

Modelisation of light transmission through surfaces with optical coating in Geant4

L. Cappellugola, M. Dupont, C.-H. Sung, V. Sharyy, D. Yvon and C. Morel

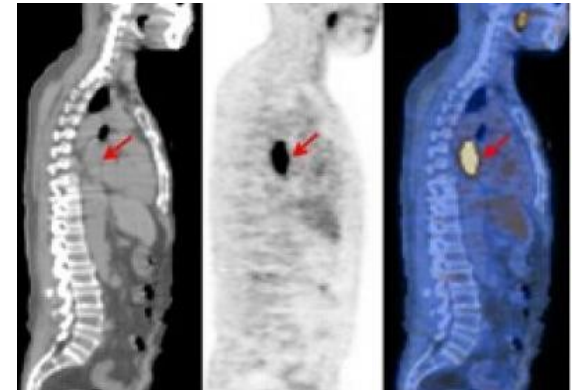
CONTENTS

- I. Introduction to TOF-PET
- II. Goal of the ClearMind project
- III. Analytical simulation of the impact of the thin layer on a visible photon transmission
- IV. Implementation of interferences and frustrated transmission in Geant4
- V. Experimental studies on Photek test cells

I. Introduction to TOF-PET

PET

- **Functional** imaging technique used in nuclear medicine
- Use **radiotracers** depending on the target (^{18}F -FDG)
- **Gamma rays** detected by scintillator
- Image is reconstructed to form **three-dimensional image**
- **PET/CT** (PET/Scan) overlay of both images



TOF-PET

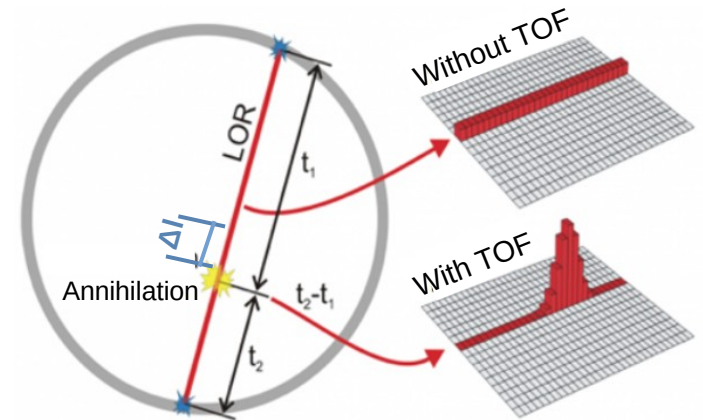
- Taking care of **the difference between the arrival time** of the two photons on a pair of detectors

$$\Delta t = (t_2 - t_1) \pm CTR$$

$$\Delta l = c \frac{\Delta t}{2} \pm c \frac{CTR}{2} \quad CTR = 10 \text{ ps} \quad c = 30 \text{ cm} \cdot \text{ns}^{-1} \rightarrow \Delta l = c \frac{\Delta t}{2} \pm 1.5 \text{ mm}$$

State-of-the-art clinical CTR = 215 ps

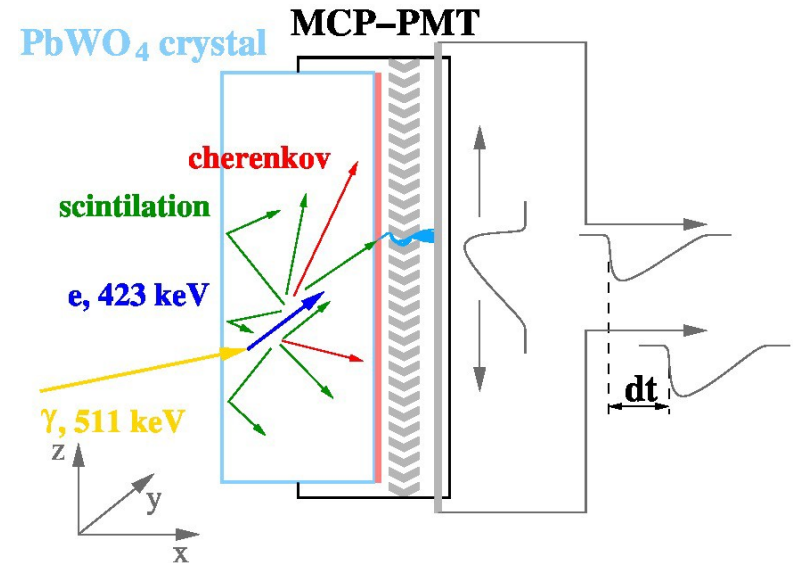
- TOF-PET → improve **SNR** or reduce patient **dose**



II. Goal of the ClearMind project

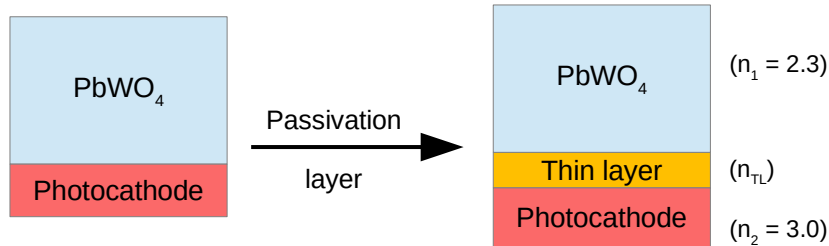
Goal of ClearMind project

- Collaboration between 5 labs
- New PET detector with improved spatio-temporal resolution
 - **PbWO₄** crystal: Cerenkov radiator (21 ph/event) and scintillator (200 ph/event), with fast constants (~2 ns)
 - Deposit the photoelectric layer directly on the crystal: **scintronic crystal**
 - Use **Micro-Channel Plate (MCP)**
 - Measure DOI

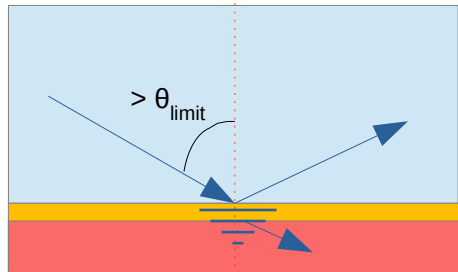


III. Analytical simulation of the impact of the thin layer on a visible photon transmission

Passivation layer introduction



Oxidation of the photocathode by the lead tungstate → **Thin passivation layer** needed



Generates:

- Interference phenomenon at the interfaces
- For $\theta > \theta_{limit}$ an evanescent wave is produced and allows **frustrated transmission**

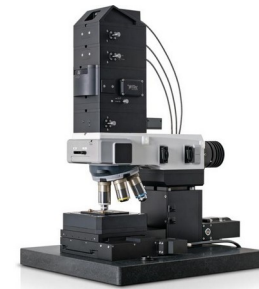


Iridescence phenomenon

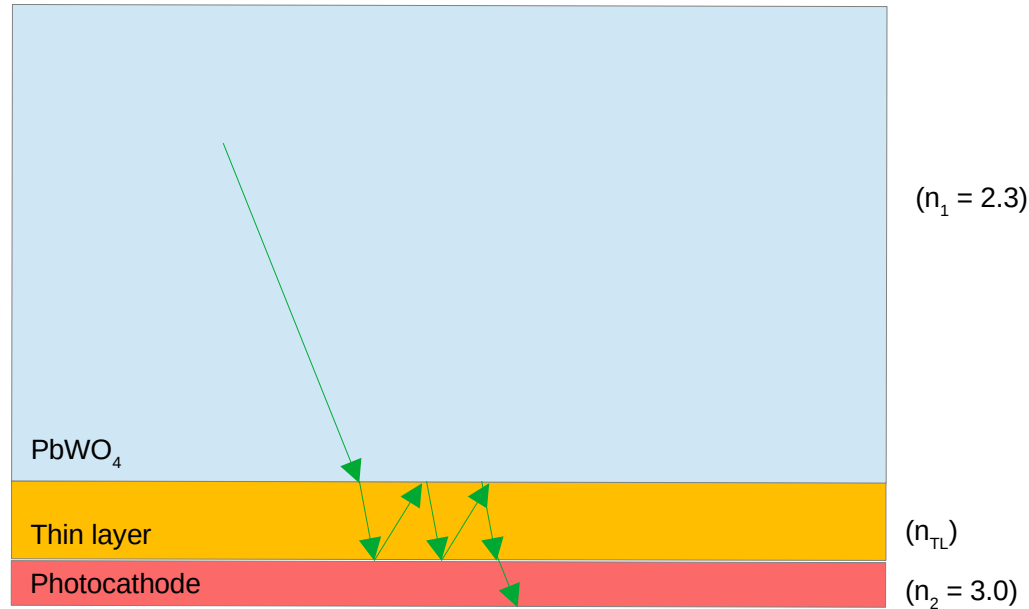
If $n_1 > n_2$:

$$\theta_{limit} = \arcsin\left(\frac{n_2}{n_1}\right)$$

Near field microscopy



Passivation layer introduction



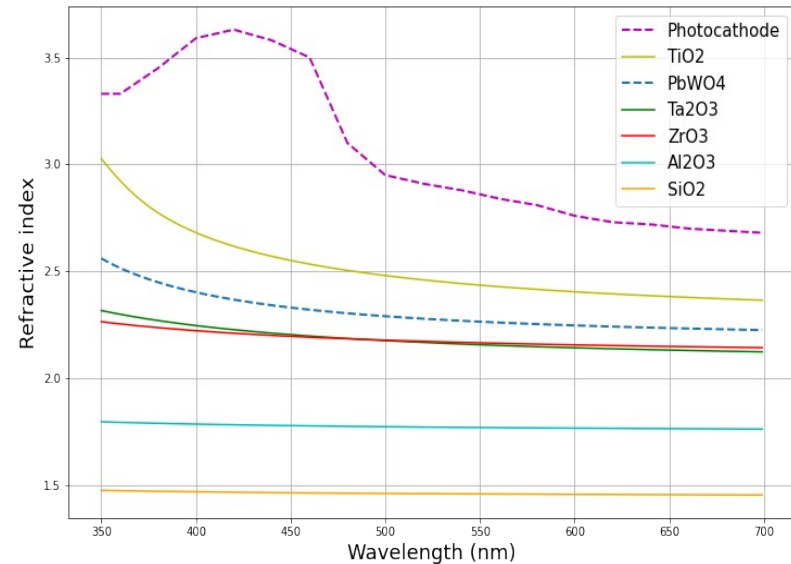
Formulas of reflection and transmission through a thin layer

		Reflection	Transmission		R and T	
Simple Interface	Normal incidence	$r_{ij,TE} = r_{ij,TM} = \frac{n_i - n_j}{n_i + n_j}$	$t_{ij,TE} = t_{ij,TM} = \frac{2n_i}{n_i + n_j}$	Fresnel coefficients	$R = r ^2$	
	Oblique incidence	$\theta_1 < \theta_{\text{limit}}$	$r_{ij,TE} = \frac{n_i \cos \theta_i - n_j \cos \theta_j}{n_i \cos \theta_i + n_j \cos \theta_j}$ $r_{ij,TM} = \frac{n_i \cos \theta_j - n_j \cos \theta_i}{n_i \cos \theta_j + n_j \cos \theta_i}$	$t_{ij,TE} = \frac{2n_i \cos \theta_i}{n_i \cos \theta_i + n_j \cos \theta_j}$ $t_{ij,TM} = \frac{2n_i \cos \theta_i}{n_i \cos \theta_j + n_j \cos \theta_i}$	$r_{TE} + 1 = t_{TE}$ $n_1(1 - r_{TM}) = n_2 t_{TM}$	$T_I = \frac{n_{\text{end}}}{n_{\text{beg}}} t ^2$
		$\theta_1 > \theta_{\text{limit}}$	Total reflection			
Thin layer	Normal incidence	$r = \frac{r_{12} + r_{23} \cdot e^{2i\beta}}{1 + r_{12} \cdot r_{23} \cdot e^{2i\beta}}$	$t = \frac{t_{12} t_{23} e^{i(k_2 - k_3)d}}{1 + r_{12} r_{23} e^{2i\beta}} \approx \frac{t_{12} t_{23} e^{i\beta}}{1 + r_{12} r_{23} e^{2i\beta}}$	$\beta = k_2 d$ $k_2 = \frac{2\pi}{\lambda_2} = n_2 \frac{2\pi}{\lambda_0} = \frac{n_2}{n_1} \frac{2\pi}{\lambda_1}$	$R + T_I \neq 1$	
	Oblique incidence	$\theta_1 < \theta_{\text{limit}}$	$r = \frac{r_{12} + r_{23} \cdot e^{2i\beta}}{1 + r_{12} \cdot r_{23} \cdot e^{2i\beta}}$	$t = \frac{t_{12} t_{23} e^{i\beta}}{1 + r_{12} r_{23} e^{2i\beta}}$	$\beta = k_2 d \cos \theta_2$	$T_P = \frac{n_c \cos \theta_c}{n_b \cos \theta_b} t ^2$
		$\theta_1 > \theta_{\text{limit}}$	$r = \frac{r_{12} + r_{23} \cdot e^{2\beta}}{1 + r_{12} \cdot r_{23} \cdot e^{2\beta}}$	$t = \frac{t_{12} t_{23} e^{\beta}}{1 + r_{12} r_{23} e^{2\beta}}$	$\beta = -k_0 d y$	$R + T_P = 1$
			\triangle Taking r_i for simple interface et $\theta < \theta_{\text{limit}}$ replacing $n_2 \cos(\theta_2)$ by iy $r_{12,TE} = \frac{n_1 \cos \theta_1 - iy}{n_1 \cos \theta_1 + iy}$ $r_{12,TM} = \frac{n_1 iy - n_2^2 \cos \theta_1}{n_1 iy + n_2^2 \cos \theta_1}$	$t_{12,TE} = \frac{2n_1 \cos \theta_1}{n_1 \cos \theta_1 + iy}$ $t_{12,TM} = \frac{2n_1 n_2 \cos \theta_1}{n_1 iy + n_2^2 \cos \theta_1}$	$k_0 = \frac{2\pi}{\lambda_0}$ $y = \sqrt{n_1^2 \sin^2 \theta_1 - n_2^2}$	

M. Born and E. Wolf, Principles of Optics : Electromagnetic Theory of Propagation, Interference and Diffraction of Light, ch. Basic properties of electromagnetic field. Elsevier, June 2013.

Comparison of passivation layer materials

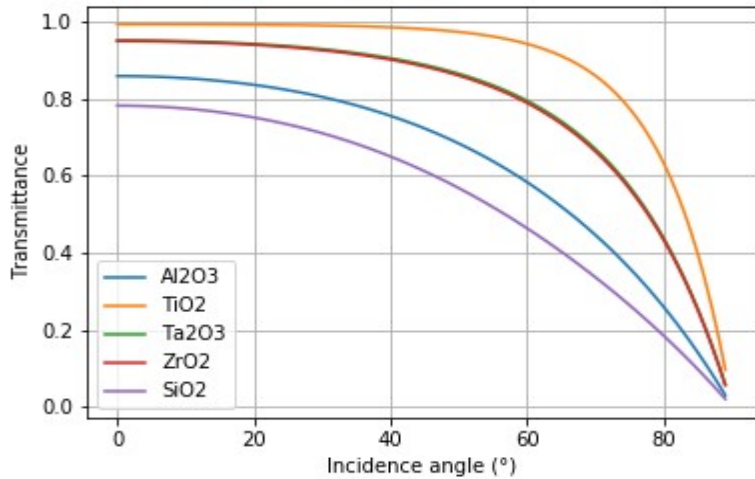
- Comparison of:
 - Zirconium oxide, ZrO_3
 - Tantalum oxide, Ta_2O_3
 - Aluminium oxide, Al_2O_3
 - Titanium oxide, TiO_2
 - Silicon oxide/Quartz, SiO_2
- No frustrated transmission with TiO_2



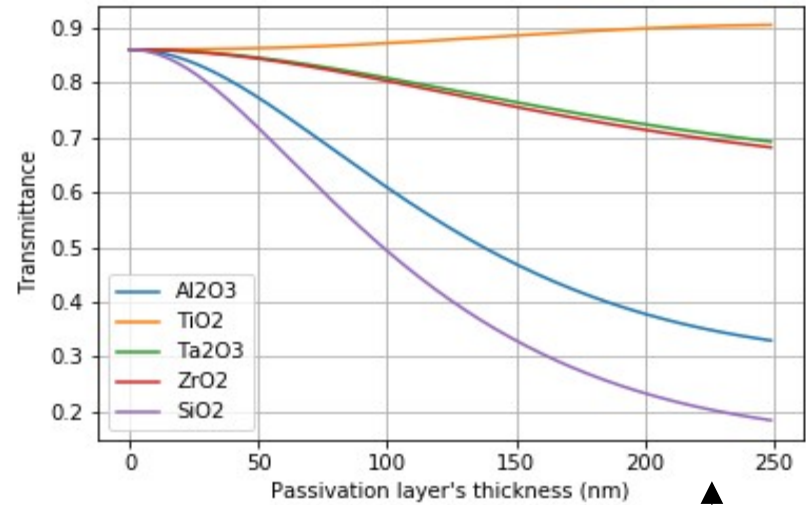
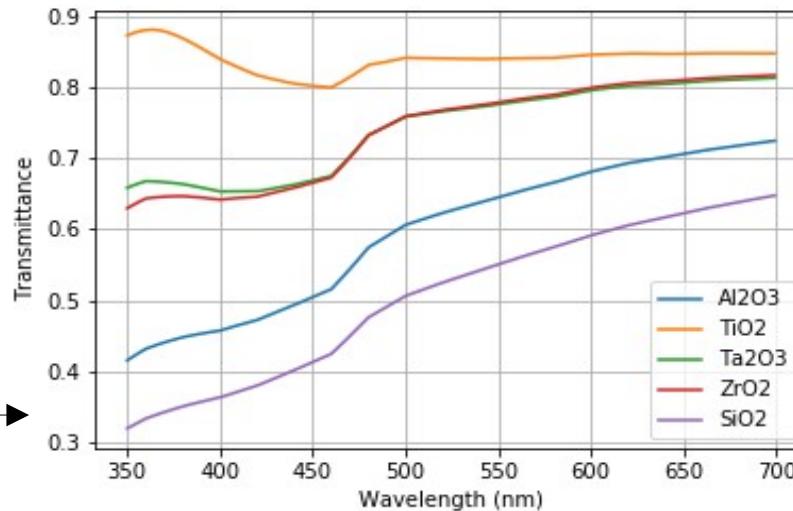
Refractive index as a function of the wavelength

Comparison of passivation layer materials

Transmittance as a function of incidence angle and integrated over PWO emission spectrum for a 100 nm-thick passivation layer



Transmittance as a function of wavelength integrated over incidence angles for a 100 nm-thick passivation layer



Transmittance as a function of layer thickness and integrated over PWO emission spectrum and incidence angles

IV. Implementation of interferences and frustrated transmission in Geant4

Integration of interferences and frustrated transmission due to a thin layer in Geant4

G4OpBoundaryProcess.h

```

void DielectricMetal();
void DielectricDielectric();
void DielectricLUT();
void DielectricLUTDAVIS();
void DielectricDichroic();
void CoatedDielectricDielectric();
    
```



DetectorConstruction.cc

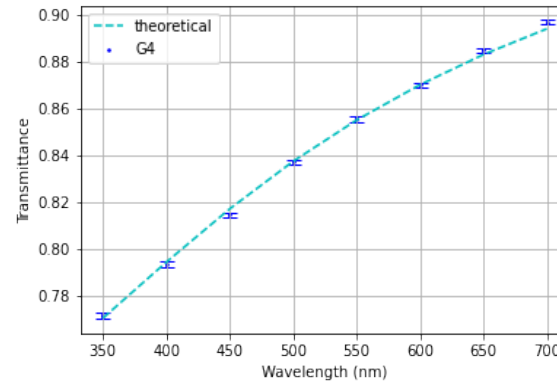
```

G4OpticalSurface* OpSurface1 = new G4OpticalSurface("op_Crystal1->Crystal2");

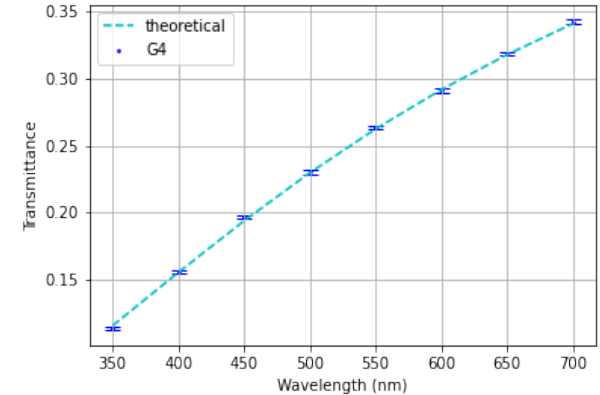
G4LogicalBorderSurface* Surface1 = new G4LogicalBorderSurface("lo_Crystal1->Crystal2",physCrystal1,
physCrystal2,OpSurface1);

OpSurface1->SetType(coating);
OpSurface1->SetModel(unified);
OpSurface1->SetFinish(polished);
    
```

0°



80°

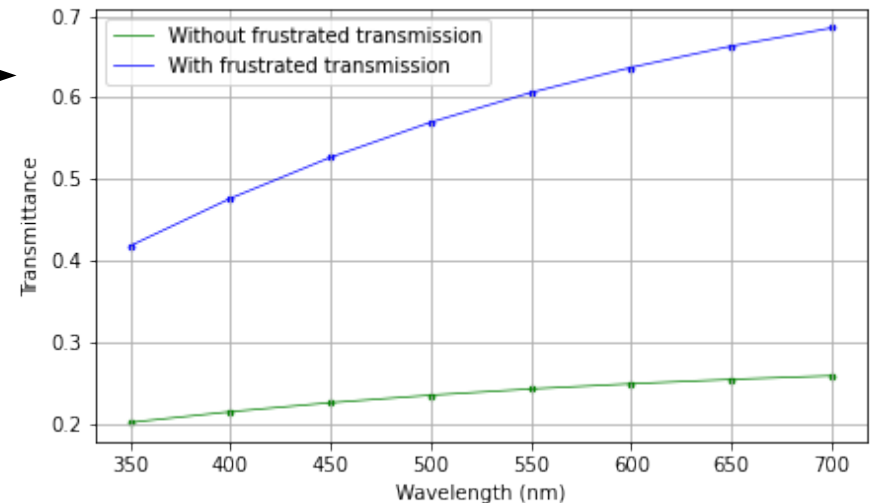


Example of transmittance for a visible photon passing through a thin layer of 100 nm SiO₂ as a function of wavelength for two incidence angles

What is the importance of frustrated transmission through a thin layer?

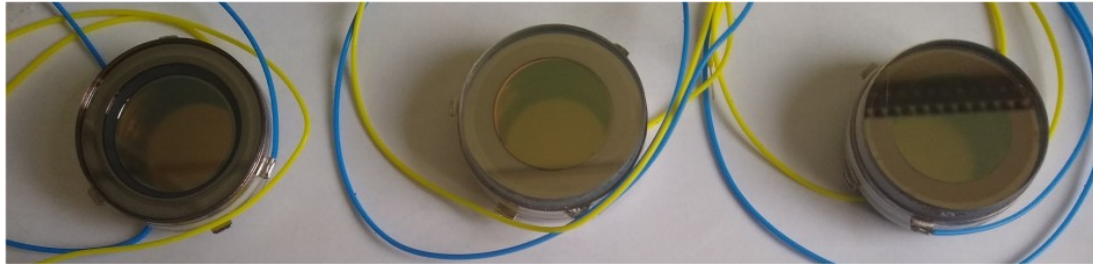
Transmittance through a thin layer as a function of wavelength integrated over incidence angles, with and without frustrated transmission

- Simulation of transmittance through thin layer with frustrated transmission for large angles (blue curve) and with total reflection only for large angles (green curve)
- The transmittance is **two times increased** thanks to frustrated transmission



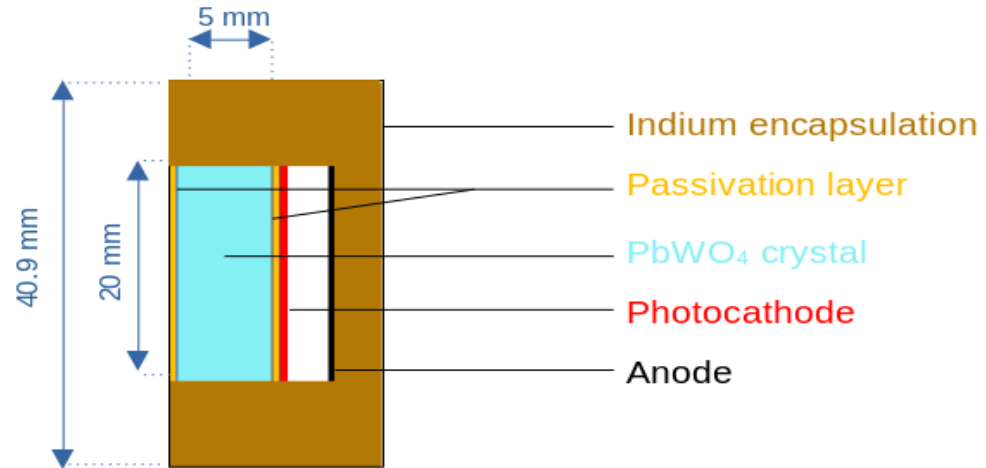
V. Experimental studies on Photek test cells

Experimental studies on Photek test cells



- Photek test cells:

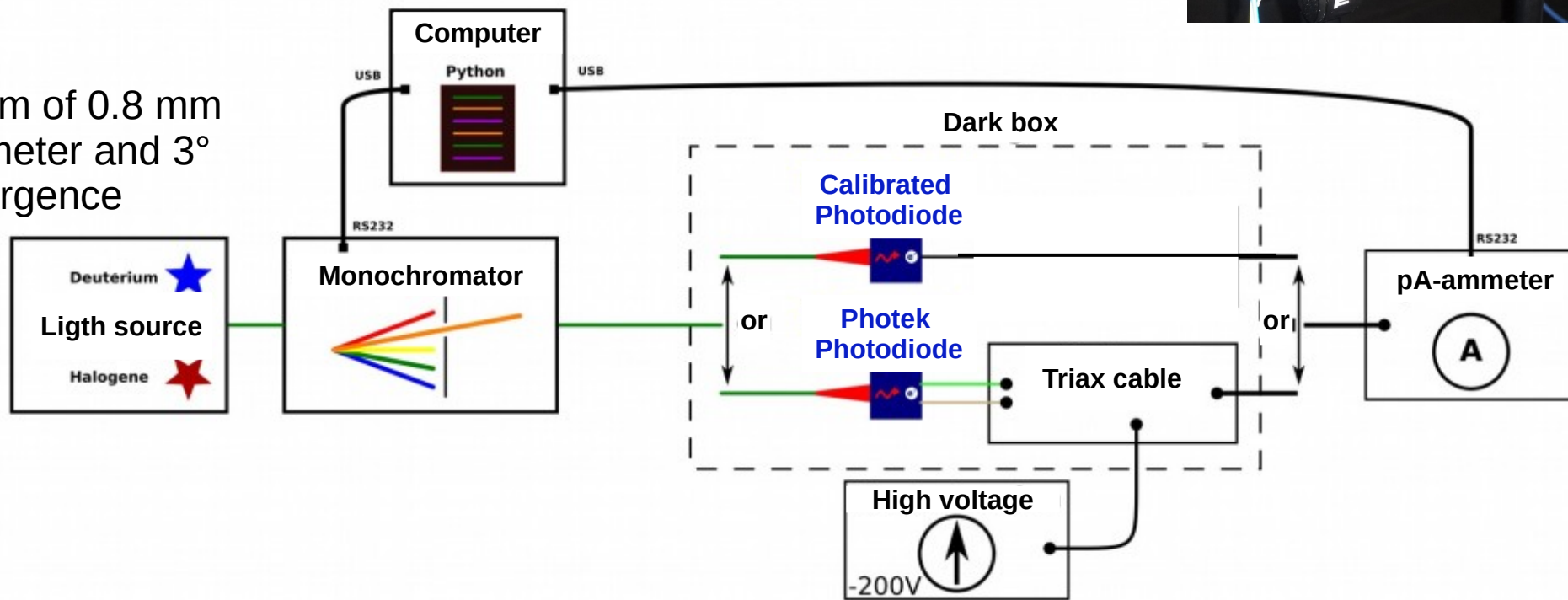
- SiO_2 , without thin layer
- PbWO_4 2018
- PbWO_4 2021



Measurement setup

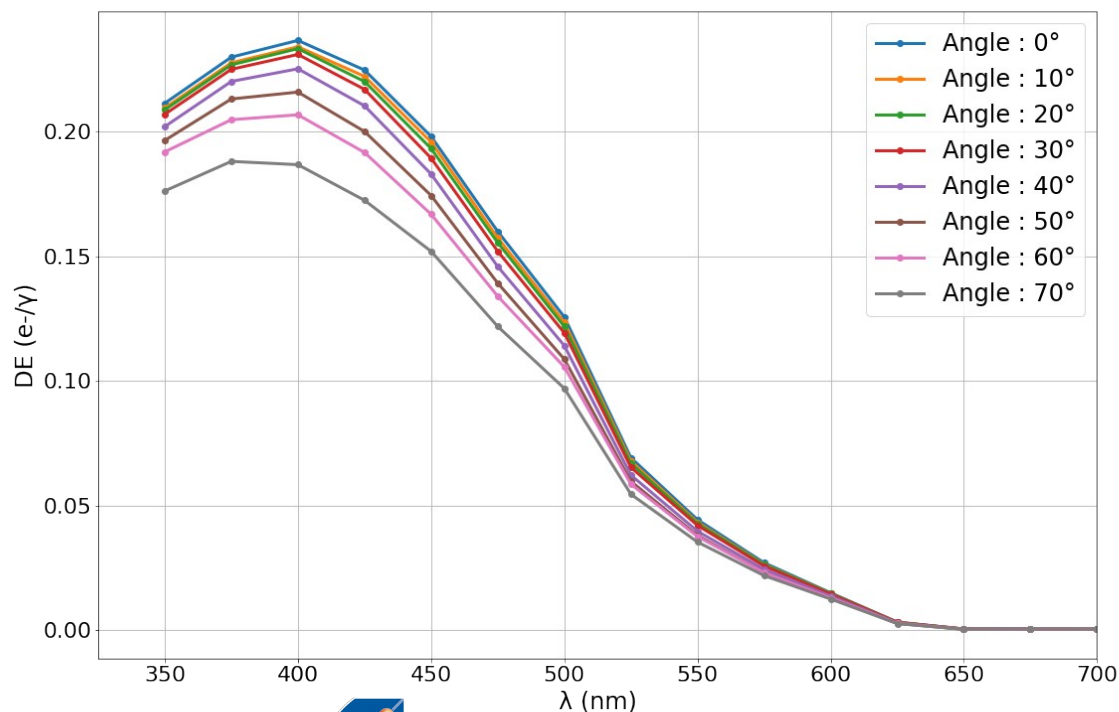


Beam of 0.8 mm diameter and 3° divergence

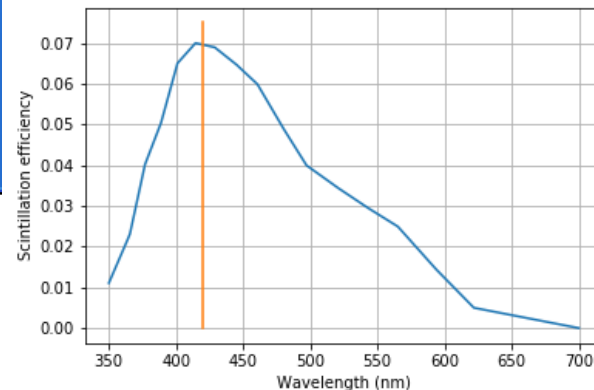


Analysis of experimental data

Detection Efficiency (DE) of Photek PWO2018 as a function of wavelength (λ)



Emission spectrum of lead tungstate



$$DE \equiv QE \times \text{Transmittance}$$

$$DE = \frac{S_{\text{PHOTEK}} h c}{e \lambda}$$

S_{PHOTEK} : Sensitivity of Photek test cells [A/W]

$$S_{\text{PHOTEK}} = \frac{I_{\text{PHOTEK}} S_{\text{CAL}}}{I_{\text{CAL}}}$$

Work in progress...

Conclusion and perspectives

- The **theoretical description** of the passivation layer shows an impact on the transmittance of visible photons
- This theoretical model has been integrated in **Geant4** to describe an interface containing a thin layer
- **Measurements are carried on at CEA-Saclay** for assessment

Thank you for your attention