



Science and
Technology
Facilities Council

AGATA Week Mechanics

February 2021

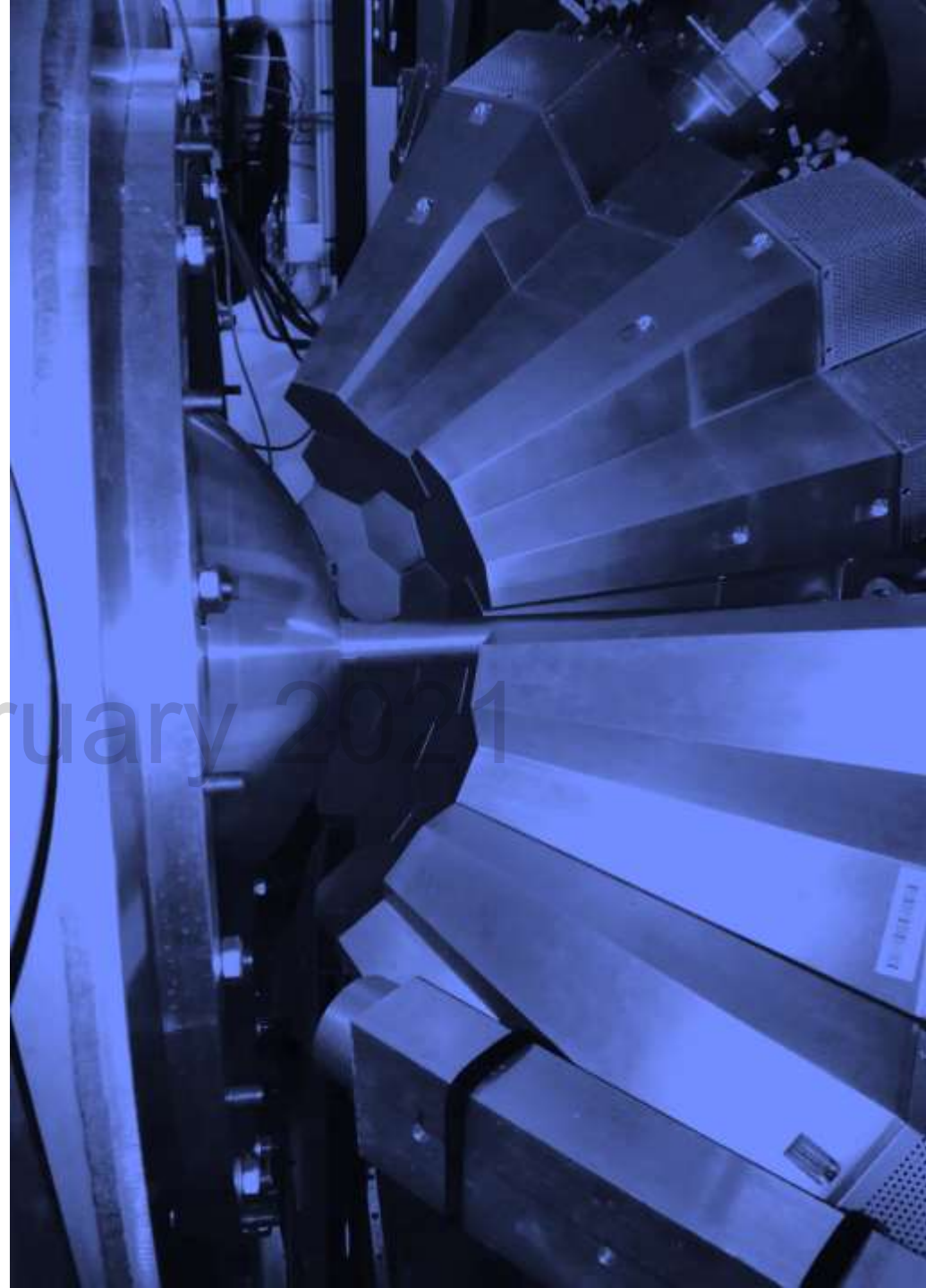
Richard Smith
STFC Daresbury Laboratory



Introduction

- Who am I?
- What am I doing here?
- Why am I here?

AGATA Week February 2011





Ian

Alan

**Bid farewell to Ian Burrows & Alan Grant,
we thank them both for their hard work & we wish them
a very happy retirement 😊**



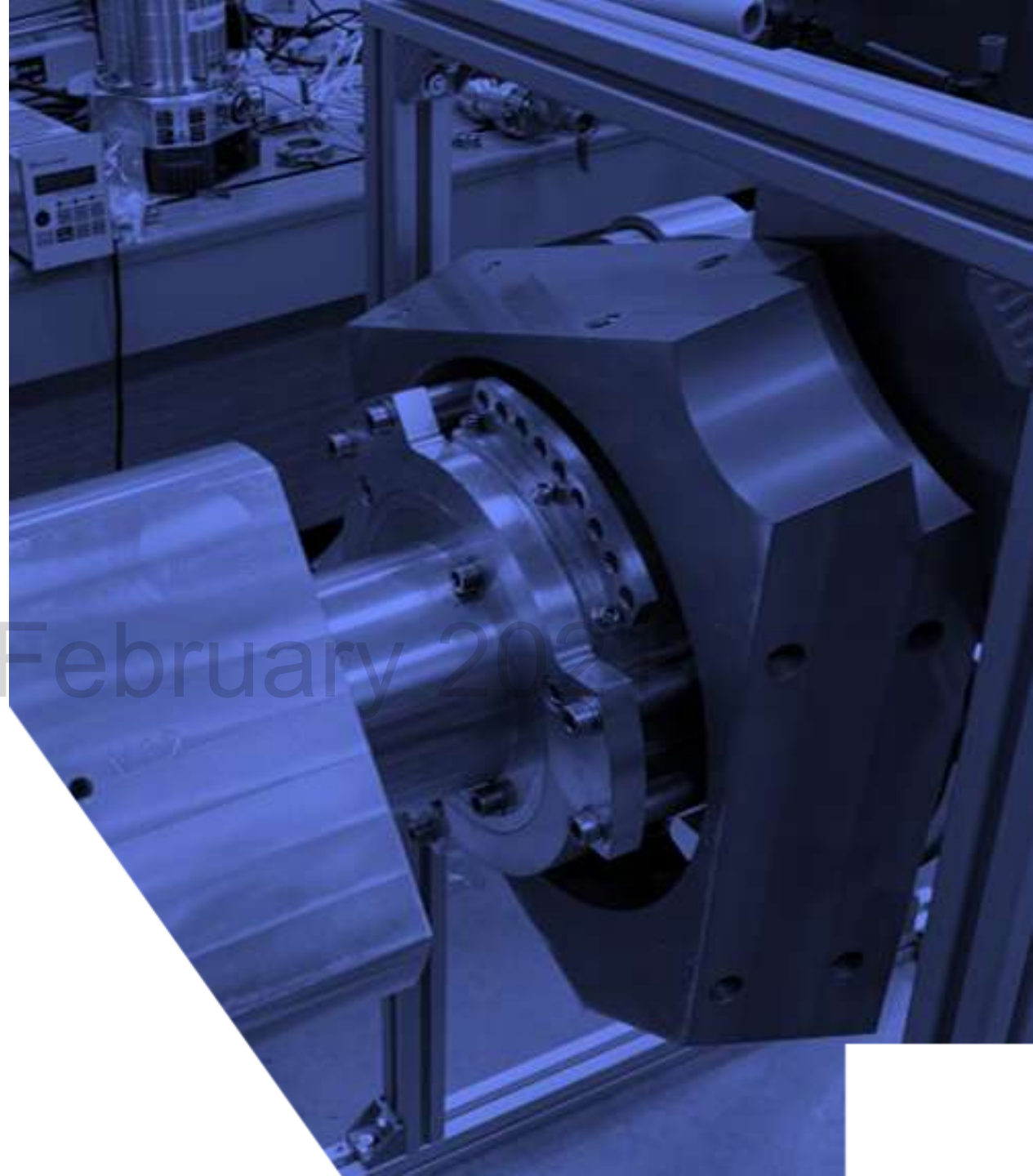
Ian and Alan's farewell gift

Mechanics Update

AGATA Week February 2025

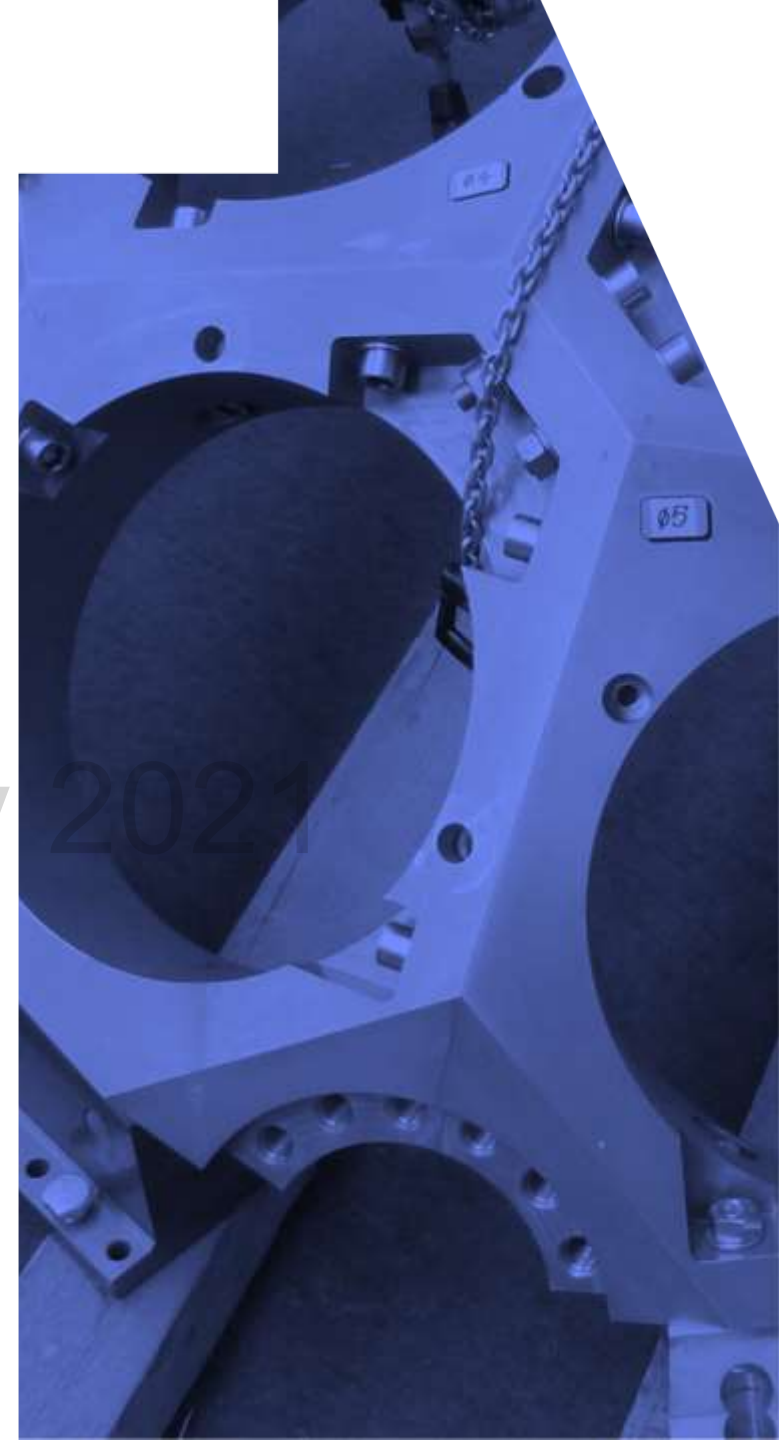


Science and
Technology
Facilities Council



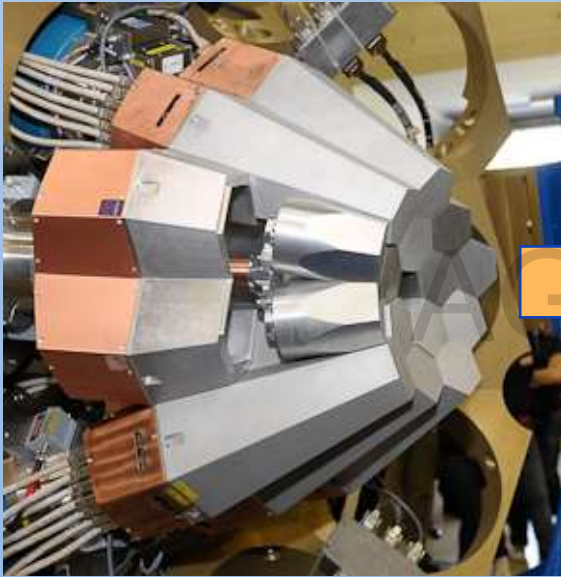
Mechanics update - Topics

- Support structure design for 2π array
- Conceptual design for 4π array
- Finite Element Analysis of the support structure & 2π array
- Support structure manufacture and assembly progress
- Associated mechanics:
 - ATC mounting rings (10 sets)
 - ATC Patch box mounting revision
 - ATC mounting leadscrew extension
 - Review lifting procedure for the ATC
 - ATC handling fixture
- Looking forward – What is next?



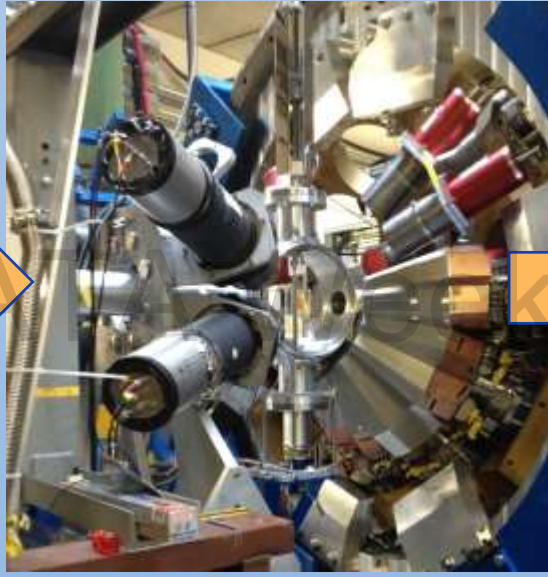
Support structure evolution

2010-2012
Legnaro, Italy
15 detectors



AGATA at LNL

2012-2014
GSI, Germany
25 detectors



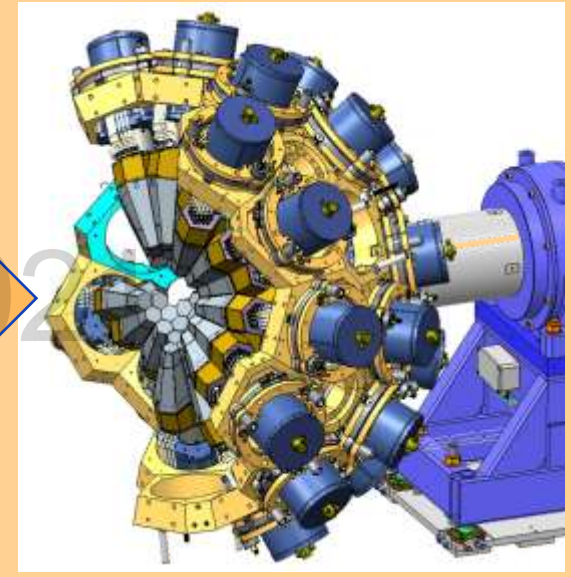
AGATA at GSI

2014-2021
GANIL, France
45 detectors



AGATA at GANIL

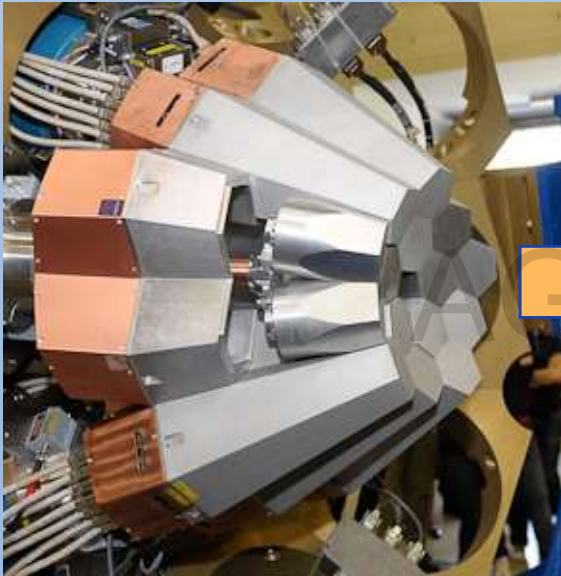
2021-2024
Legnaro, Italy
87 detectors



AGATA at LNL

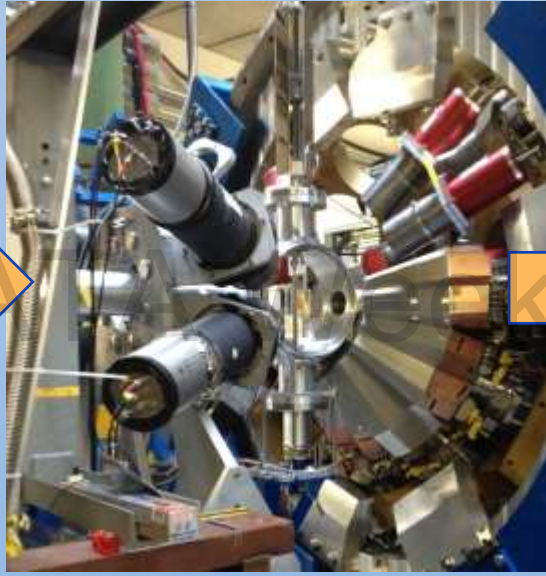
Support structure evolution

2010-2012
Legnaro, Italy
15 detectors



AGATA at LNL

2012-2014
GSI, Germany
25 detectors



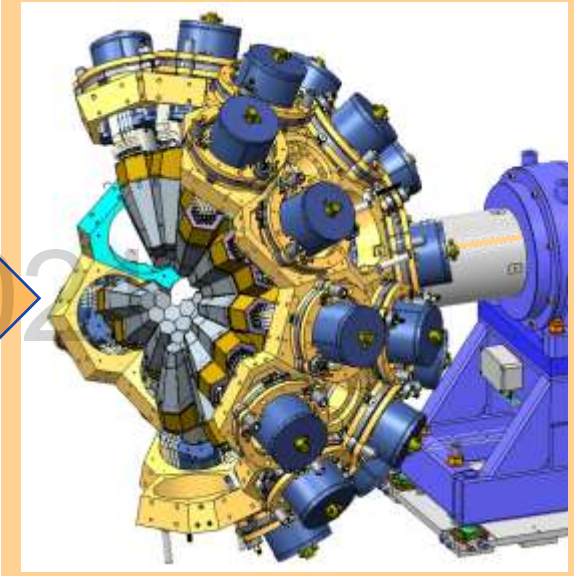
AGATA at GSI

2014-2021
GANIL, France
45 detectors



AGATA at GANIL

2021-2024
Legnaro, Italy
87 detectors



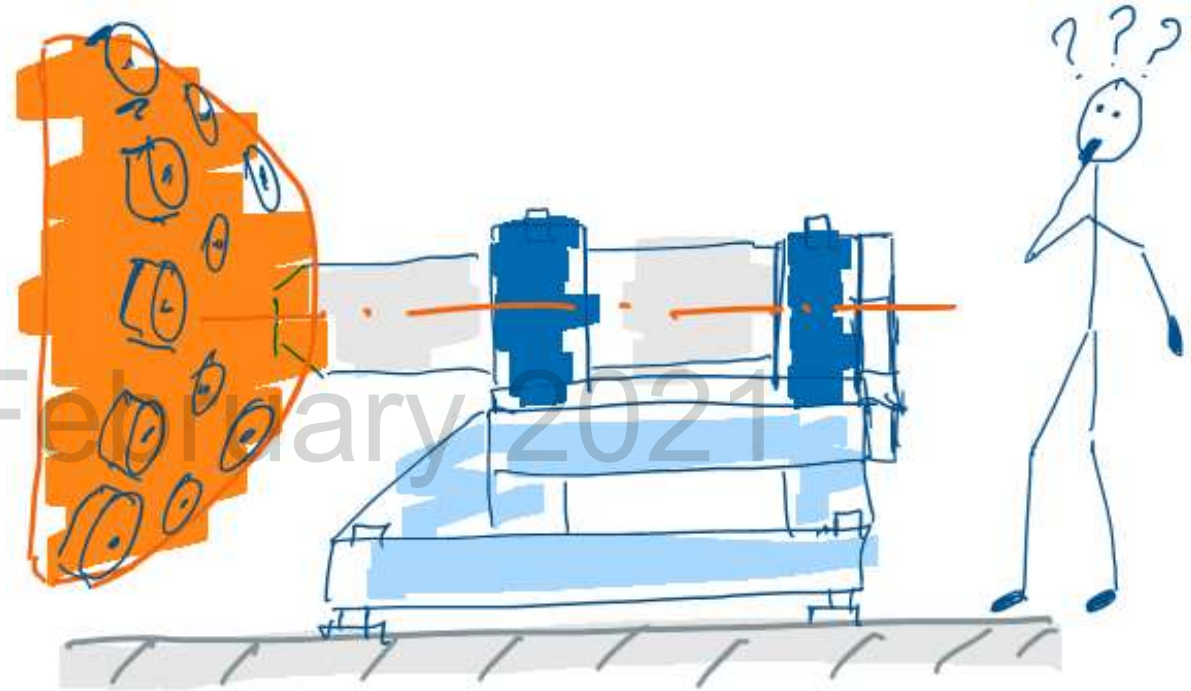
AGATA at LNL

Future facilities
180 detectors

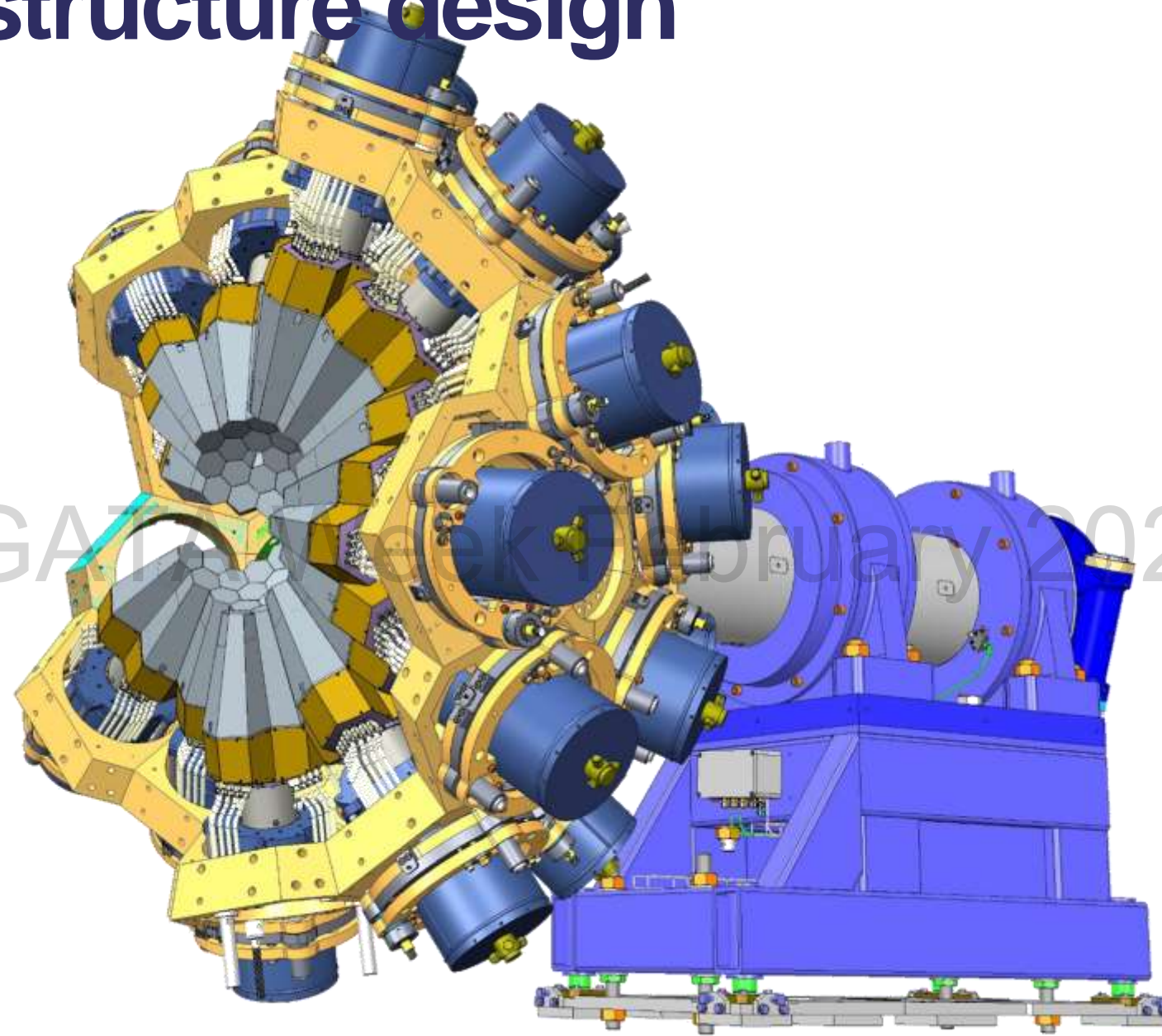


Support structure design

- Support 2π configuration (90 detectors)
- Design adaptable for future 4π array
- Assist mounting & unmounting the ATCs
- Stiff structure with high level of repeatability
- Adjustable frame to allow alignment
- Support LN_2 manifold $\sim 250\text{kg}$
- Interface with area at LNL & future sites



Support structure design

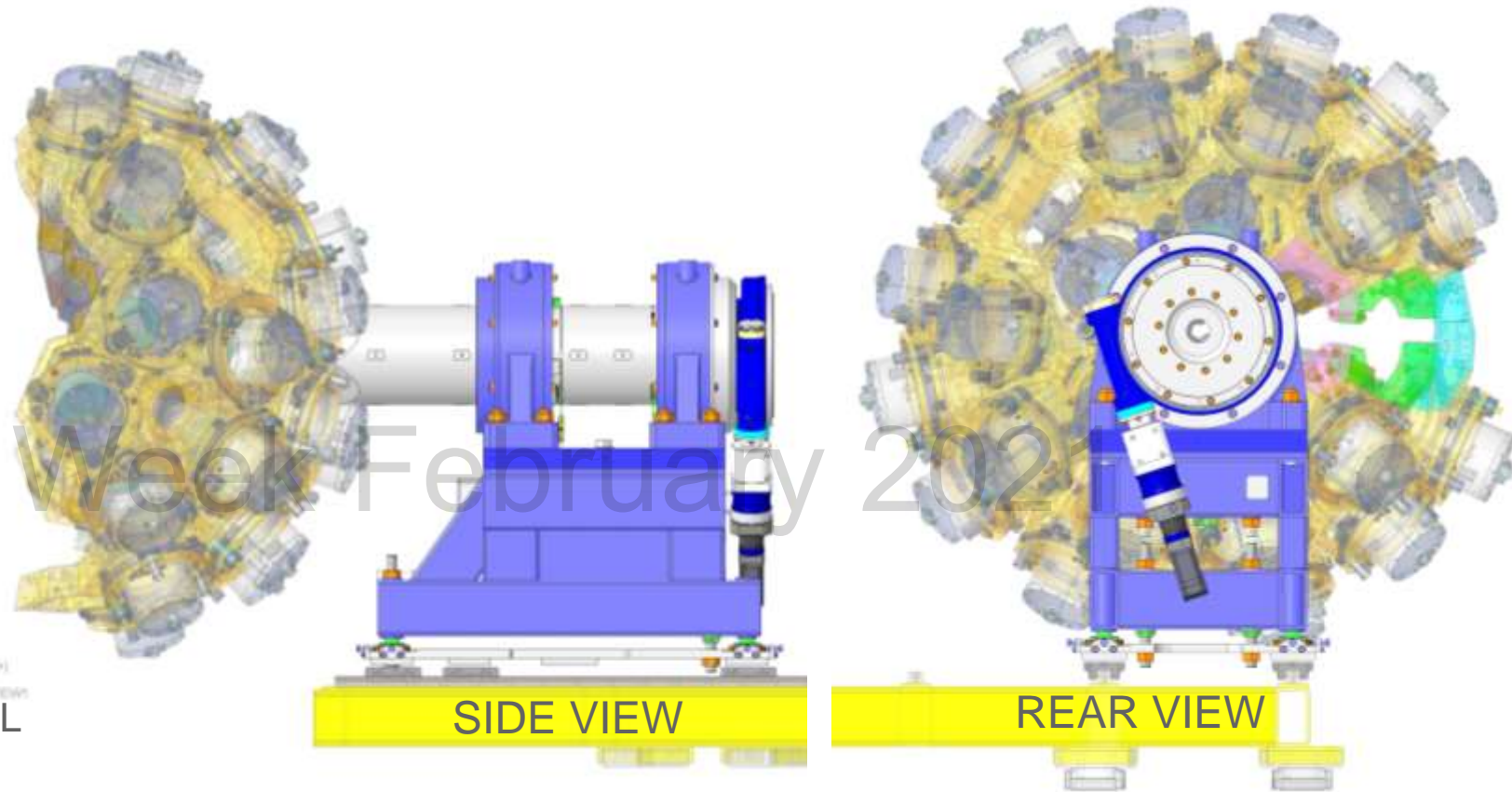


AGAT Book February 2021



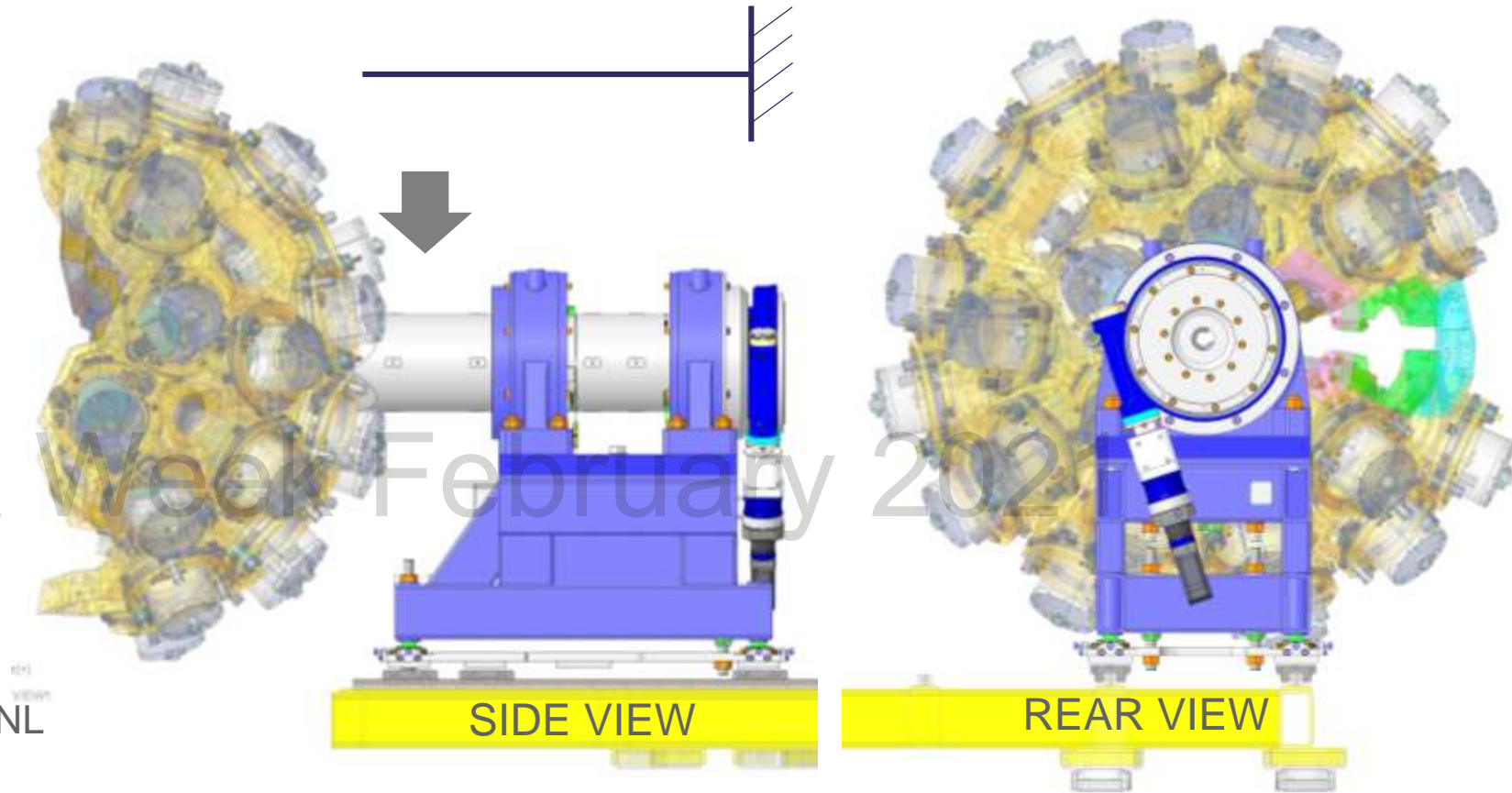
Support structure

- Cantilever design
- 360mm diameter hollow steel shaft
- Spherical roller bearings & housings
- Slewing drive
- Stepper motor driven
- Dual gearbox (combined ratio 80:1)
- Optical encoder feedback
- Mechanical limit switches
- Fabricated main frame
- Kinematic adjustment
- Interface with rail carriage system at LNL
- Multiple survey points



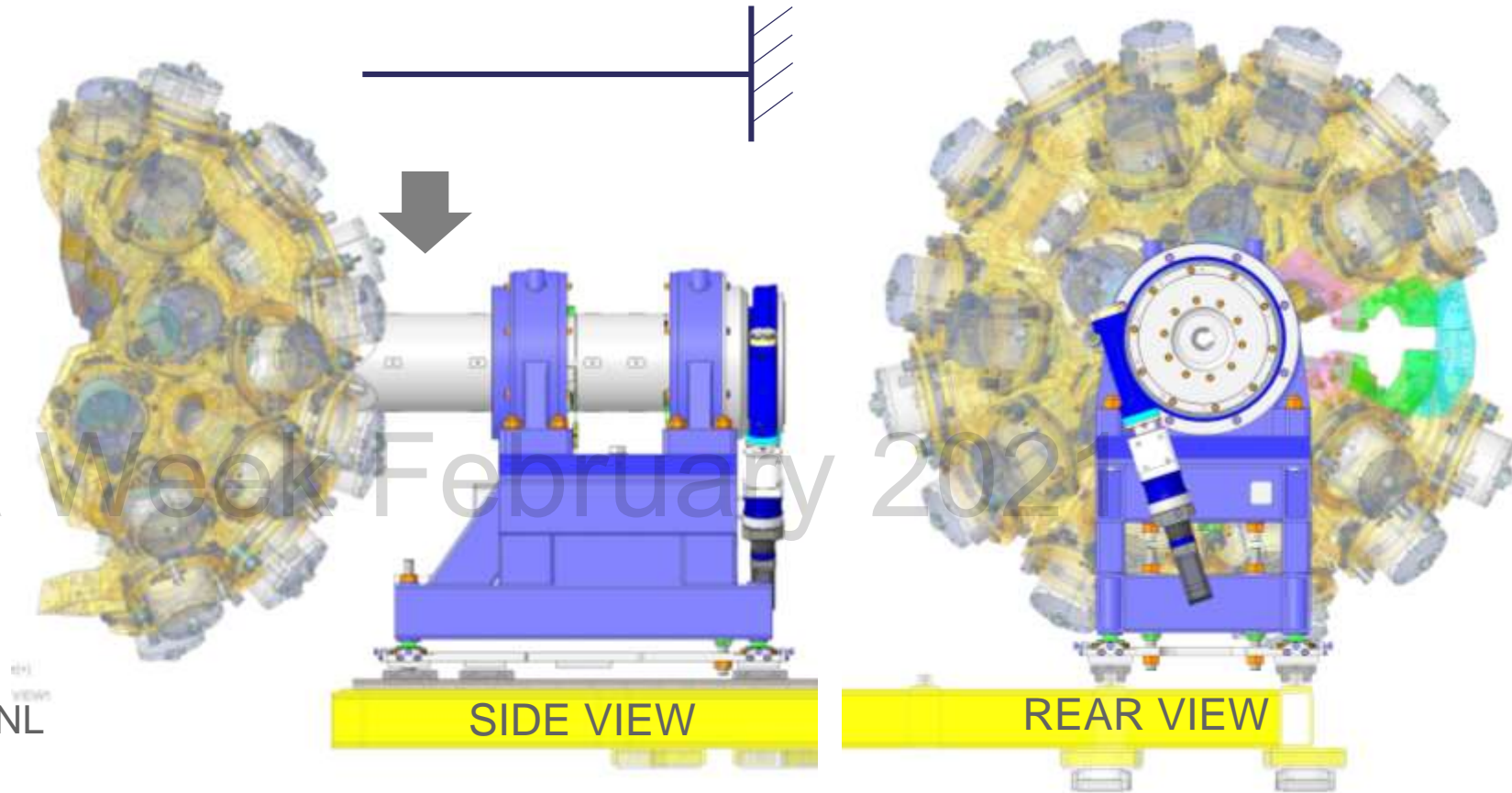
Support structure

- **Cantilever design**
- 360mm diameter hollow steel shaft
- Spherical roller bearings & housings
- Slewing drive
- Stepper motor driven
- Dual gearbox (combined ratio 80:1)
- Optical encoder feedback
- Mechanical limit switches
- Fabricated main frame
- Kinematic adjustment
- Interface with rail carriage system at LNL
- Multiple survey points



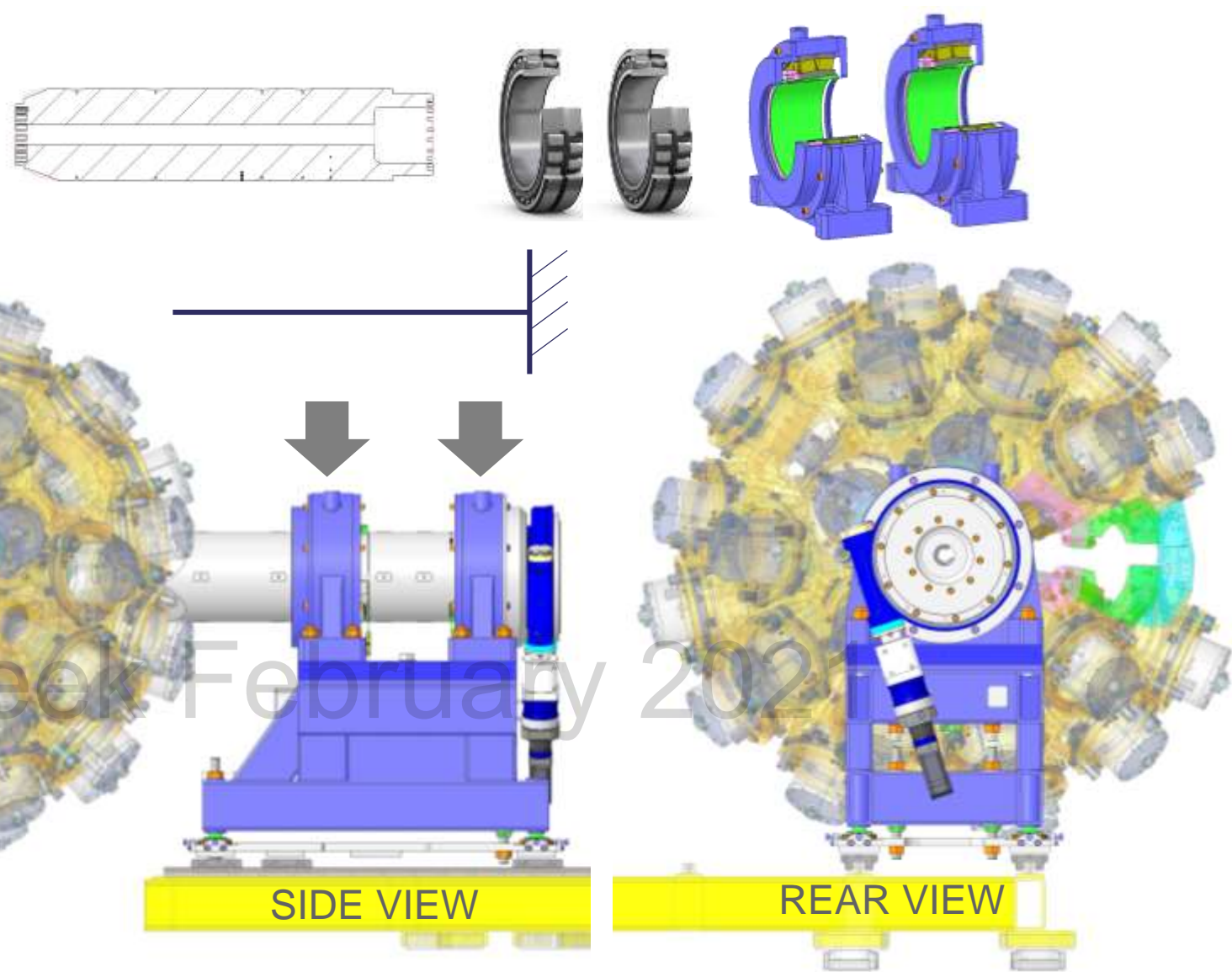
Support structure

- Cantilever design
- **360mm diameter hollow steel shaft**
- Spherical roller bearings & housings
- Slewing drive
- Stepper motor driven
- Dual gearbox (combined ratio 80:1)
- Optical encoder feedback
- Mechanical limit switches
- Fabricated main frame
- Kinematic adjustment
- Interface with rail carriage system at LNL
- Multiple survey points



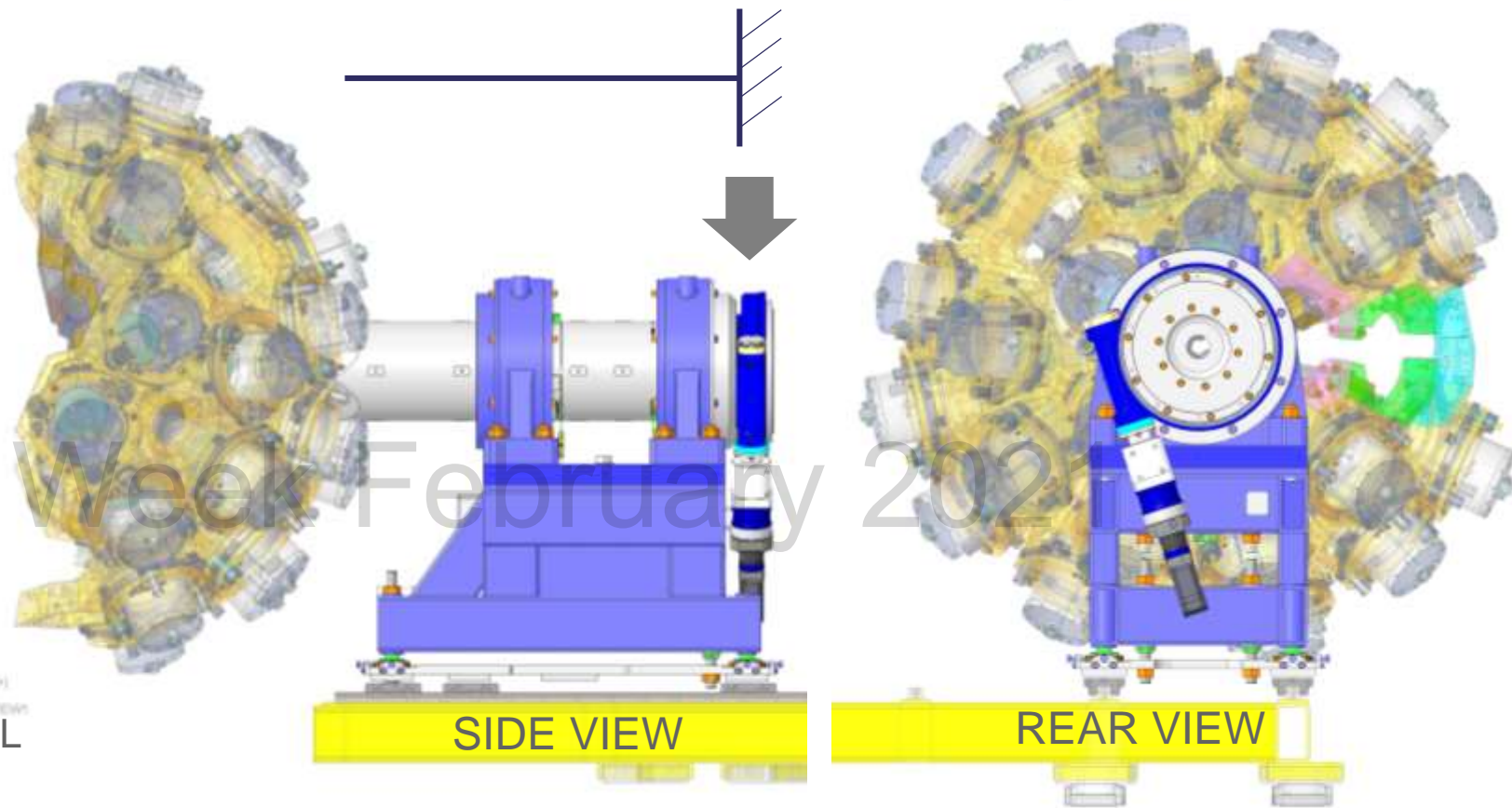
Support structure

- Cantilever design
- 360mm diameter hollow steel shaft
- **Spherical roller bearings & housings**
- Slewing drive
- Stepper motor driven
- Dual gearbox (combined ratio 80:1)
- Optical encoder feedback
- Mechanical limit switches
- Fabricated main frame
- Kinematic adjustment
- Interface with rail carriage system at LNL
- Multiple survey points



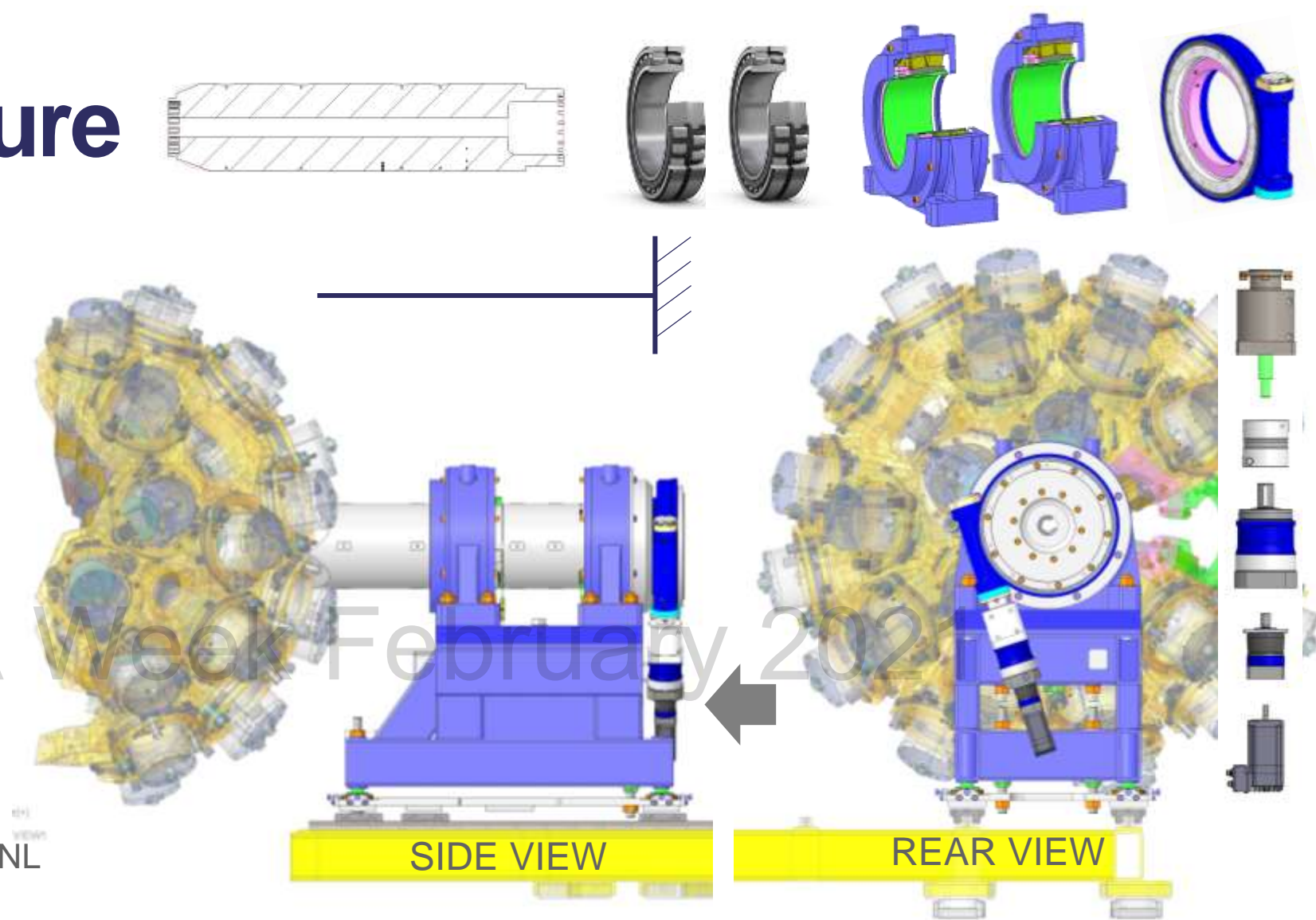
Support structure

- Cantilever design
- 360mm diameter hollow steel shaft
- Spherical roller bearings & housings
- **Slewing drive**
- Stepper motor driven
- Dual gearbox (combined ratio 80:1)
- Optical encoder feedback
- Mechanical limit switches
- Fabricated main frame
- Kinematic adjustment
- Interface with rail carriage system at LNL
- Multiple survey points



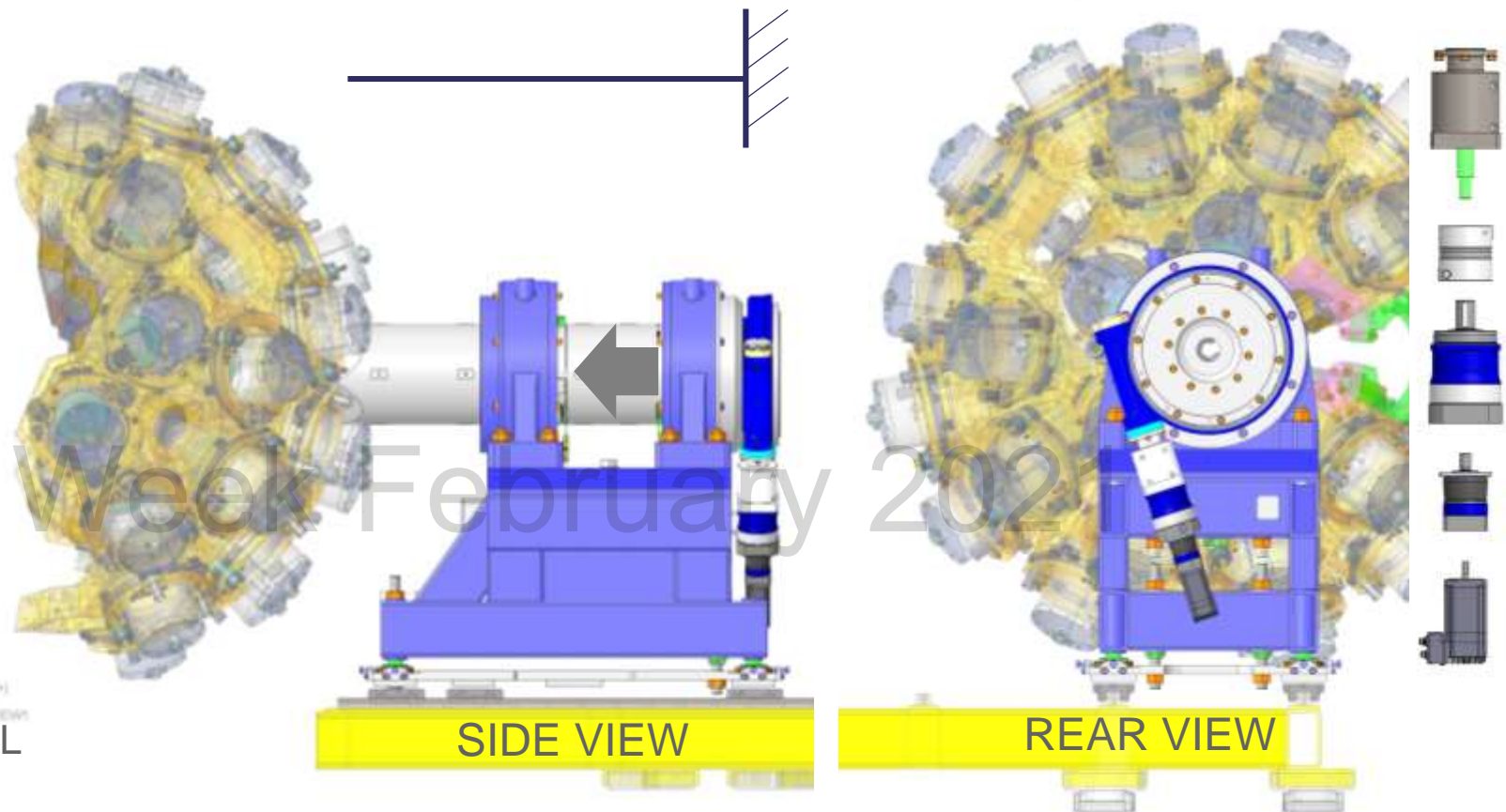
Support structure

- Cantilever design
- 360mm diameter hollow steel shaft
- Spherical roller bearings & housings
- Slewing drive
- **Stepper motor driven**
- **Dual gearbox (combined ratio 80:1)**
- Optical encoder feedback
- Mechanical limit switches
- Fabricated main frame
- Kinematic adjustment
- Interface with rail carriage system at LNL
- Multiple survey points



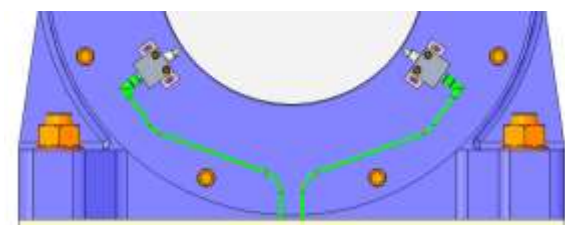
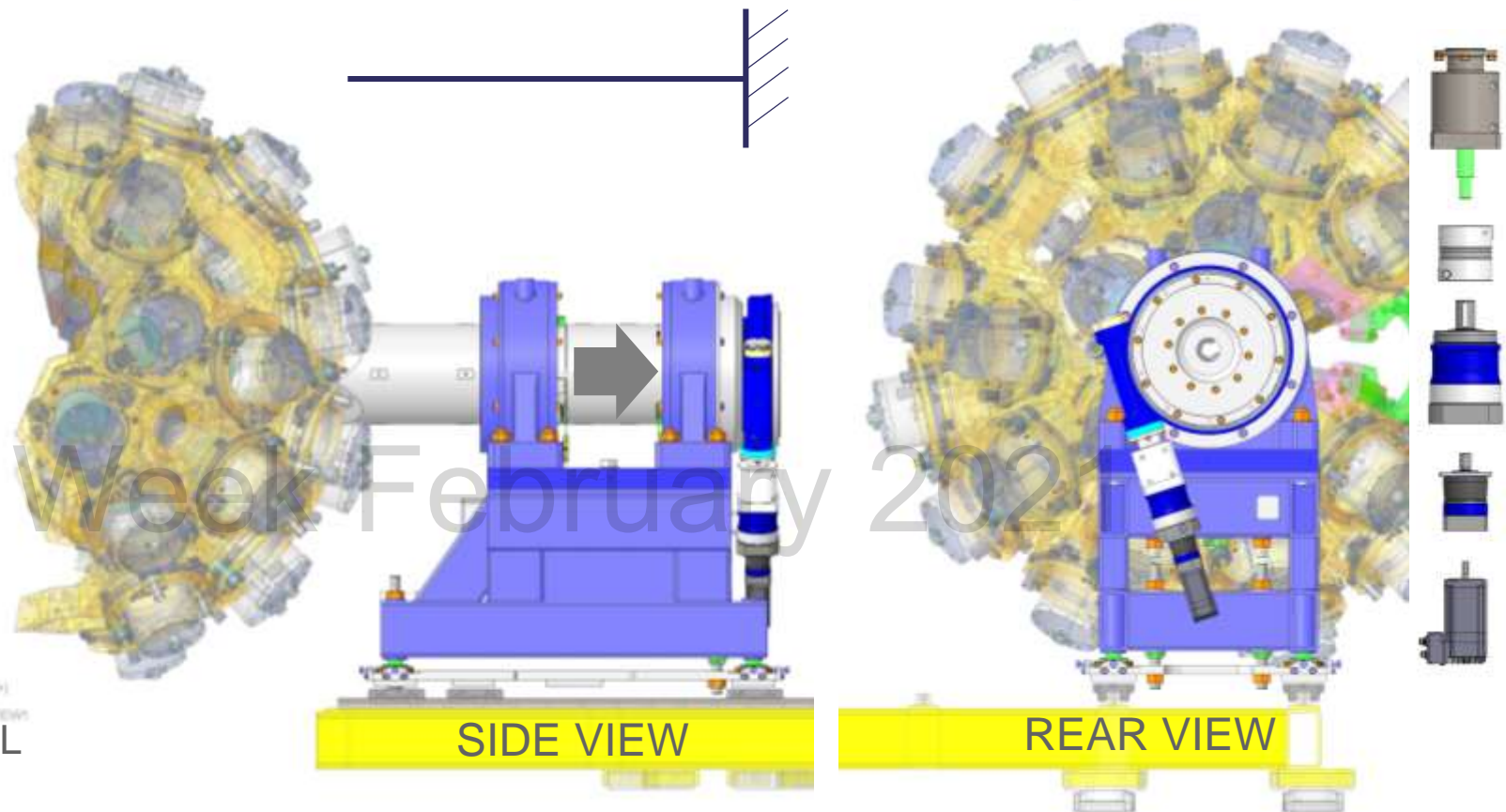
Support structure

- Cantilever design
- 360mm diameter hollow steel shaft
- Spherical roller bearings & housings
- Slewing drive
- Stepper motor driven
- Dual gearbox (combined ratio 80:1)
- **Optical encoder feedback**
- Mechanical limit switches
- Fabricated main frame
- Kinematic adjustment
- Interface with rail carriage system at LNL
- Multiple survey points



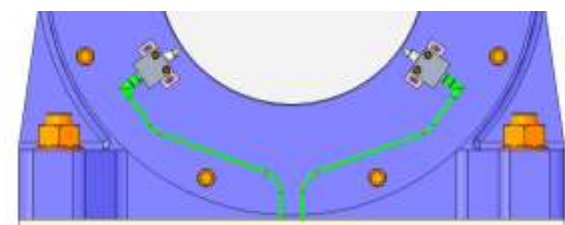
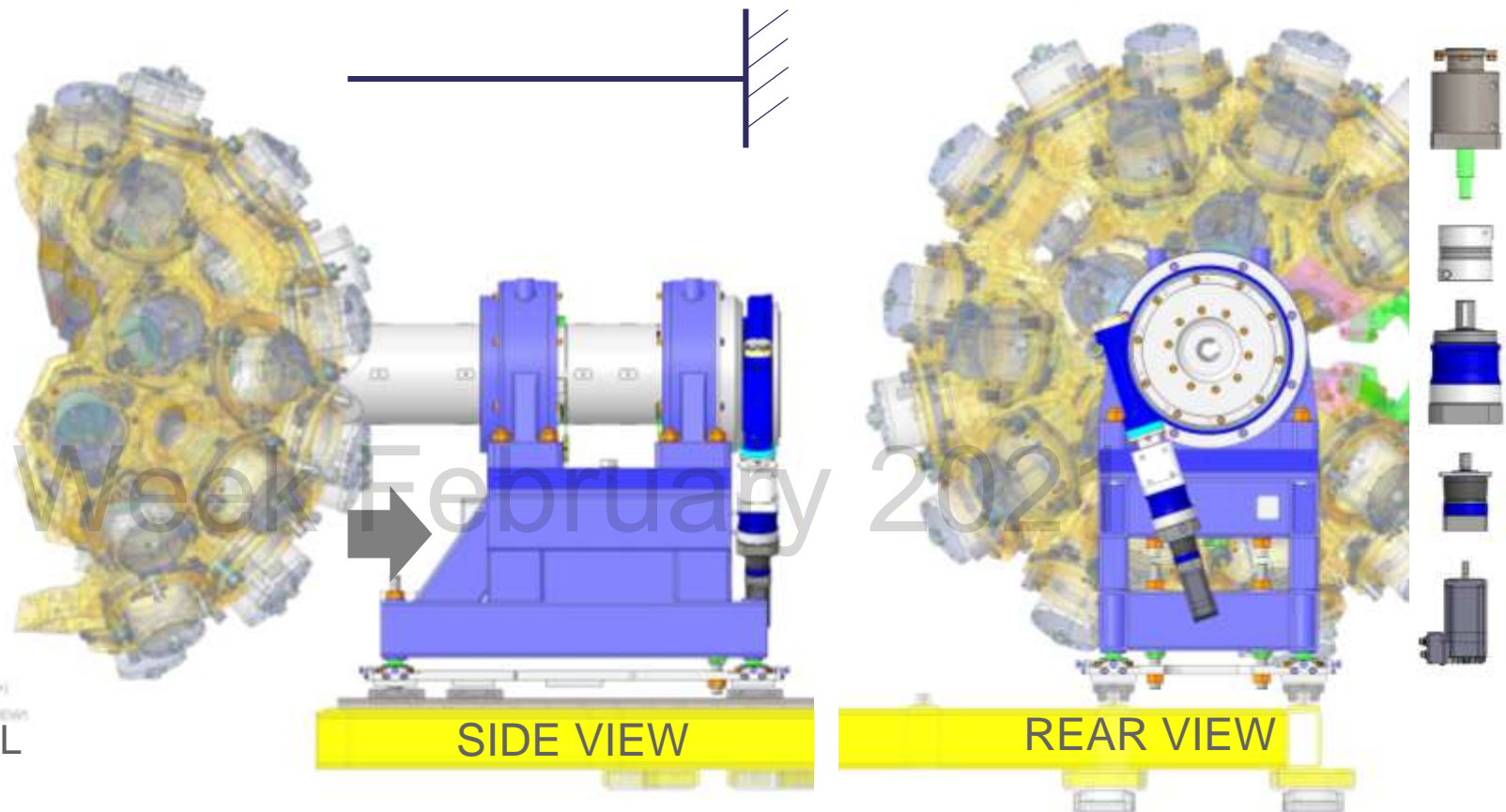
Support structure

- Cantilever design
- 360mm diameter hollow steel shaft
- Spherical roller bearings & housings
- Slewing drive
- Stepper motor driven
- Dual gearbox (combined ratio 80:1)
- Optical encoder feedback
- **Mechanical limit switches**
- Fabricated main frame
- Kinematic adjustment
- Interface with rail carriage system at LNL
- Multiple survey points



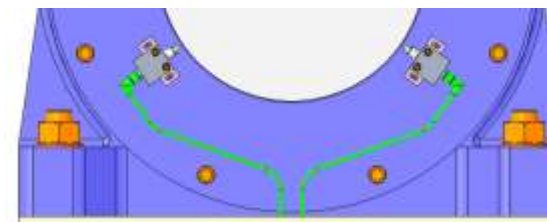
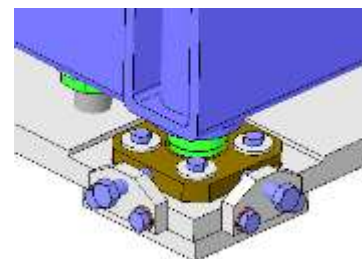
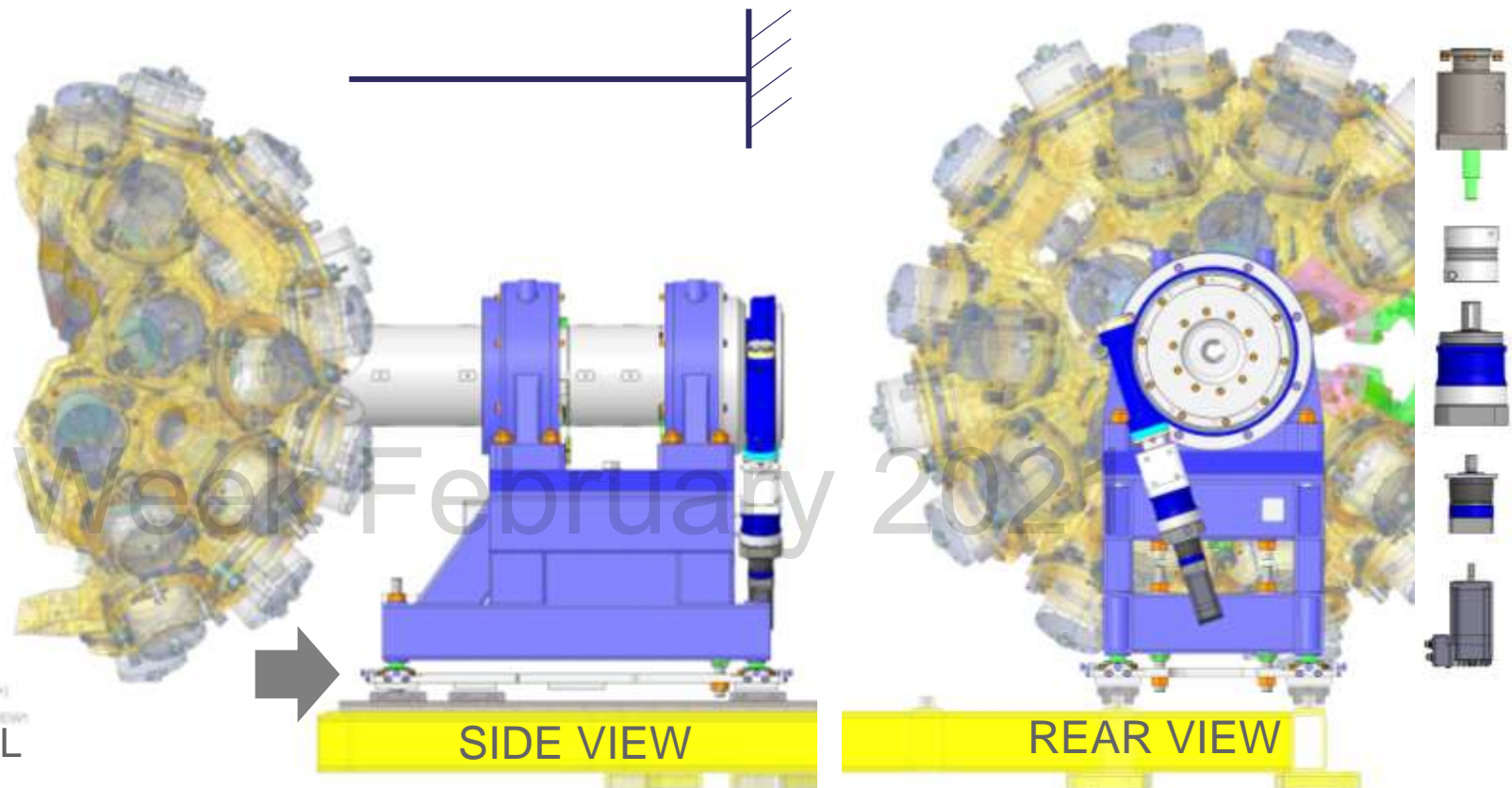
Support structure

- Cantilever design
- 360mm diameter hollow steel shaft
- Spherical roller bearings & housings
- Slewing drive
- Stepper motor driven
- Dual gearbox (combined ratio 80:1)
- Optical encoder feedback
- Mechanical limit switches
- **Fabricated main frame**
- Kinematic adjustment
- Interface with rail carriage system at LNL
- Multiple survey points



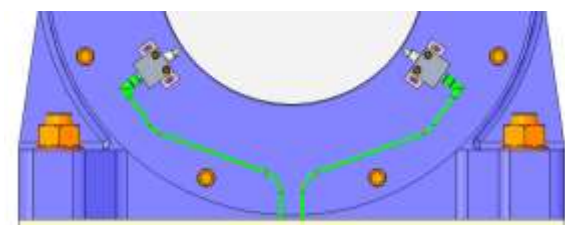
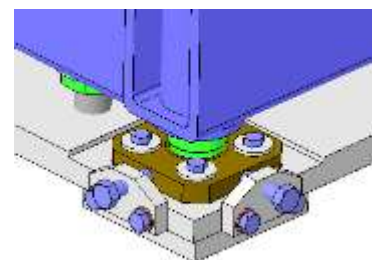
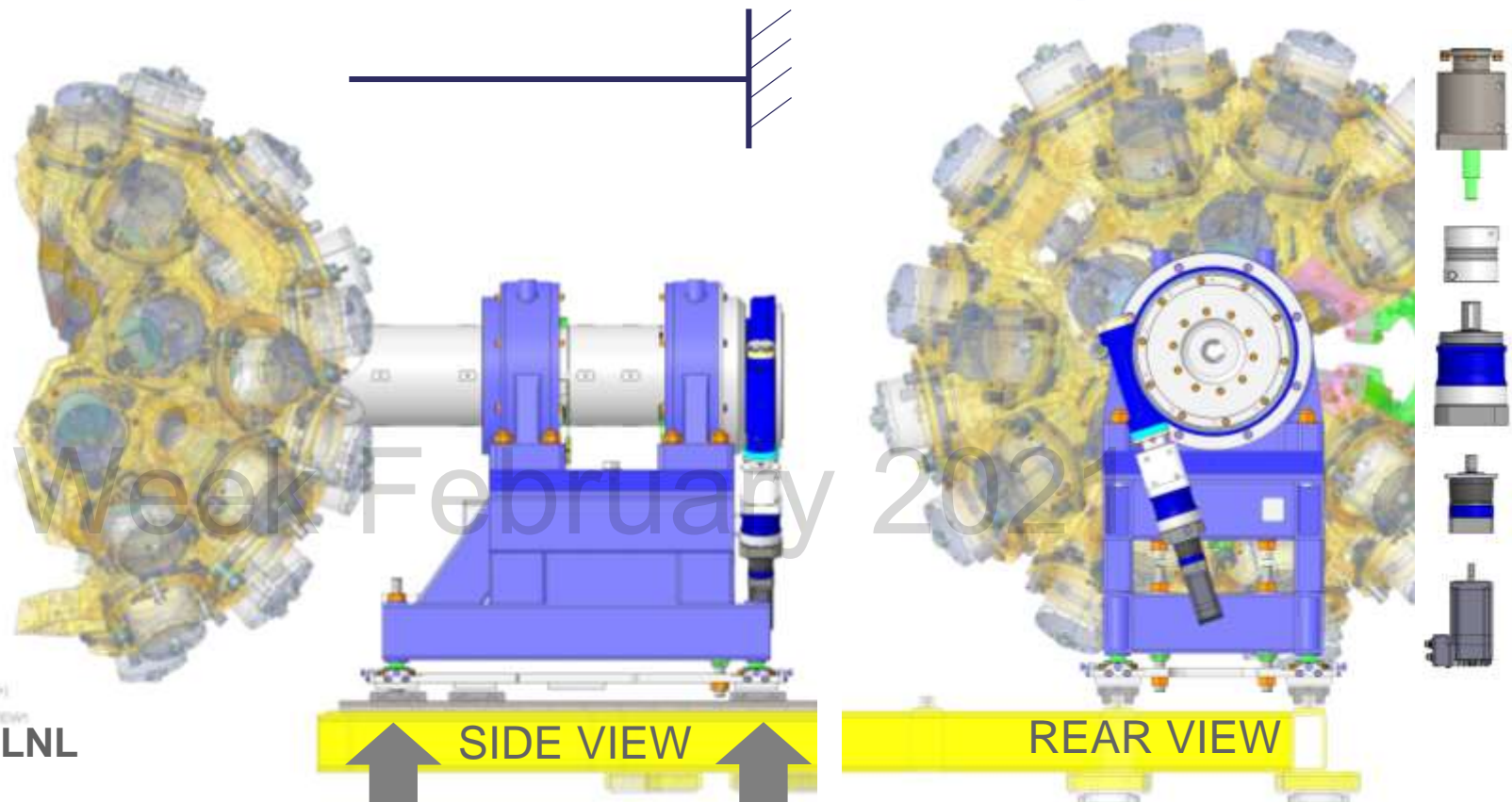
Support structure

- Cantilever design
- 360mm diameter hollow steel shaft
- Spherical roller bearings & housings
- Slewing drive
- Stepper motor driven
- Dual gearbox (combined ratio 80:1)
- Optical encoder feedback
- Mechanical limit switches
- Fabricated main frame
- **Kinematic adjustment**
- Interface with rail carriage system at LNL
- Multiple survey points



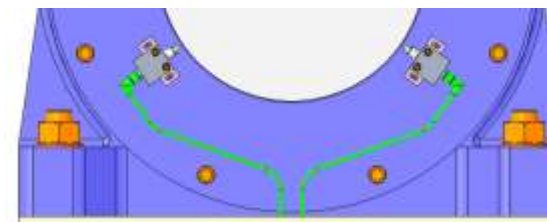
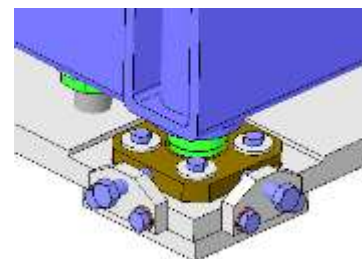
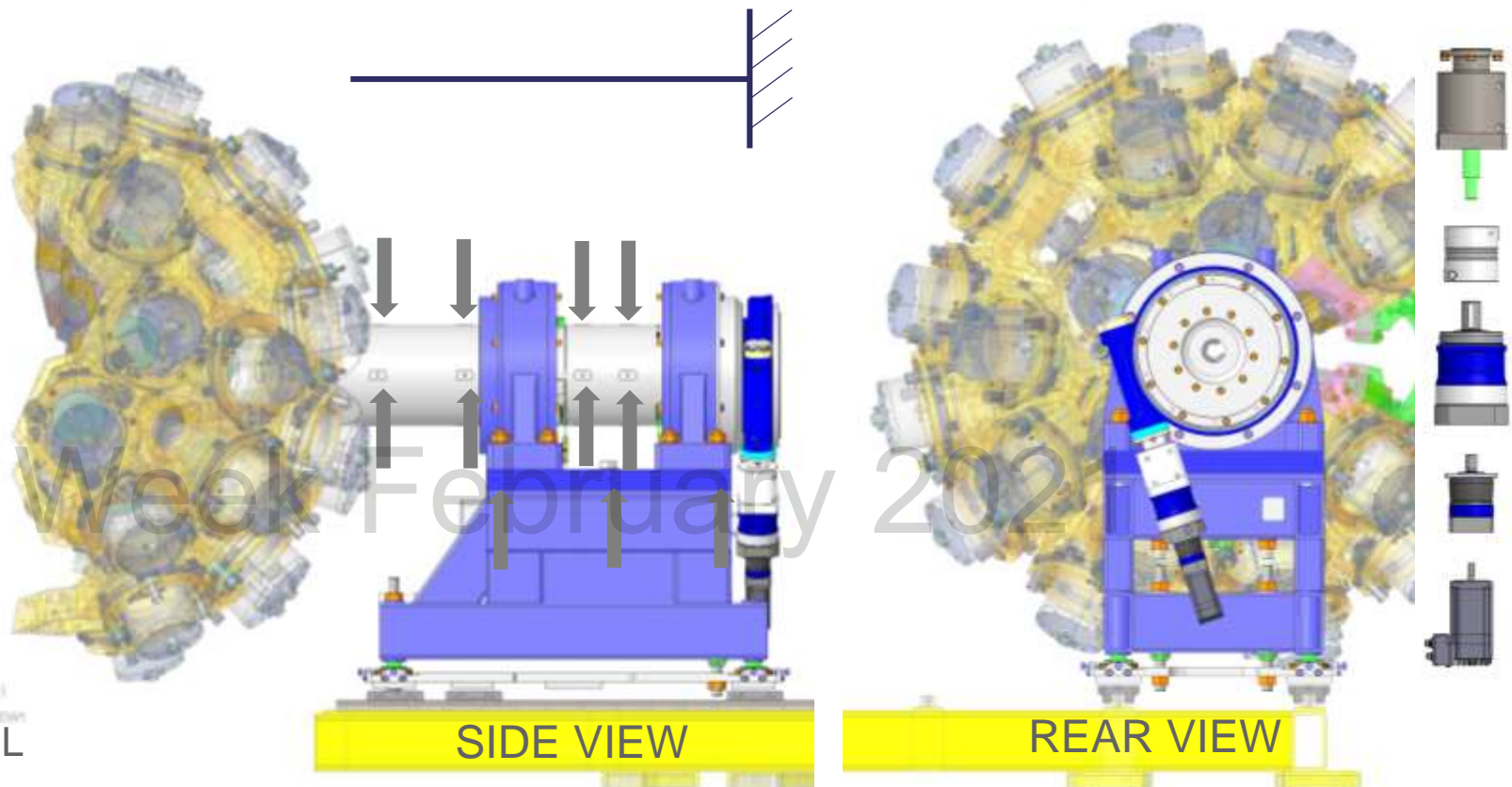
Support structure

- Cantilever design
- 360mm diameter hollow steel shaft
- Spherical roller bearings & housings
- Slewing drive
- Stepper motor driven
- Dual gearbox (combined ratio 80:1)
- Optical encoder feedback
- Mechanical limit switches
- Fabricated main frame
- Kinematic adjustment
- **Interface with rail carriage system at LNL**
- Multiple survey points



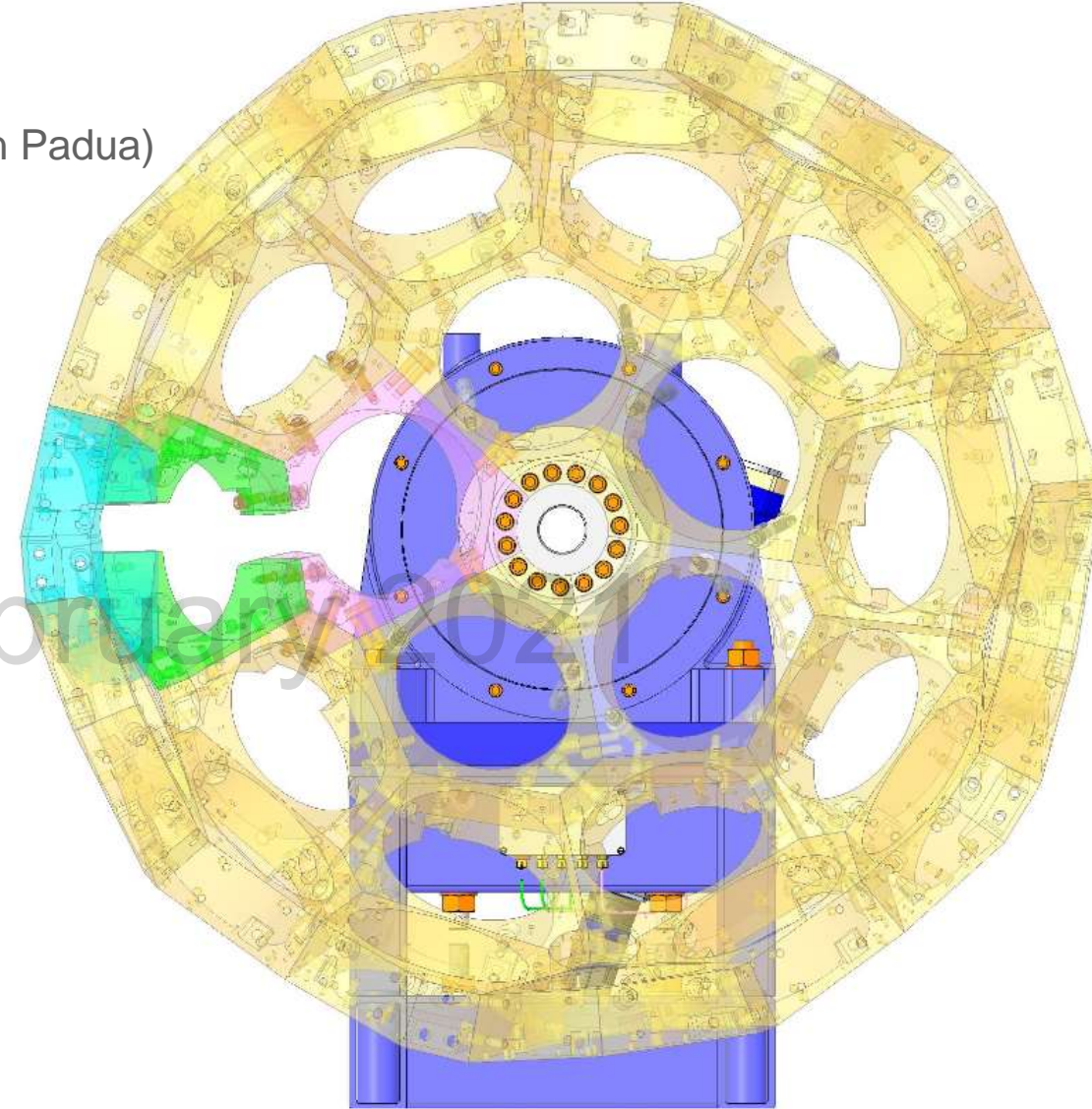
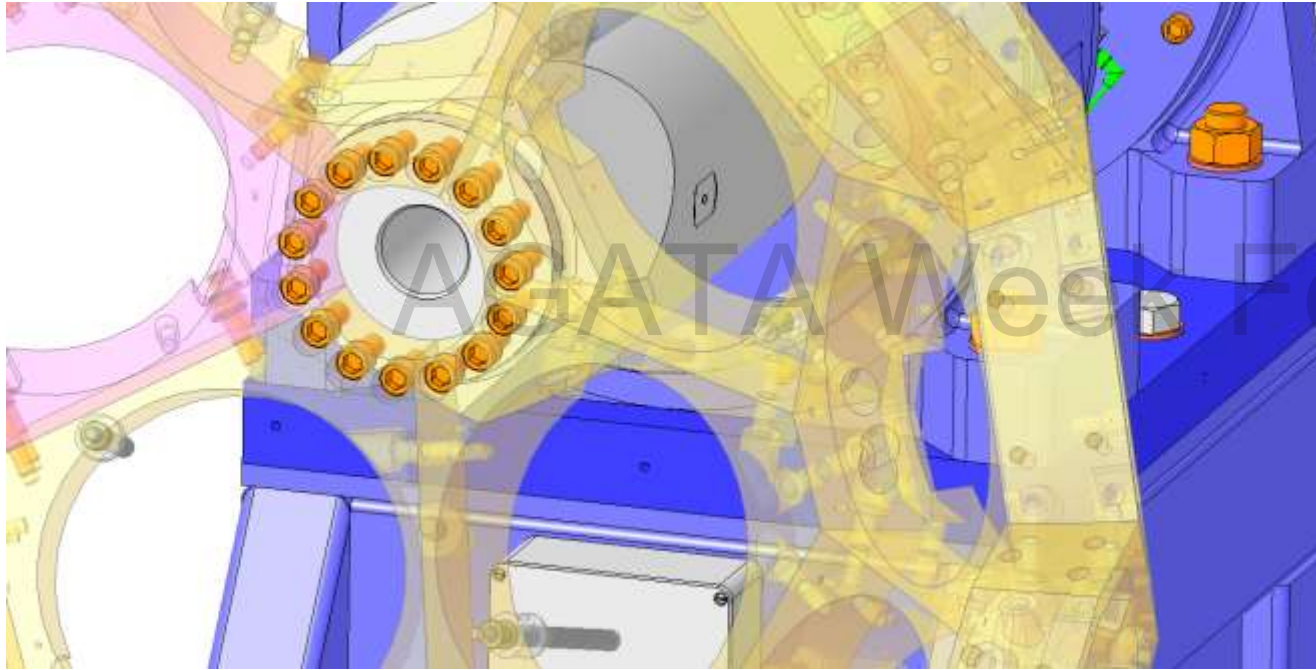
Support structure

- Cantilever design
- 360mm diameter hollow steel shaft
- Spherical roller bearings & housings
- Slewing drive
- Stepper motor driven
- Dual gearbox (combined ratio 80:1)
- Optical encoder feedback
- Mechanical limit switches
- Fabricated main frame
- Kinematic adjustment
- Interface with rail carriage system at LNL
- **Multiple survey points**



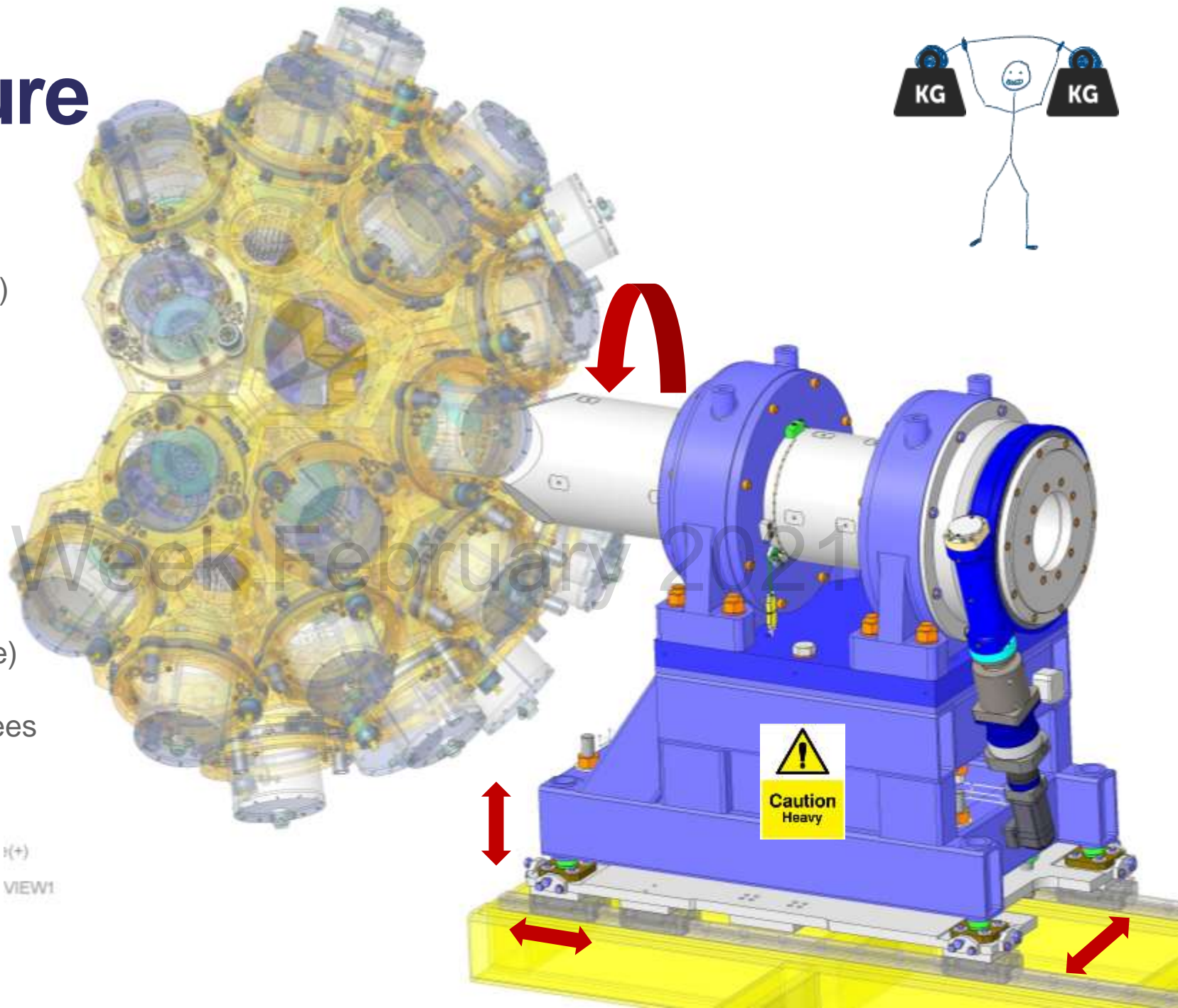
Support structure

- 5 revised flanges with through holes (currently being manufactured in Padua)
- Flanges secured to shaft with M20 fasteners



Support structure

- ± 85 degrees rotation
- Supports 4000kg (ATCs & LN₂ manifold)
- Weighs ~3700kg (support alone)
- +/- 15mm lateral adjustment
- +/-25mm vertical adjustment
- Rotation controlled via PC or jog box
- 2 motion stop buttons (one on each side)
- Current speed ~3 minutes 0 to 85 degrees

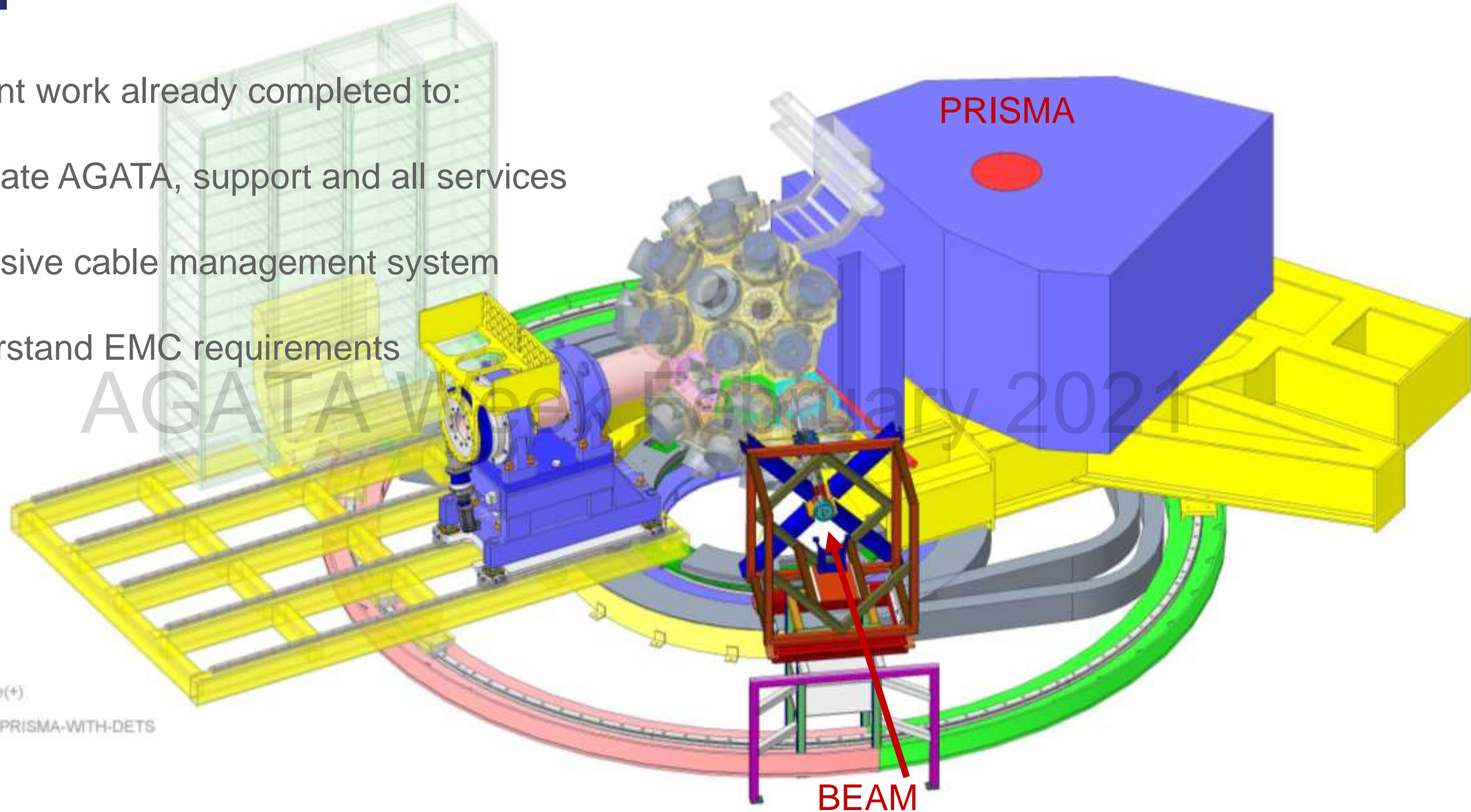


(+)
VIEW1

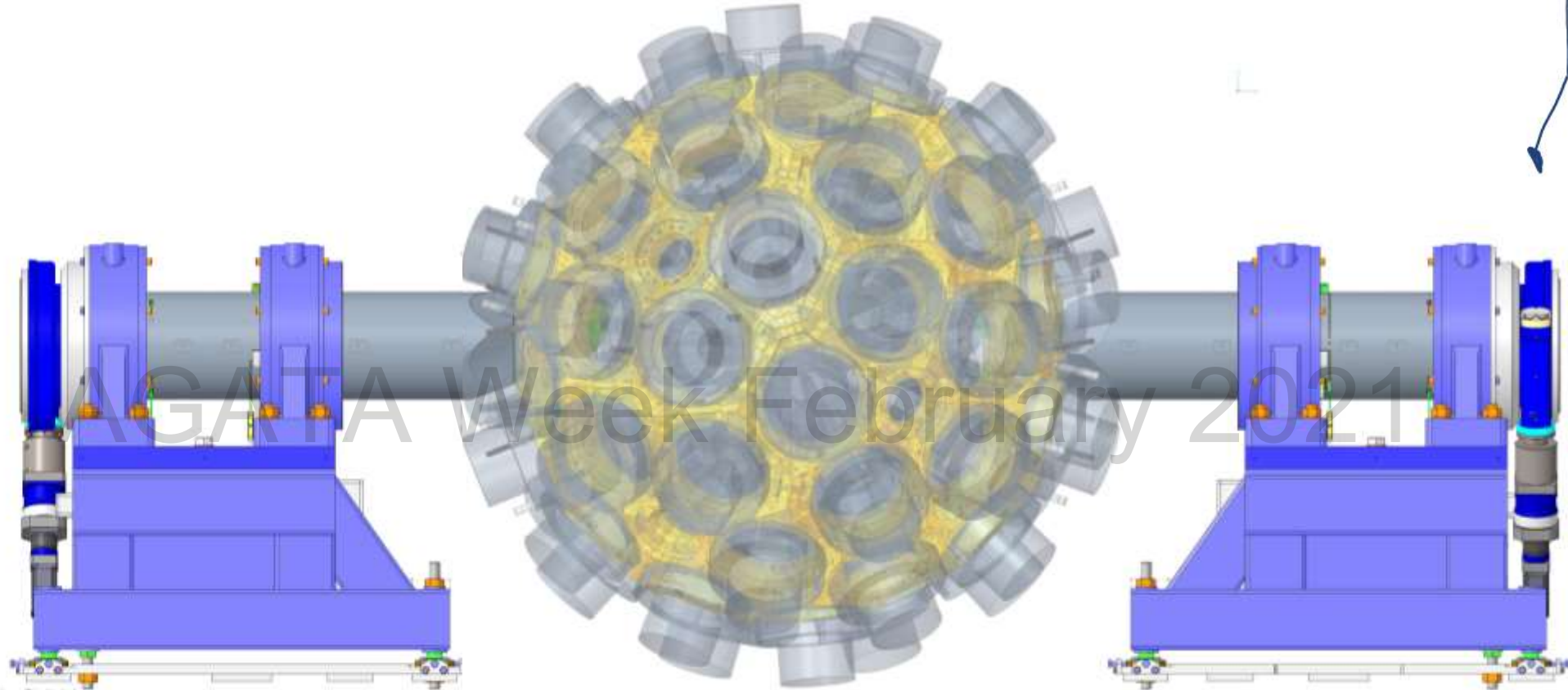
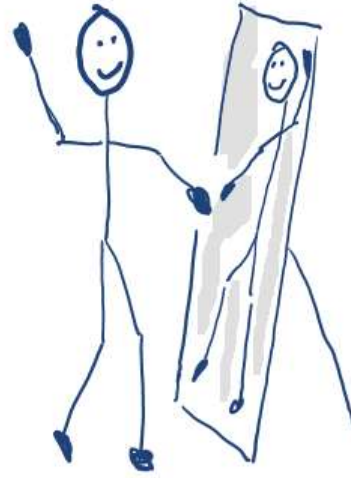
Support structure at LNL

Significant work already completed to:

- Integrate AGATA, support and all services
- Extensive cable management system
- Understand EMC requirements



4π Support structure



Style State:Master Style(+)

Finite Element Analysis

AGATA Week February 2022



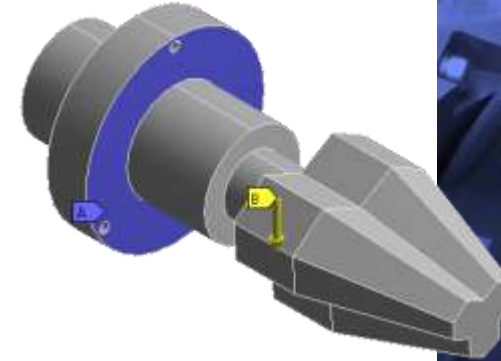
Science and
Technology
Facilities Council



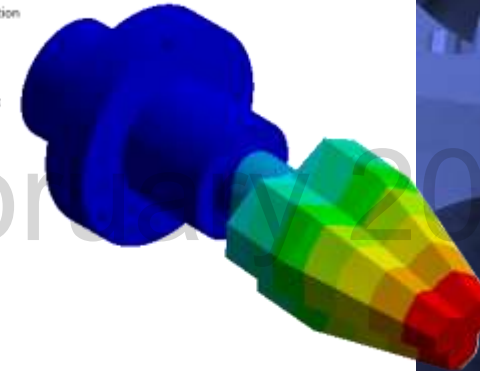
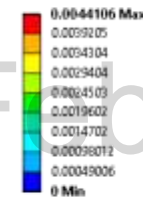
Finite Element Analysis

- Expected deflection range of complete system
- Directional deflection characteristics
- LN₂ manifold impact and orientation
- Relative deflection of triple cluster
- Flange cut-out for LNL campaign

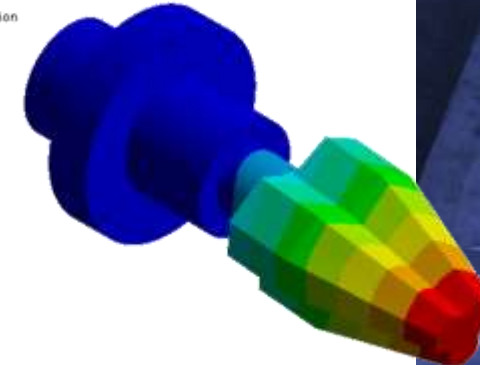
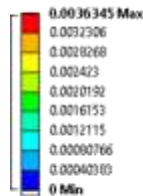
A Fixed Support
B Standard Earth Gravity: 9806.6 mm/s²



D: Al Alloy
Total Deformation
Type: Total Deformation
Unit: mm
Time: 1
18/08/2020 14:43



E: Structural Steel
Total Deformation
Type: Total Deformation
Unit: mm
Time: 1
18/08/2020 14:46



Finite Element Analysis

Stress von Mises (WCS)
(MPa)

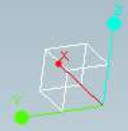
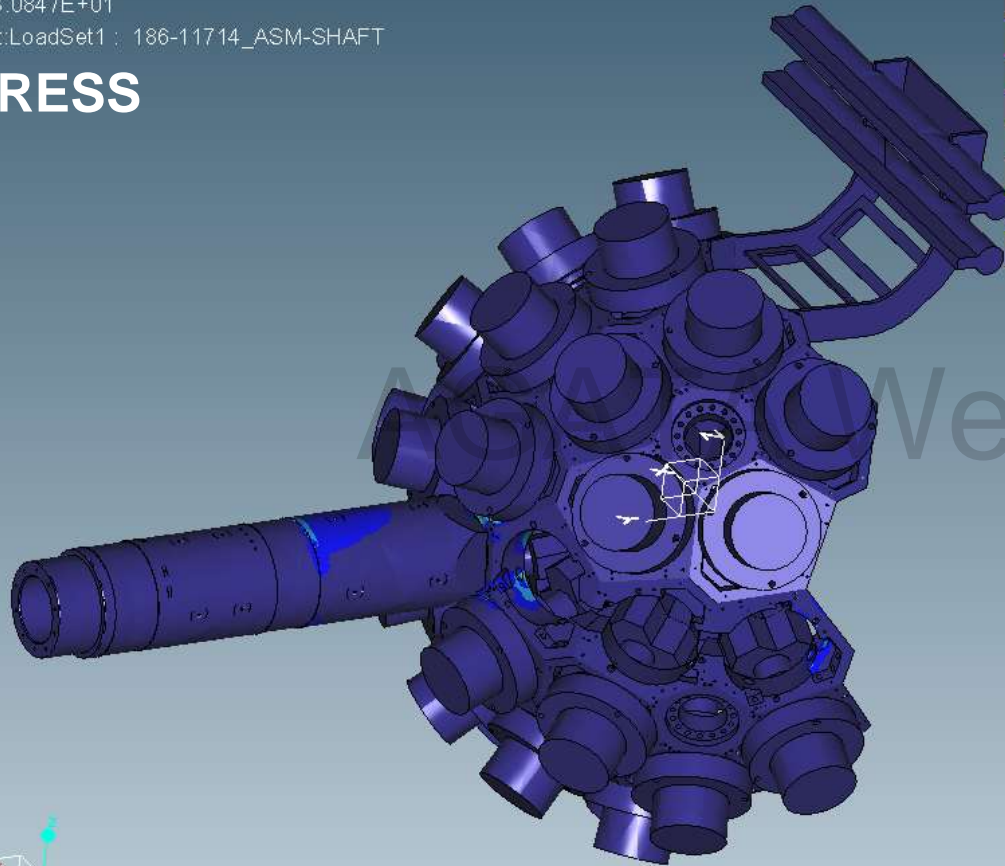
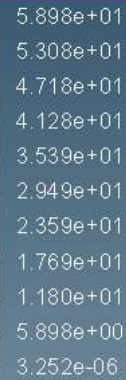
Deformed

Scale 3.0847E+01

Loadset:LoadSet1 : 186-11714_ASM-SHAFT

STRESS

58.9 MPa MAX



von Mises Stress Animation

Displacement Mag (WCS)
(mm)

Deformed

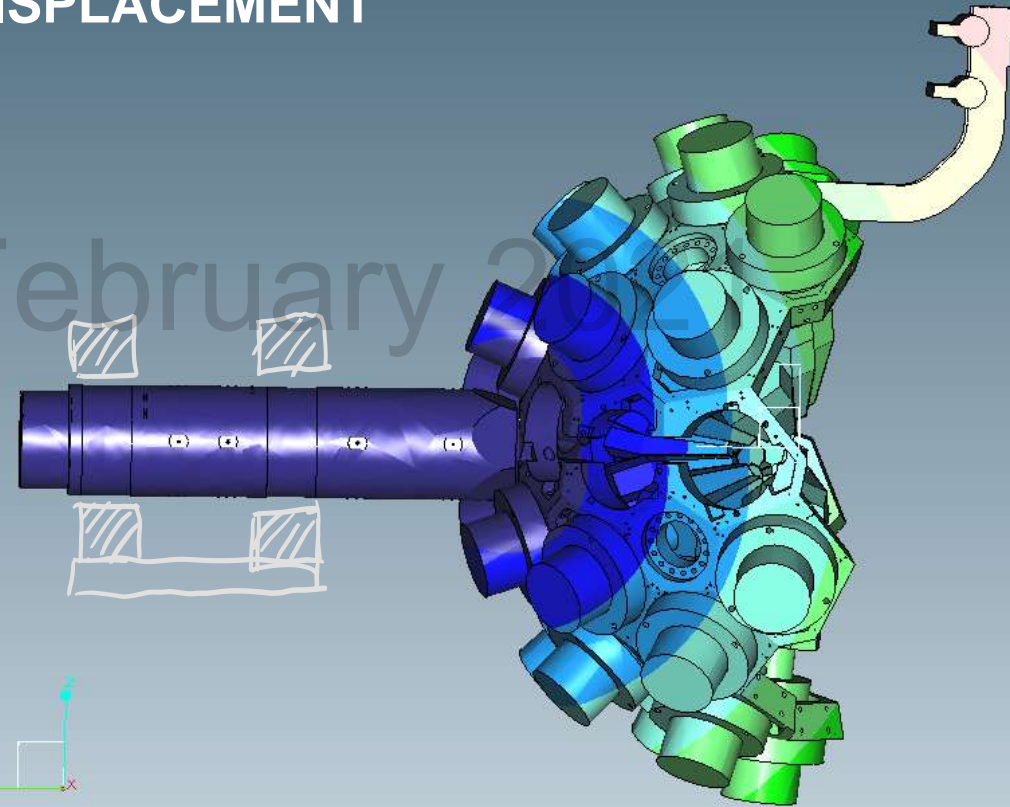
Max Disp 2.0456E+00

Scale 3.0847E+01

Loadset:LoadSet1 : 186-11714_ASM-SHAFT

DISPLACEMENT

2.04mm MAX

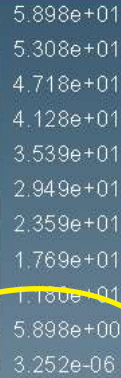


Displacement Magnitude Fringe

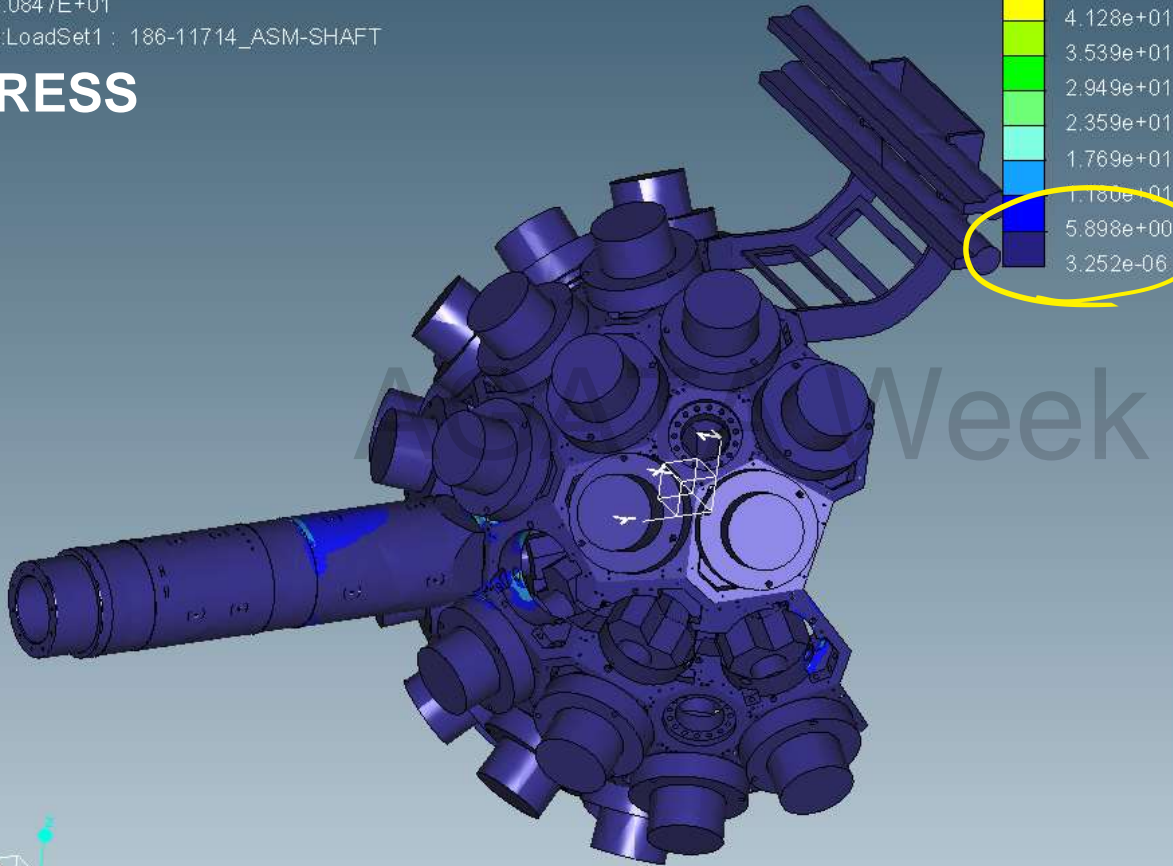
Finite Element Analysis

Stress von Mises (WCS)
(MPa)
Deformed
Scale 3.0847E+01
Loadset:LoadSet1 : 186-11714_ASM-SHAFT

58.9 MPa MAX

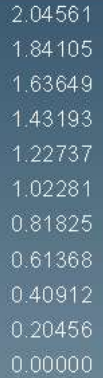


STRESS

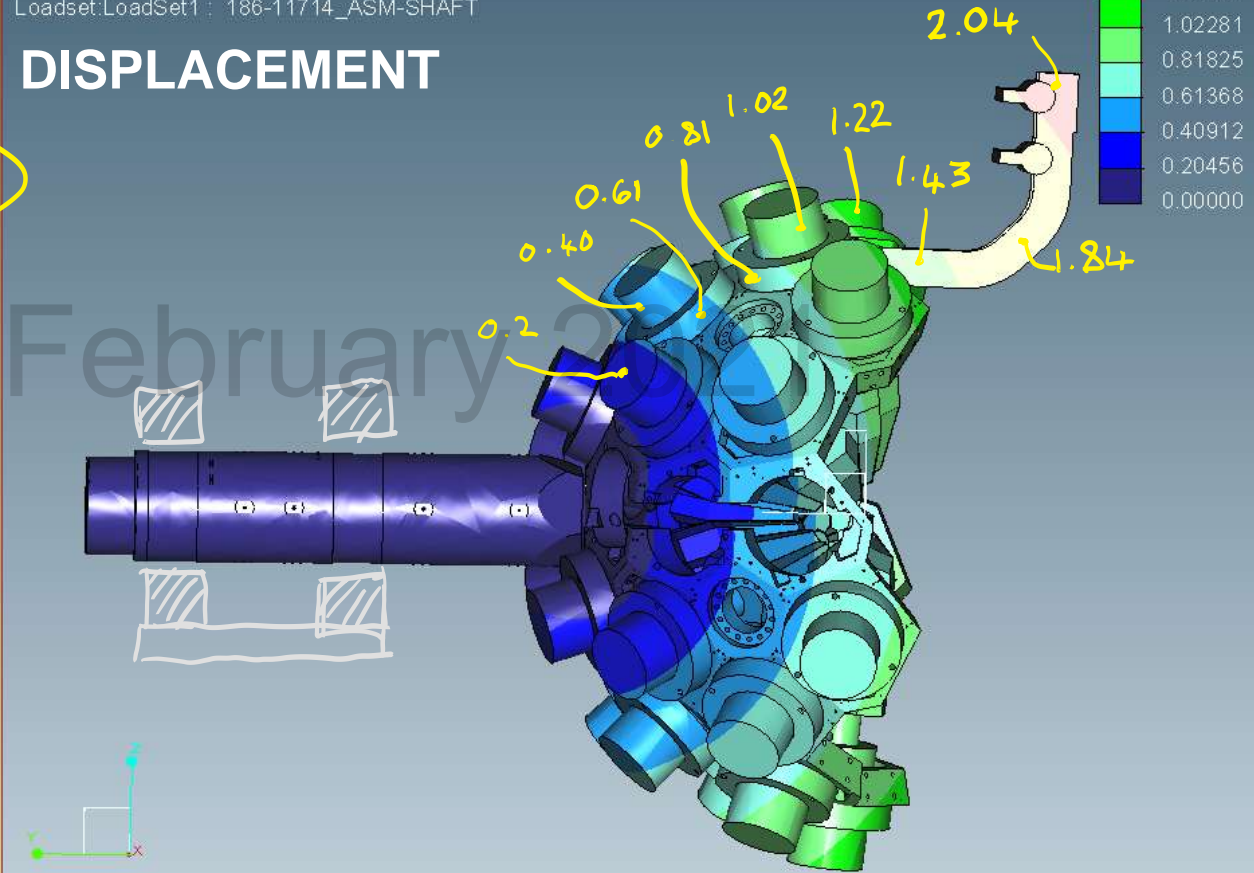


Displacement Mag (WCS)
(mm)
Deformed
Max Disp 2.0456E+00
Scale 3.0847E+01
Loadset:LoadSet1 : 186-11714_ASM-SHAFT

2.04mm MAX



DISPLACEMENT

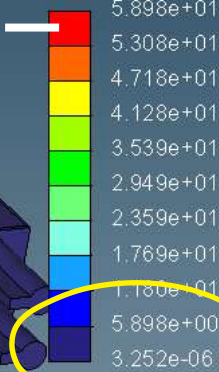


FEA

During installation/removal of the triple clusters, survey of the honeycomb should be performed at regular intervals to bring the 'target point' back into the desired position.

Stress von Mises (WCS)
(MPa)
Deformed
Scale 3.0847E+01
Loadset:LoadSet1 : 186-11714_ASM-SHAFT

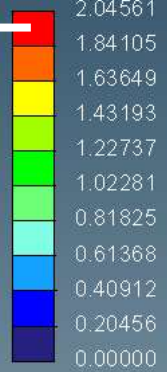
58.9 MPa MAX



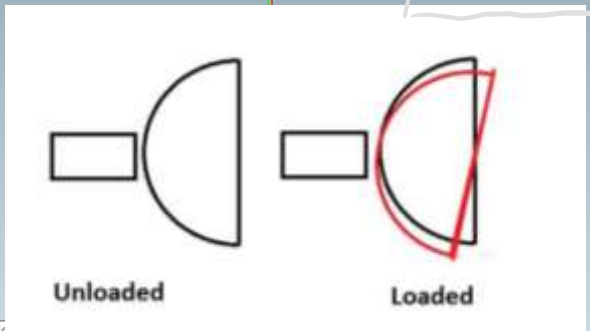
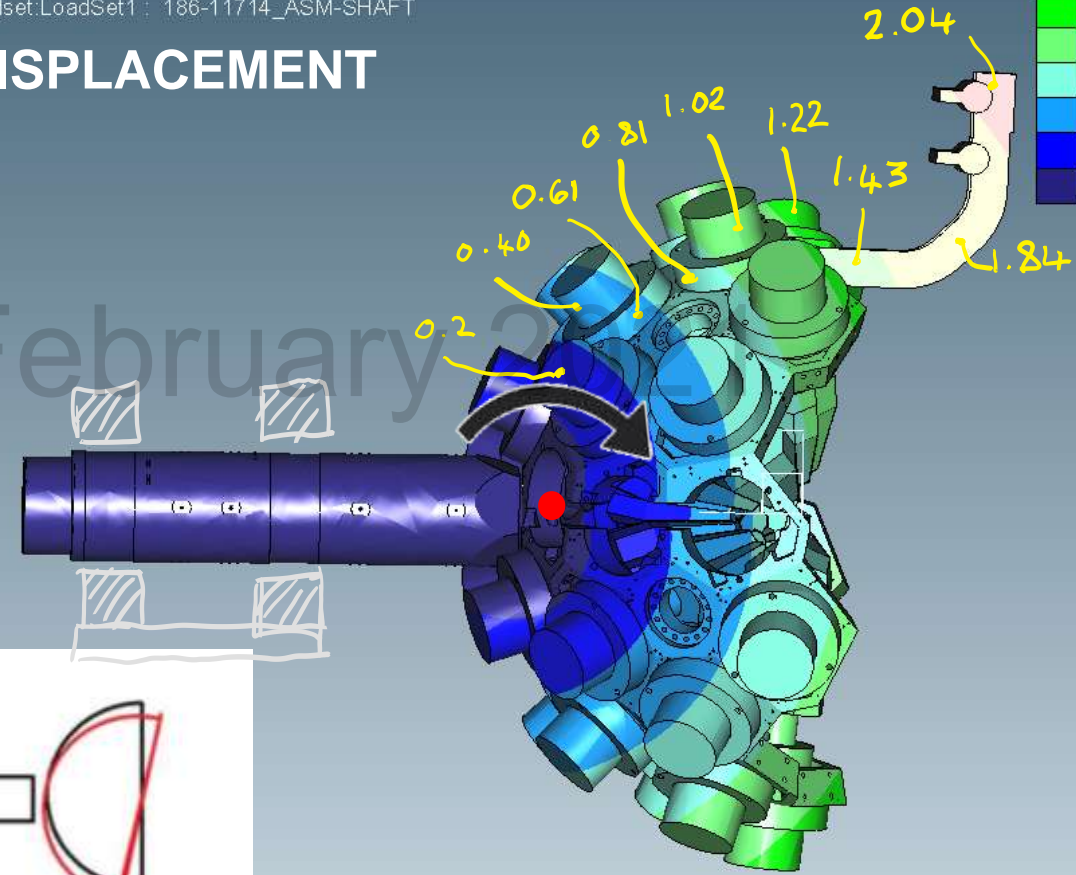
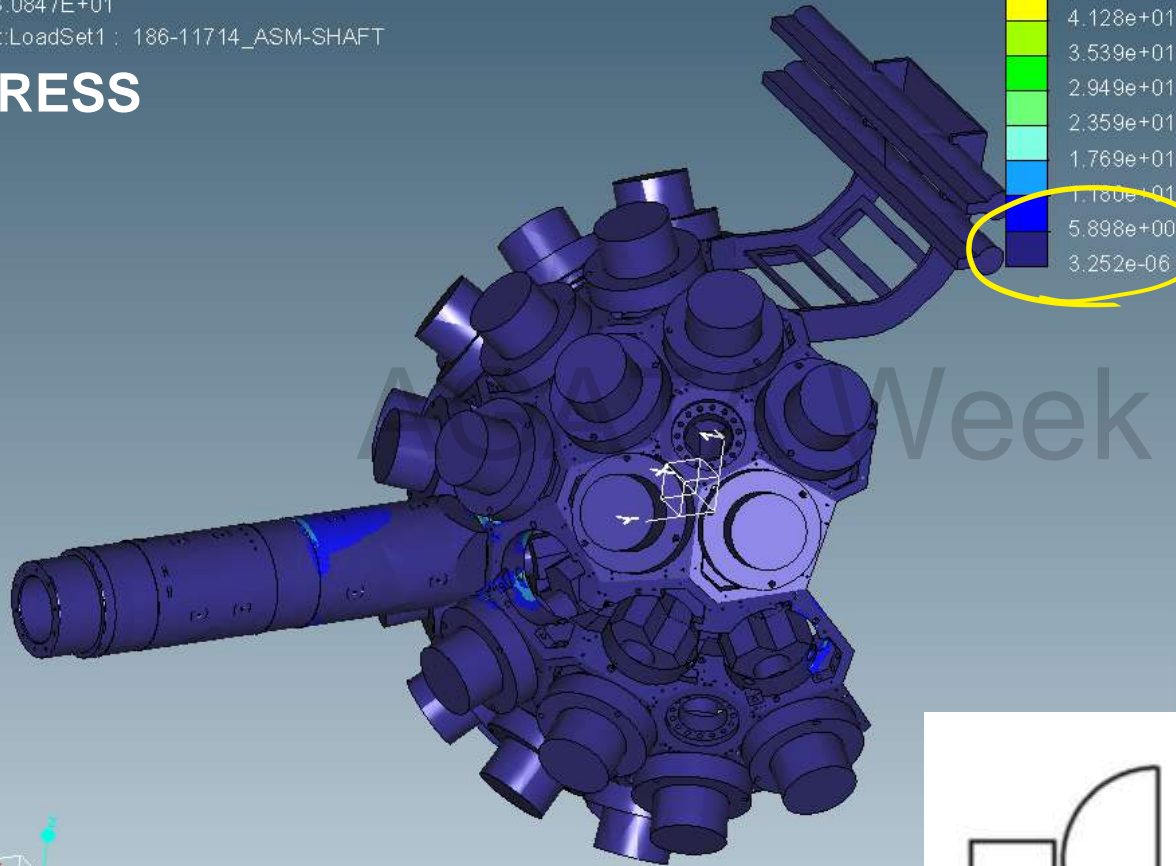
Displacement Mag (WCS)
(mm)
Deformed
Max Disp 2.0456E+00
Scale 3.0847E+01
Loadset:LoadSet1 : 186-11714_ASM-SHAFT

DISPLACEMENT

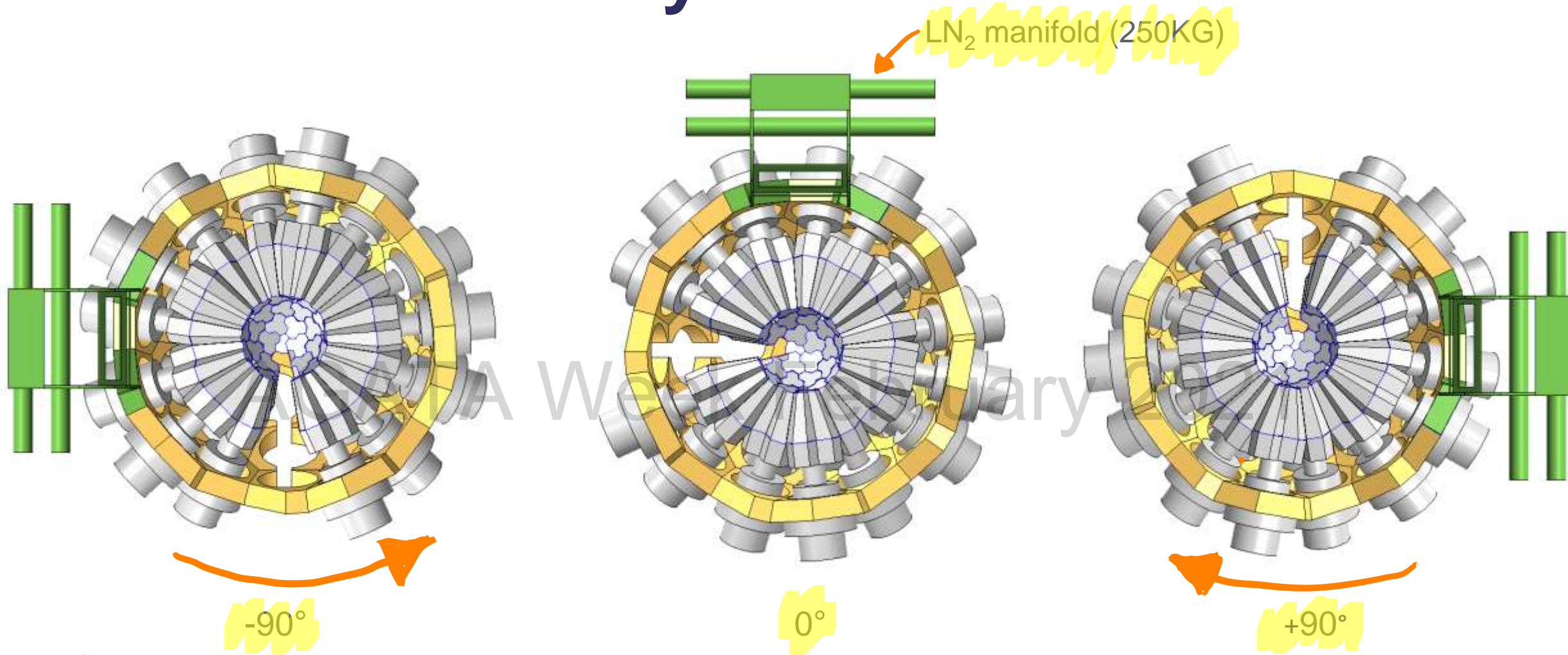
2.04mm MAX



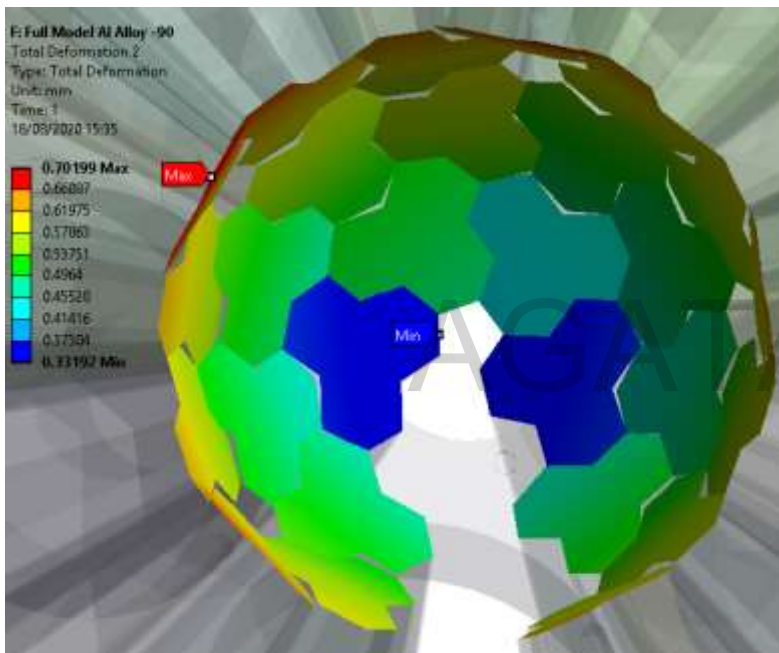
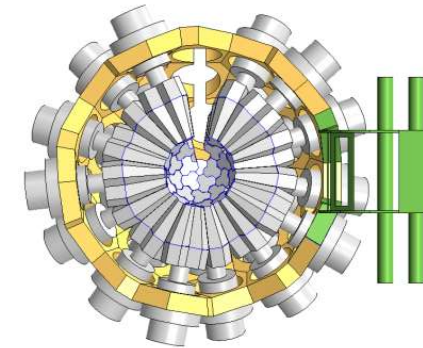
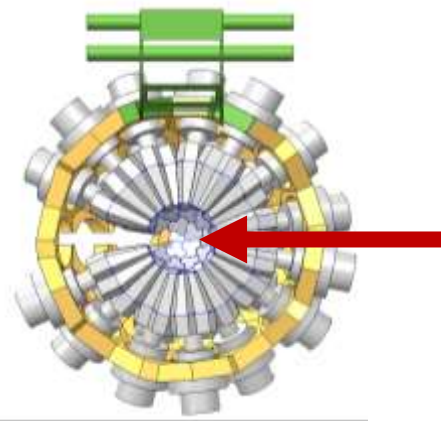
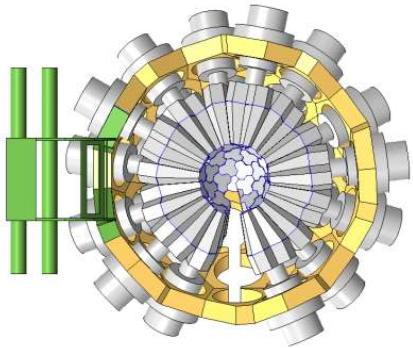
STRESS



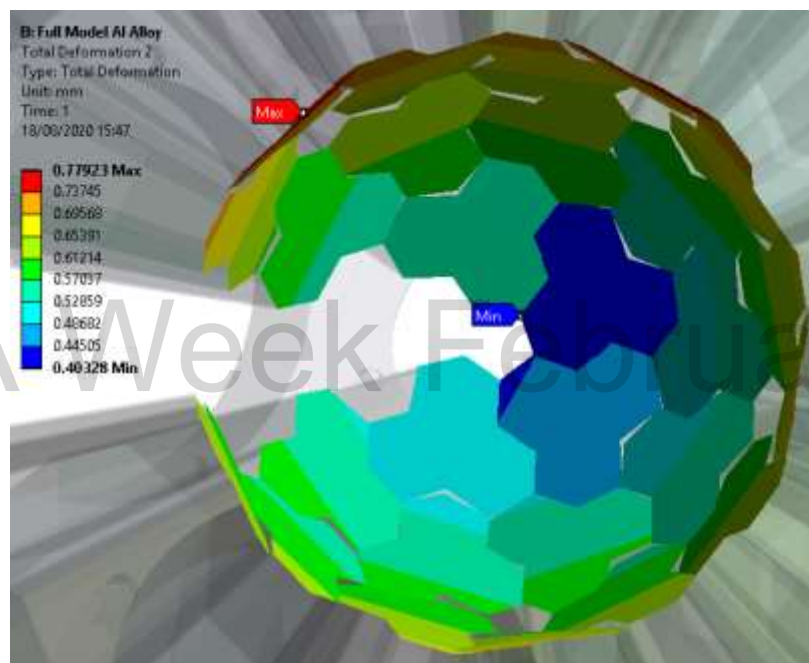
Finite Element Analysis



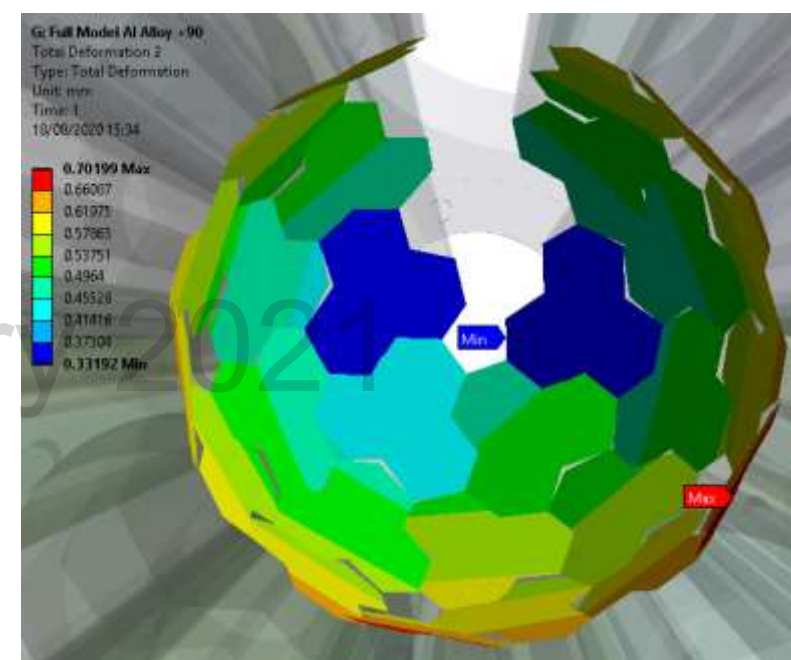
The worst case triple cluster deflection is found in the 0° position with the liquid nitrogen manifold above the array



-90°

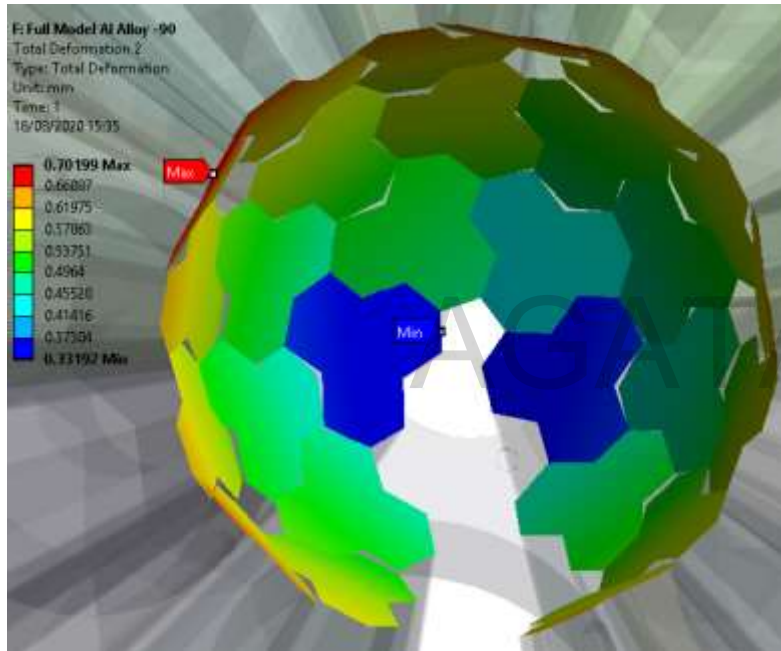
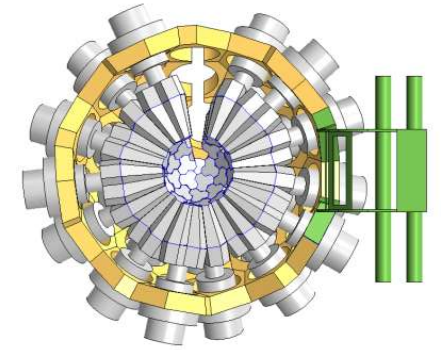
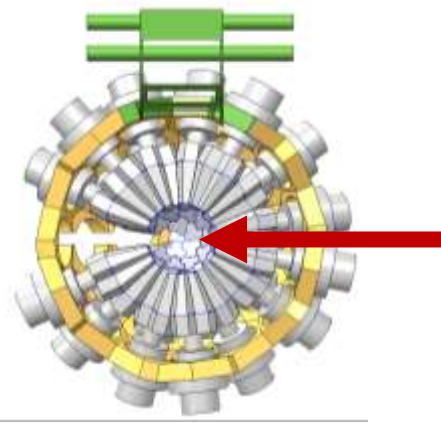
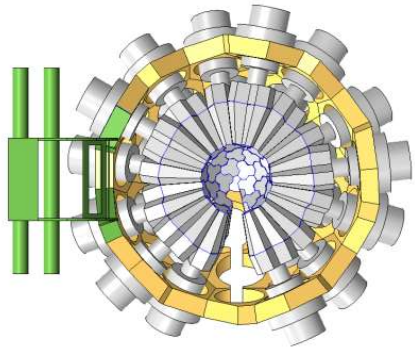


0°

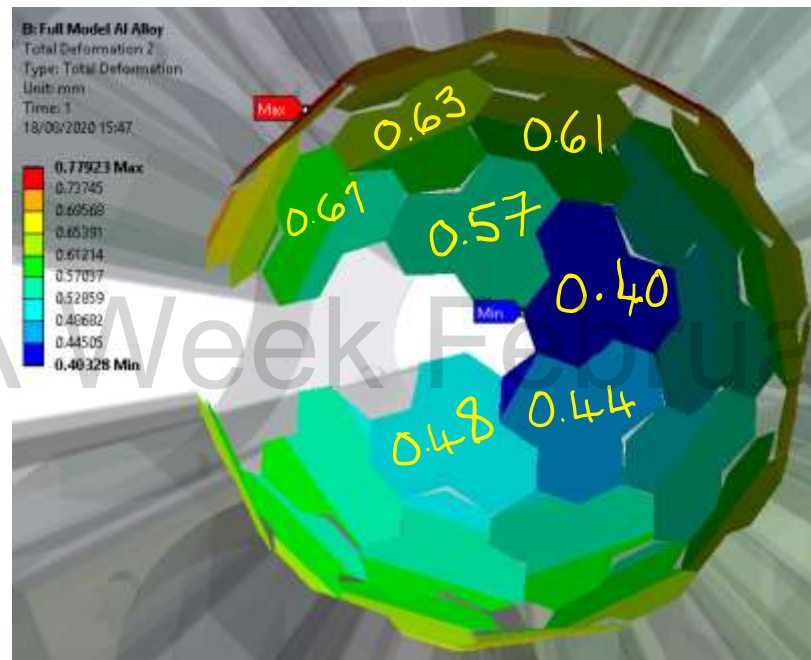


+90°

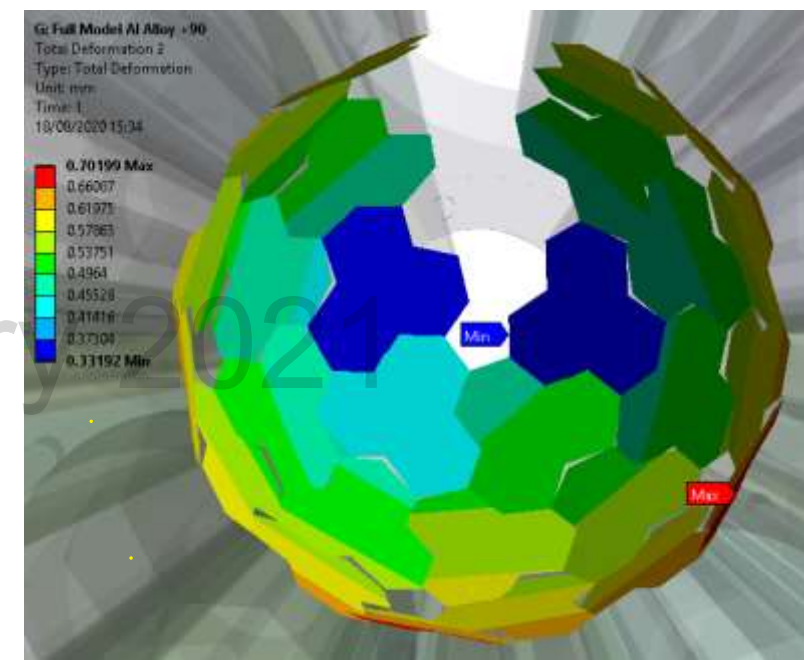
The triple cluster's deflections range from 0.33 - 0.78 mm, in the same direction
Nominal clearance between clusters ~1.0mm - 0.5mm



-90°



0°



+90°

The triple cluster's deflections range from 0.33 - 0.78 mm, in the same direction
The relative movement of neighbouring triple clusters is less than 0.2 mm

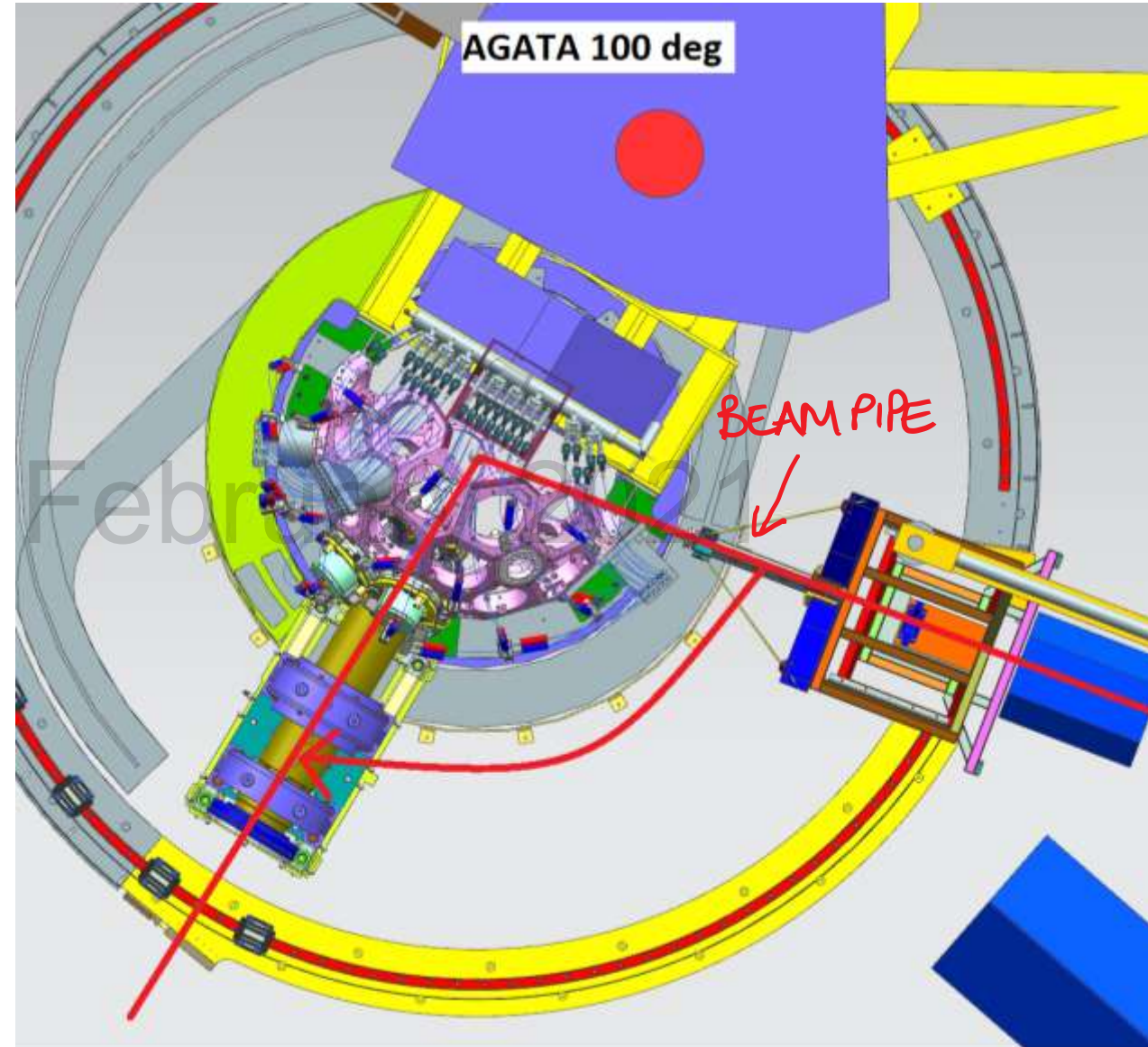
FEA – Main takeaways

- Shaft deflection insignificant
- Main deflection due to the array pivoting at the interface between shaft and array
- Max triple cluster deflection 0.78mm
- **Relative movement of neighbouring triple clusters is less than 0.2 mm for all load cases**
- Minimal compression of the array, but it does deform slightly
- Manufacturing & alignment errors the biggest issue when it comes to potential clashes

It is recommended that when installing all the triple clusters for the first time, do not drive them in to their final position until all the clusters have been fitted and no further rotation of the array is required.

FEA - Flange #26 cut-out at LNL

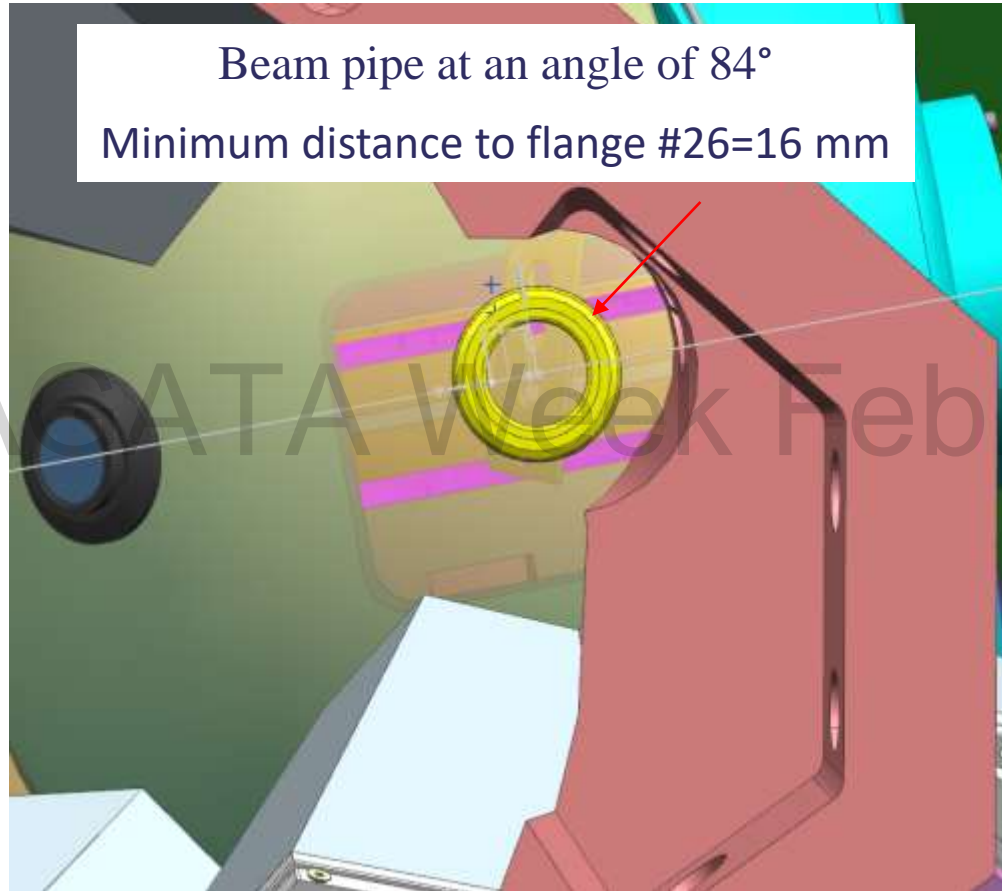
- Flange aperture restriction on beam pipe
- Limits beam range between 80° - 99°
- Proposal to add cut-out to outer flange



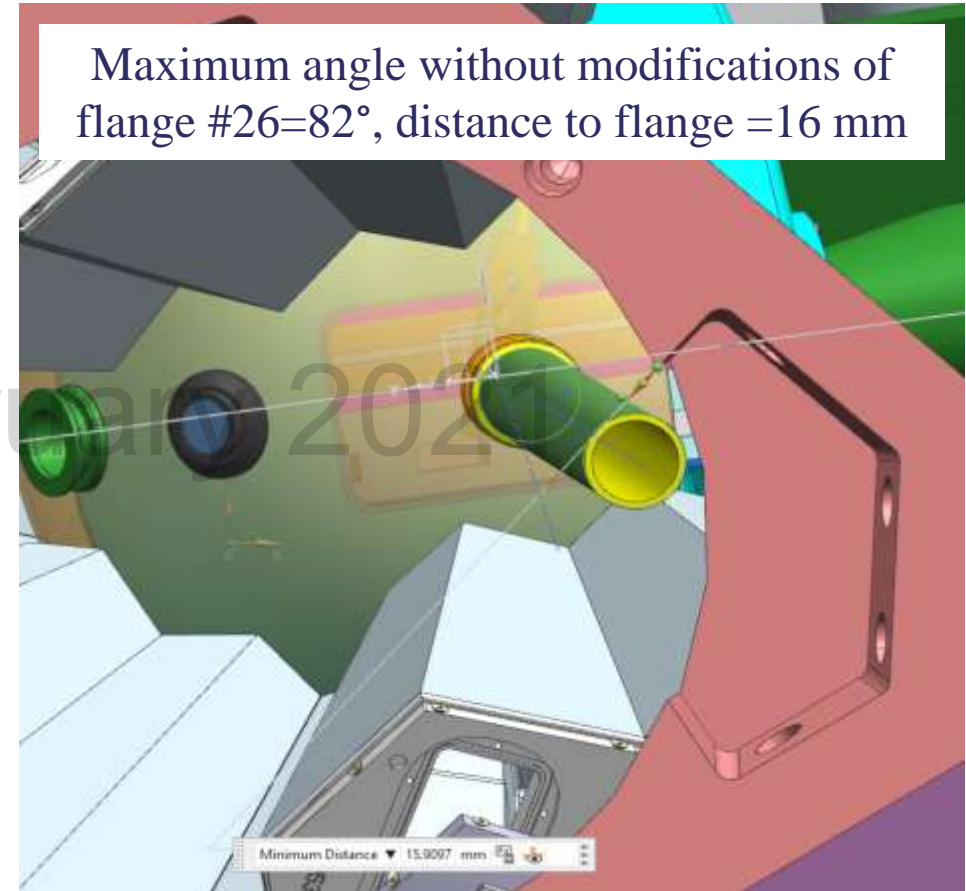
Flange #26 Cut-out

Details provided by Giovanna Benzoni and flange model from Fabio Tomasi

Beam pipe at an angle of 84°
Minimum distance to flange #26 = 16 mm

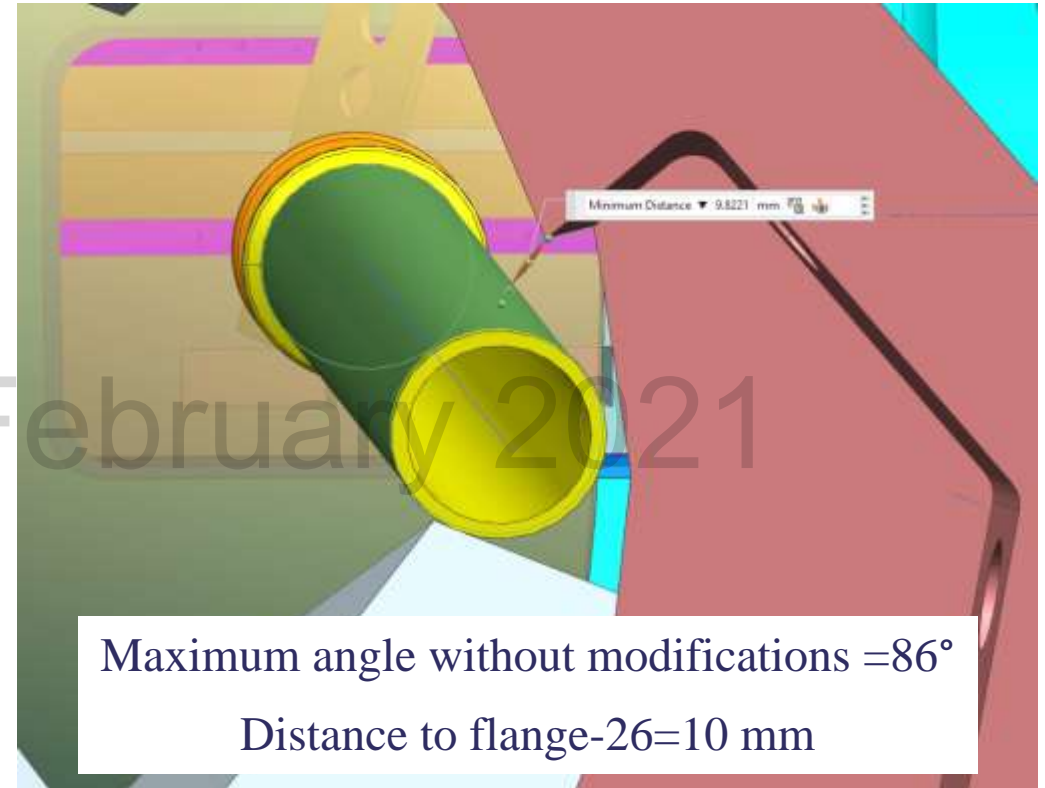
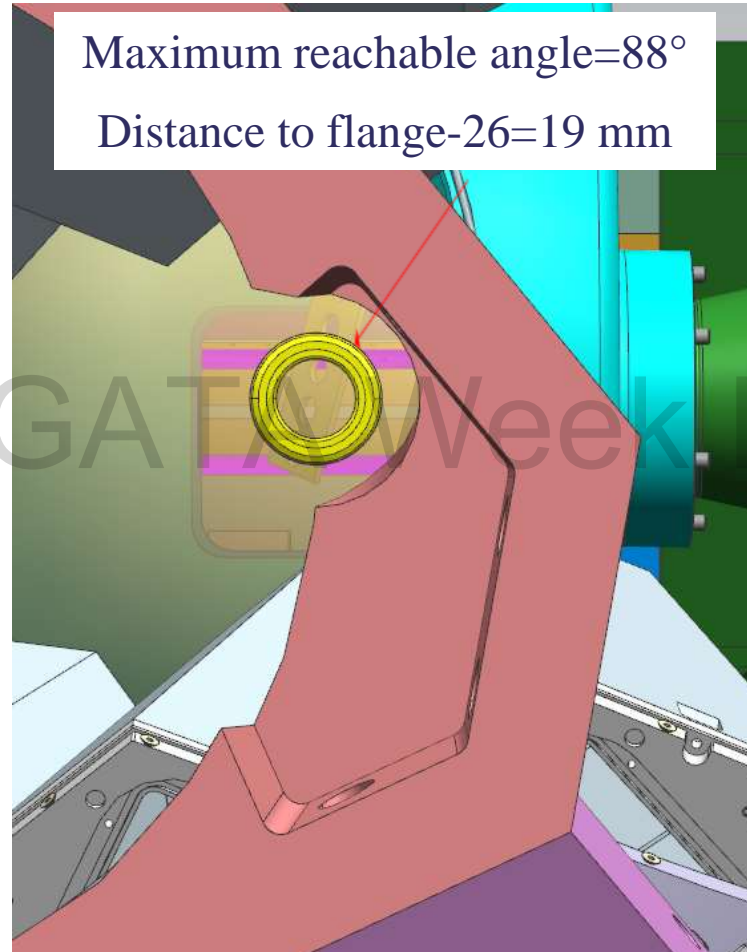


Maximum angle without modifications of
flange #26 = 82° , distance to flange = 16 mm



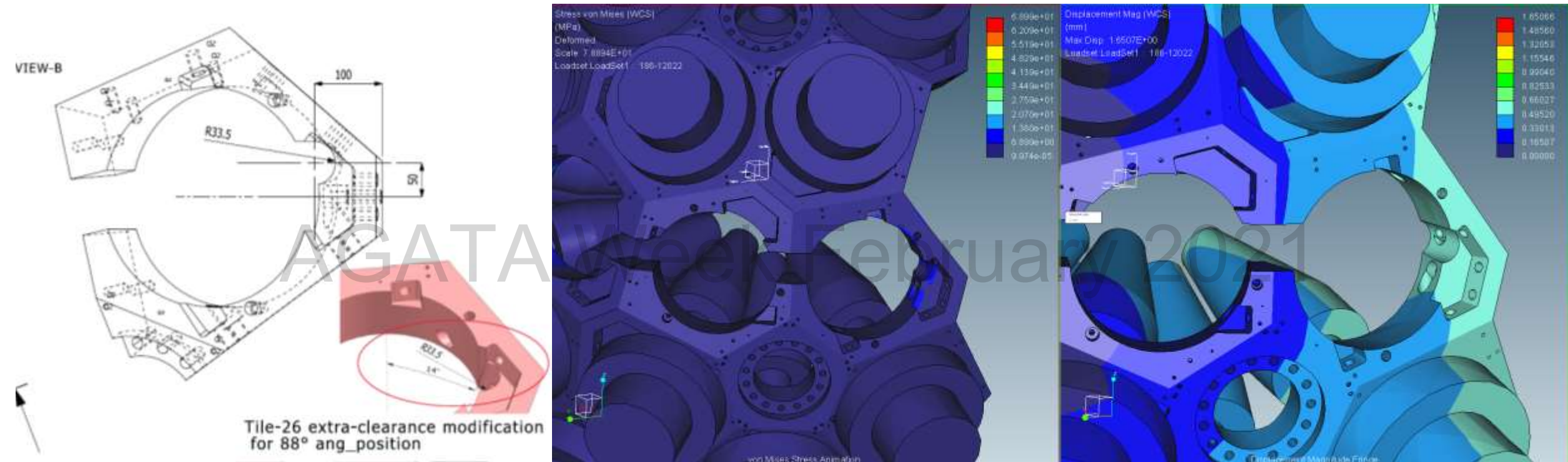
Flange #26 Cut-out

Details provided by Giovanna Benzoni and flange model from Fabio Tomasi



FEA - Flange #26 conclusion

Extra cut-out to flange #26 has minor effect on stress and negligible impact on deflection

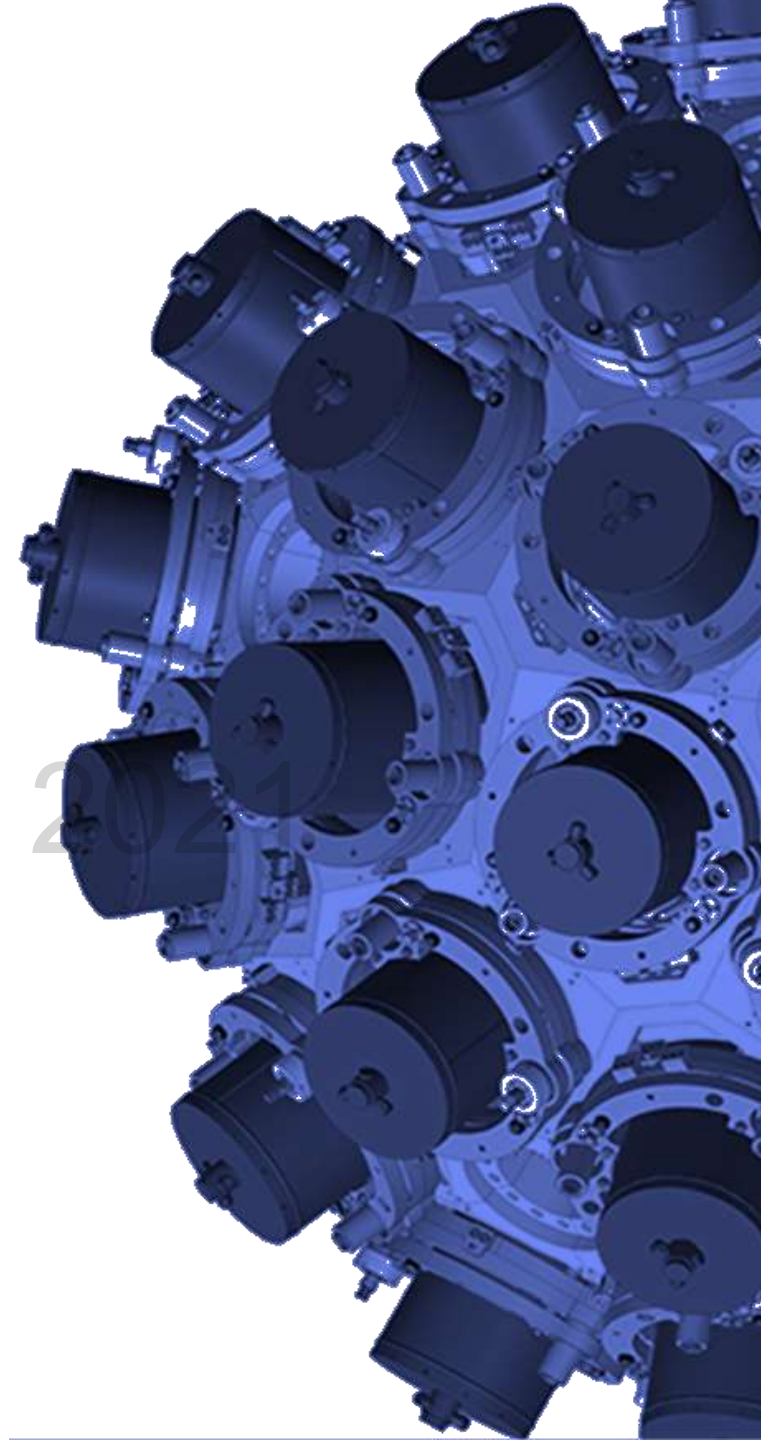


Support Structure Manufacture & Assembly Progress

AGATA Week February 2024



Science and
Technology
Facilities Council





November 2020



November 2020

February 2021



ACATA Week February 2021

November 2020



December 2020

SO-1159
M16 x 45 SHCS
M16 x 35 SHCS

SO-1159
M38 x 180 SHCS
to fit bottom plate
on Housings

SO-1159
Adjuster Screw

SO-1159
M36 x 125 Hex
Housing

SO-1159
Fill
Washer

Thick Washer
SO-1159
Fisher Block
M12 x 35 Hex-Head
M12 Washer
SO-1159

443879
Part
444013

443879
Part
444013



December 2020



AGATA Week February 2021

December 2020



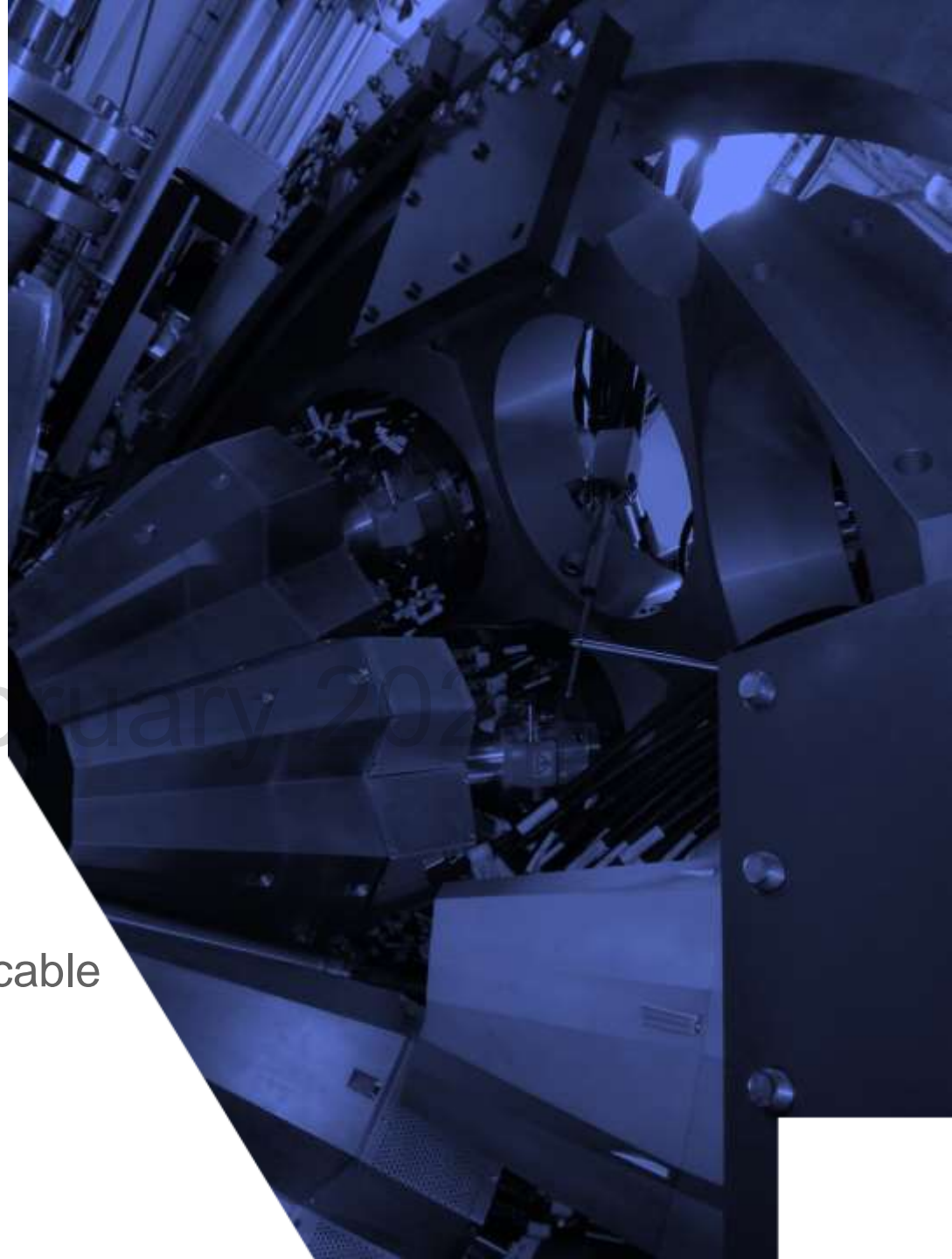
AGATA
AGATA
AGATA

AGATA January 2021

January 2021

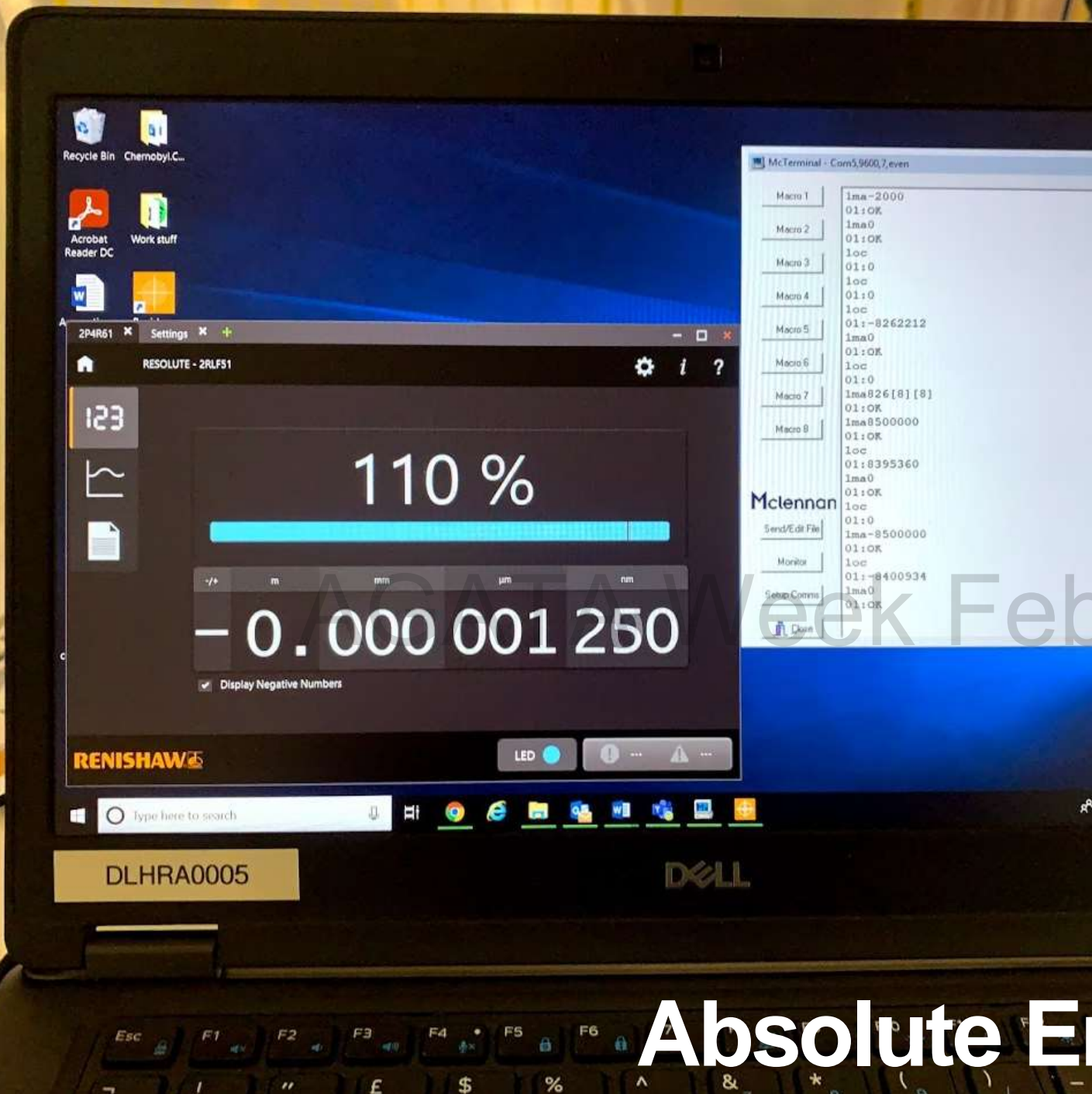
Motion control system

- Absolute optical encoder (rotation control)
- Software limits
- Mechanical limit switches
- Mechanical stop
- 2 motion stop buttons on the support
- 1 extra motion stop to be mounted at Legnaro
- Remote jog box control +/- (with fast jog) on a 5m cable





Absolute Encoder

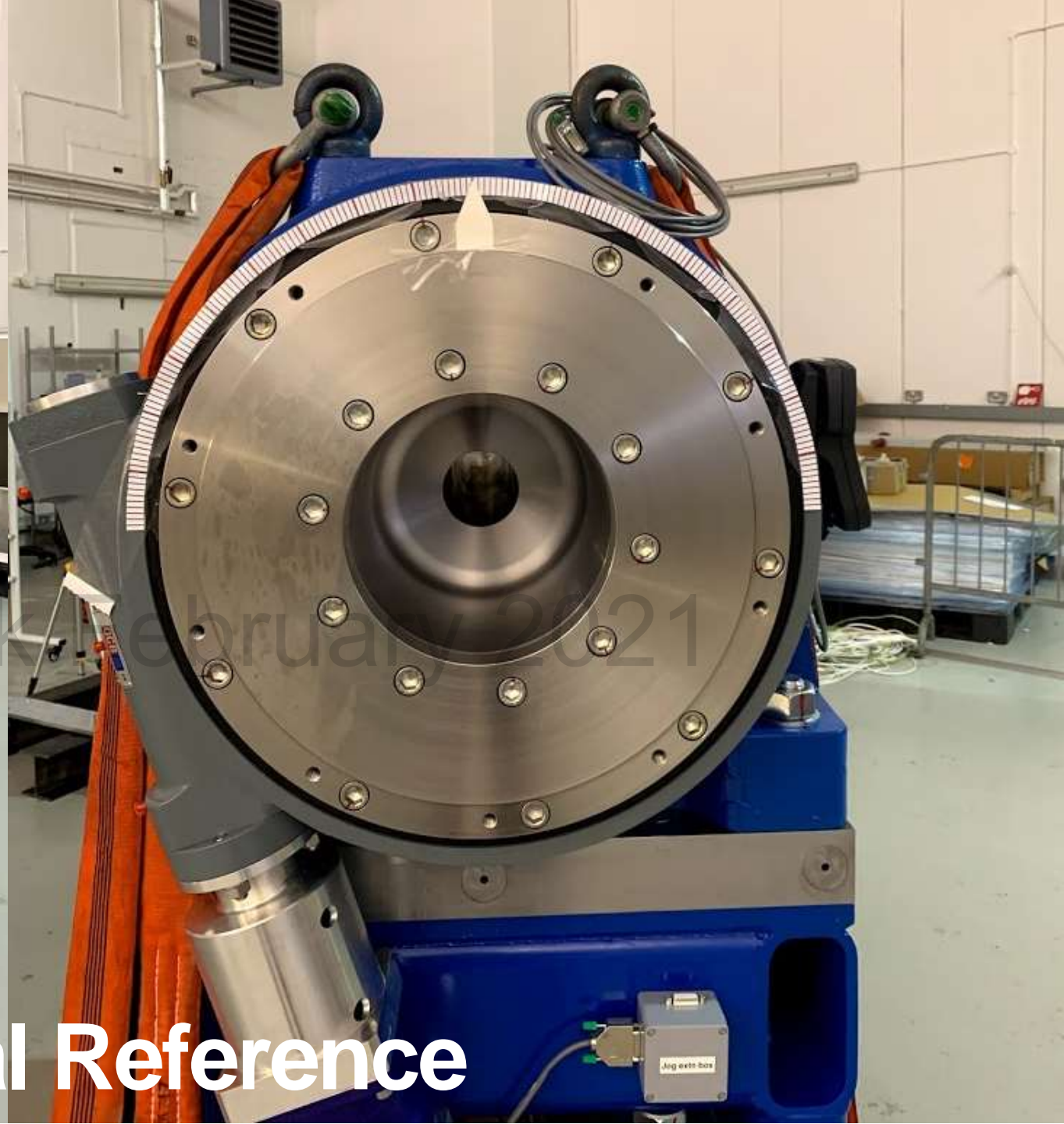


Absolute Encoder

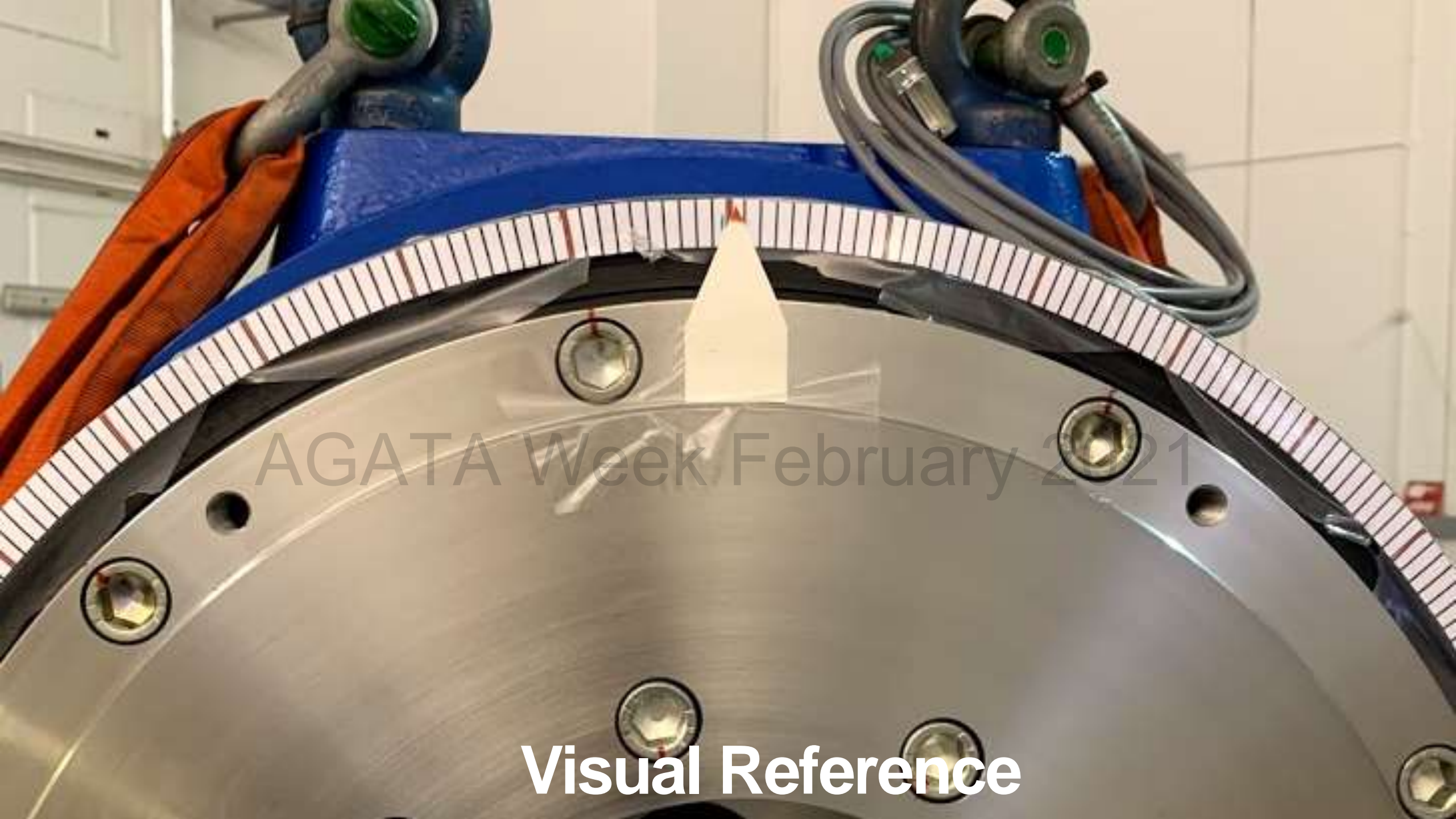


Absolute Encoder





Visual Reference

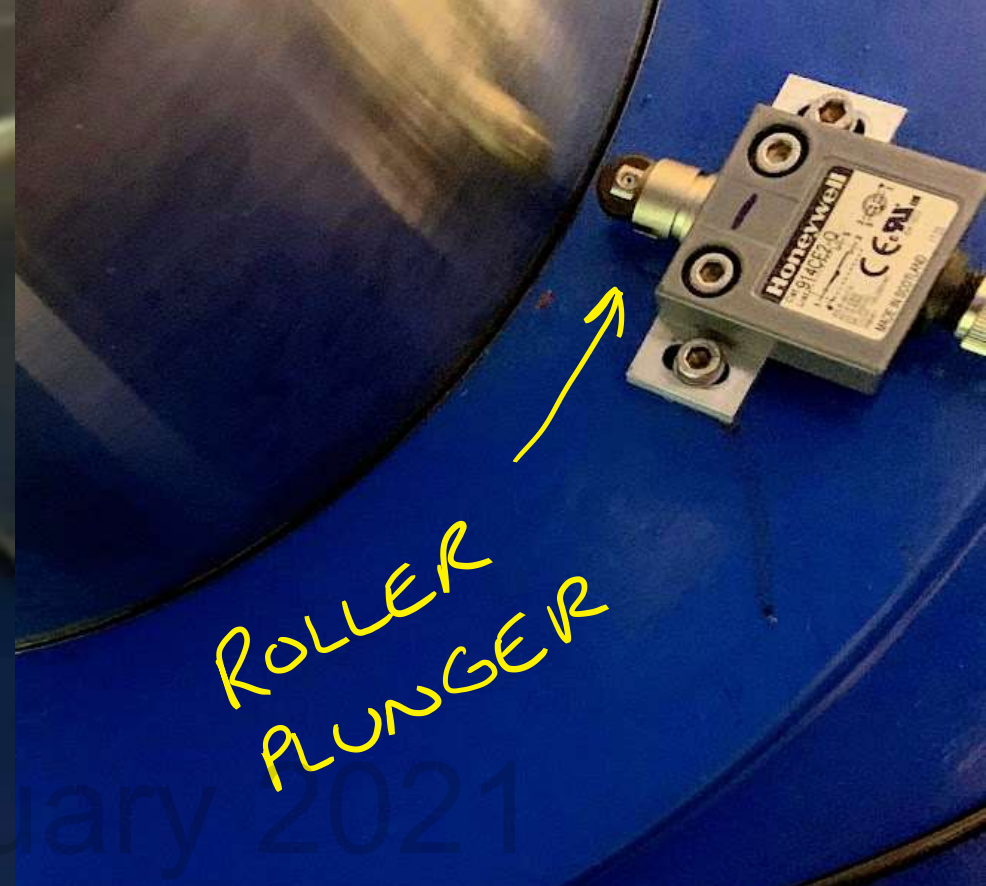


AGATA Week February 2021

Visual Reference



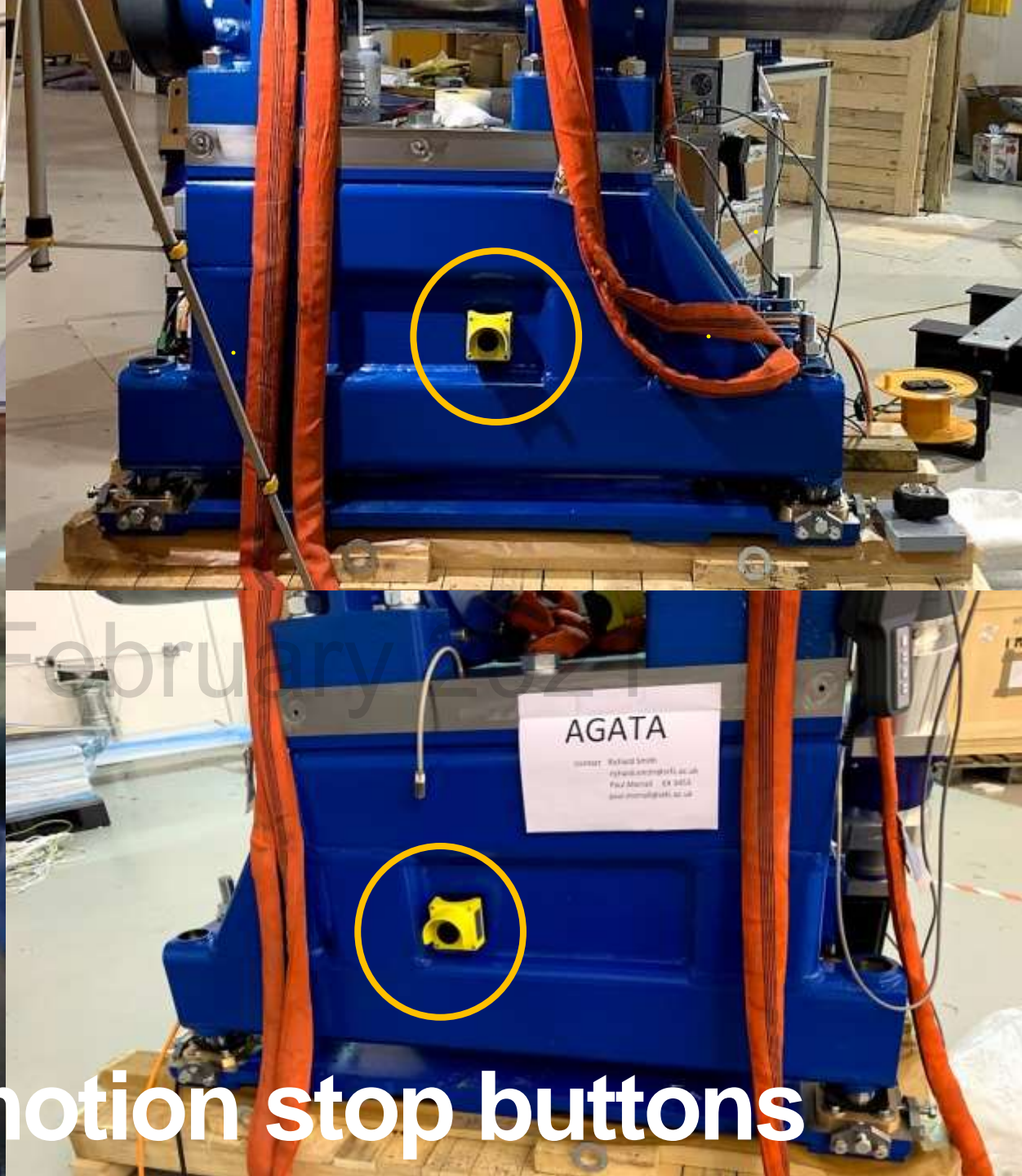
Mechanical limit switches



AC Week February 2021

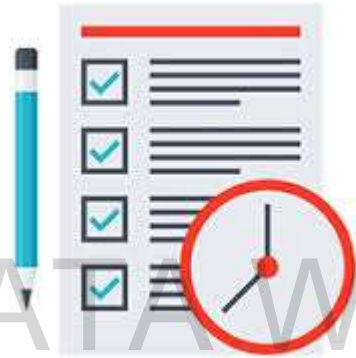


Mechanical limit switches



Remote jog box & motion stop buttons

What is next for the support?

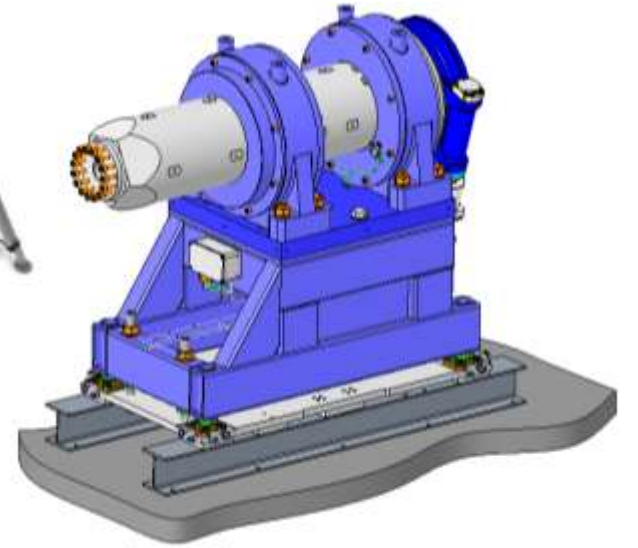


AGATA Week February 2024



Mechanical tests

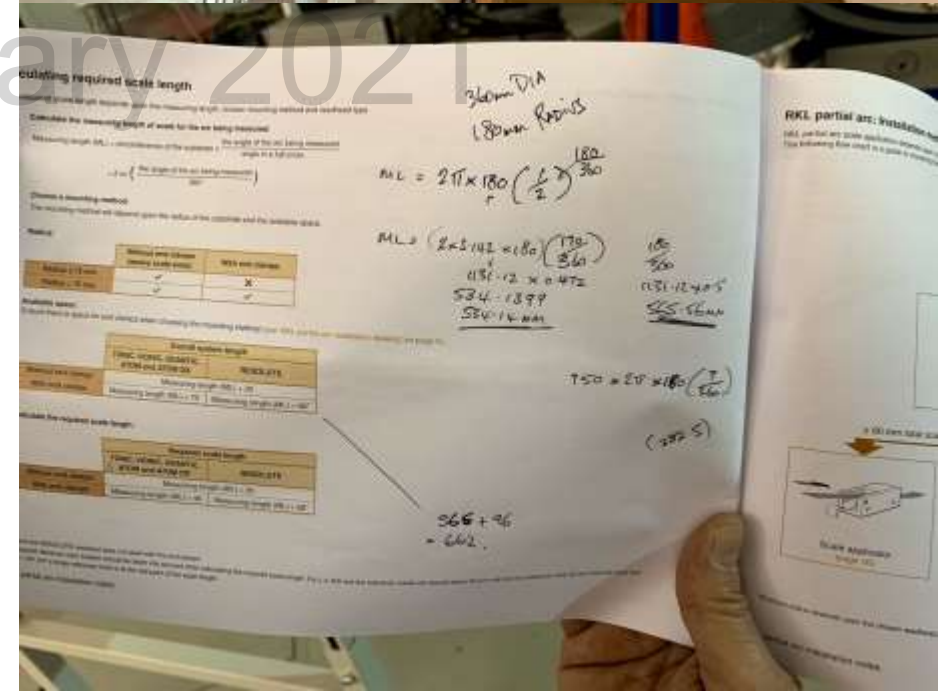
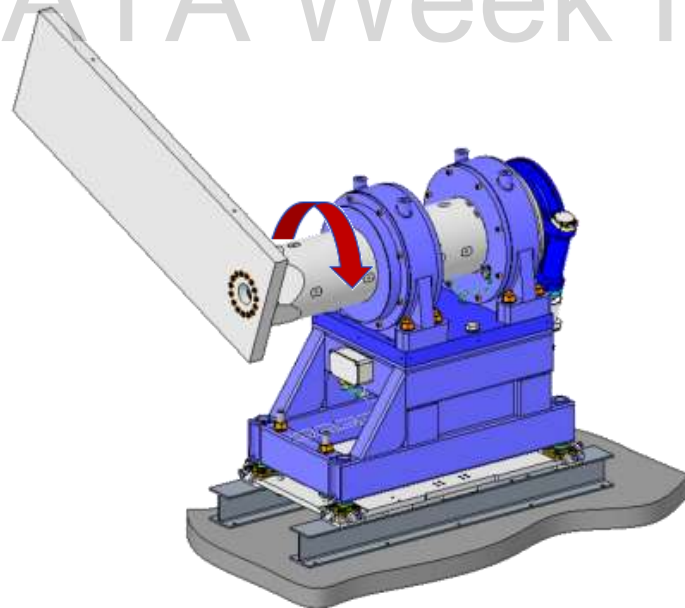
- Anchor support to floor
- Survey and align (obtain baseline figures)
- Rotate 750kg test weight (offset load of 5 ATCs + manifold)
- Evaluate mechanical performance
- Further load tests with increased load



Control system tests

- Repeatability tests with weight
- Tune (detune) the system (encoder sensitivity window)
- Set suitable acceleration profile
- Support complete – On target for end of March

AGATA Week February 2021



Associated Mechanics

AGATA Week February 20

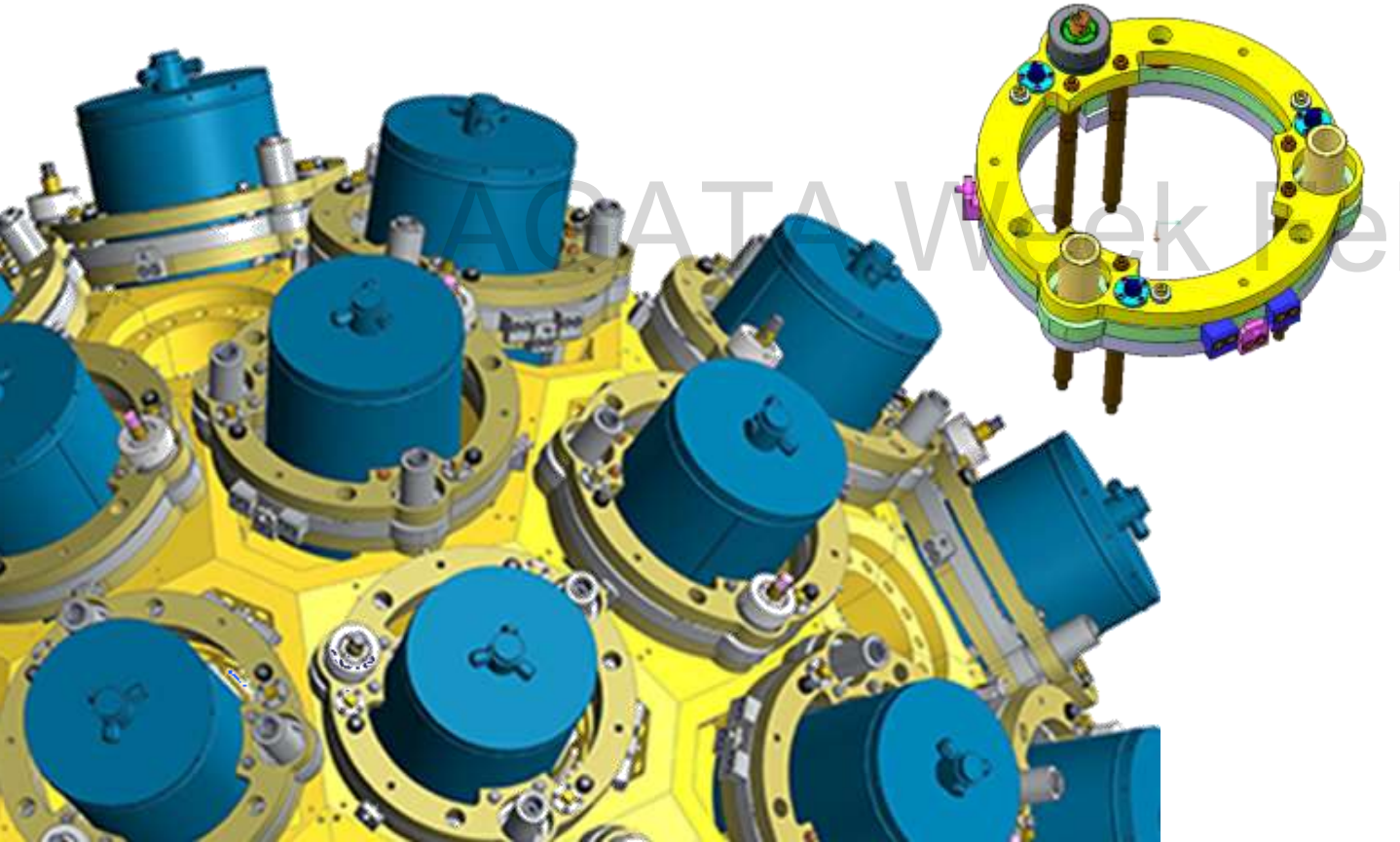


Science and
Technology
Facilities Council



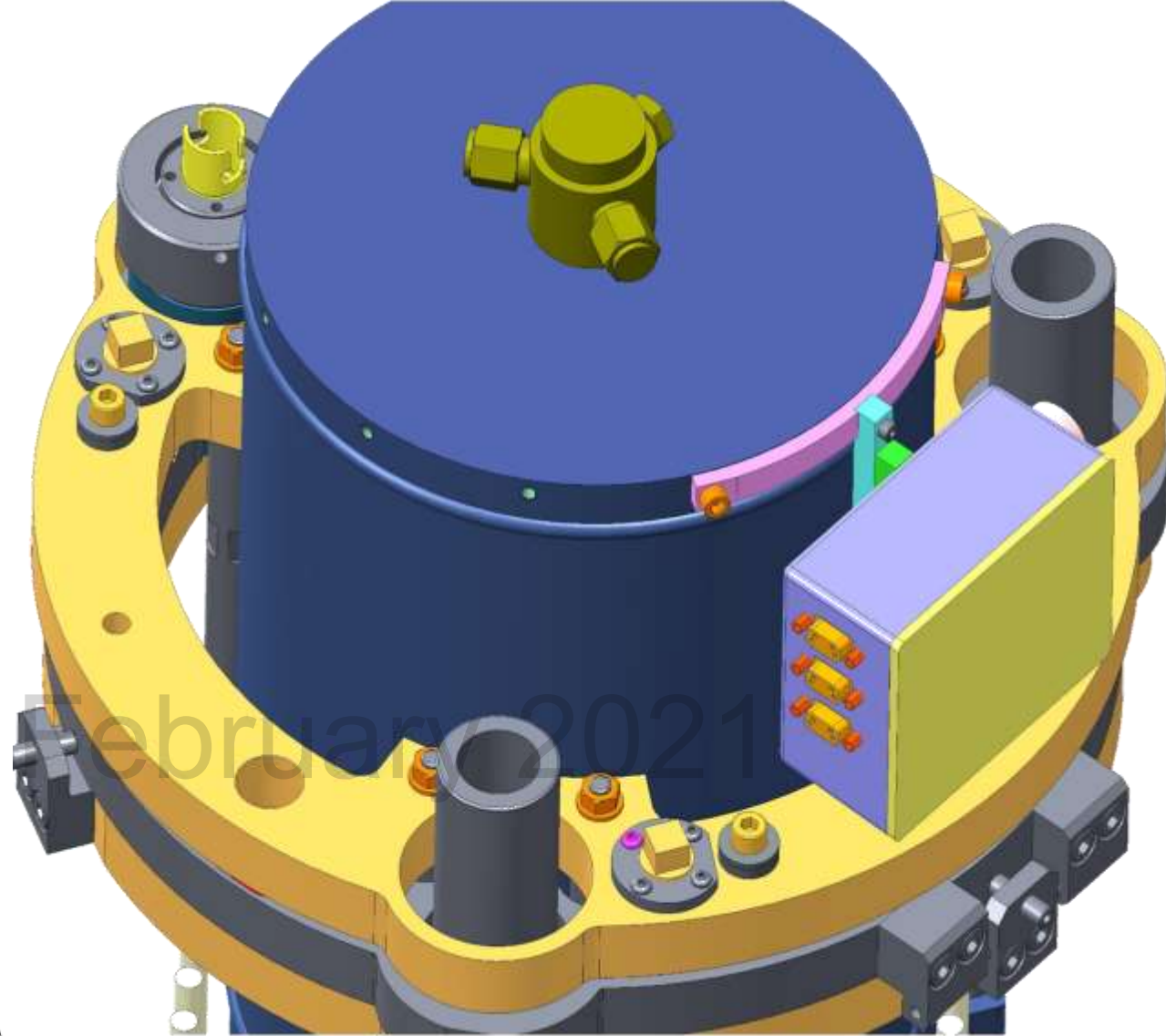
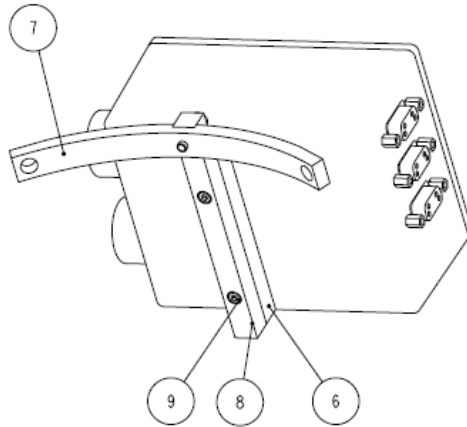
ATC mount rings

- 10 rings assembled at Daresbury
- Completed and ready to ship



Patch box

- Two piece construction
- Easier to access and remove
- Allows removal with ATC mounted
- Manufactured and ready to ship





GANIL

Leadscrew extension



GANIL

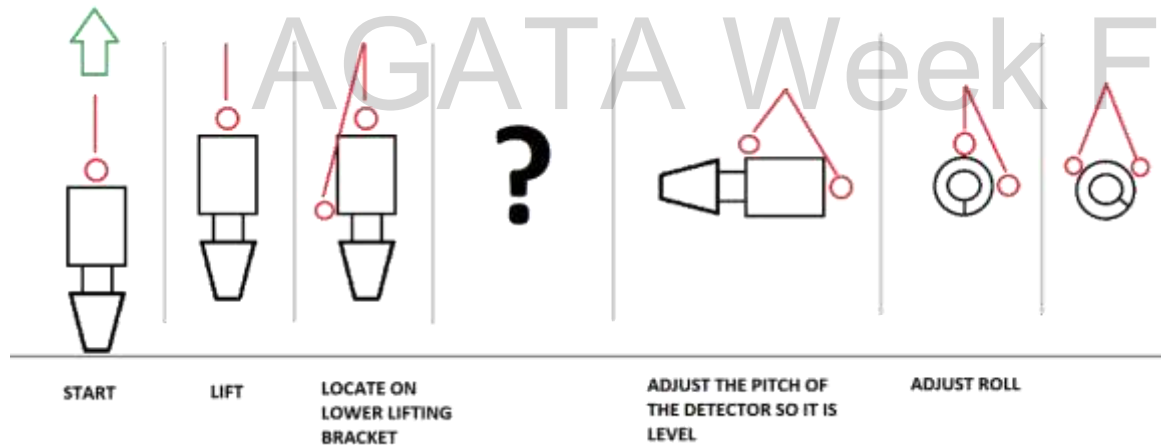
Leadscrew extension

ATC handling & installation

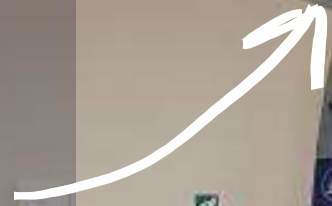


ATC handling

- Working with lifting specialists to determine the optimal way to lift and rotate the ATC safely
- Tests restart once new lifting hardware delivered
- Installation with the dummy ATC and fixture at various angles to be included in tests



**ATC
handling
fixture**

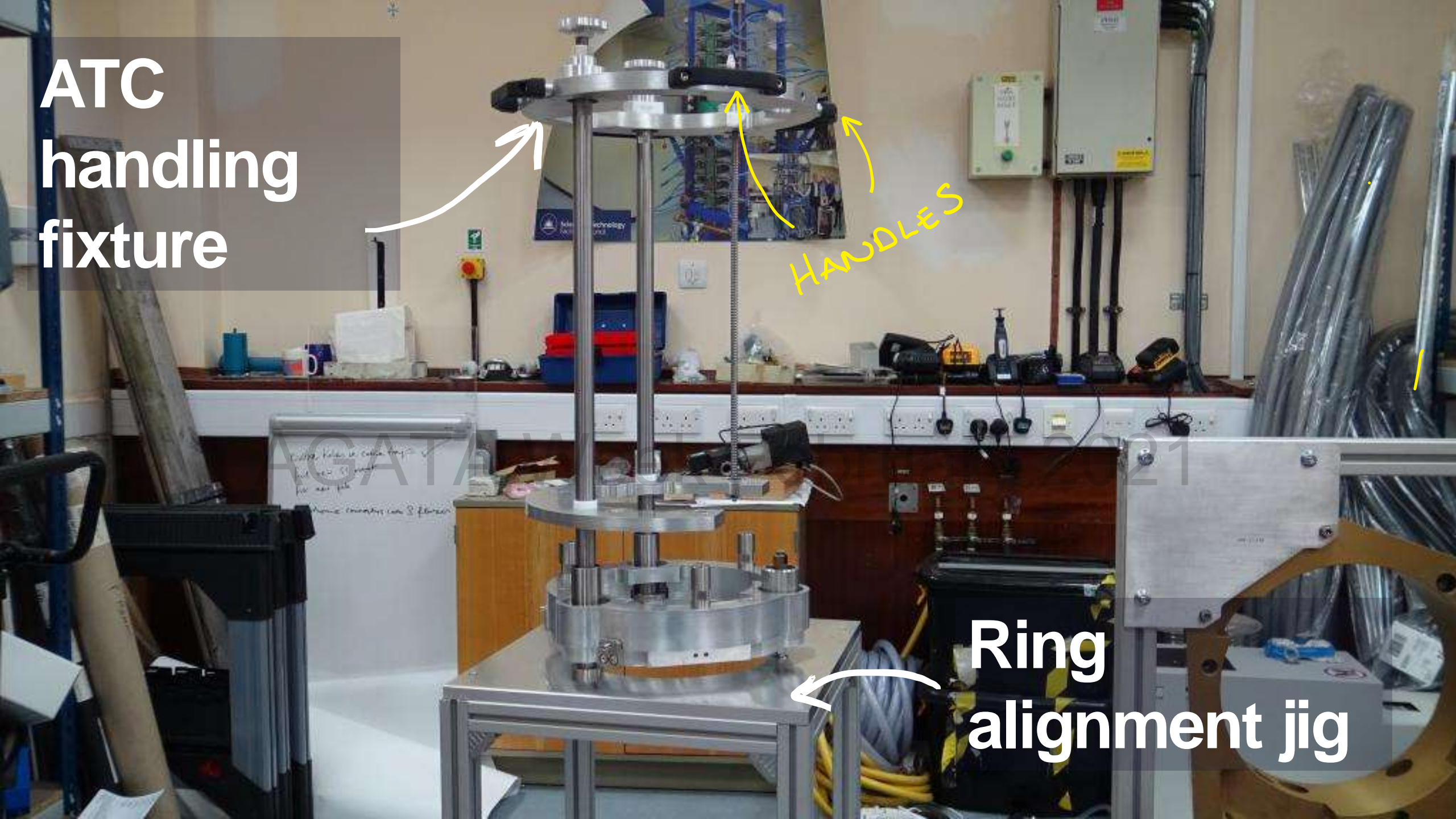


HANDLES

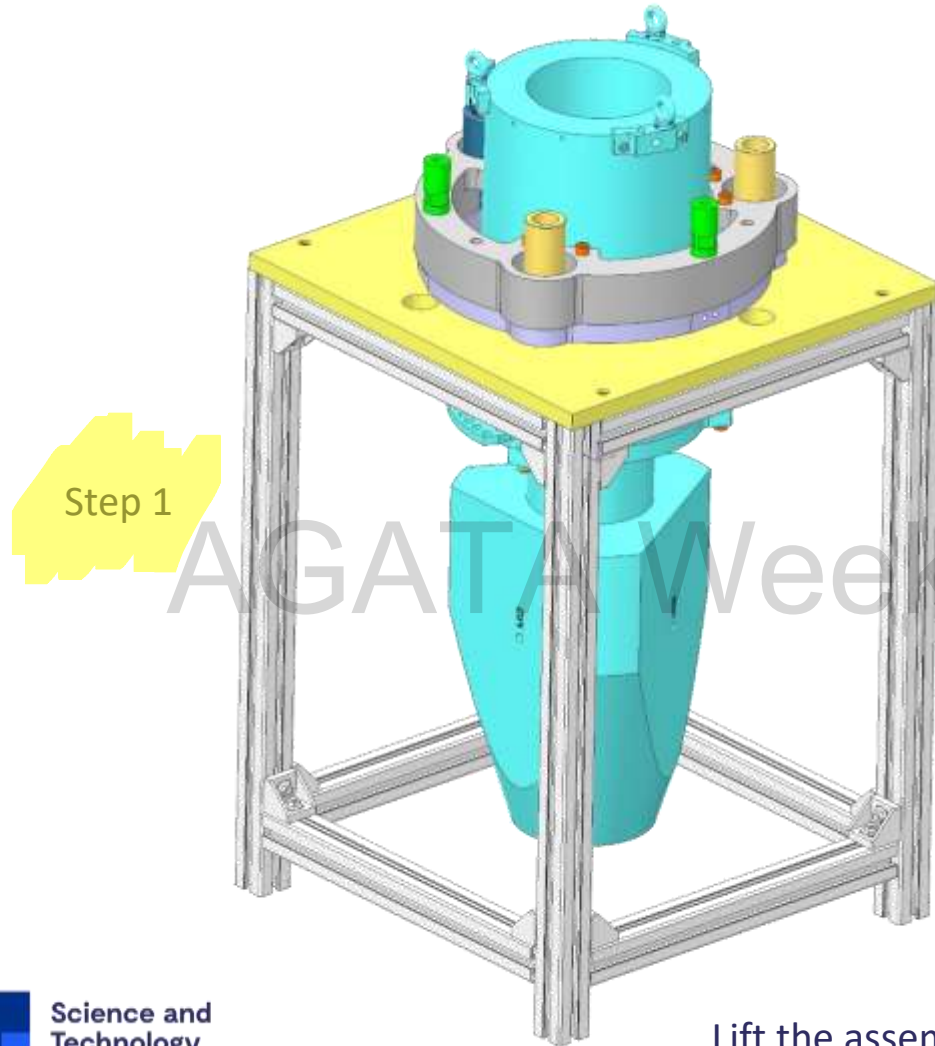


AGATA

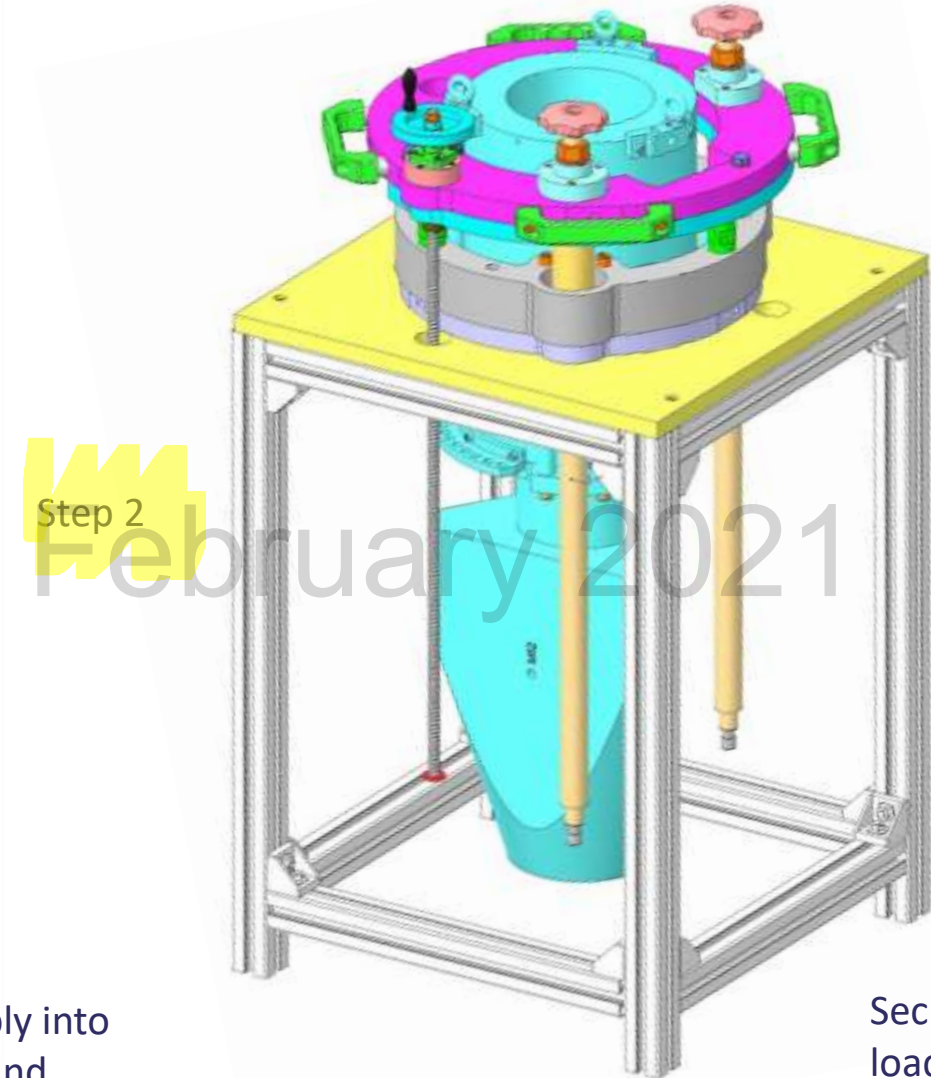
**Ring
alignment jig**



ATC handling fixture



Lift the assembly into the support stand

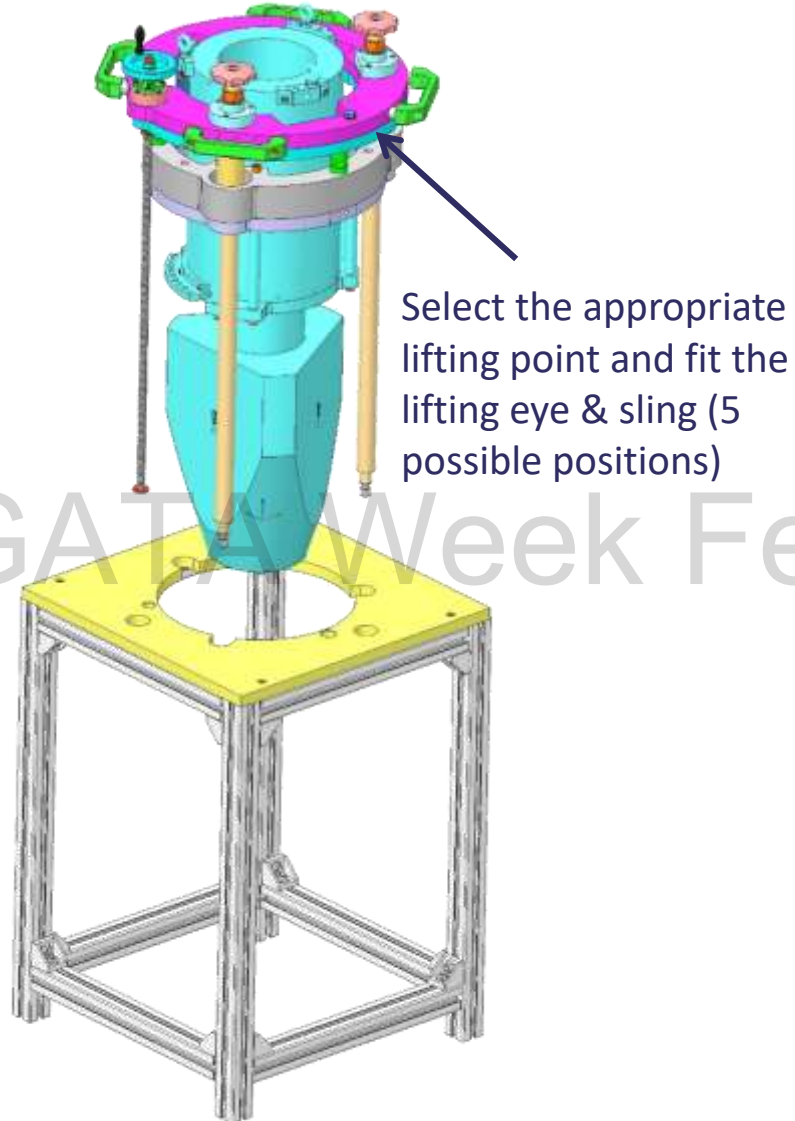


Securely attach the loading fixture to the dummy adjusting ring

ATC handling fixture

Step 3

Lift the assembly from the tripod stand using a crane/hoist



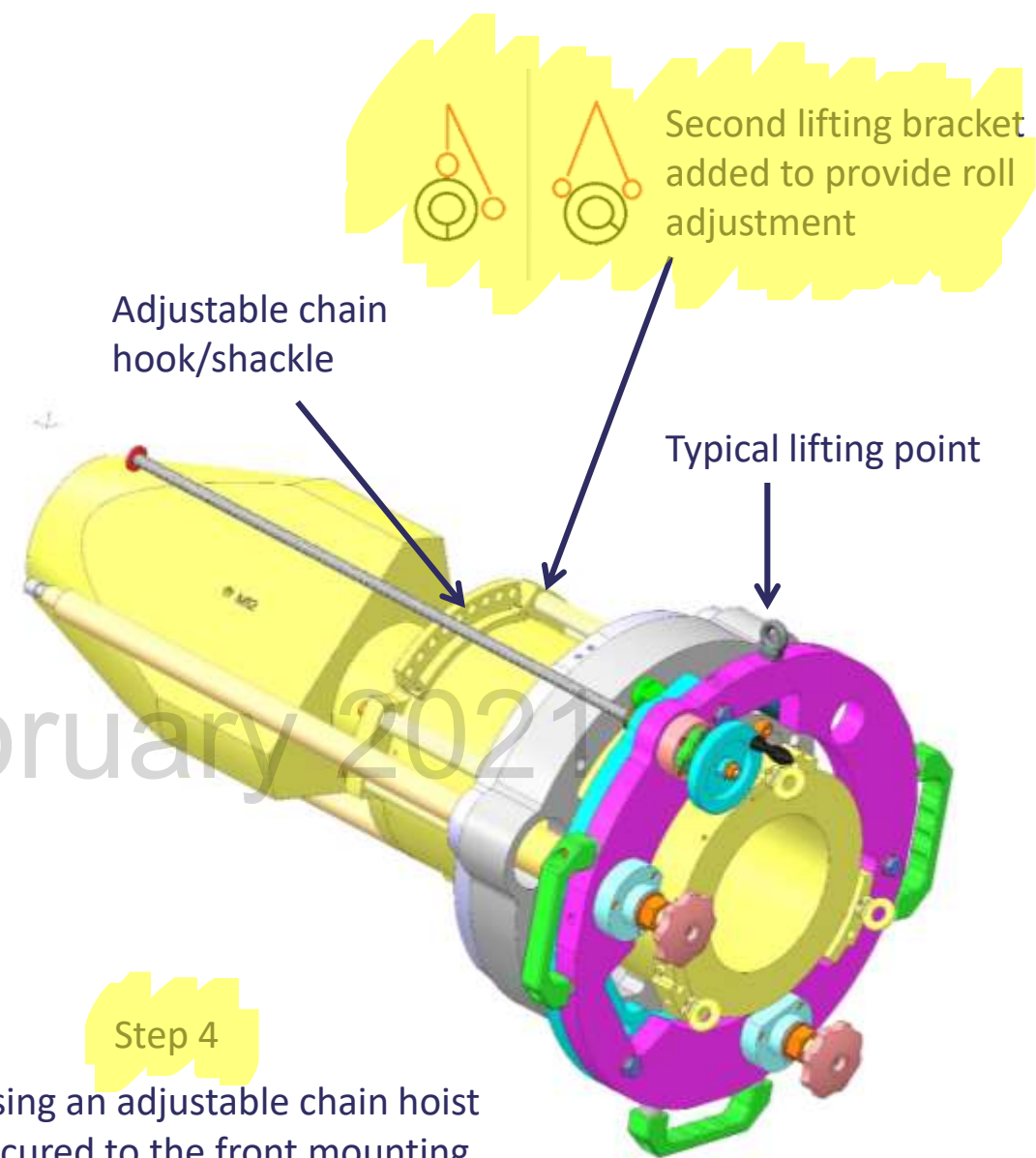
Adjustable chain hook/shackle

Typical lifting point

Second lifting bracket added to provide roll adjustment

Step 4

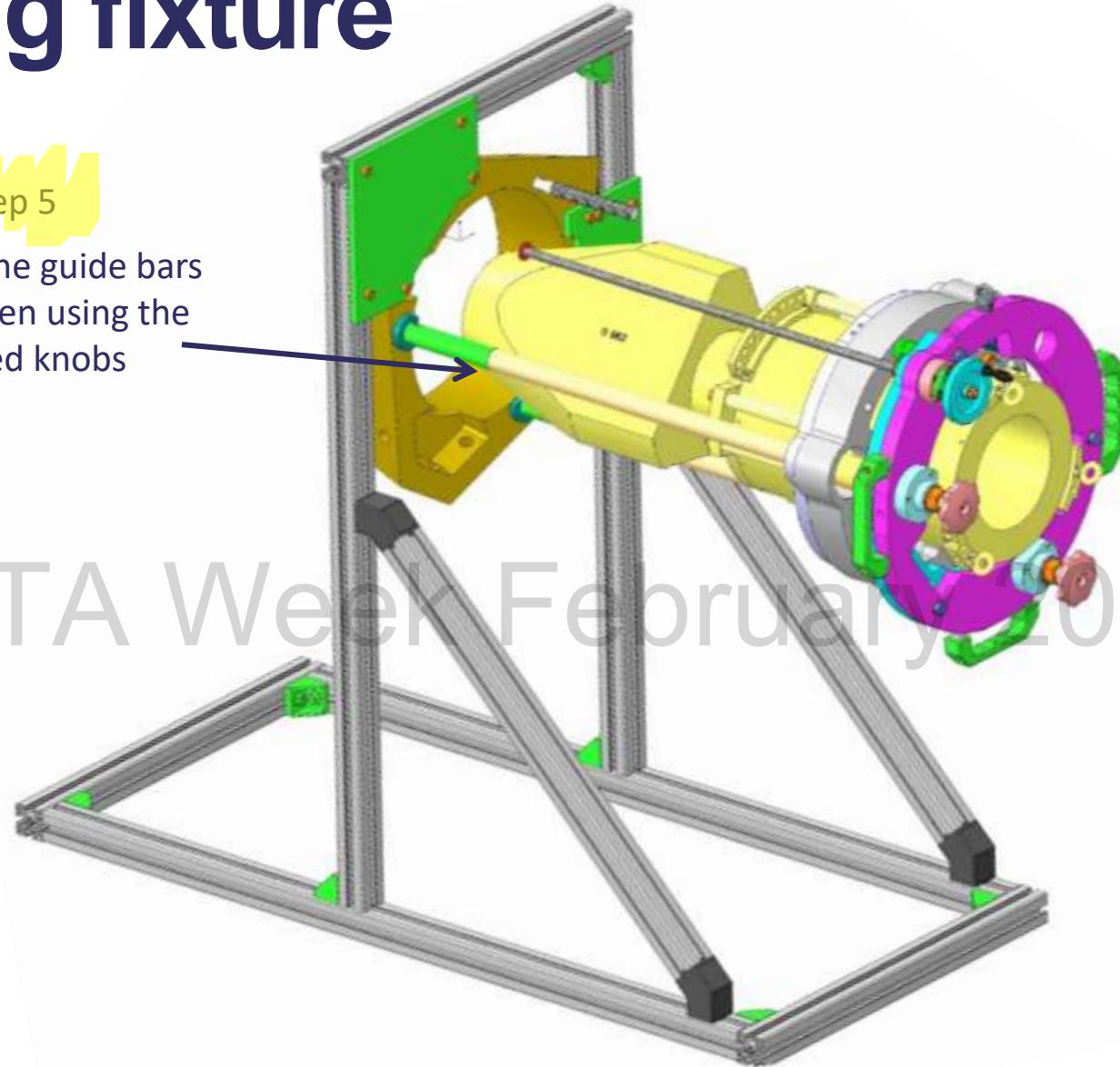
Using an adjustable chain hoist secured to the front mounting point, bring to the horizontal orientation



ATC handling fixture

Step 5

Engage the guide bars and tighten using the sculptured knobs

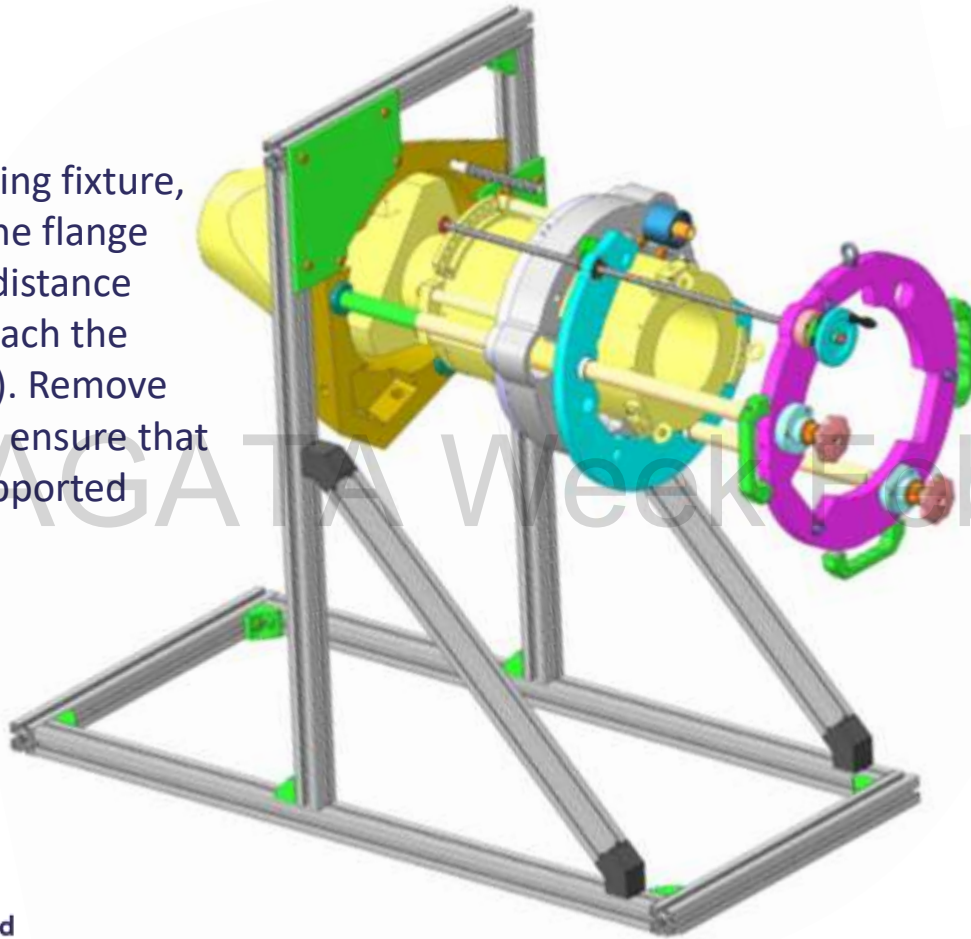


AGATA Week February 2021

ATC handling fixture

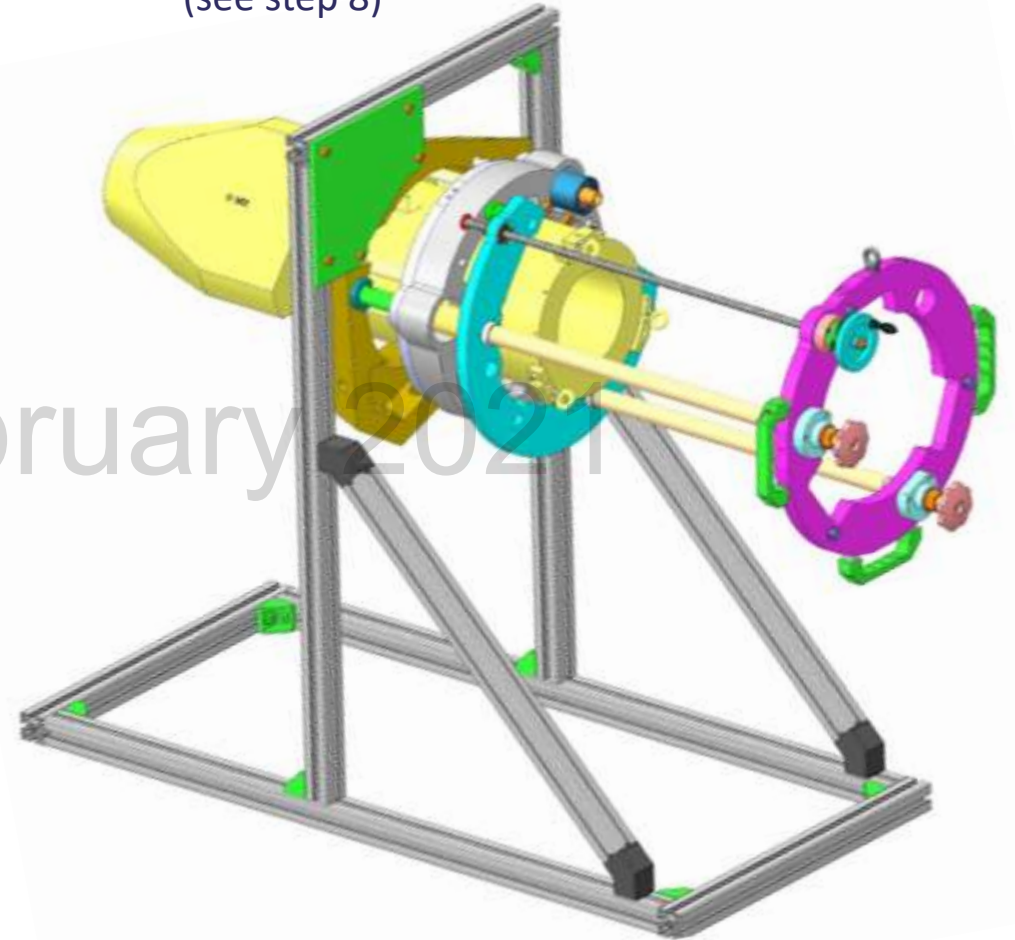
Step 6

Still attached to the loading fixture, wind the detector into the flange using the hand wheel – distance ~350 mm in order to ‘attach the digitiser cables’ (real life). Remove the adjustable chain and ensure that the rear end remains supported



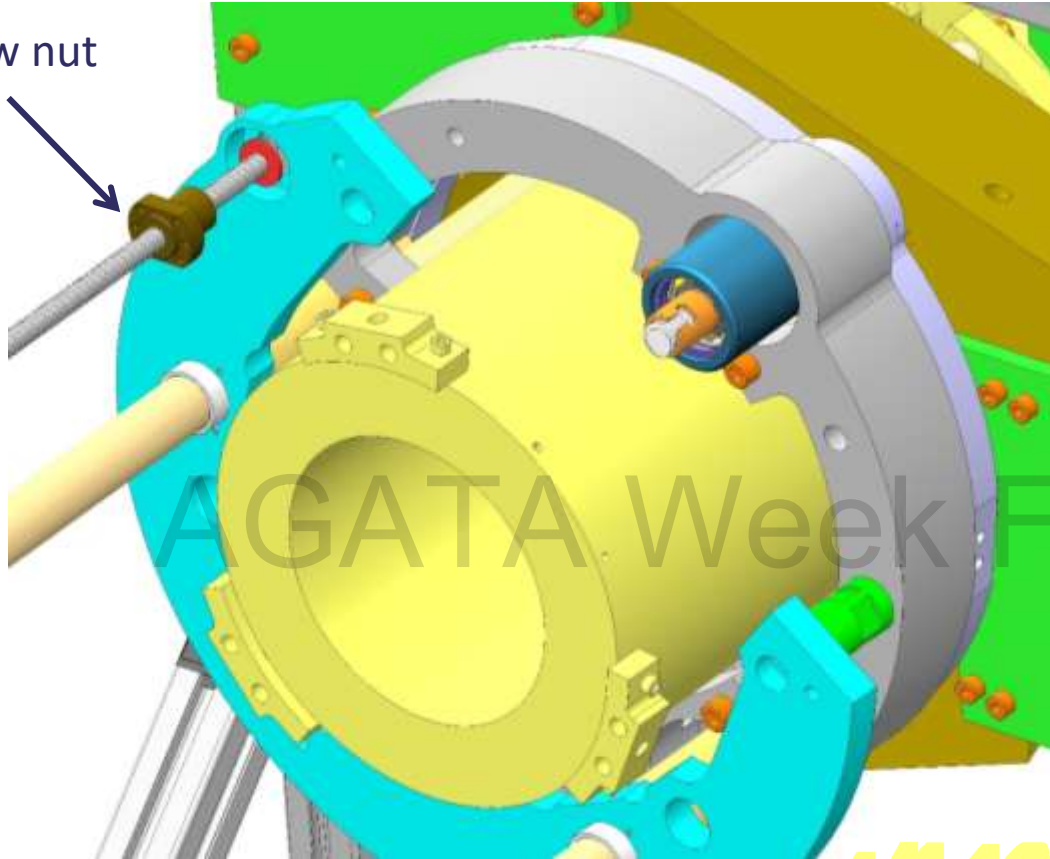
Step 7

Continue to wind the detector into the flange until the leadscrew nut engages with the end of the leadscrew then disconnect the ballscrew nut (see step 8)



ATC handling fixture

Ballscrew nut



Step 8

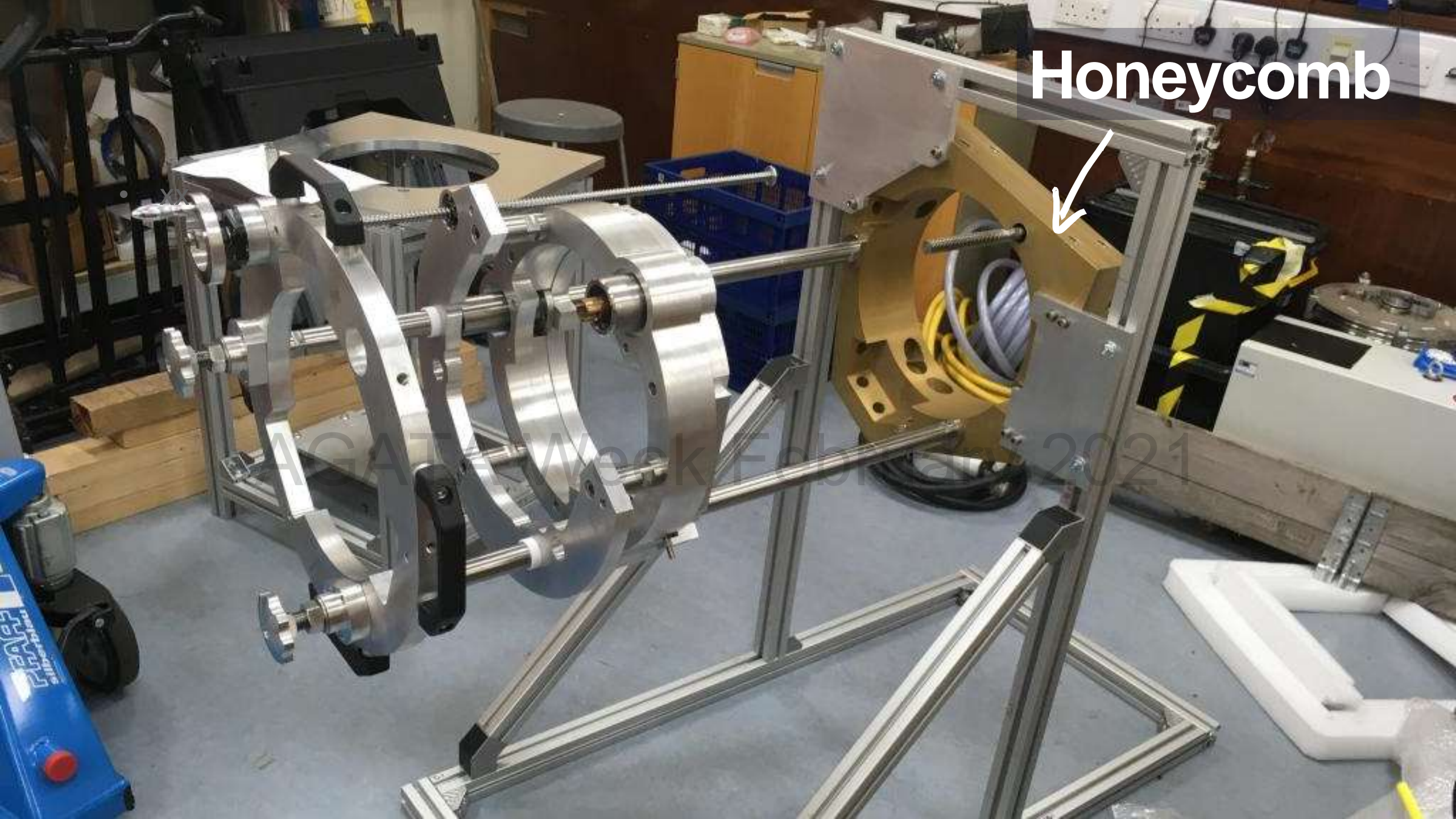


Remove the loading fixture and continue to wind the detector into the flange.
Removal is the reverse of this procedure

Honeycomb



AGATE Week Festival 2021





AGATA Week February 2021

Dummy detector



VCAIA Weekly

FACOM

JBL



GATA Week February 2020

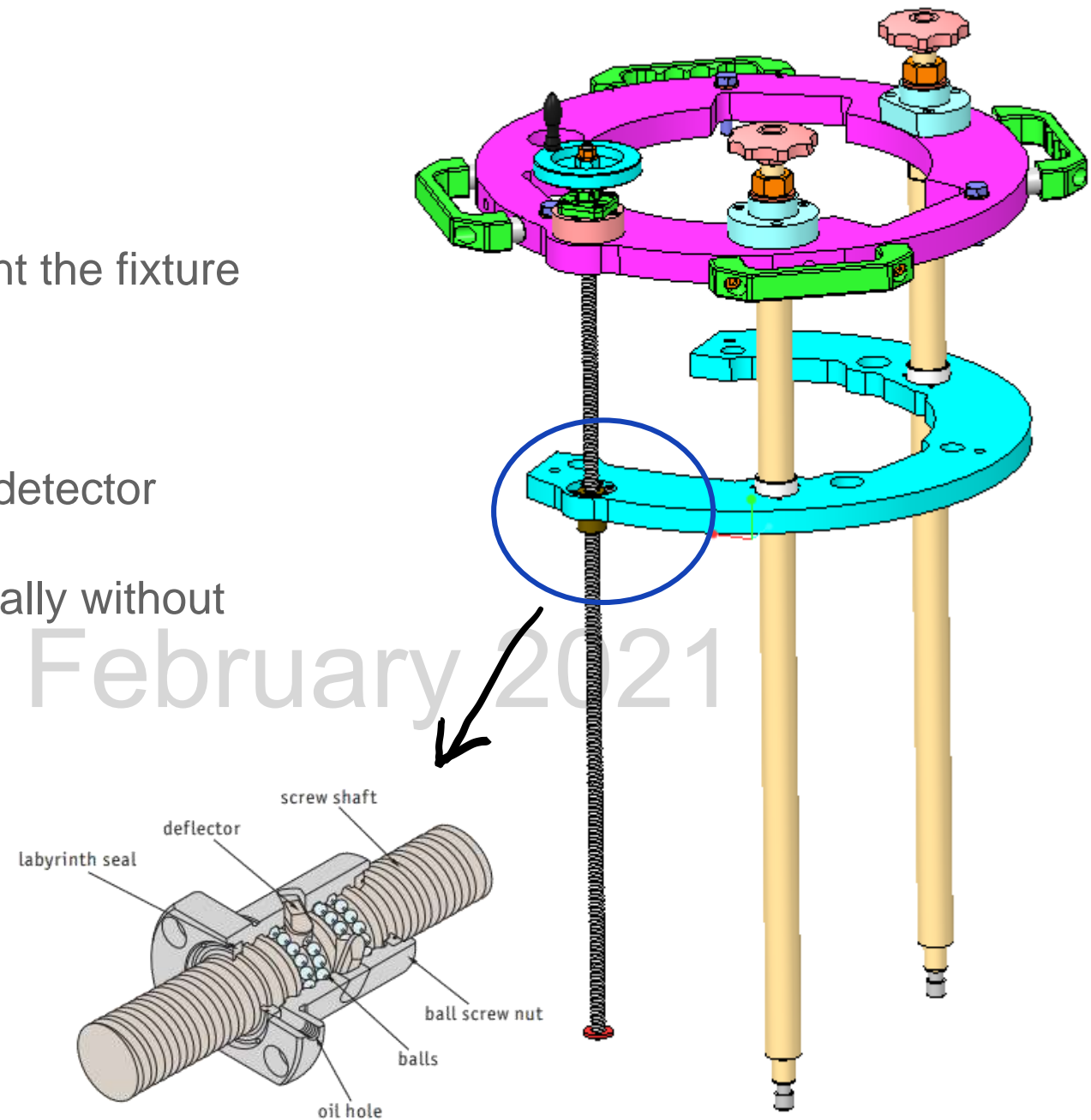


AGATA Week February 2021



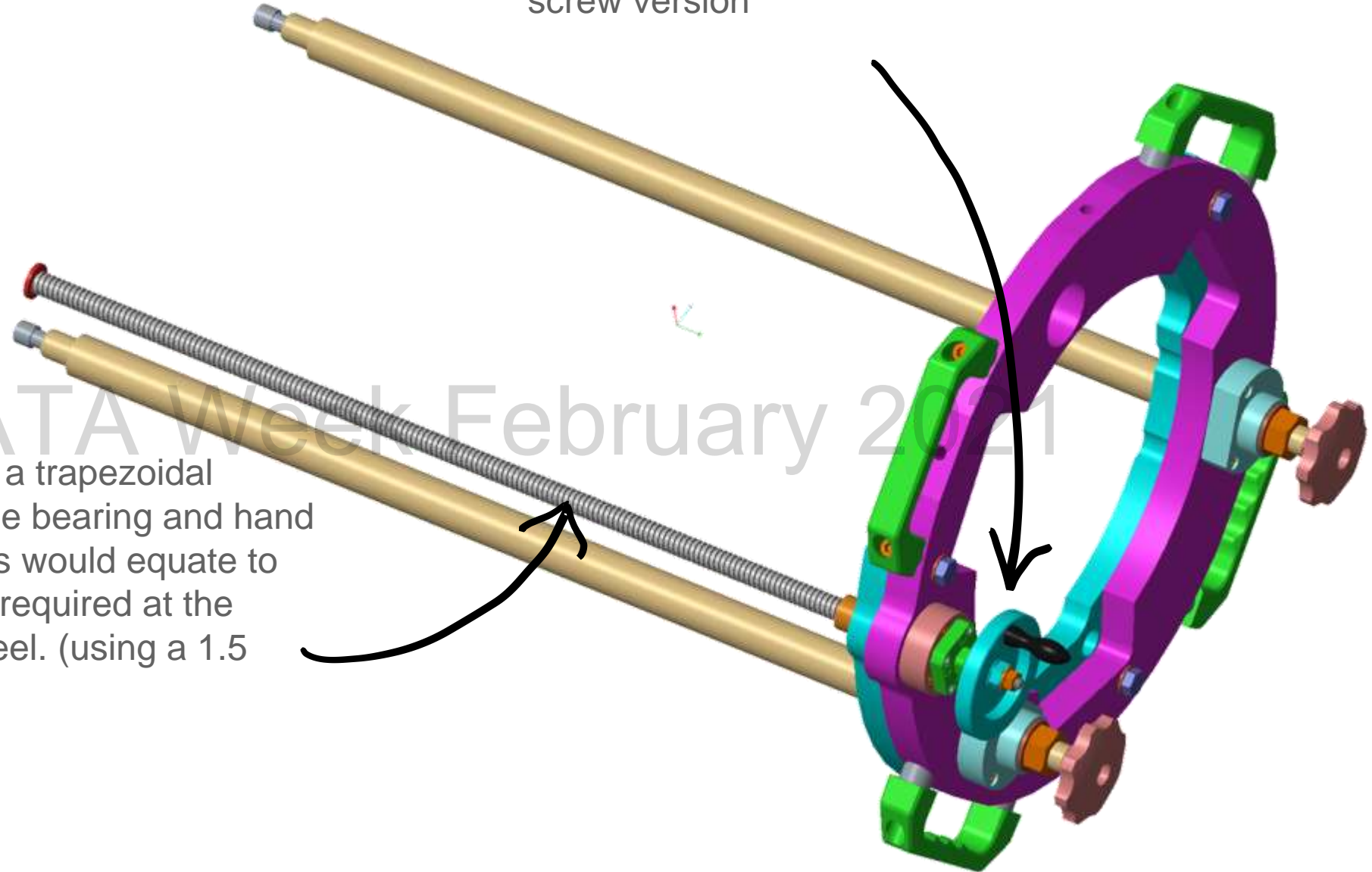
ATC handling fixture

- Insufficient friction in the system to prevent the fixture back-driving when operated at an angle
- Uses a low friction ballscrew to drive the detector
- Current design can only be used horizontally without risking damage to detector
- Design revised



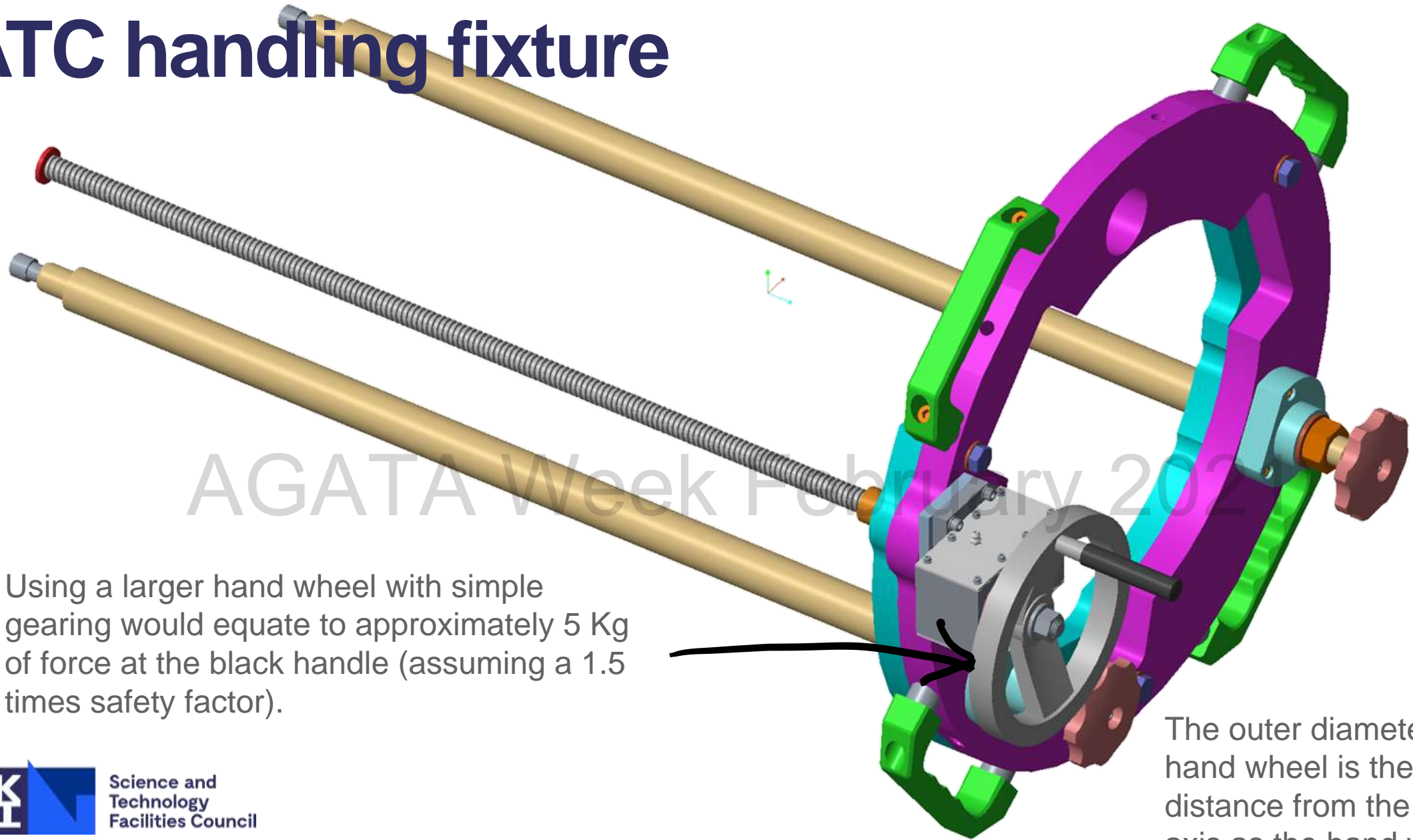
ATC handling fixture

The force at the black handle is estimated to be 3.5 Kg (with 1.5 times safety factor) for the original ball screw version



Replacing the ball screw with a trapezoidal screw and nut and keeping the bearing and hand wheel the same. However this would equate to approximately 13 Kg of force required at the black handle on the hand wheel. (using a 1.5 times safety factor).

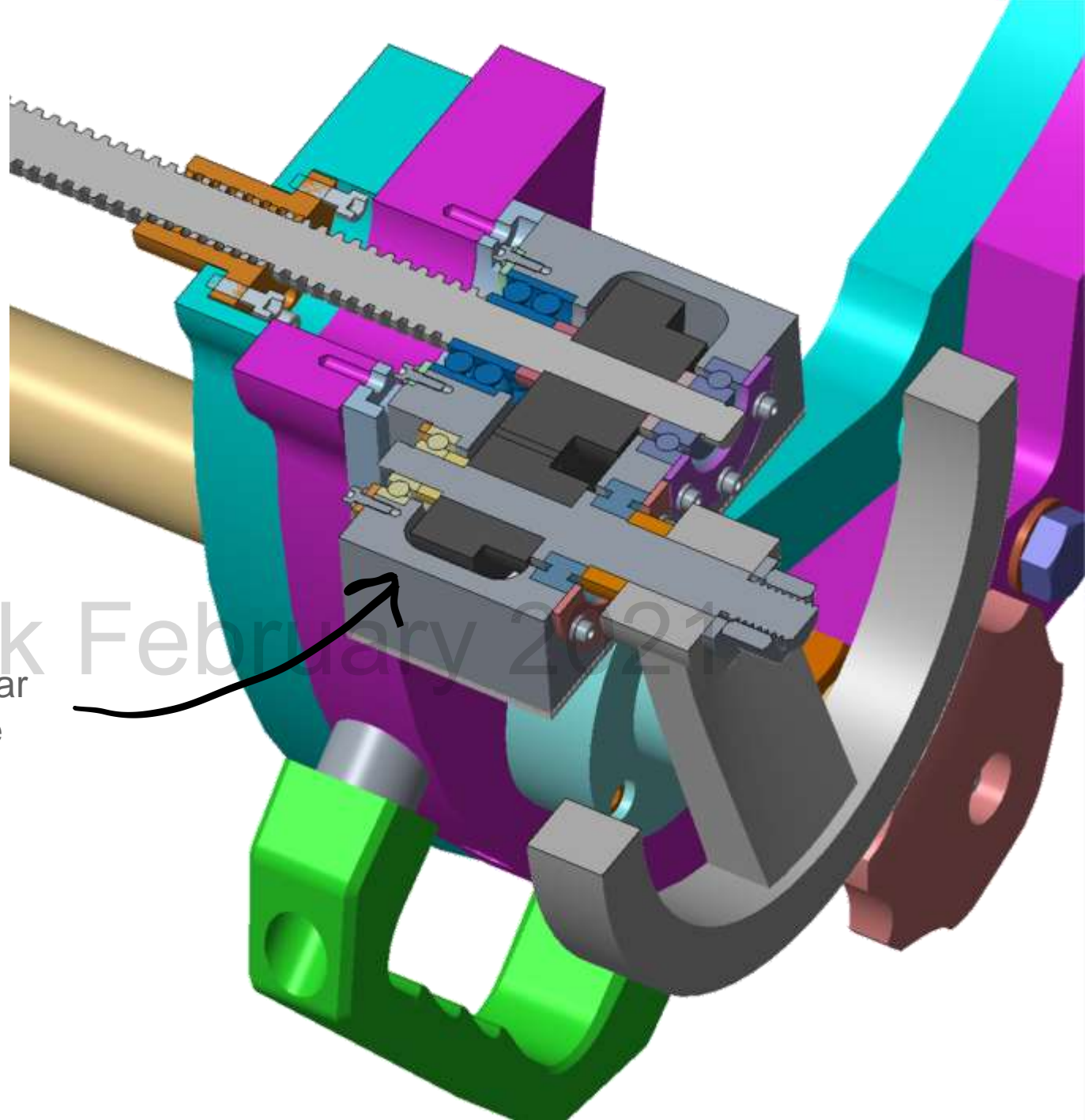
ATC handling fixture



Using a larger hand wheel with simple gearing would equate to approximately 5 Kg of force at the black handle (assuming a 1.5 times safety factor).

The outer diameter of this hand wheel is the same distance from the detector axis as the hand wheel for the original ball screw thread

ATC handling fixture



Having a smaller driving gear and a larger driven gear gives a torque advantage. However the speed of the screw will be reduced.

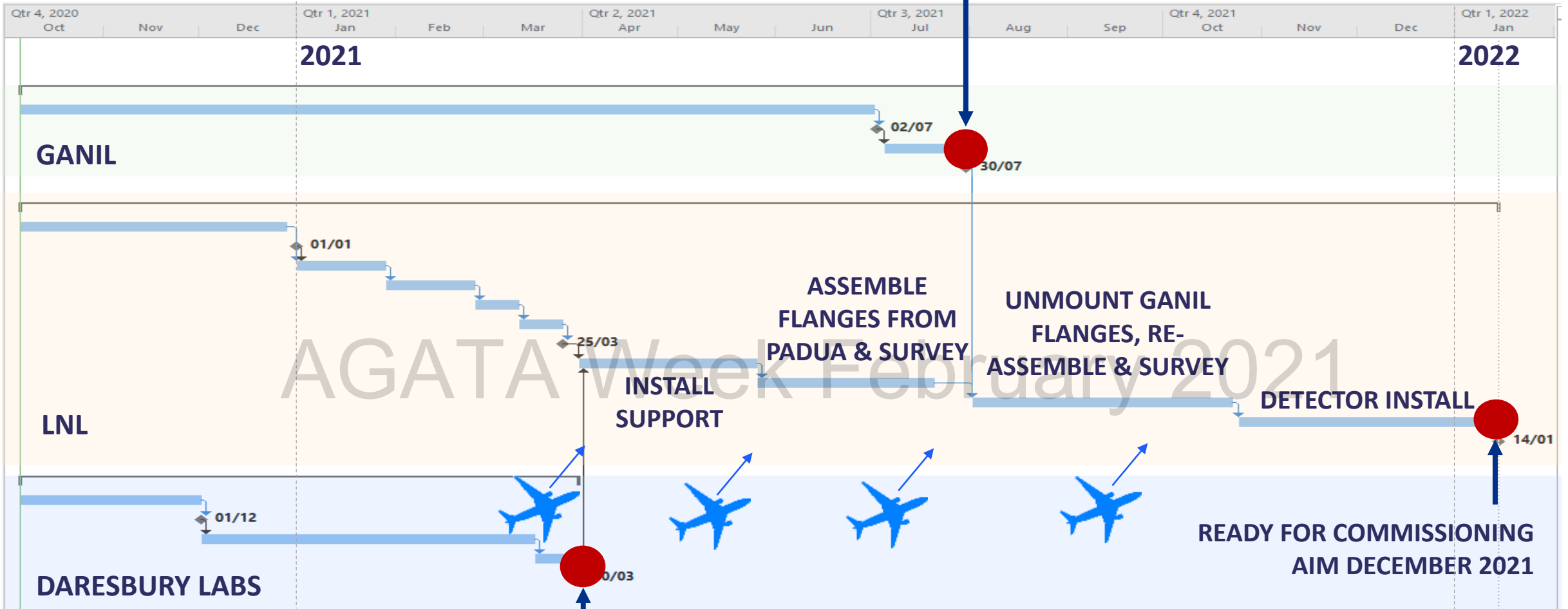
Mechanics - Looking forward

AGATA Week February 2021



Timescales (Pre-COVID)

AGATA SHIPPED FROM GANIL
JULY



COVID impact

National lockdowns

Workshops closed

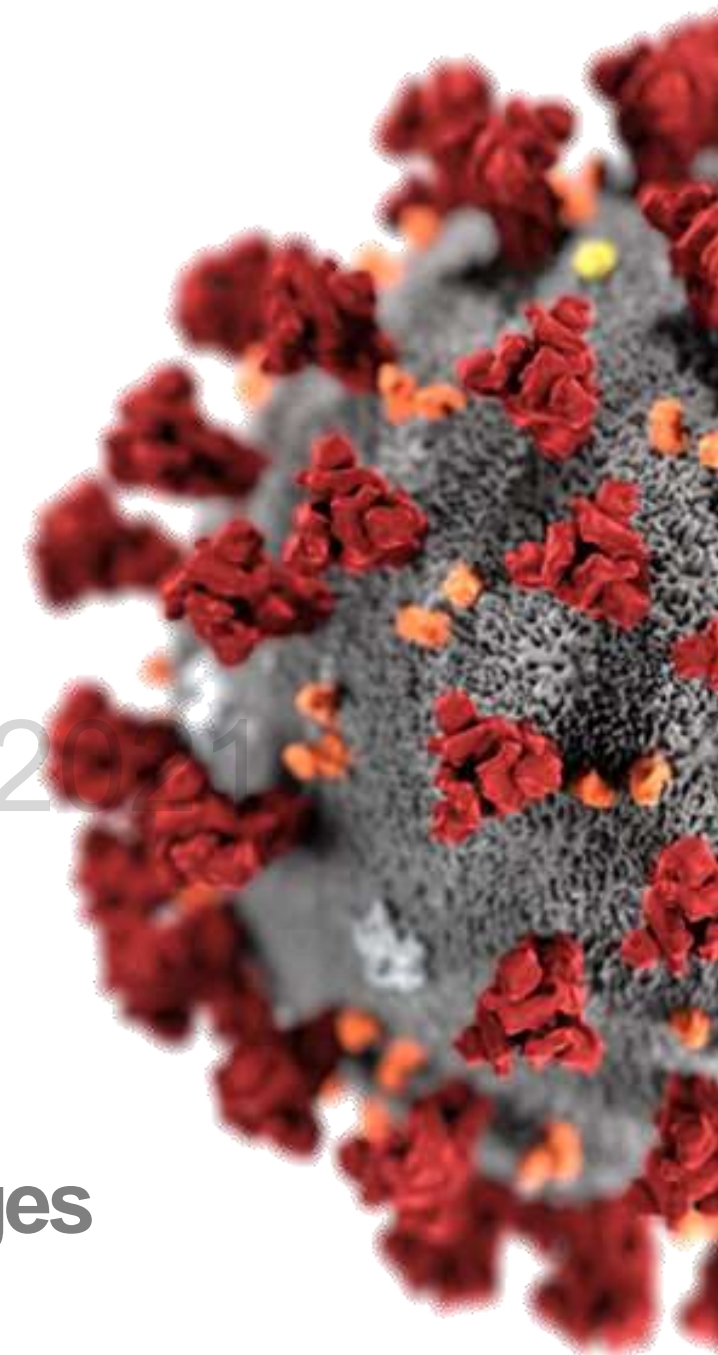
Limited staff

AGATA Week February 2021

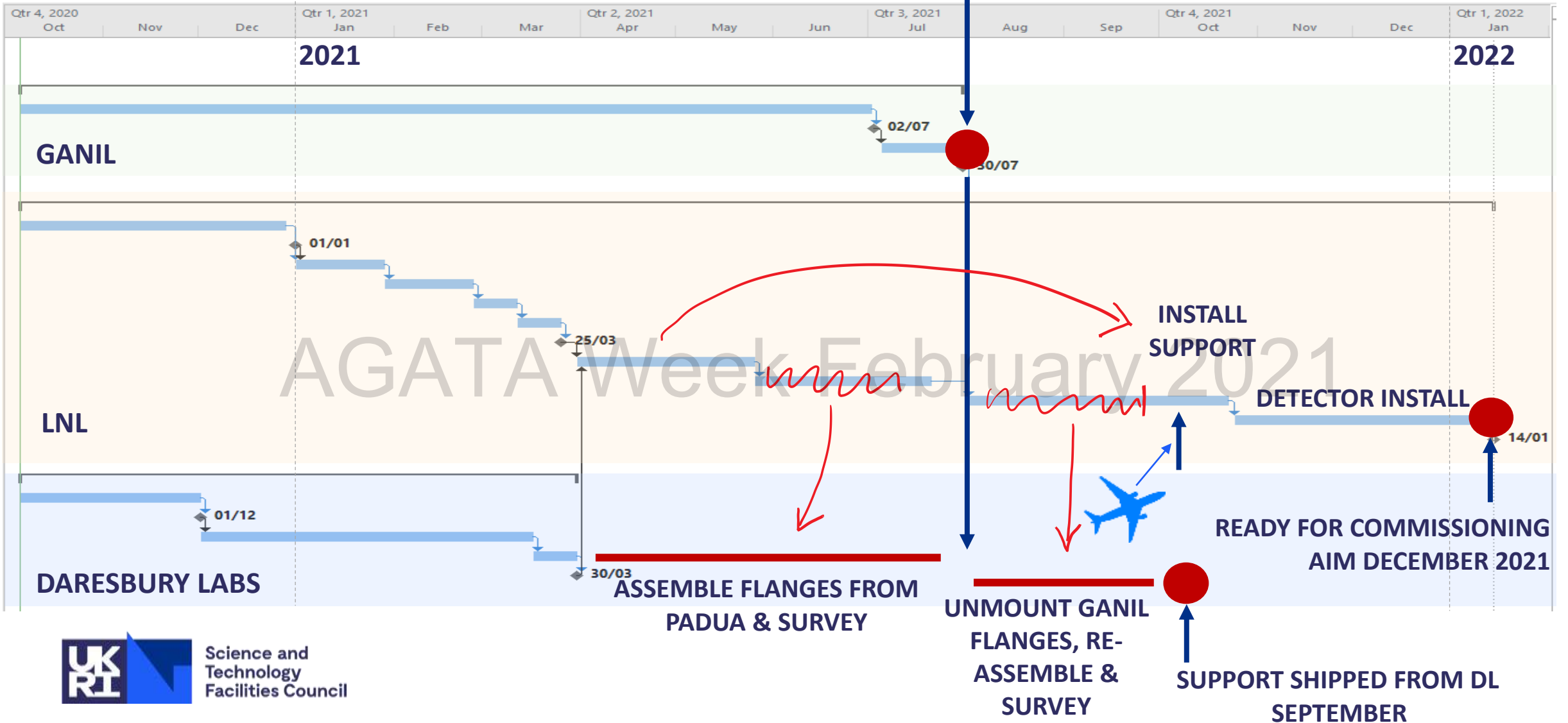
Supply chain issues

Travel restrictions

Material shortages



Timescales (Revised)



Assembly & survey at DL

- Ship 20 new flanges from Padua to Daresbury (1st batch end March)
- Ship the 15 flanges from GANIL direct to Daresbury (est. July)
- Assemble 30 flanges on shaft at Daresbury & survey into position
- Unmount 30 flange array as a single piece & ship with support to LNL (September)
- This pushes the need for international travel to later in the year
- Overcomes current travel restriction issues & allows work to progress
- Reduce the number and duration of visits to LNL ☹️



Assembly & survey at DL

- Opportunity to check shaft & flange interface whilst still in the UK
- Corrective action can then be taken at Daresbury or by the supplier
- Allows Daresbury team to become familiar with assembly & survey
- Refine processes whilst Daresbury team have all their equipment available to hand
- Prevents the need for a second building for storing support at Legnaro

The current situation has provided us with a few opportunities to

derive some positives 😊

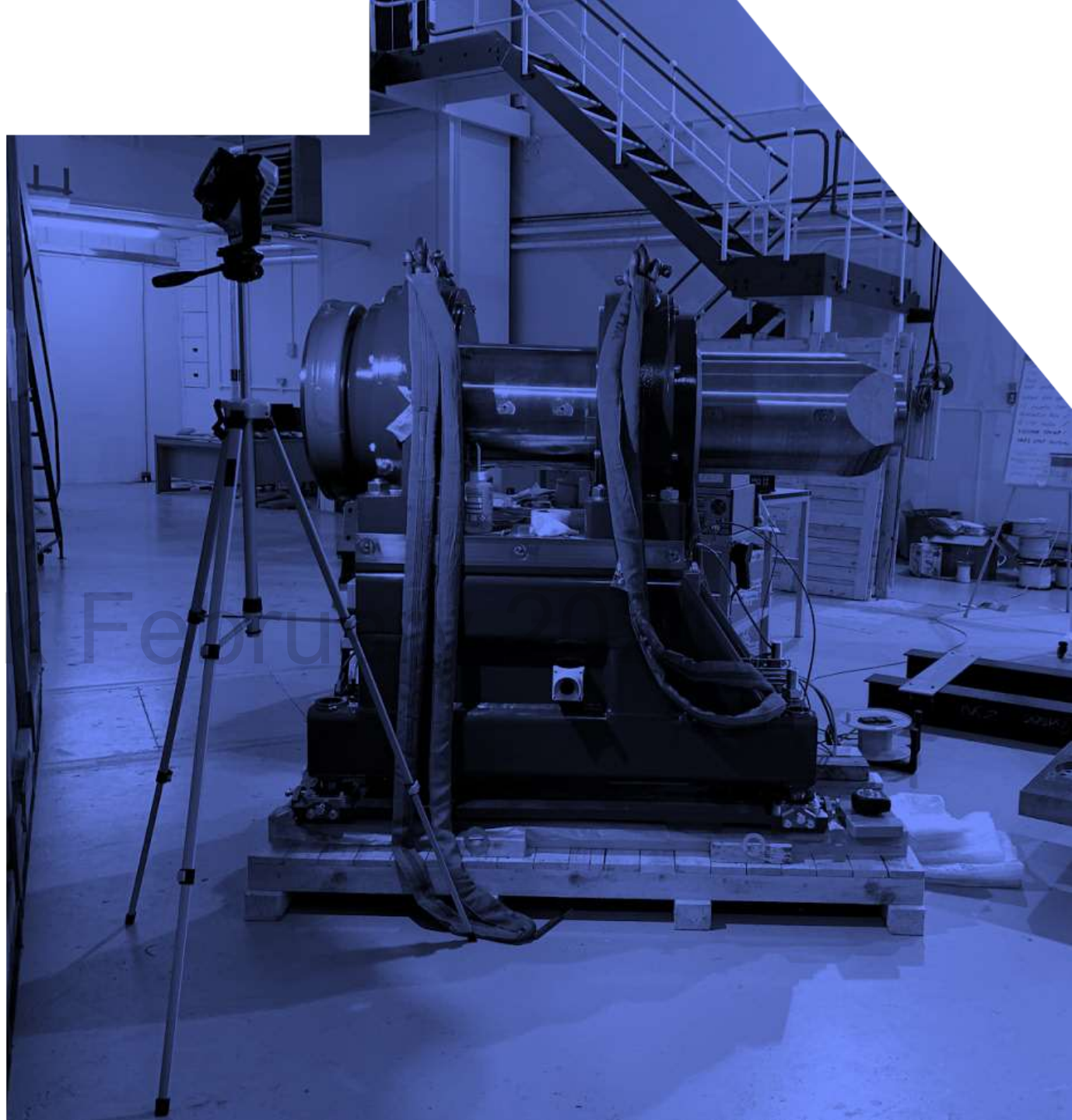


Summary

- Overall mechanics is progressing well
- Schedule is adapting to the changes and obstacles
- Busy year with a lot of developments
- Support structure is on target
- Tests on ATC lifting & handling process are ongoing
- Production of flanges at Padua progressing well
- Focused on shipping full array & support in September



Thank you
AGATA Wee



Science and
Technology
Facilities Council