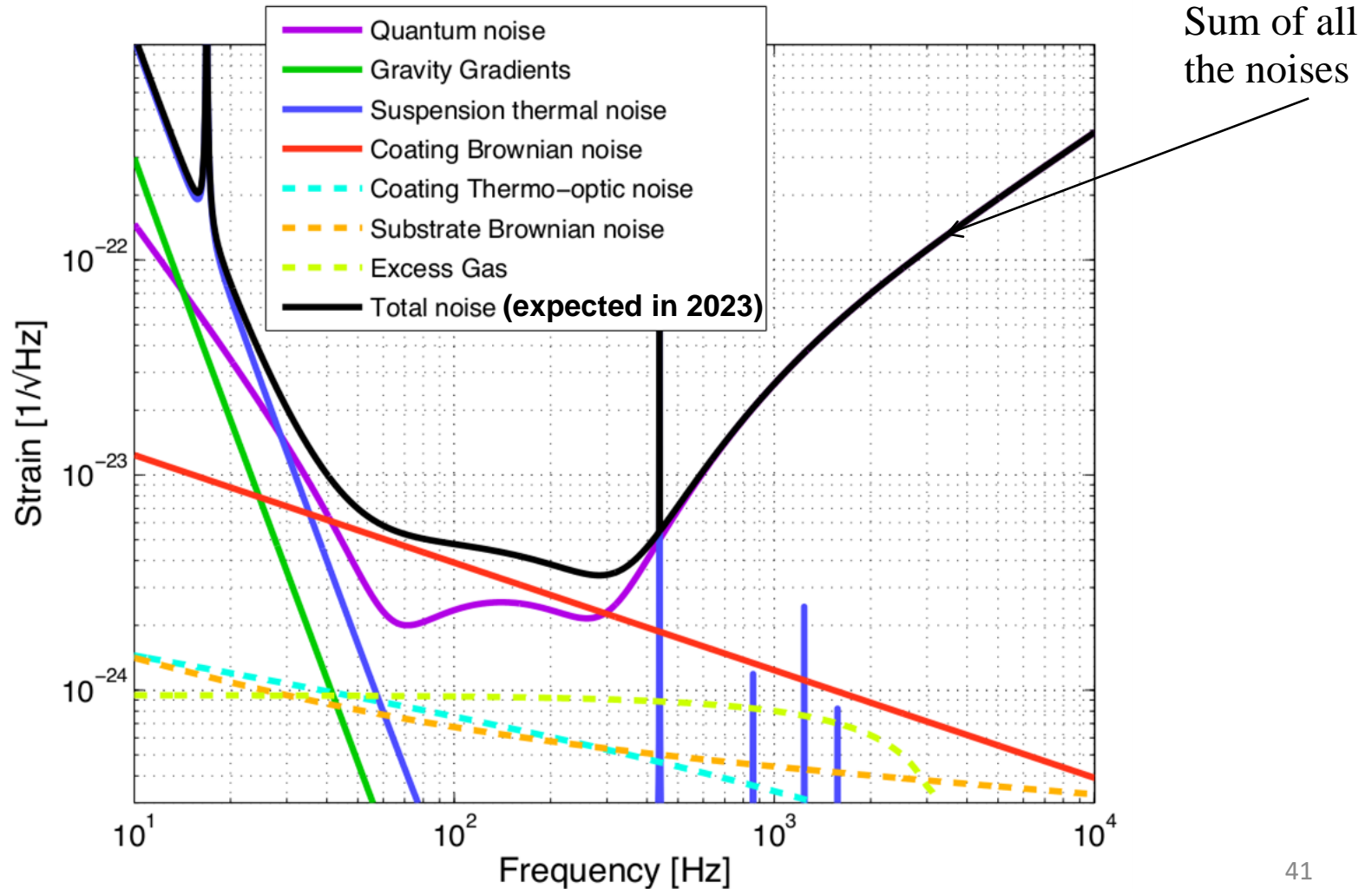
→ can detect  $h \sim 10^{-26}$



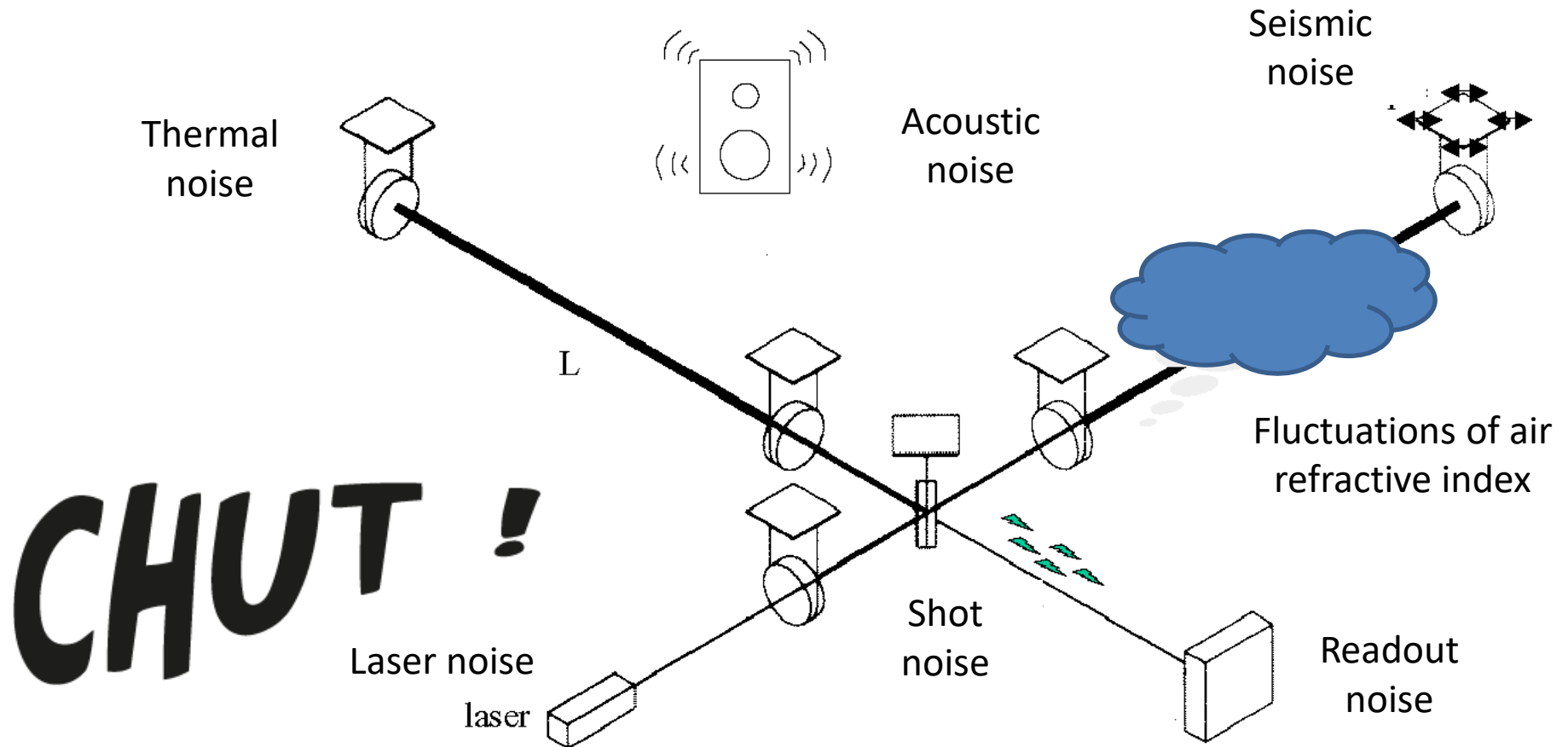
# Nominal sensitivity of Advanced Virgo

Fundamental noise only

Possible technical noise not shown



# Fundamental noise sources



# Under vacuum

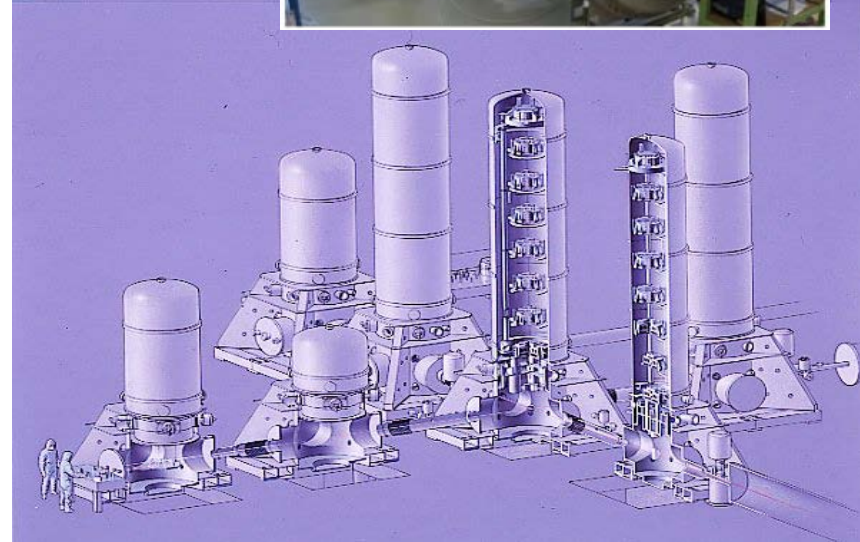


## Goals

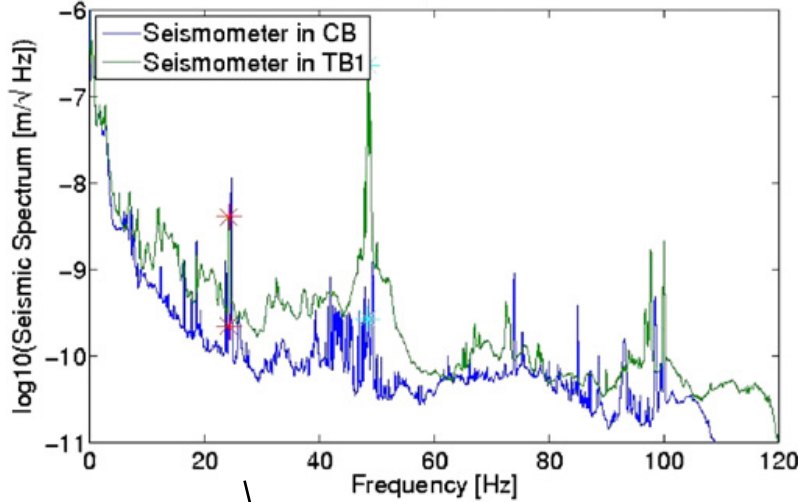
- ❑ Isolation against acoustic noise
- ❑ Avoid measurement noise due to fluctuations of air refractive index
- ❑ Keep mirrors clean

## Advanced Virgo vacuum in a few numbers:

- ❑ Volume of vacuum system: 7000 m<sup>3</sup>
- ❑ Different levels of vacuum:
  - 3 km arms designed for up to 10<sup>-9</sup> mbar (Ultra High Vacuum)
  - ~10<sup>-6</sup> - 10<sup>-7</sup> mbar in mirror vacuum chambers (« towers »)
- ❑ Separation between arms and towers with cryotrap links

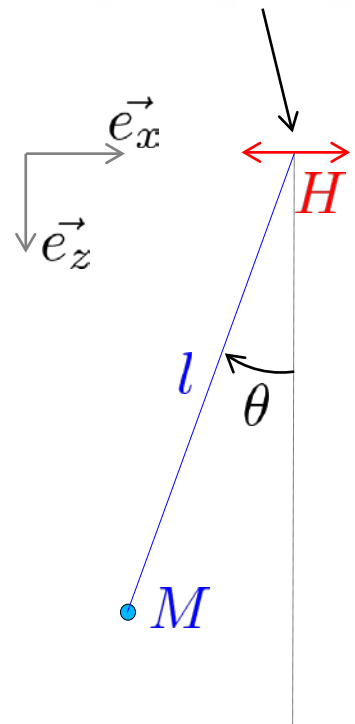


# Seismic noise and suspended mirrors



Ground vibrations up to  $\sim 1 \mu\text{m}/\sqrt{\text{Hz}}$  at low frequency decreasing down to  $\sim 10 \text{ pm}/\sqrt{\text{Hz}}$  at 100 Hz

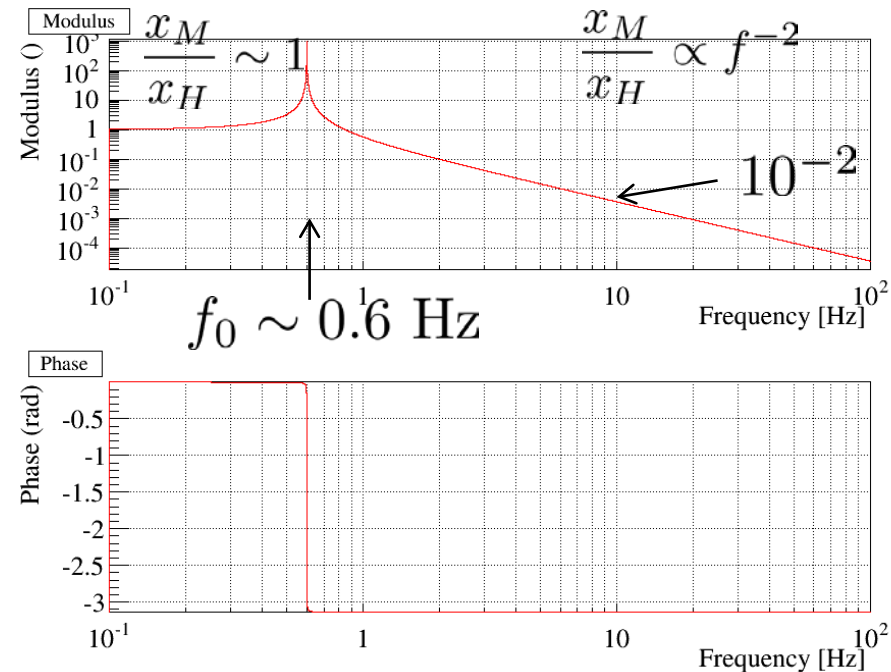
$\gg 10^{-19} \text{ m}/\sqrt{\text{Hz}}$  needed to detect GW !!



Assuming  $\delta x_H$  small and sinusoidal and  $\theta$  small:

$$\underline{x}_M = \underline{\mathcal{H}} \times \underline{x}_H$$

Transfer function



# Seismic noise: Virgo super-attenuators



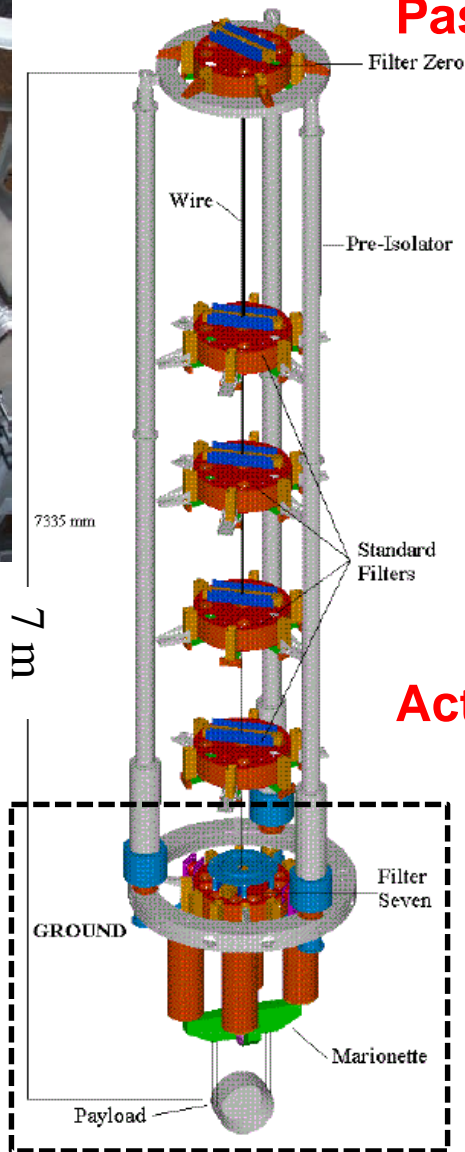
**Passive attenuation:** 7 pendulum in cascade

$$\text{At } 10 \text{ Hz: } \frac{x_{\text{mirror}}}{x_{\text{ground}}} \sim (10^{-2})^7 = 10^{-14}$$

$$x_{\text{ground}} \sim 10^{-9} \text{ m}/\sqrt{\text{Hz}}$$

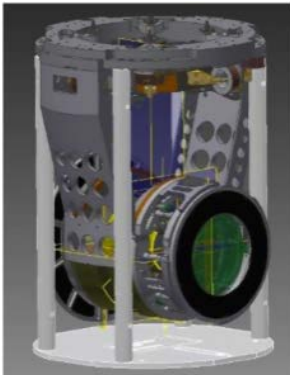
$$\rightarrow x_{\text{mirror}} \sim 10^{-23} \text{ m}/\sqrt{\text{Hz}}$$

This noise directly modifies the positions of the mirror surfaces, and thus  $\delta\Delta L$  and  $h_{\text{rec}}(t)$  !



**Active controls** at low frequency

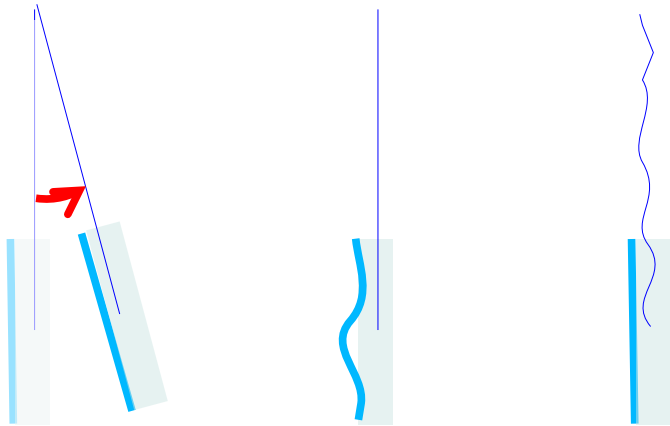
- Accelerometers or interferometer data
- Electromagnetic actuators
- Control loops



# Thermal noise (pendulum and coating)

Microscopic thermal fluctuations

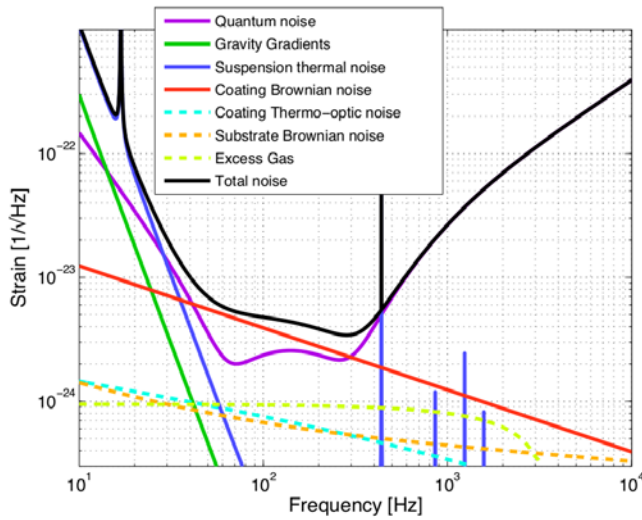
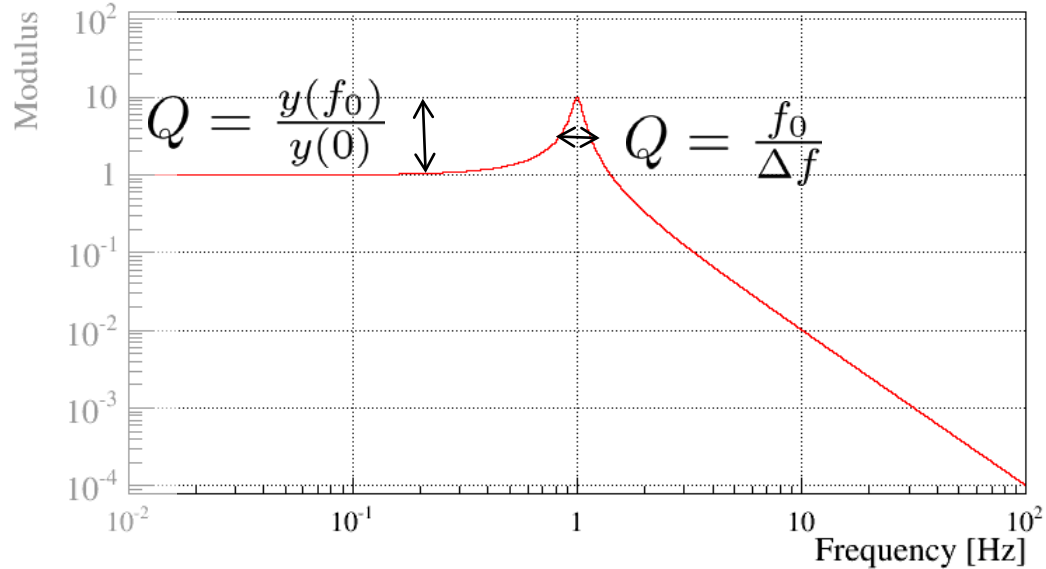
→ dissipation of energy through excitation of the macroscopic modes of the mirror



Pendulum mode  
 $f < 40$  Hz

“Mirror” mode  
 $f > \text{few kHz}$

“Violin” modes  
 $f > 40$  Hz

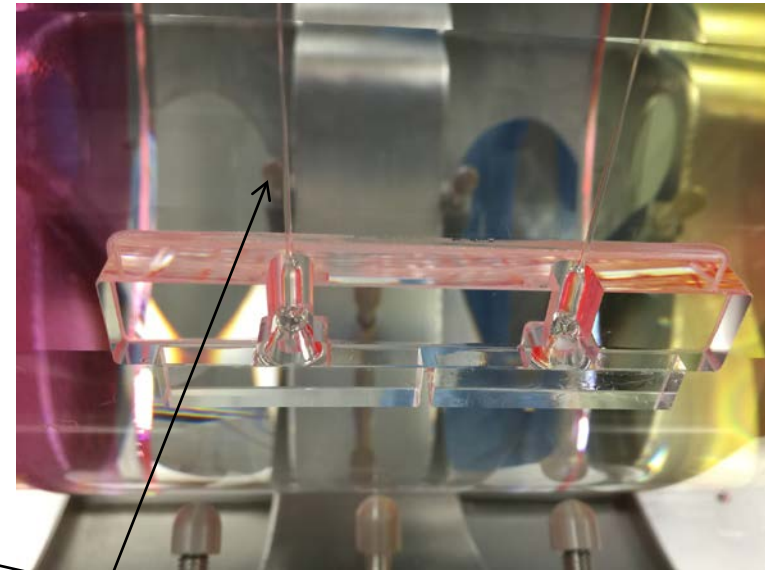
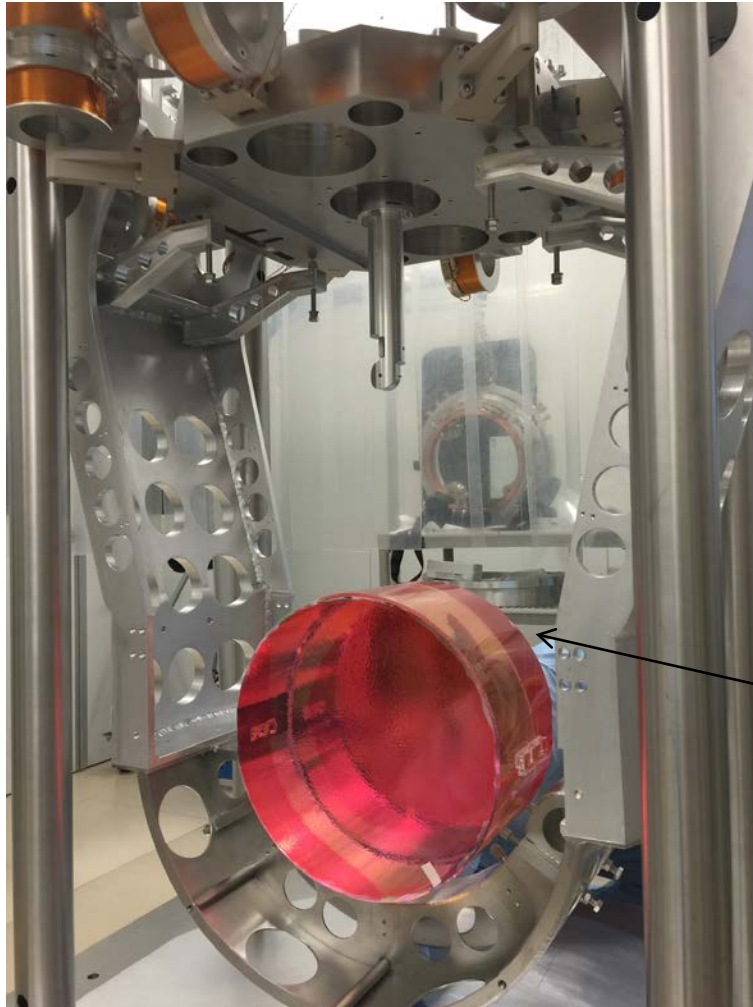


This noise directly modifies the positions of the mirror surfaces, and thus  $\delta\Delta L$  and  $h_{rec}(t)$  !

**We want high quality factors Q to concentrate all the noise in a small frequency band**

# Reduction of thermal noise: monolithic suspensions

- Increase the quality factor of the mirrors (with respect to steel wires)
- **Monolithic suspension** developed in labs in Perugia and Rome



Fused-silica fibers:

- Diameter of 400  $\mu\text{m}$
- length of 0.7 m
- Load stress: 800 Mpa

# Reduction of thermal noise: mirror coating



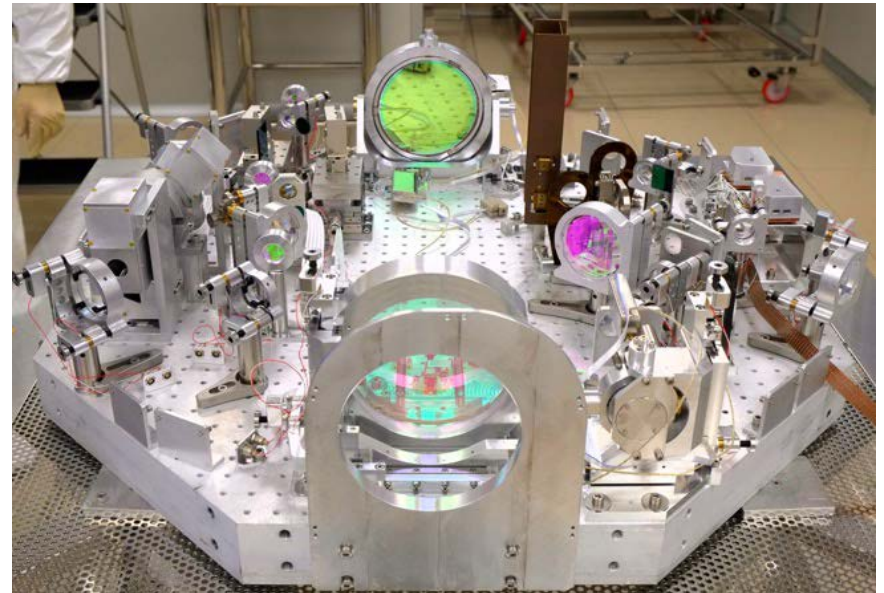
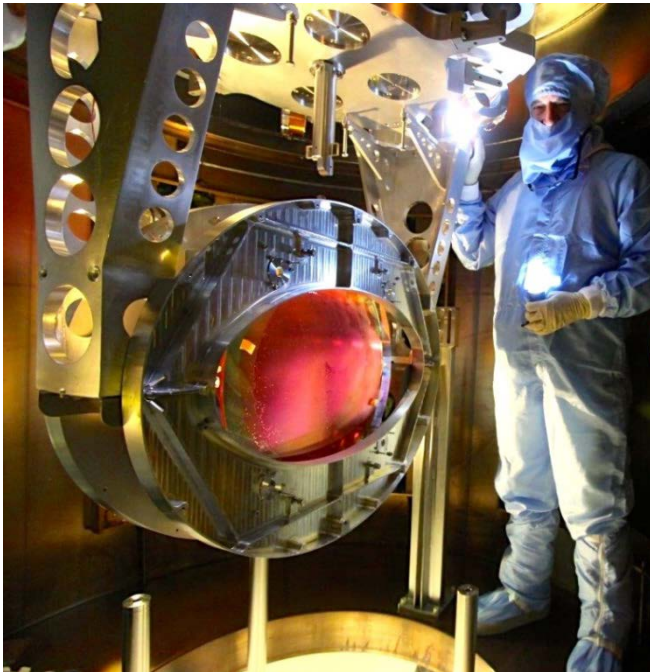
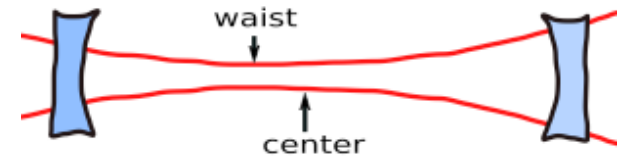
40 kg mirrors of Advanced Virgo  
35 cm diameter, 40 cm width  
Suprasil fused silica

- Currently the main source of thermal noise
- Very high quality mirror coating developed in a lab close to Lyon (Laboratoire des Matériaux Avancés)
- R&D to improve mechanical properties of coating
- Cryogenics mirrors (at Kagra, future detectors)
  - other substrate
  - other coating
  - other wavelength



# Thermal noise: coupling reduction

- Reduce the coupling between the laser beam and the thermal fluctuations
  - **use large beams**: fluctuations averaged over larger surface
  - Thermal Noise  $\sim 1/D$ , with  $D$  = beam diameter
- Impact of large beams:
  - Require large mirrors (and heavier):
    - > Advanced Virgo beam splitter diameter = 55 cm
  - High magnification telescopes to adapt beam size to photodetectors (from  $w=50$  mm on mirrors to  $w=0.3$  mm on sensors) > require optical benches

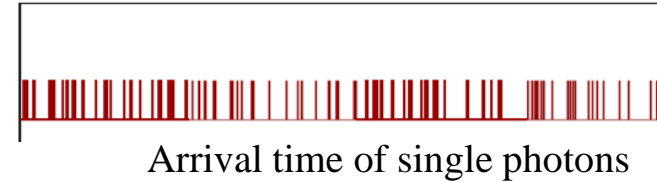


# Shot noise

## Fluctuations of arrival times of photons (quantum noise)

Power received by the photodiode:  $P_t$

$$\rightarrow N = \frac{P_t}{h\nu} \text{ photons/s on average.}$$



Standard deviation on this number:  $\sigma_N = \sqrt{N}$

$$\rightarrow \sigma_{P_t} = \sigma_N \times h\nu = \sqrt{\frac{P_t}{h\nu}} h\nu = \sqrt{P_t h\nu}$$

Virgo laser:  $\lambda = 1.064 \mu\text{m} \rightarrow \nu = \frac{c}{\lambda} \sim 2.8 \times 10^{14} \text{ Hz}$

Working point:  $P_t \sim 80 \text{ mW} \rightarrow \sigma_{P_t} = 0.1 \text{ nW}/\sqrt{\text{Hz}}$

$\rightarrow$  a variation of power is interpreted as a variation of distance  $\delta\Delta L$

$$\delta P_t = (\text{Virgo response}) \times L_0 \times h \quad h_{\text{equivalent}} = \frac{1}{L_0} \frac{\sigma_{P_t}}{(\text{Virgo response})}$$

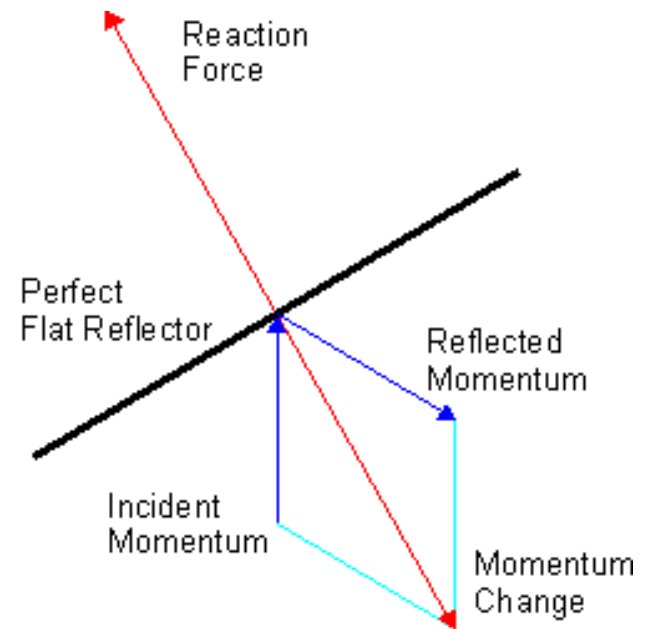
(in W/m)

$$\rightarrow \mathbf{h_{\text{equivalent}} \propto 1/\sqrt{P}}$$

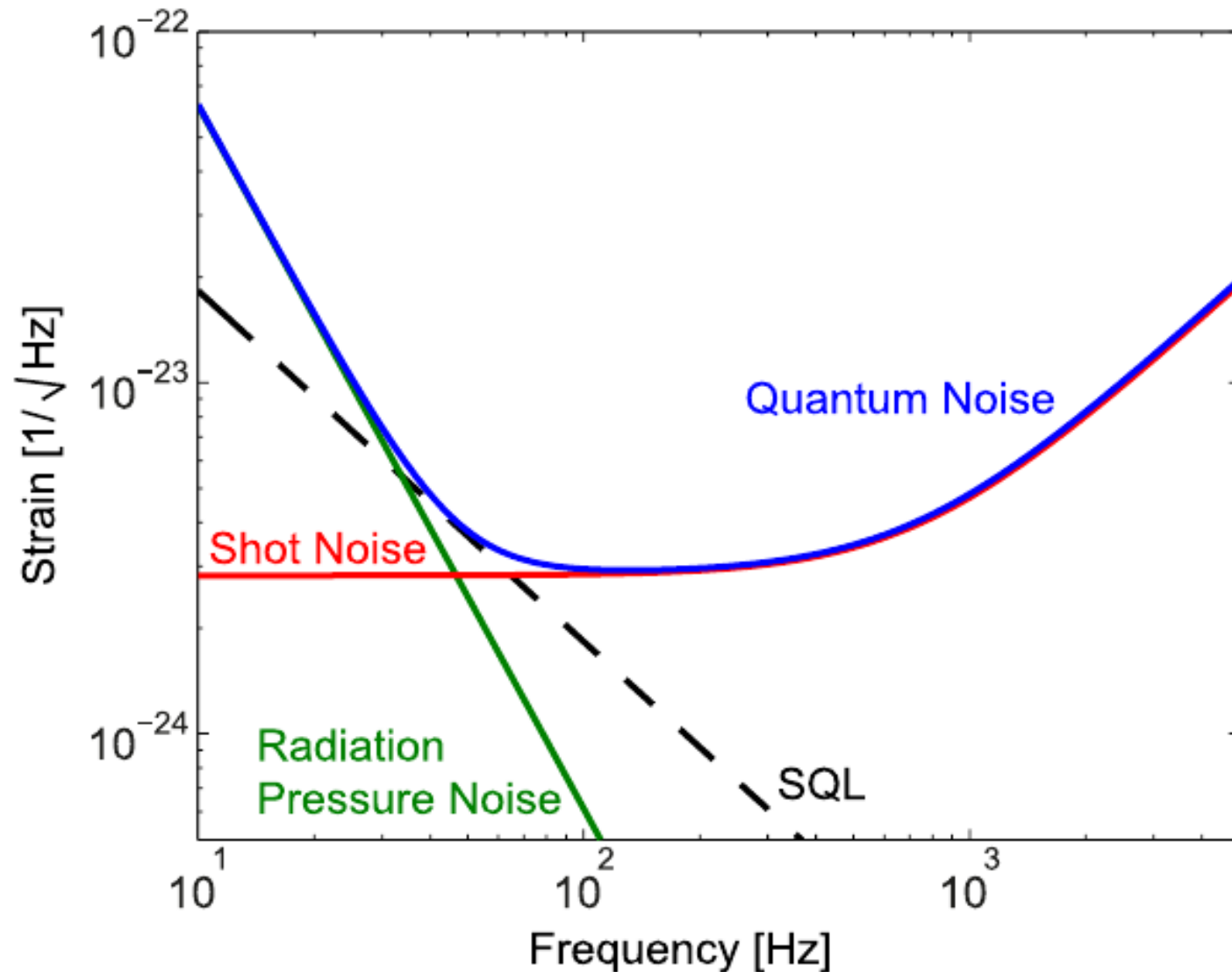
# Radiation pressure noise

- Radiation pressure: transfer of photon's momentum to the reflective surface (recoil force)
- Radiation pressure noise: due to fluctuations of number of photons hitting the mirror surfaces > mirror motion noise
- Radiation pressure noise impact at low frequency:
  - > Mirror motion filtered by pendulum mechanical response

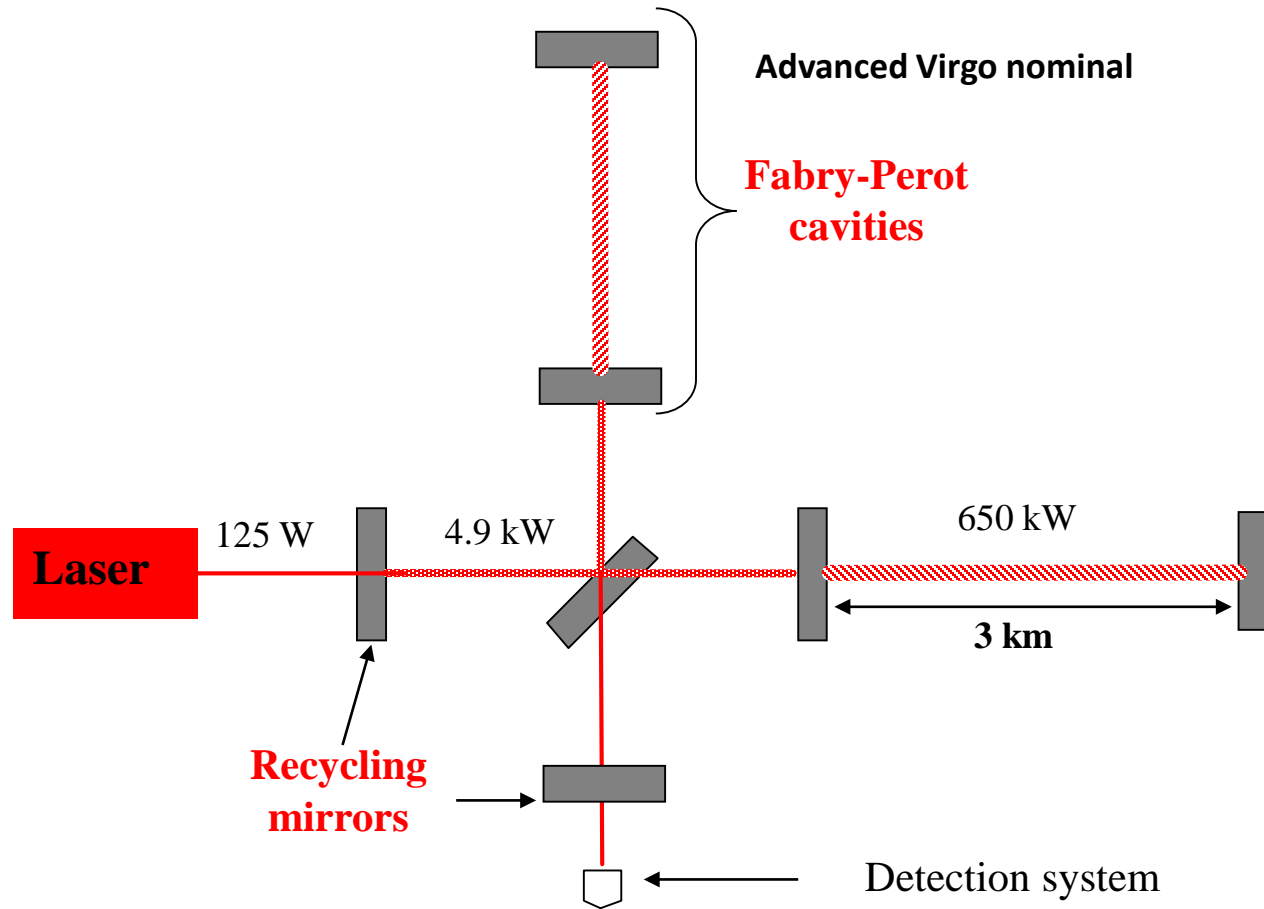
$$\rightarrow \mathbf{h}_{\text{equivalent}} \propto \sqrt{\mathbf{P}}$$



# Quantum noise in the sensitivity



# Minimizing shot noise with optical configuration



# Reduction of shot noise: high power laser

## Goal for AdV (nominal):

- continuous 200 W laser, stable monomode beam (TEM00), 1064 nm

*Only 33W currently injected in Advanced Virgo*

→ **decrease shot noise contribution**

## But limited by side-effects:

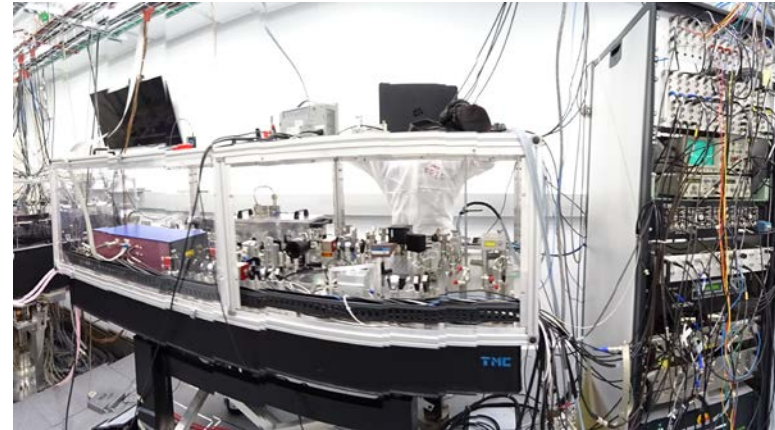
### ➤ Radiation pressure

- Increase of radiation pressure noise
- Cavities more difficult to control
- Parametric instabilities: coupling of laser high order modes with mirrors mechanical modes

### ➤ Thermal absorption in the mirrors (optical lensing)

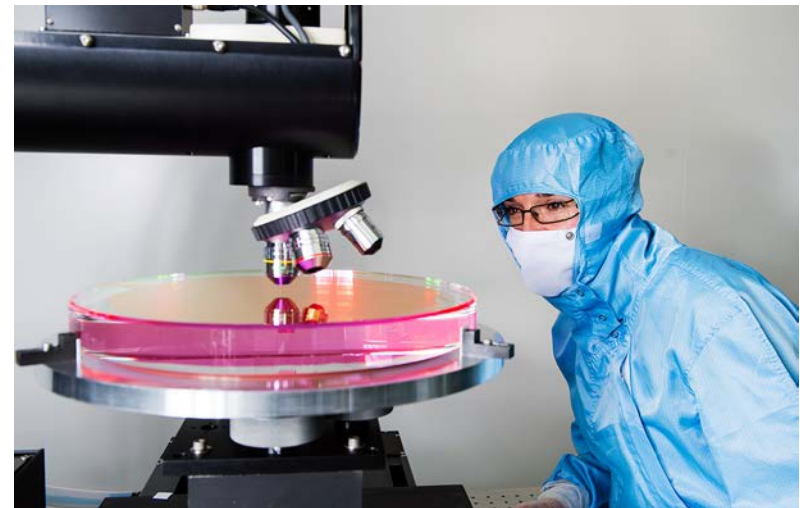
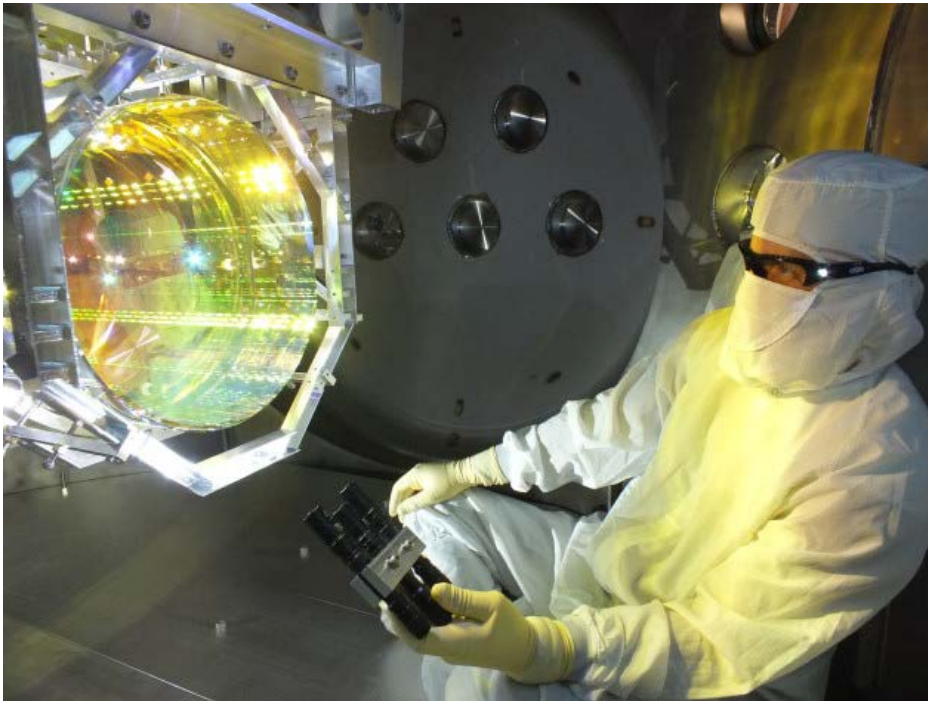
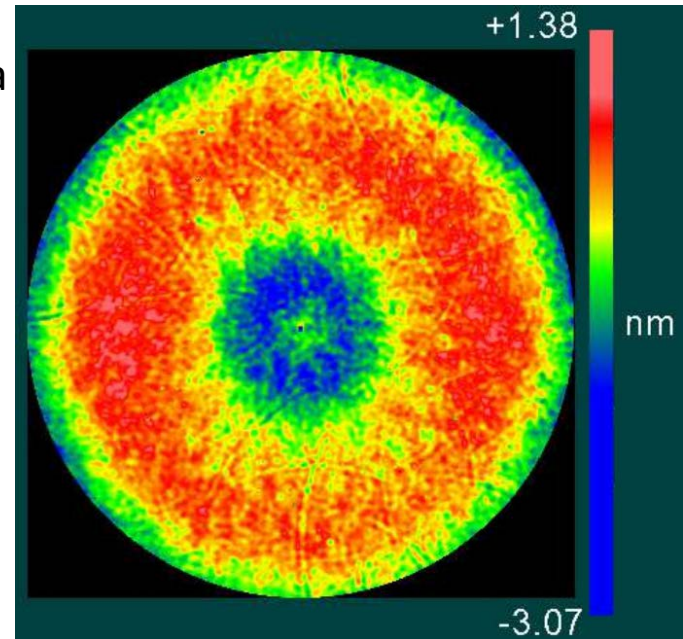
→ Need of thermal compensation system

**Avoid optical losses to not spoil high power → high quality mirrors**



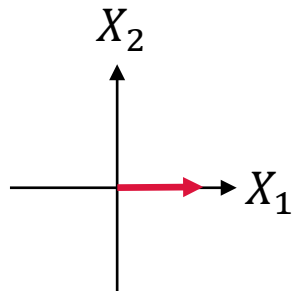
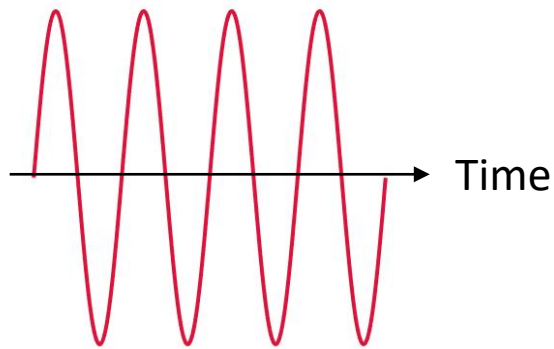
# « Perfect » mirrors

- 40 kg, 35 cm diameter, 20 cm thickness in ultra pure silica
- Uniformity of mirrors is unique in the world:
  - a few nanometers peak-to-valley
  - flatness < 0.5 nm RMS (over 150mm diameter)

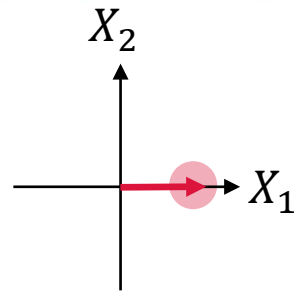
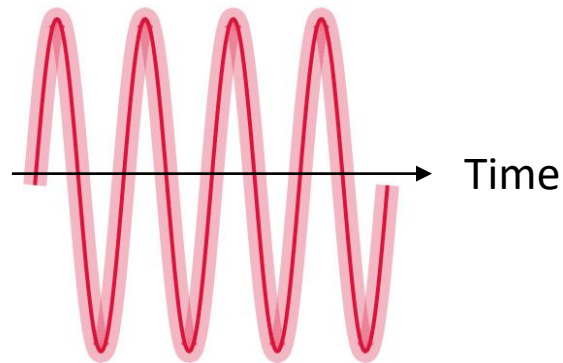


# Optical field models

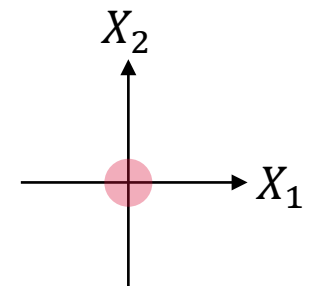
Classical picture



Coherent State

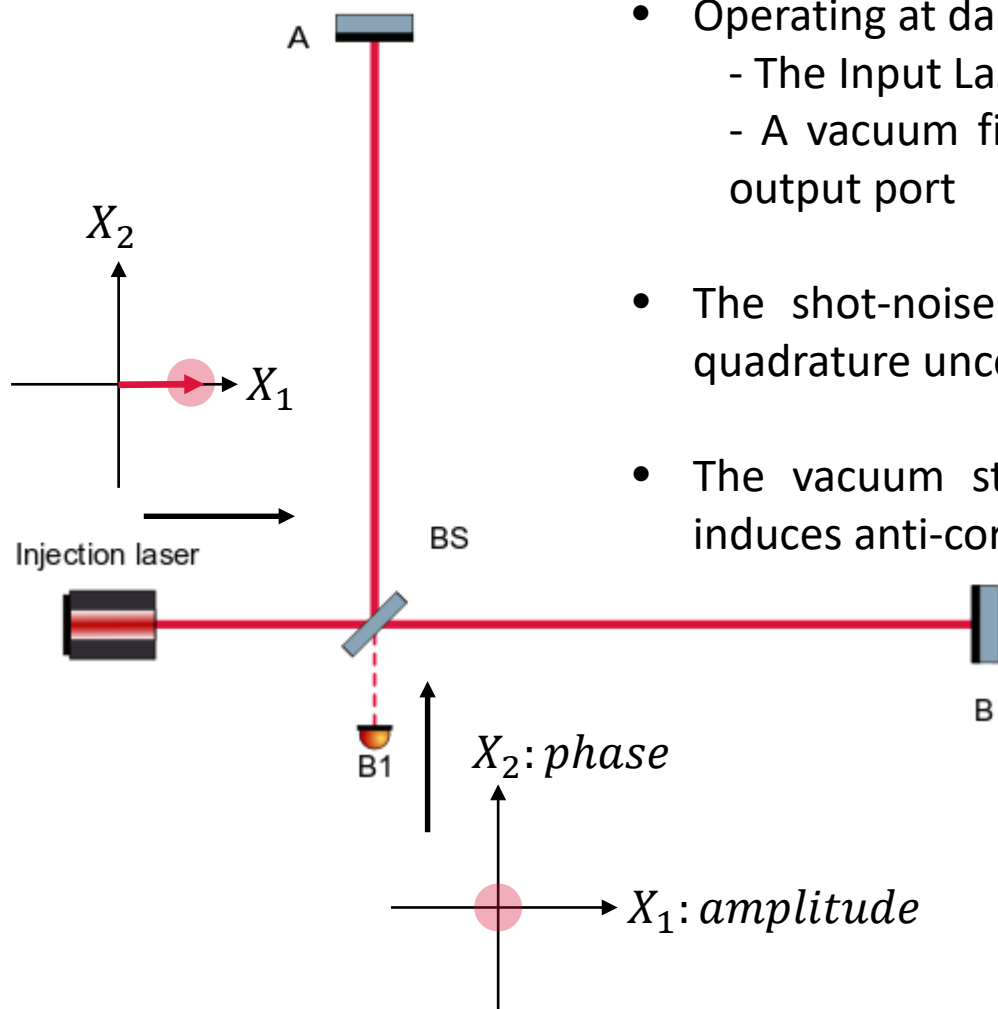


Vacuum State



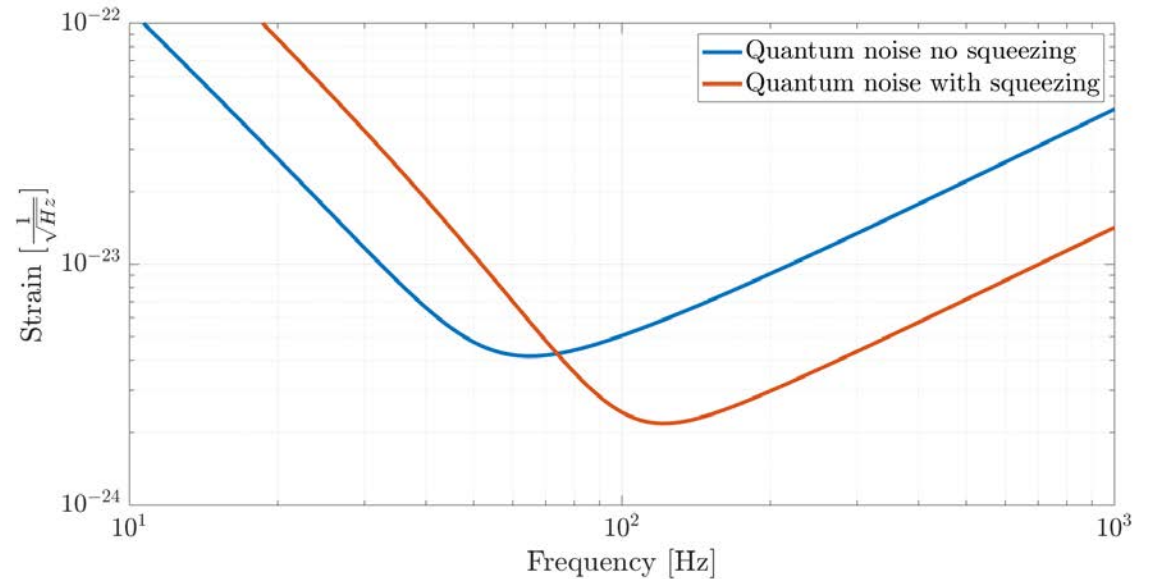
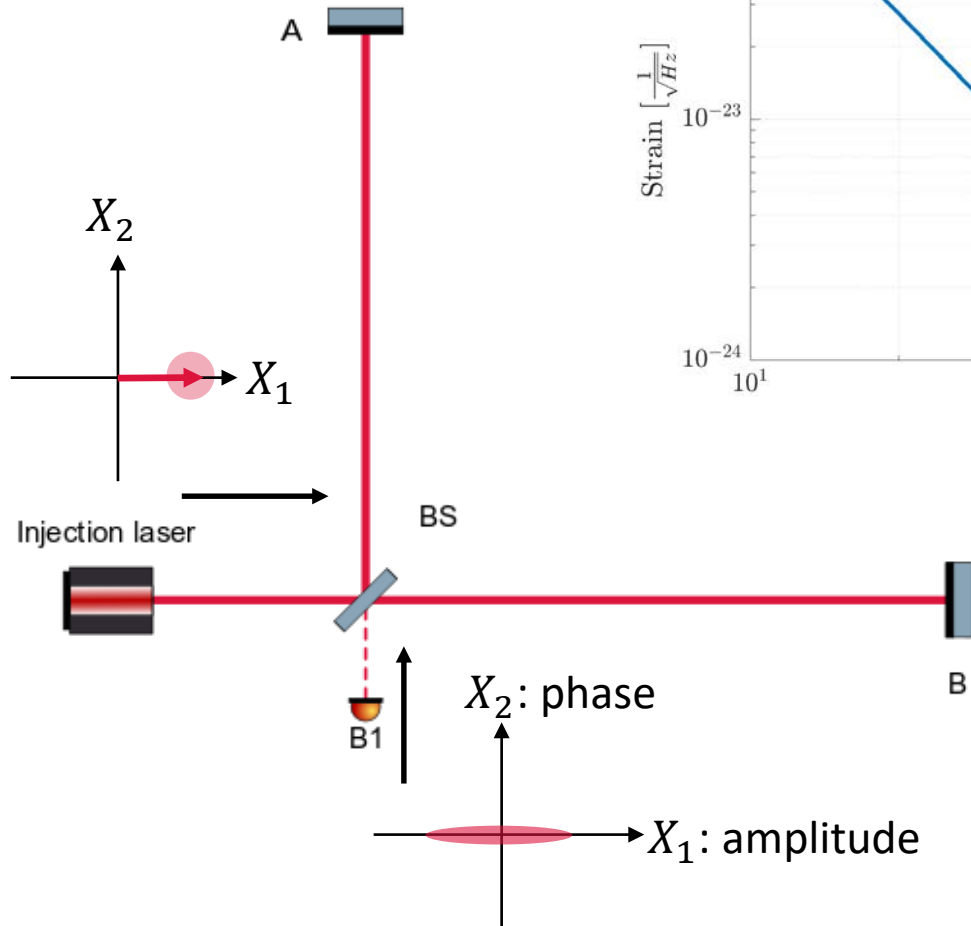


# Michelson interferometer at dark fringe and quantum noises



- Operating at dark-fringe :
  - The Input Laser is reflected back to the injection
  - A vacuum field enters the interferometer from the output port
- The shot-noise arises from the vacuum state phase quadrature uncertainty
- The vacuum state amplitude quadrature uncertainty induces anti-correlated radiation-pressure in the arms

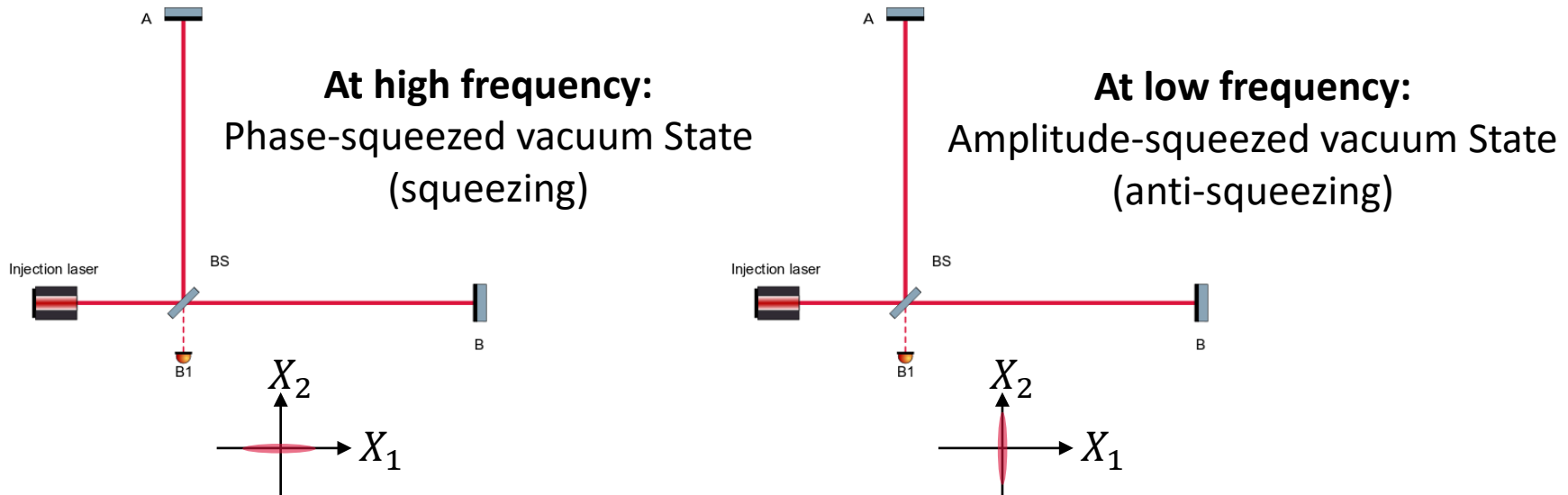
# Reduction of shot noise: squeezing



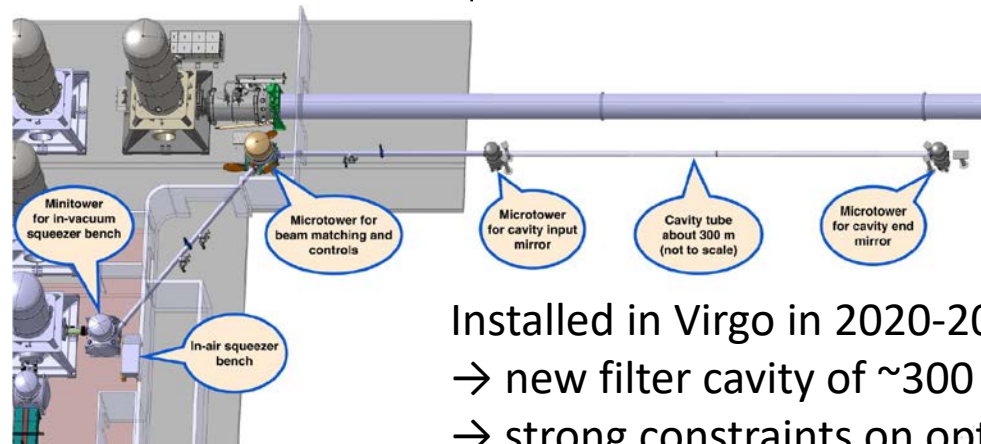
Inject a phase-squeezed vacuum state in the interferometer (squeezing)

→ **Decrease shot noise**  
**But increase radiation pressure noise**

# Reduction of quantum noise: frequency dependent squeezing



→ Decrease shot noise at high freq  
AND radiation pressure noise at low freq

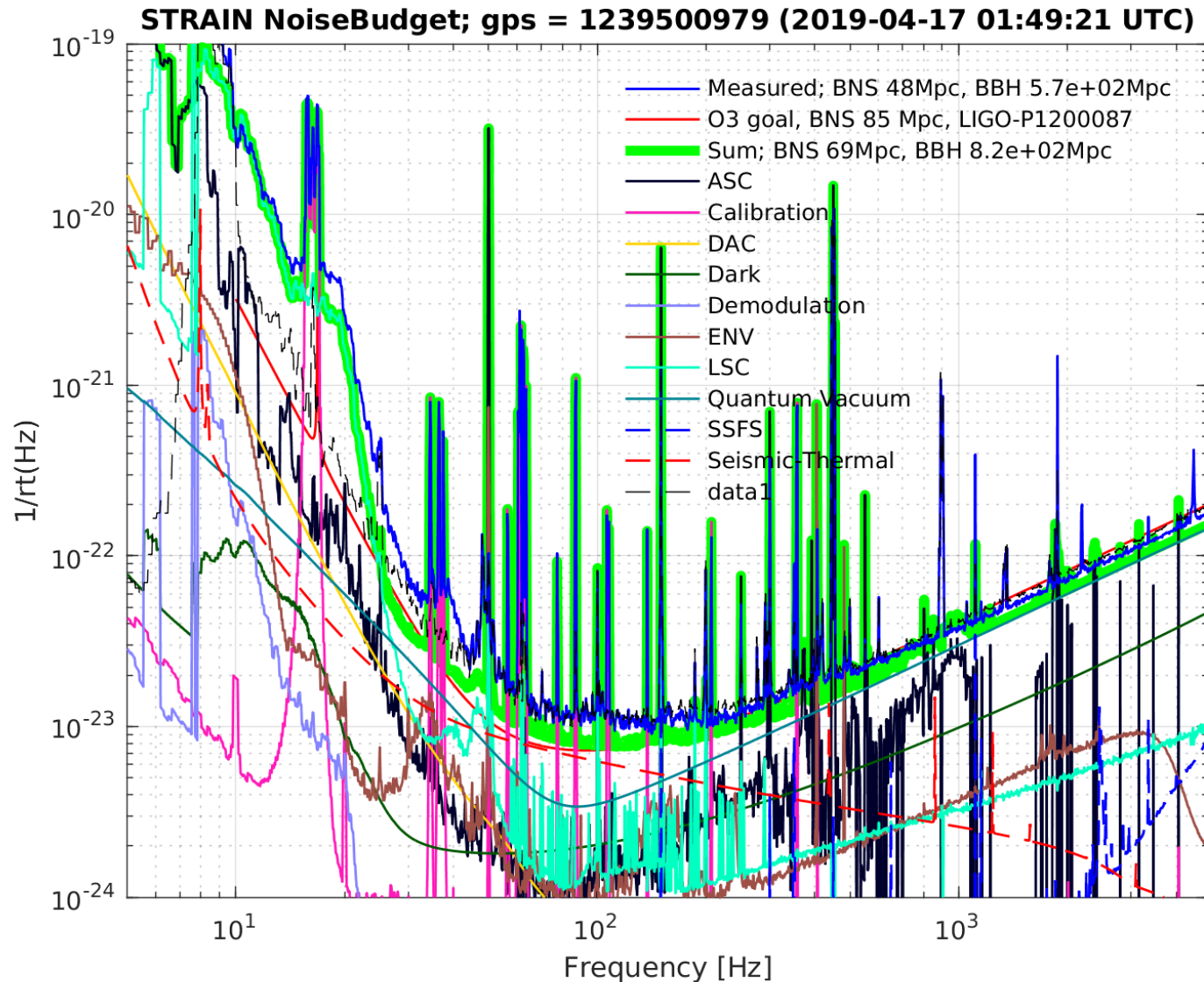


Installed in Virgo in 2020-2021

→ new filter cavity of  $\sim 300$  m, with finesse  $\sim 10000$

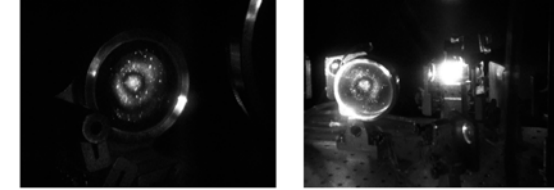
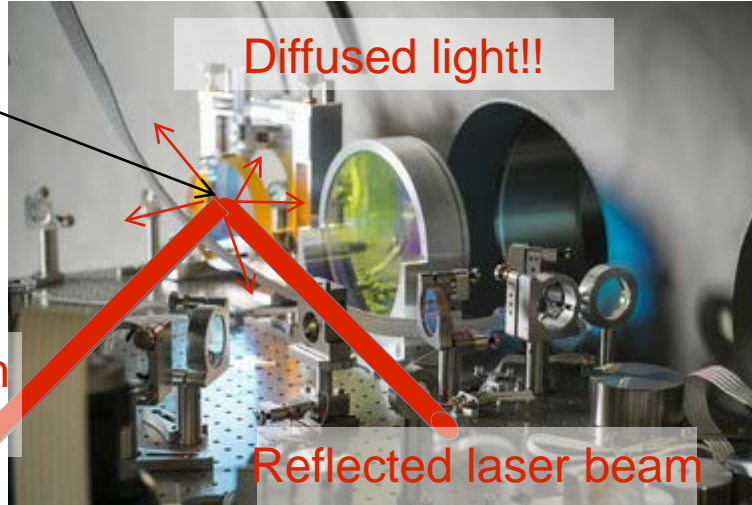
→ strong constraints on optical losses, beam matching and alignment, ...  
(suspended in vacuum optical benches)

# Example of Advanced Virgo noise budget (O3 run)



# Example of technical noise: Diffused light

Optical element  
(mirror, lens, ...)  
vibrating due to  
seismic or  
acoustic noises

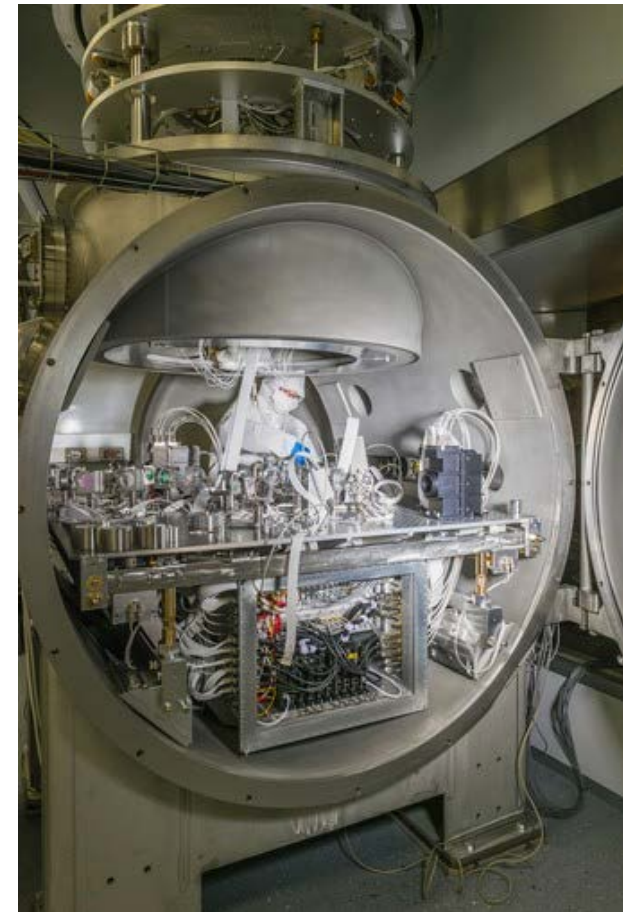


Evolution for AdVirgo: suspend  
the optical benches and place  
them under vacuum

some photons of the diffused  
light gets recombined with the  
interferometer beam

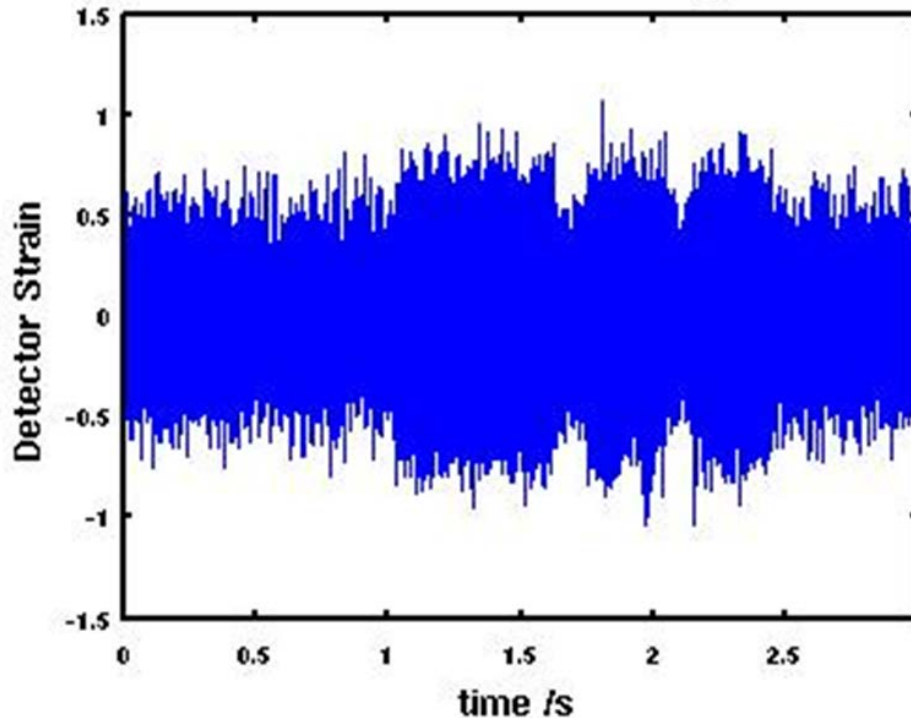
↓  
phase noise

↓  
extra power fluctuations  
(imprint of the optical element vibrations)



# Noises are not always stationary

Does this data contain the signal?



“Glitches” are impulses of noise.  
They might look like a transient GW signal

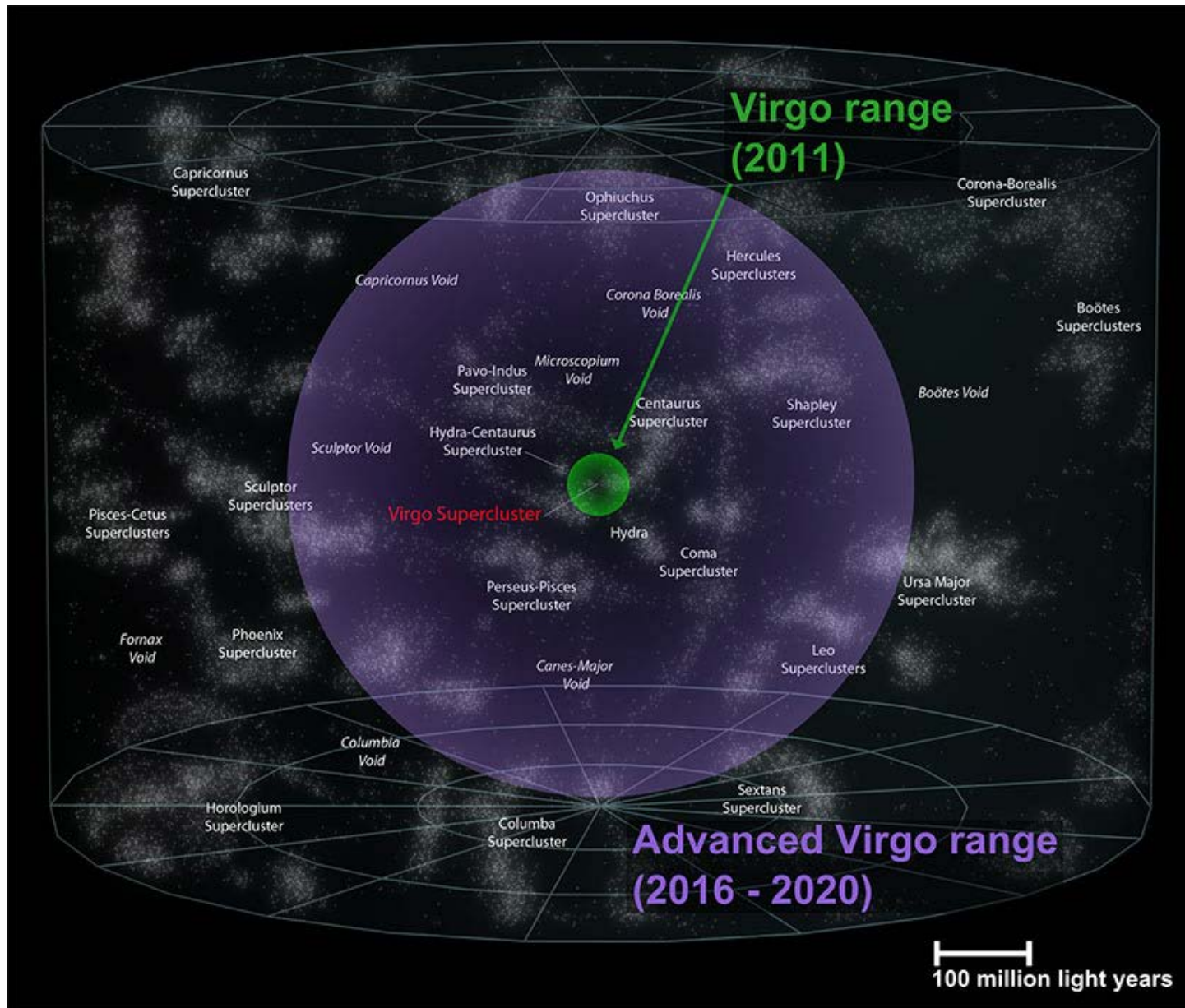


- ❑ environmental disturbances monitored with an array of sensors: seismic activities, magnetic perturbations, acoustic noises, temperature, humidity  
→ used to veto false alarm triggers due to instrumental artifacts
- ❑ requires coincidence between 2 detectors to reduce false alarm rate

# Table of Contents

- **How can we detect gravitational waves with laser interferometers?**
- **How do ground-based interferometers work?**
  - The Virgo optical configuration or how to measure  $10^{-20}$  m
  - How to maintain the ITF at its working point?
  - How to measure the GW strain  $h(t)$  from this detector?
  - Noises limiting the ITF sensitivity: how to tackle them?
- **Prospectives for interferometers and other detectors**

# From initial to advanced detectors

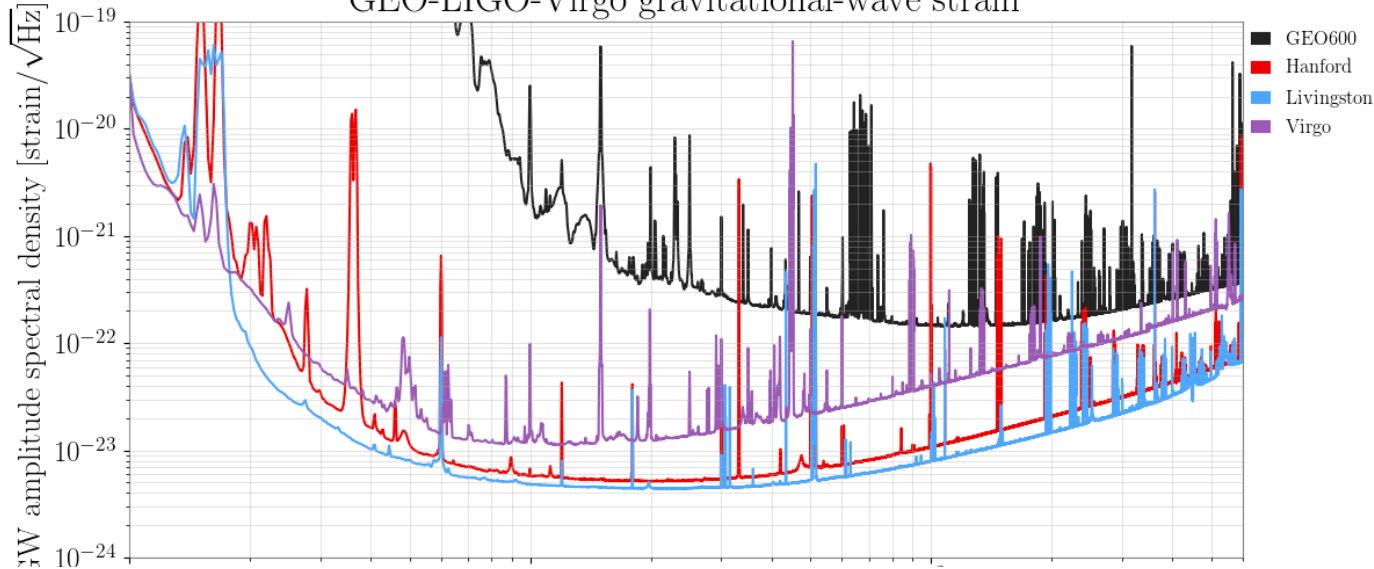




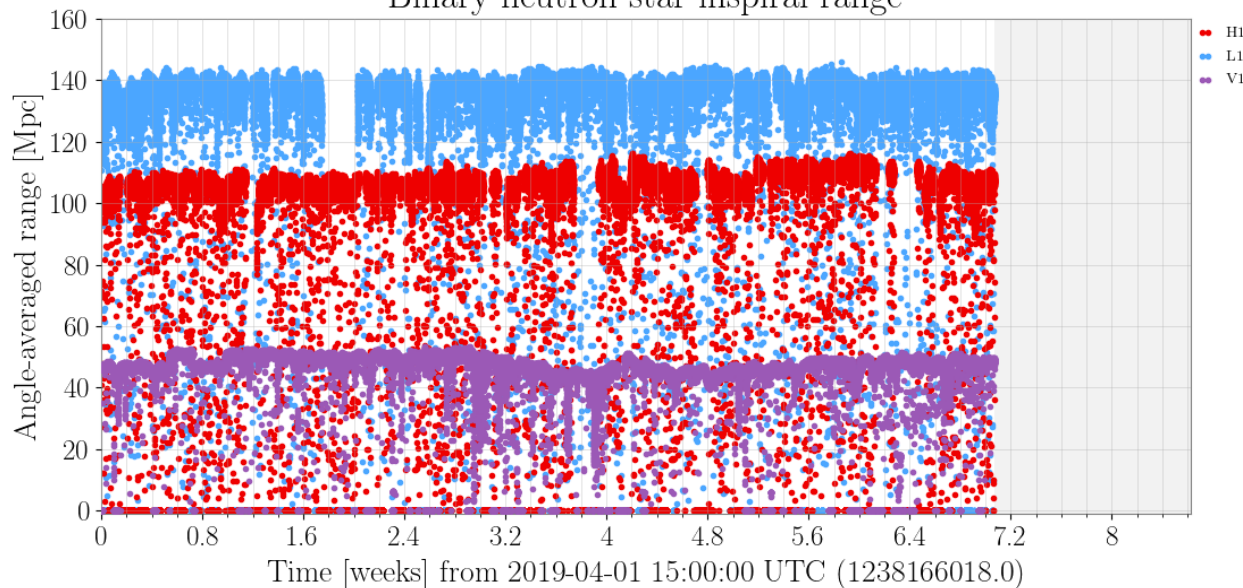
# Interferometers sensitivity during O3

[1239062418-1239148818, state: Locked]

GEO-LIGO-Virgo gravitational-wave strain



Binary neutron star inspiral range

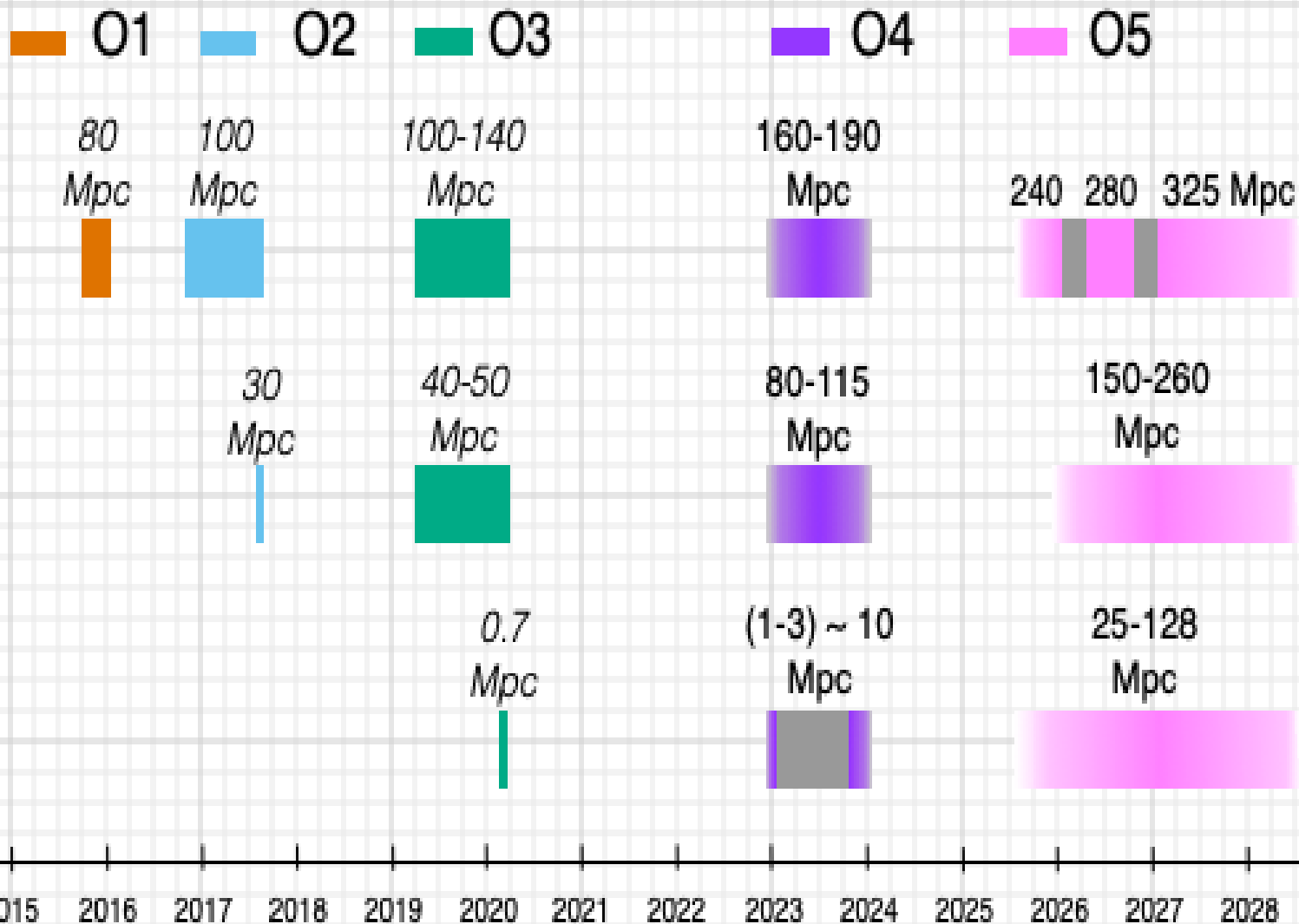


## BNS Range:

Distance at which a neutron star binary coalescence with averaged orientation over the sky can be seen with signal-to-noise ratio of 8

# Future observing runs

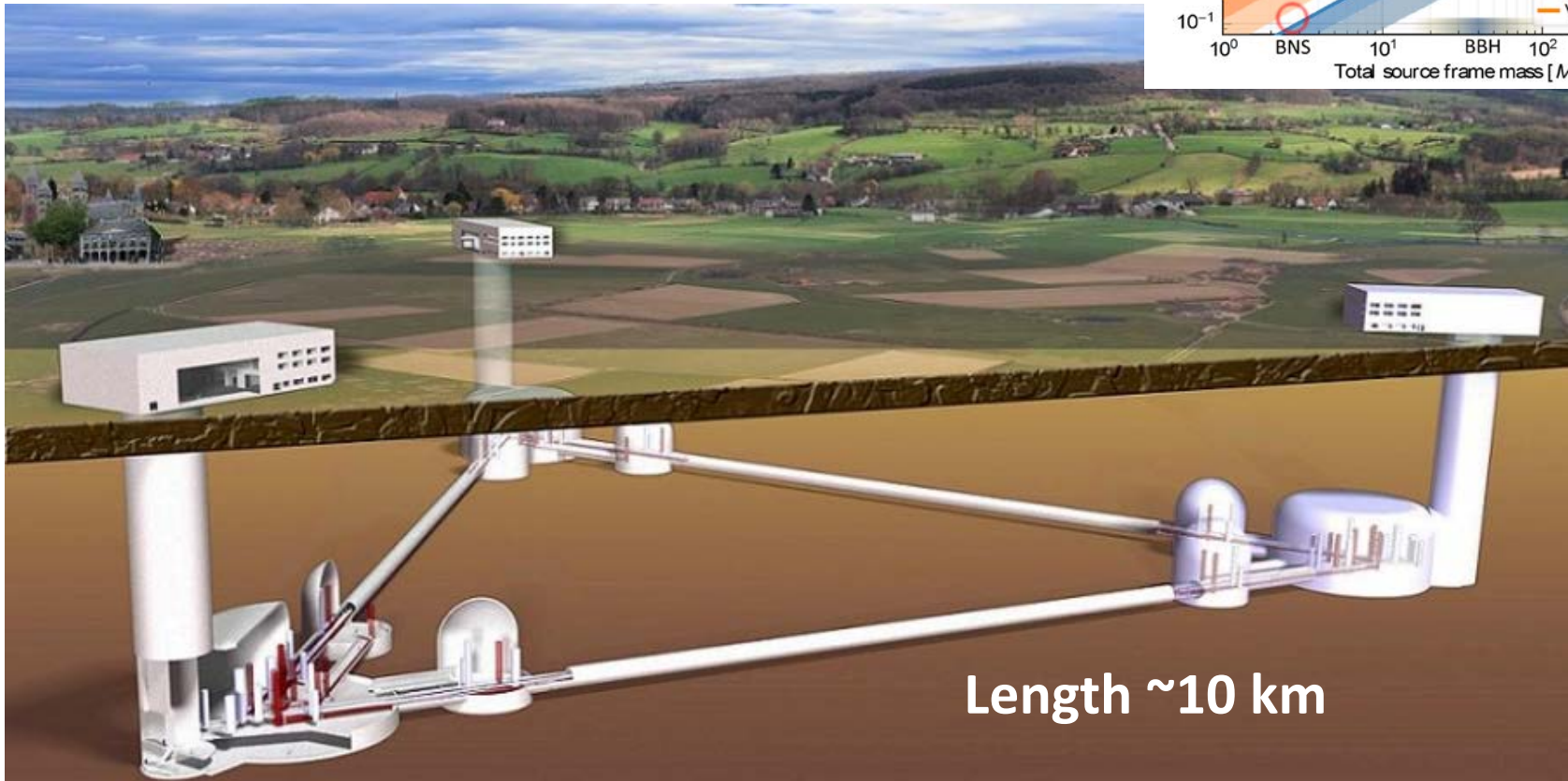
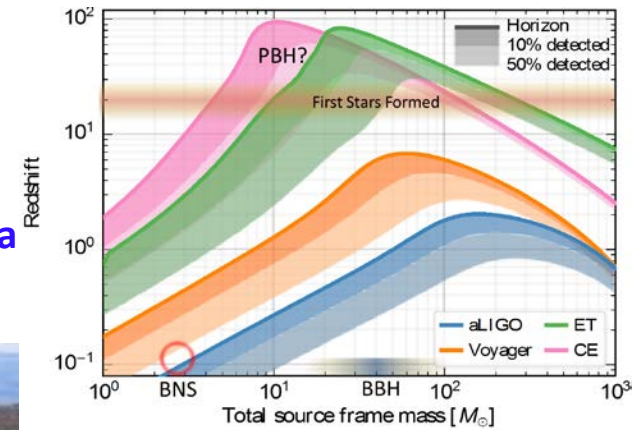
Updated  
16 March 2022



# Einstein Telescope

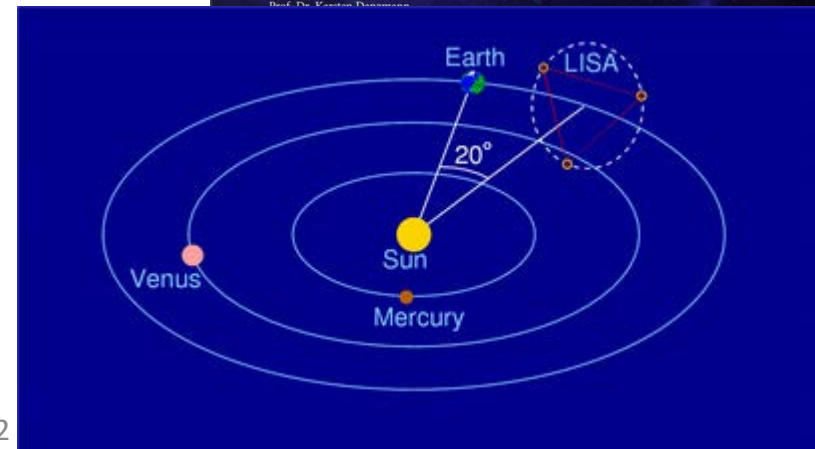
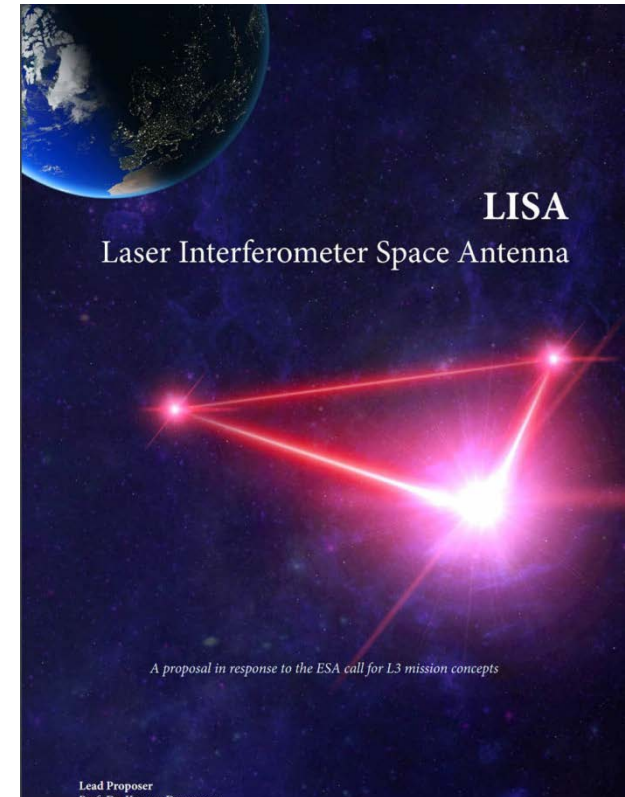
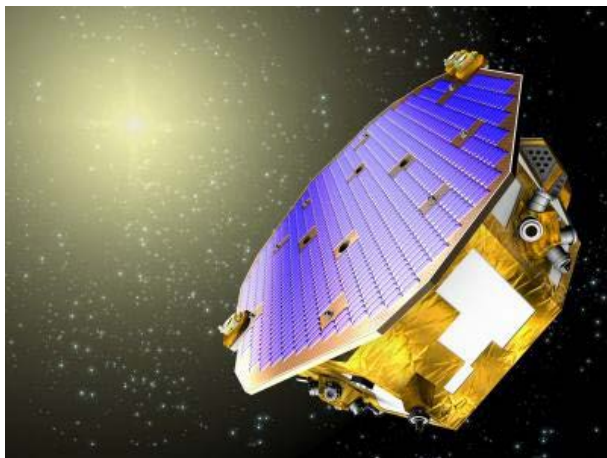
- Third generation interferometer: gain another factor 10 in sensitivity and enlarge bandwidth
- Located underground,  $\sim 10$  km arms
- Thermal noise reduction with cryogenics
- Xylophone detector: cold + hot interferometers
- In operation after 2030?

Could probe CBC signals from a large fraction of the Universe



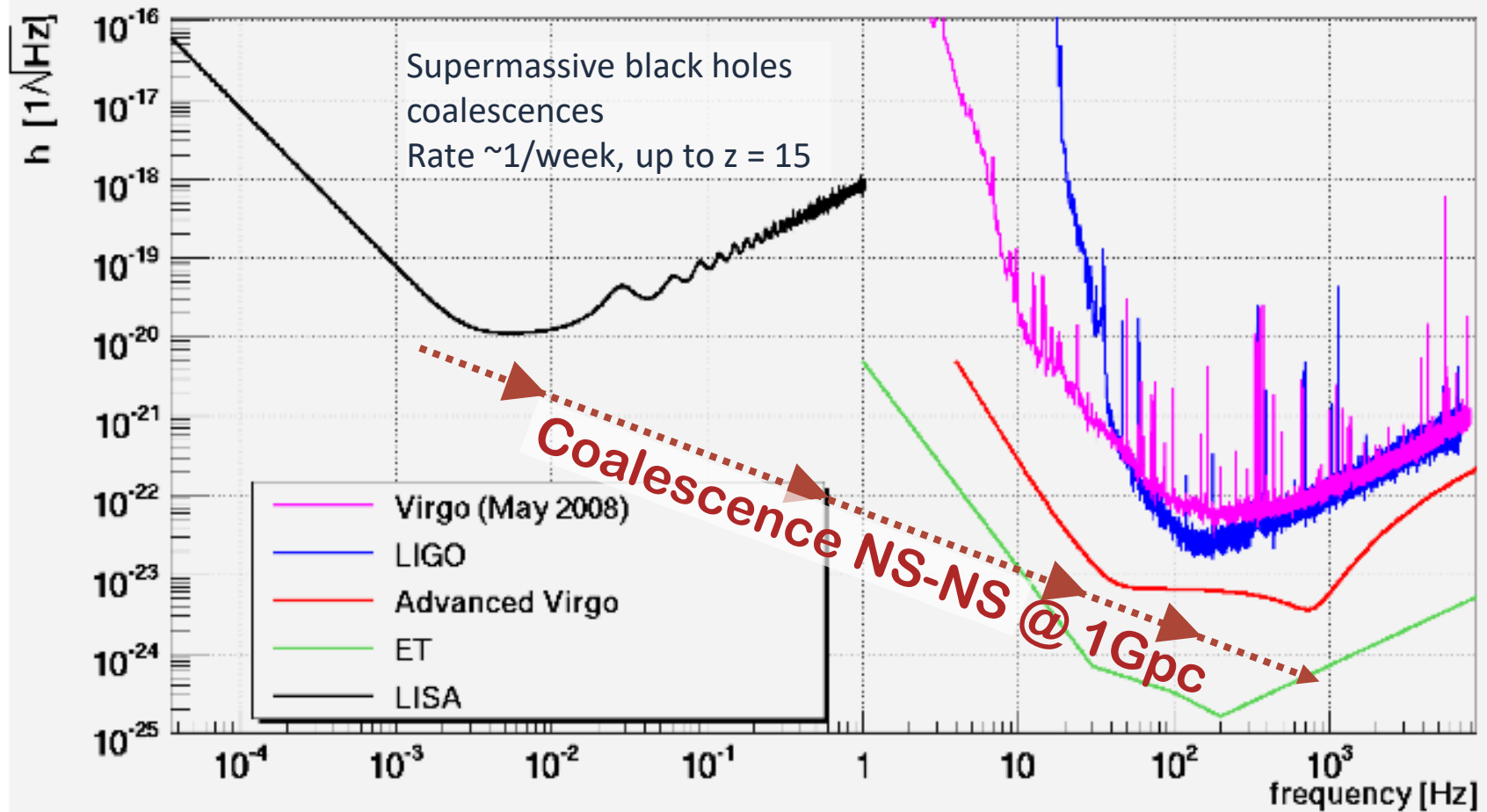
# Spatial interferometer: LISA

- **Bandwidth: 0.1 mHz to 1 Hz (2.5 million km arm length)**
- Launch of LISA in the years 2030?
  - operation for 5 to 10 years
- Successful intermediate step: LISA Pathfinder
  - launched end 2015
  - test of free-fall masses
  - validation of differential motion measurements



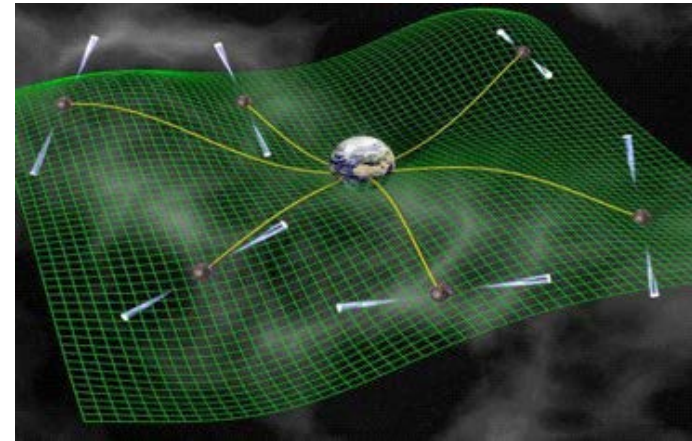
# ET and LISA performances

LISA and ground based detectors sensitivities



# Pulsars timing arrays

- **Bandwidth: 1 nHz to 1000 nHz**
- Observation of 20 ms pulsars in radio
  - GW cause the time of arrival of the pulses to vary by a few tens of nanoseconds over their wavelength
  - Weekly sampling over 5 years
- International network
  - Parkes PTA
  - North American NanoHertz Gravitational Wave Observatory
  - European PTA
- **First detections expected in the coming years!**



# A large GW spectrum to be studied...

