

# Broadband quantum noise reduction in Virgo using frequency dependent squeezing

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LAPP, 9th October 2020

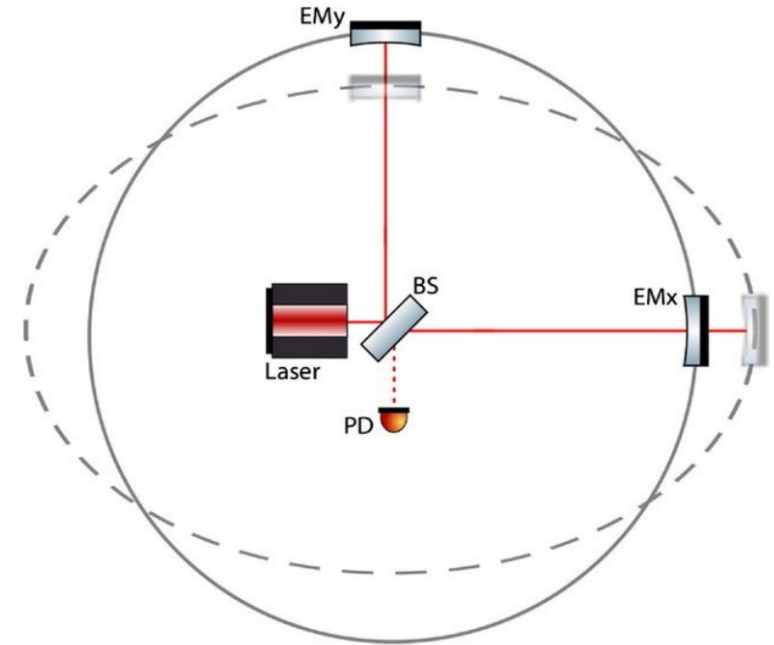
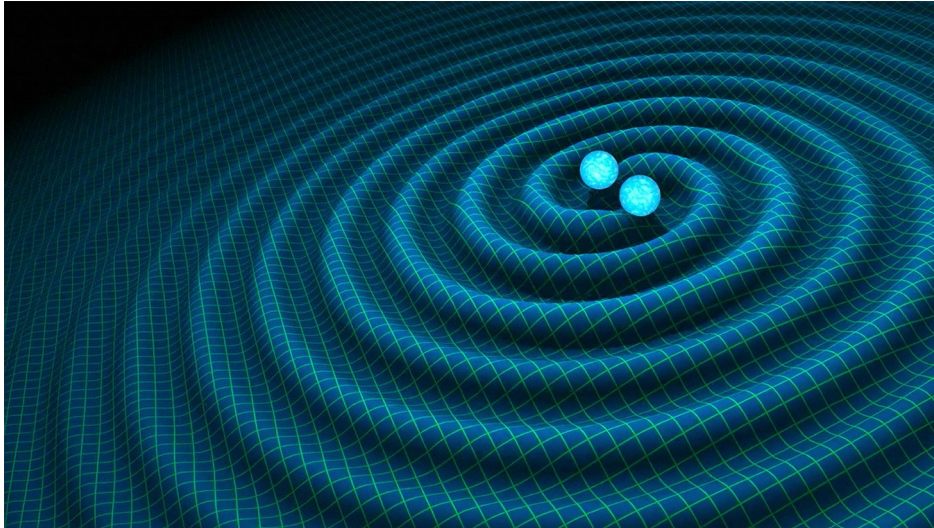
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Edwige Tournefier

**Thesis Co-Advisors:**  
Romain Bonnand  
Romain Gouaty



- **Gravitational waves** are 'ripples' in the fabric of space-time caused by some of the most violent and energetic processes in the Universe.

$$g_{\mu\nu} = \eta_{\mu\nu} + h_{\mu\nu} \rightarrow \text{small perturbation of the metric tensor}$$

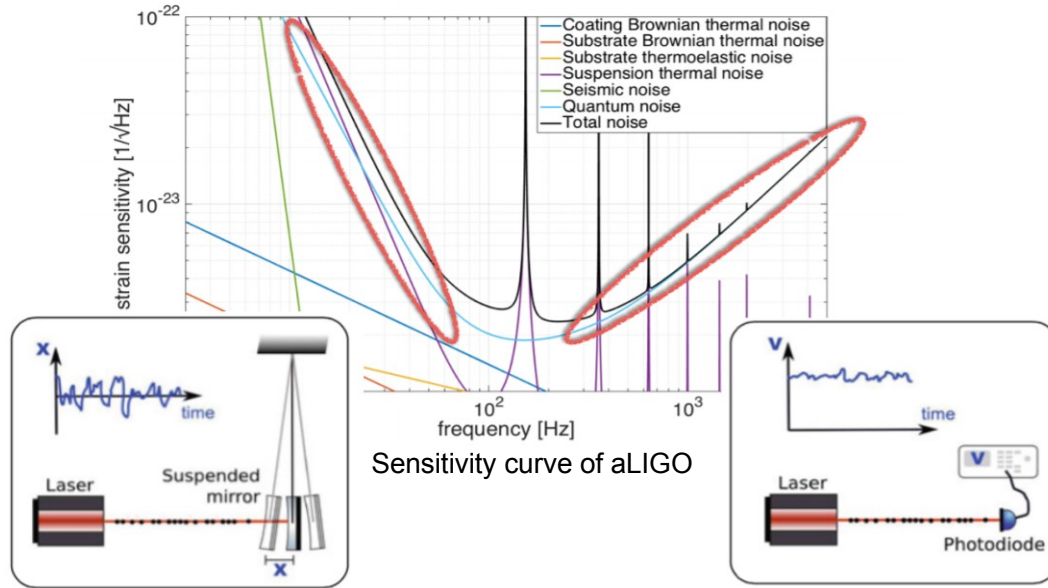


- **Detection principle:** Michelson interferometer measures the difference in phase associated to the passing gravitational wave (GW)

$$\delta\phi_{\text{GW}} = \frac{4\pi}{\lambda} \delta L_{\text{GW}} \rightarrow h = \frac{2 \delta L_{\text{GW}}}{L}$$

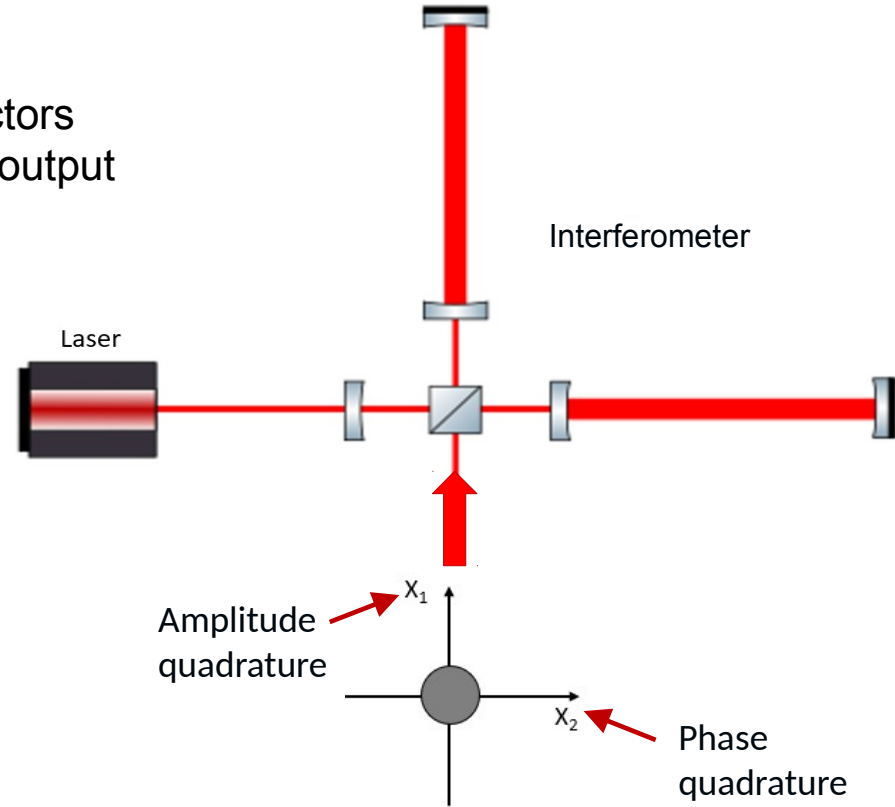
- Introduction:**

- ✓ Quantum noise (QN) limits the sensitivity of GW detectors
- ✓ QN are vacuum fluctuations entering interferometer's output port



Radiation pressure noise

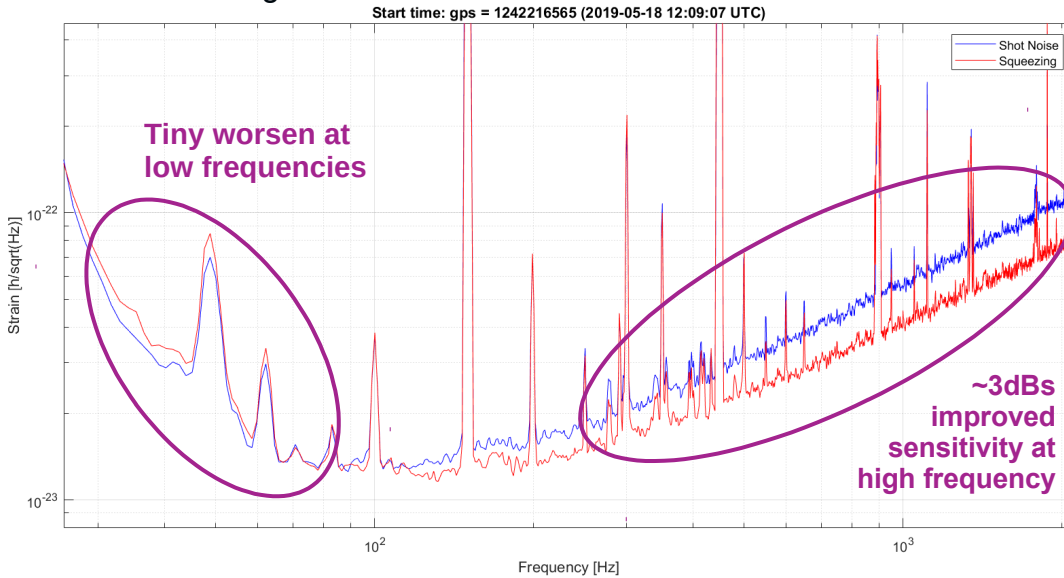
Shot noise



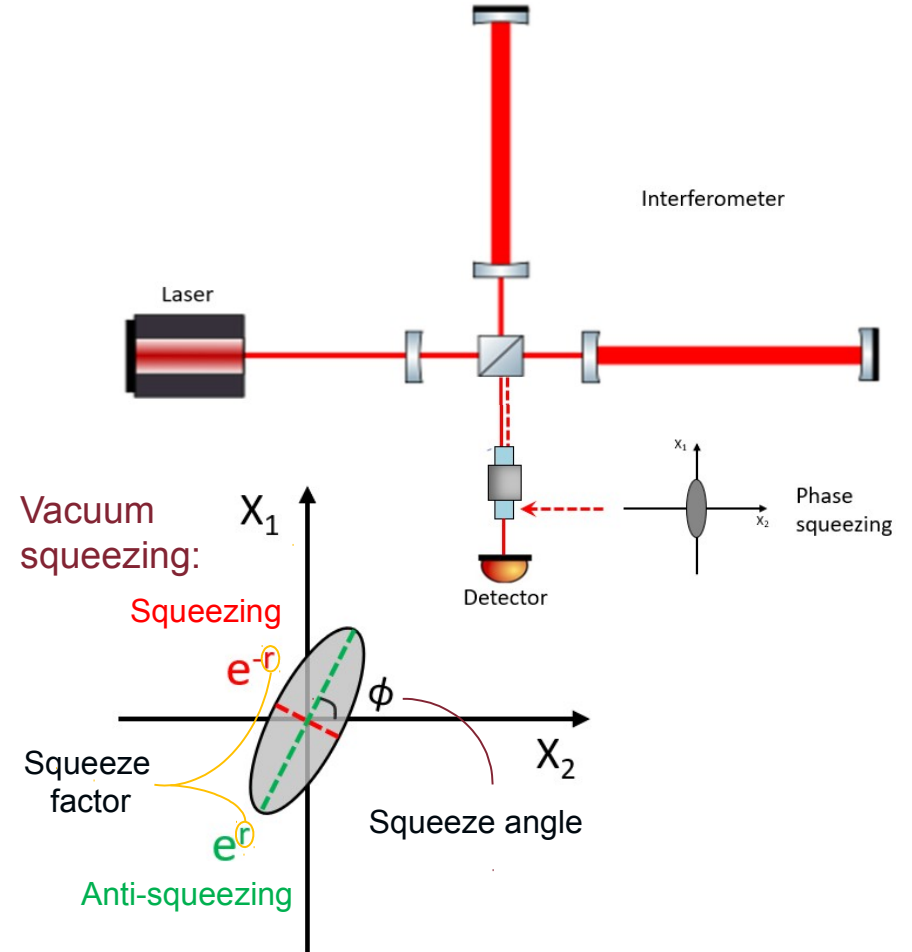
$$\hat{H} = \hbar\omega \left( \hat{a}^\dagger \hat{a} + \frac{1}{2} \right) \longrightarrow \hat{H} = \hbar\omega \left( \hat{X}_1^2 + \hat{X}_2^2 \right)$$

- **First step:**
  - ✓ Injecting squeezed vacuum states from the output port to improve sensitivity, run O3
  - ✓ Implemented in AdVirgo and aLIGO

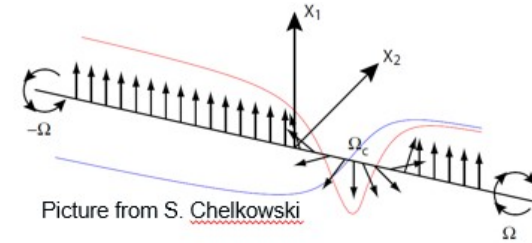
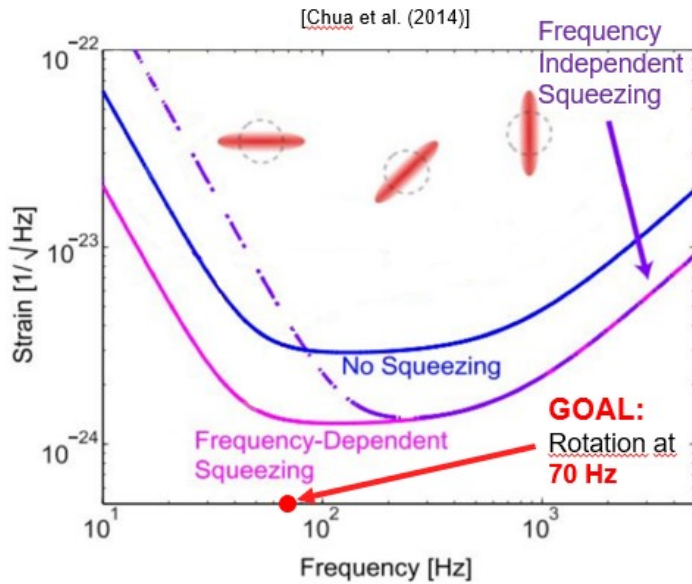
Advanced Virgo



Plot from M. Vardaro

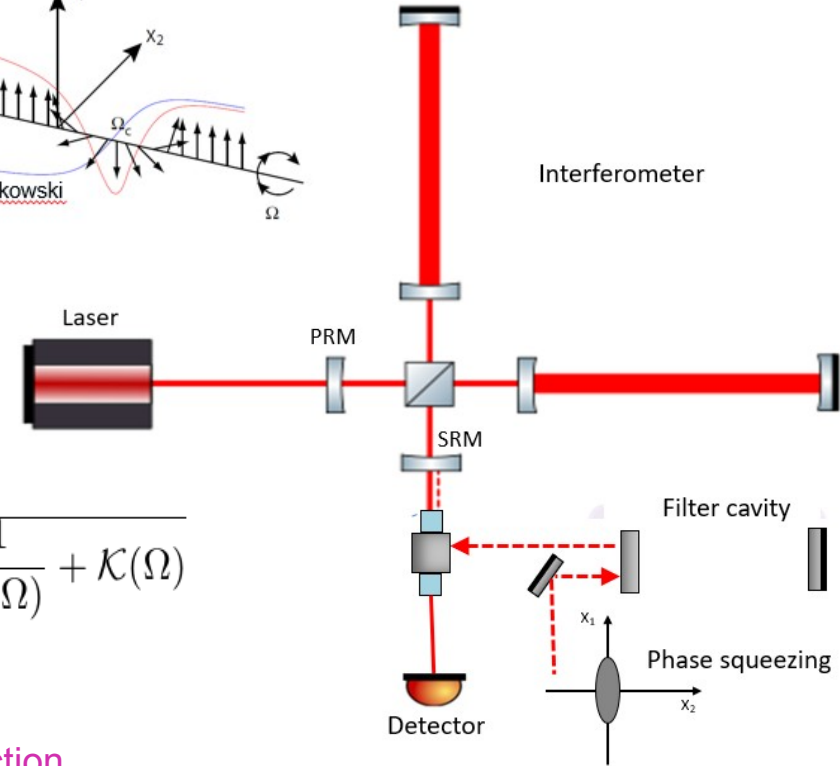


- **Next step:**
- ✓ Vacuum squeezed state angle become frequency dependent when reflected by a detuned Fabry-Perot filter cavity
- ✓ Implementation in GW detectors in O4



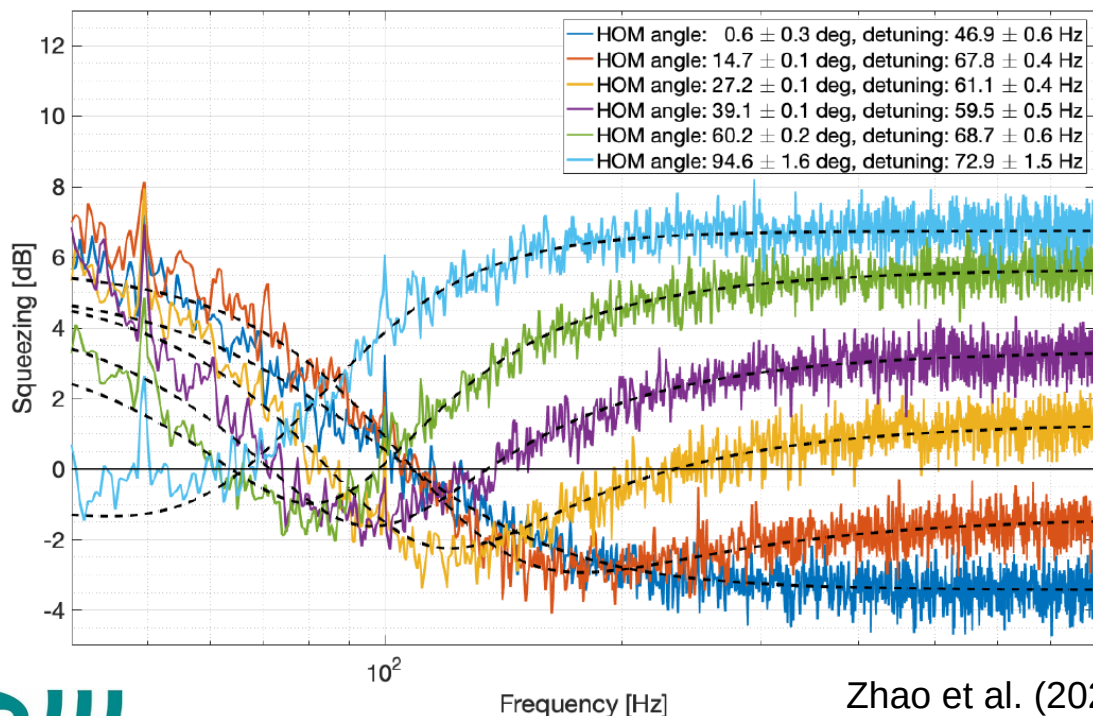
$$h(\Omega) = \frac{h_{SQL}}{\sqrt{2}} e^{-r} \sqrt{\frac{1}{\mathcal{K}(\Omega)} + \mathcal{K}(\Omega)}$$

Broadband reduction factor

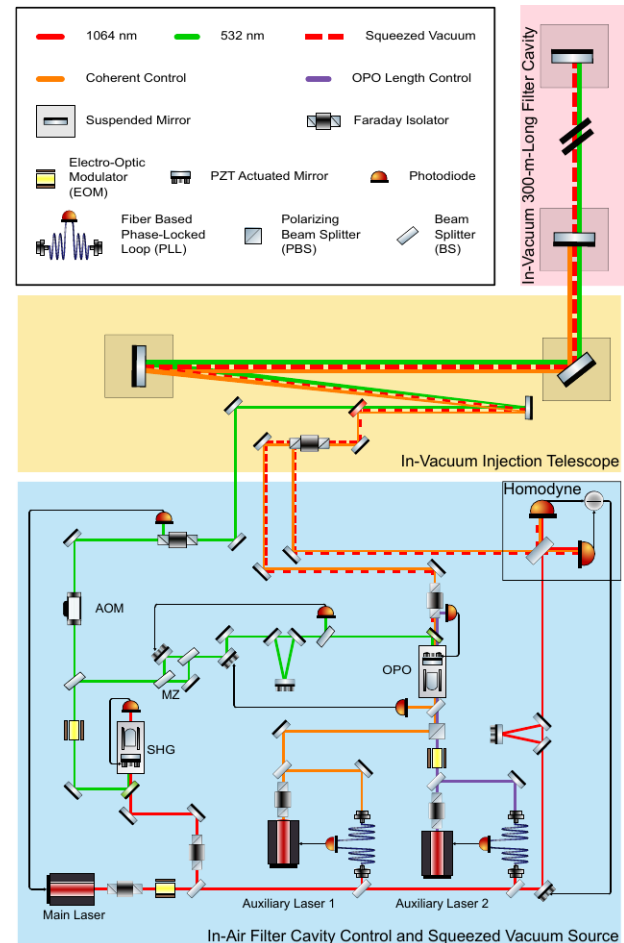




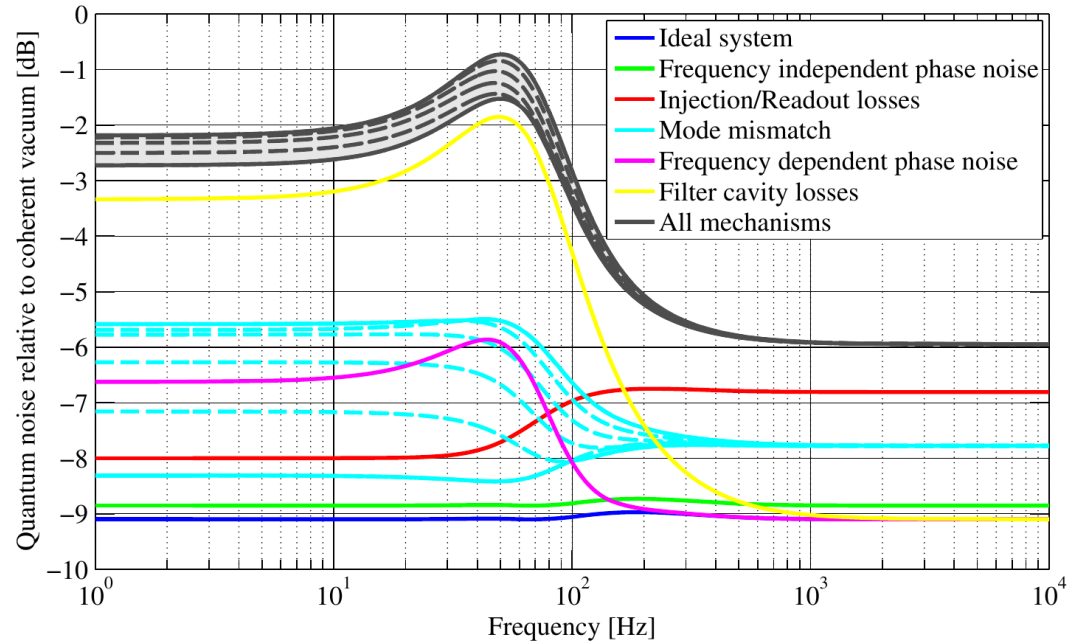
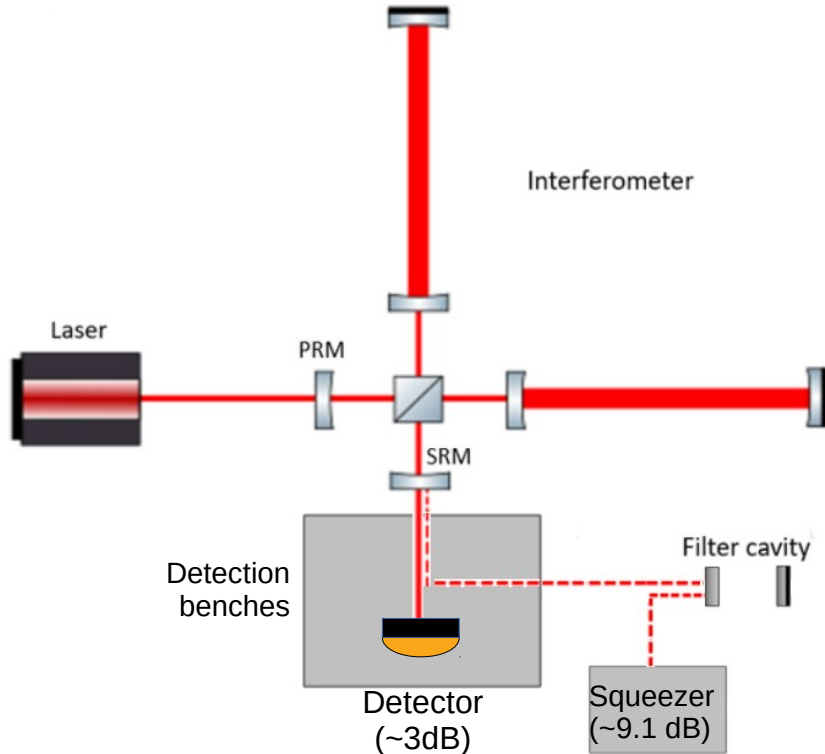
R&D experiment at NAOJ, Tokyo, Japan, was the **first demonstration** (2020) of a frequency dependent squeezed vacuum source, realized with a 300 m suspended filter cavity. The squeezing rotation takes place in the frequency region ( $\sim 100$  Hz) needed to reduce the quantum noise in the whole spectrum of advanced GW detectors.



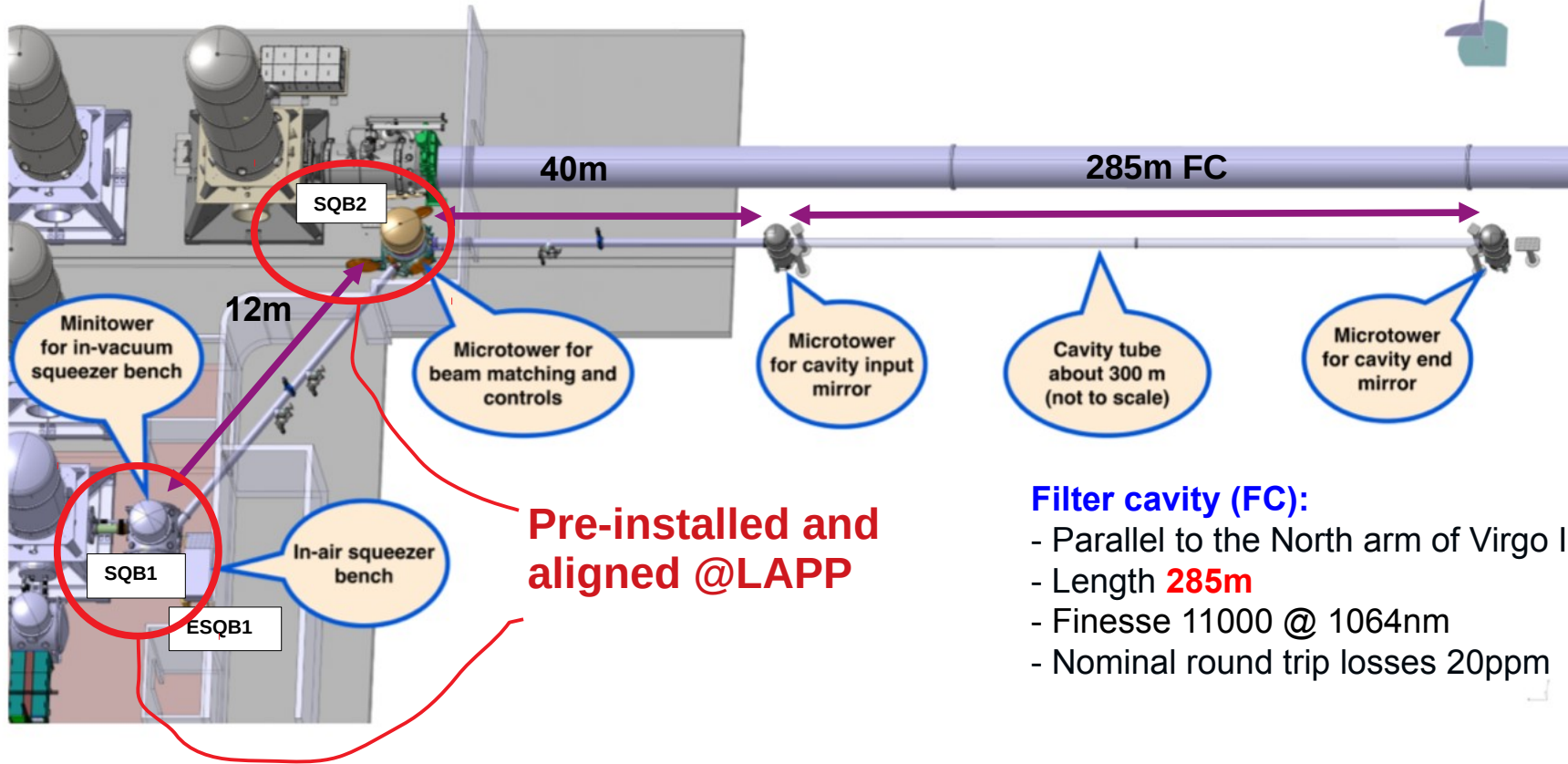
Zhao et al. (2020)



Decoherence (**optical losses + mode mismatch**) and degradation (**phase noise due to phase lock errors + stray light + cavity length fluctuations**) mechanisms limit the experimentally achievable QN reduction.



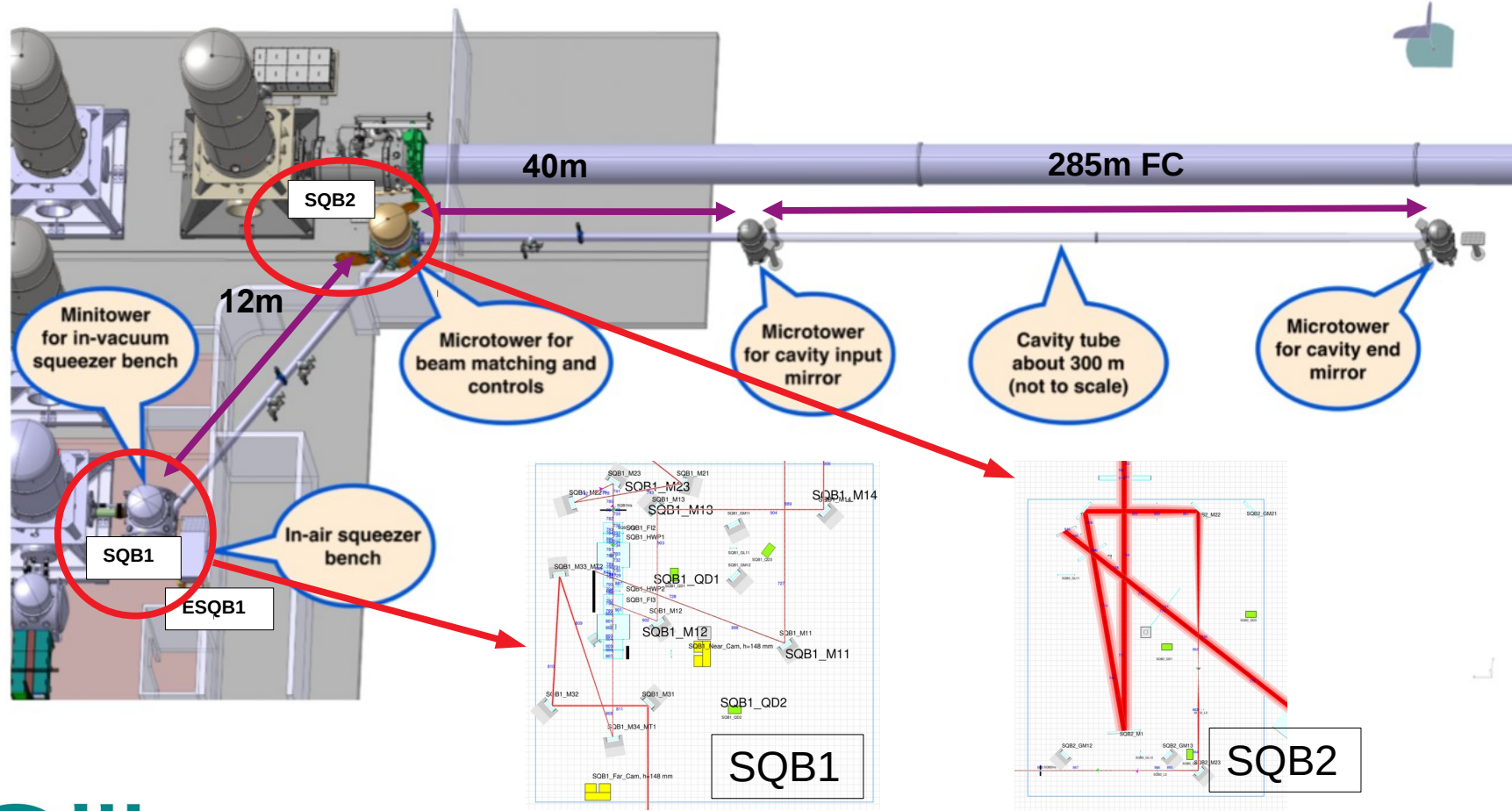
Kwee et al. (2014)



### Filter cavity (FC):

- Parallel to the North arm of Virgo ITF
- Length **285m**
- Finesse 11000 @ 1064nm
- Nominal round trip losses 20ppm

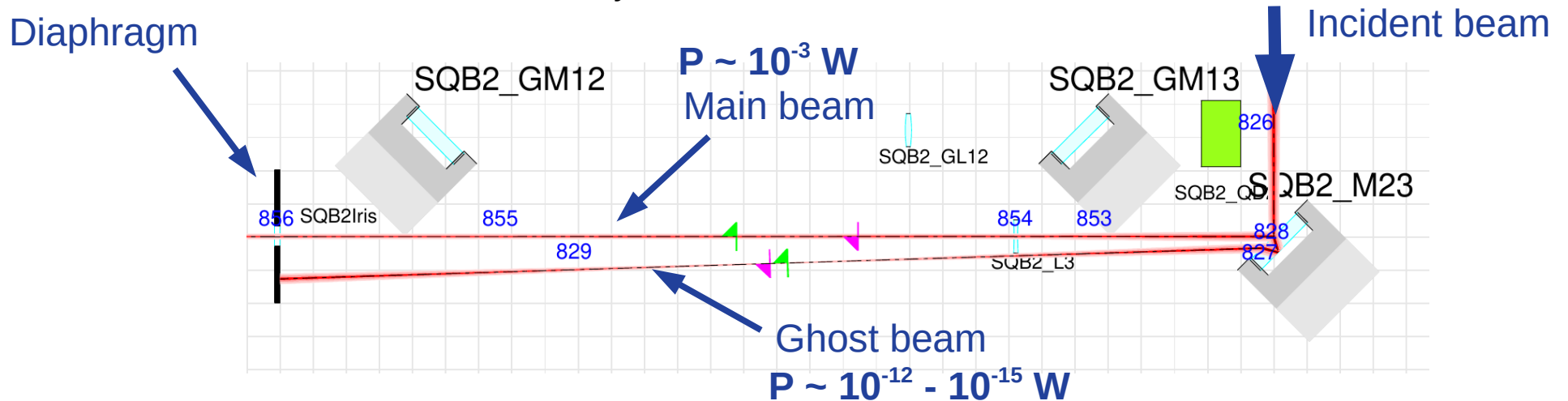




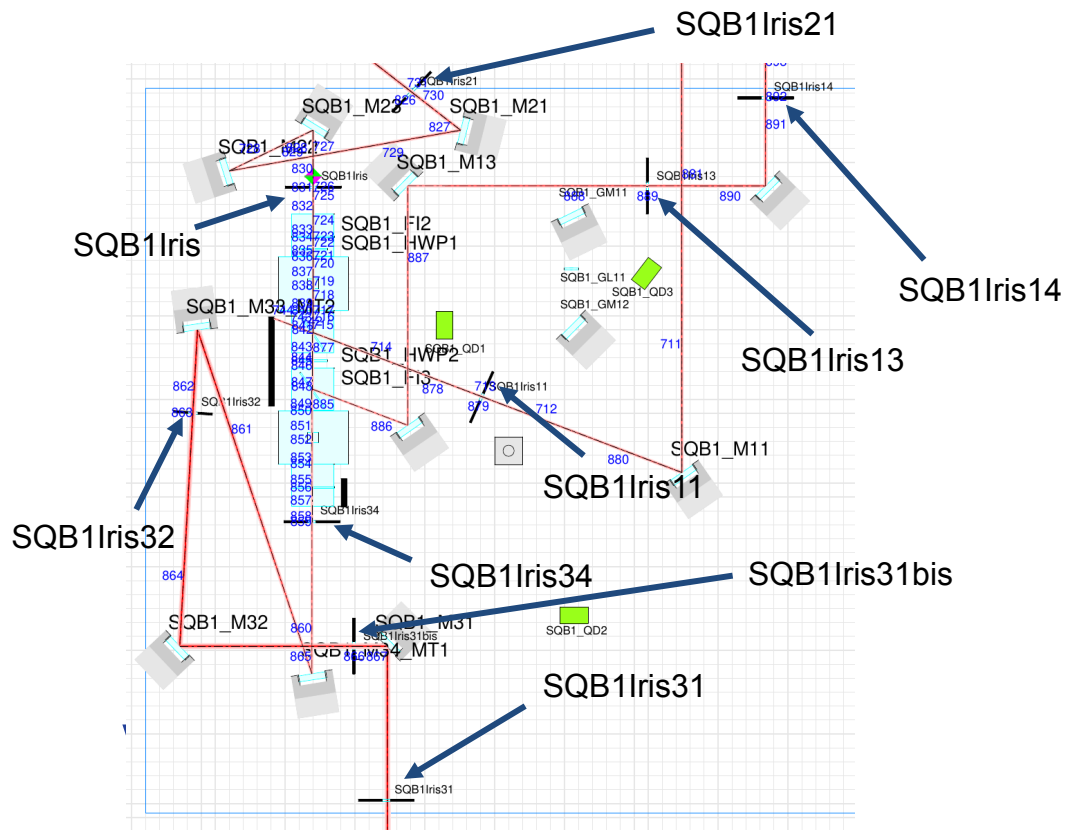
**Ghost beams:** secondary beams generated by not perfect mirror coatings:

1) we want to dump these beams to **avoid scattered light** on squeezing benches (it has been proved that the squeezing sensitivity enhancement is affected by stray light: [Virgo Logbook #48337](#), [#44990](#));

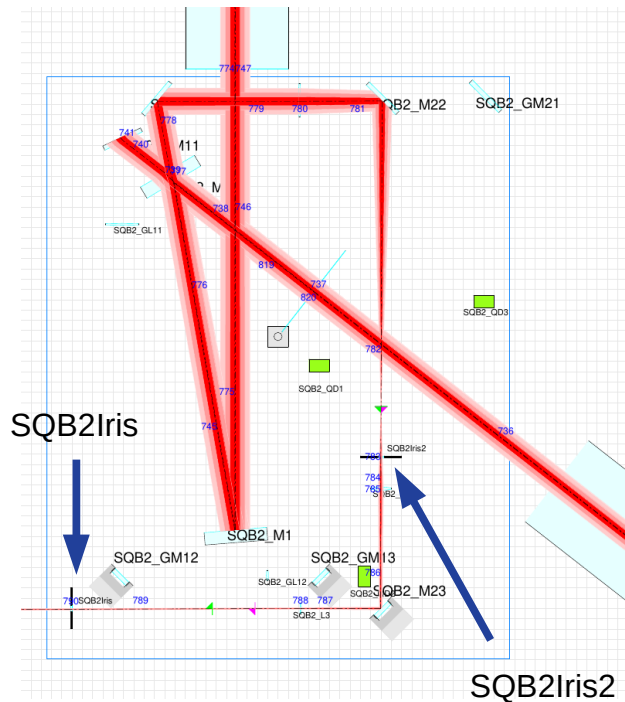
Ghost beam tracing using *Optocad*: beam transmitted by the first mirror surface and reflected by the second one.



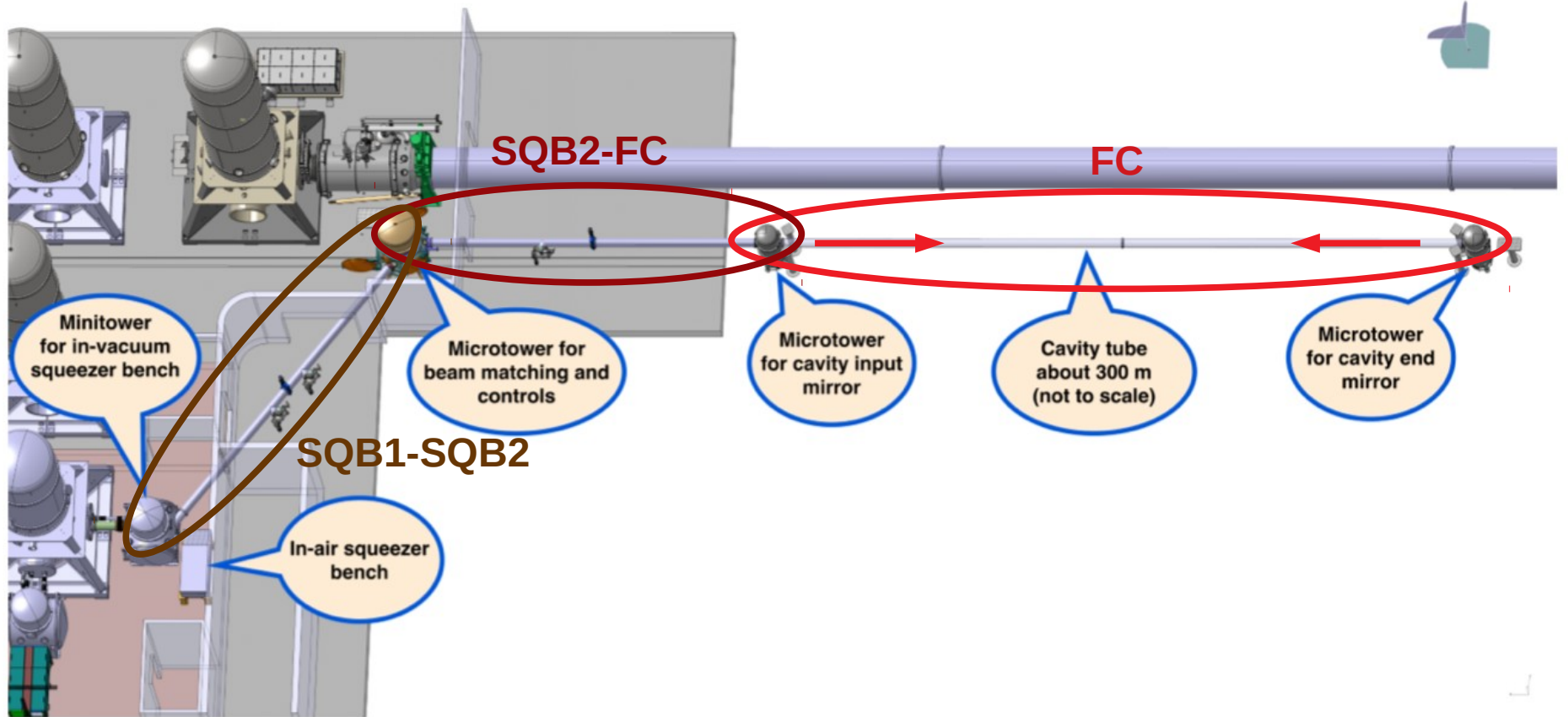
Dumping diaphragms on SQB1:



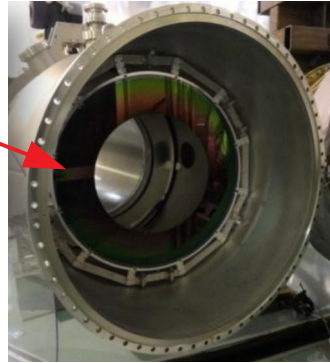
Dumping diaphragms on SQB2:



[AdV TDS: VIR-0549B-20](#)



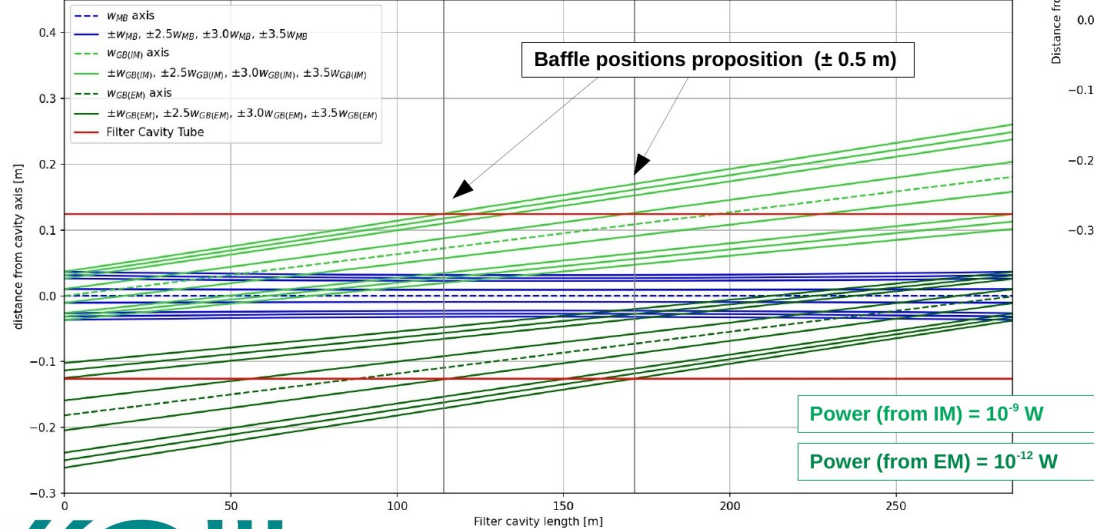
Baffle



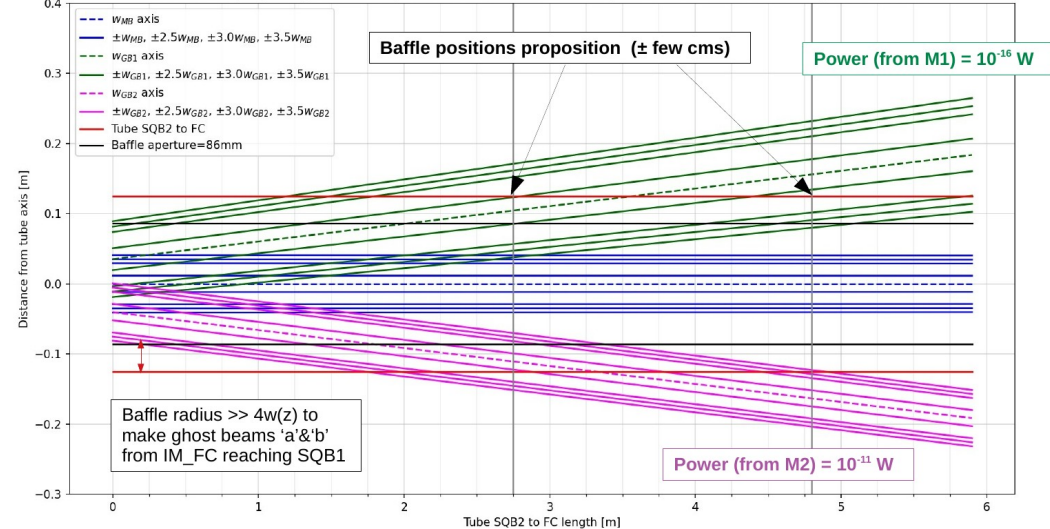
Baffles inside linking tube SQB2-FC:

Baffles inside FC:

Main beam (MB) and ghost beams (GB(IM) from Input Mirror, GB(EM) from End Mirror) propagating inside the Filter Cavity



Main beam (MB) and ghost beams (GB1 from M1 and GB2 from M2) inside TUBE SQB2 to FC; wedges M1&M2=0.5

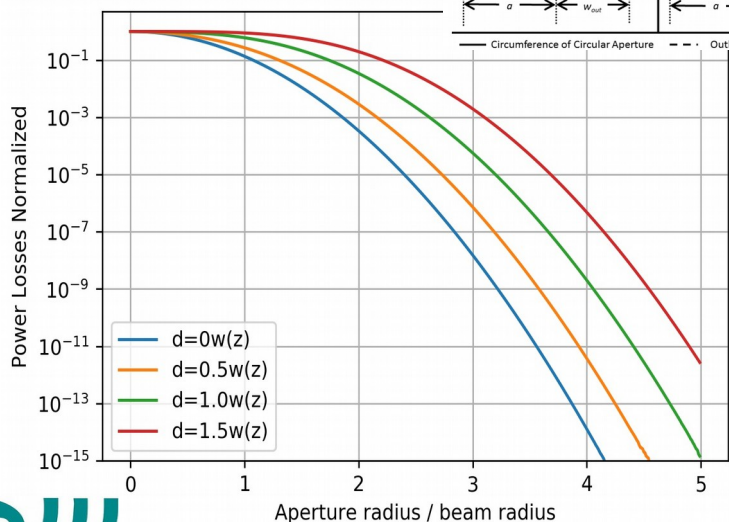
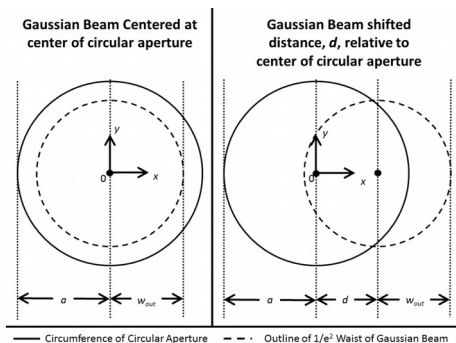




2) we need to chose an optimal size of diaphragm/baffle apertures to **limit losses** on the main beam.

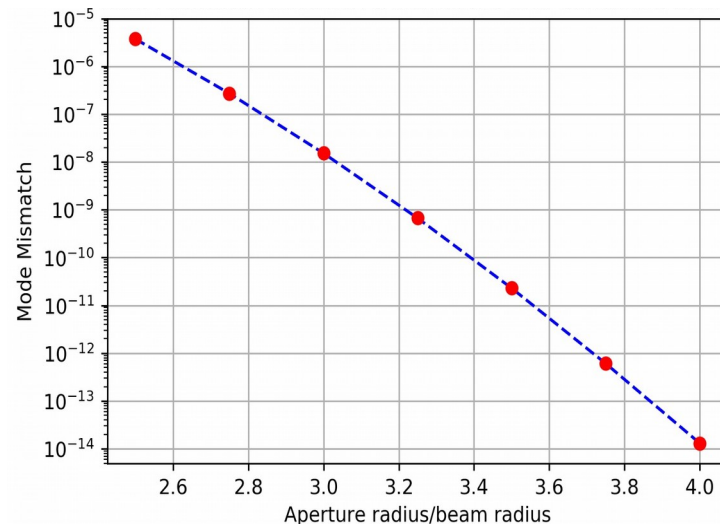
## Power losses

Since the HR coating has 3ppm power losses, we want < 1ppm losses, up to 1 w(z) displacement.

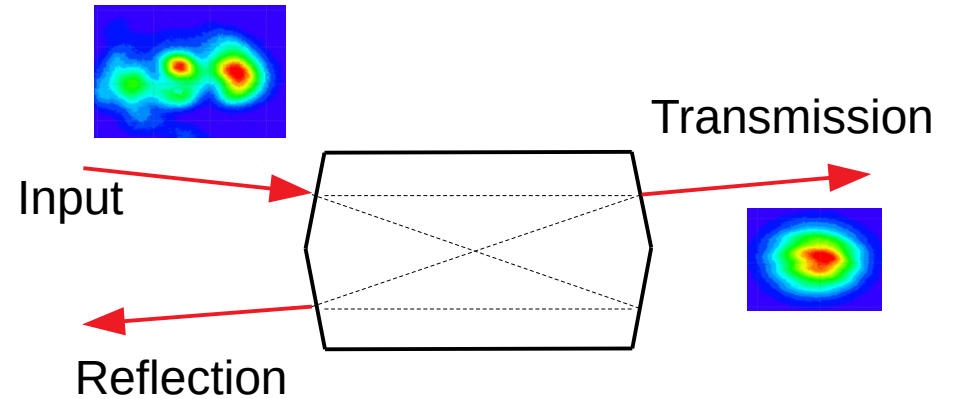
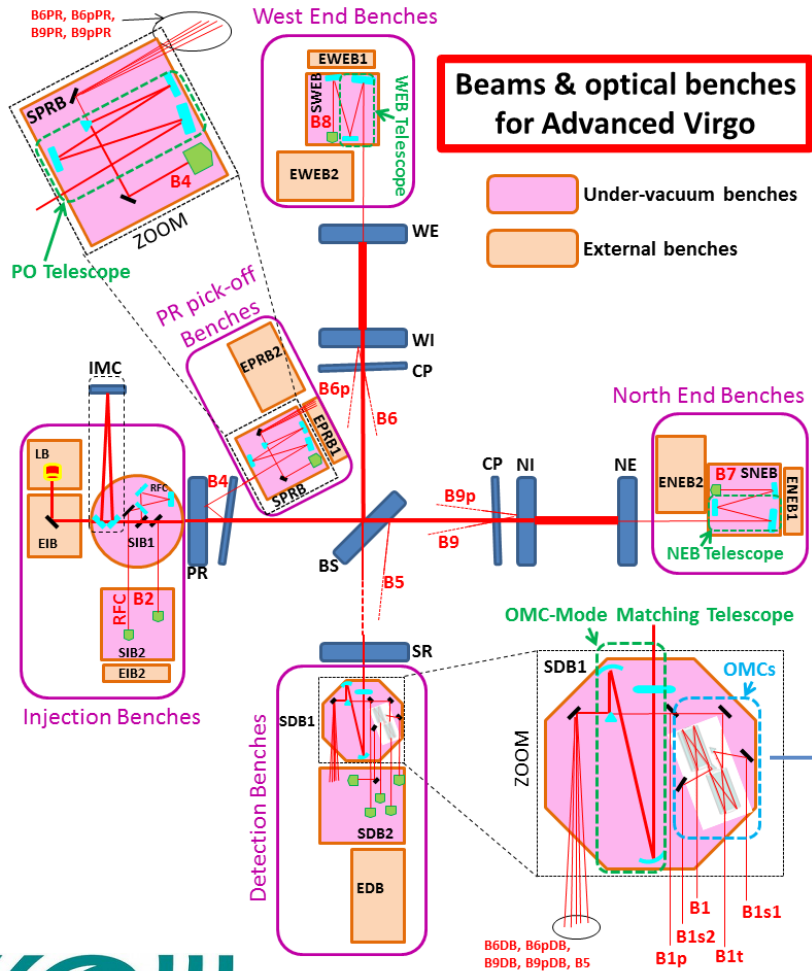


## Mode mismatch losses

The total MM requirement for FDS is 1%. We can conclude that mode mismatch due to diffraction is **negligible**.



AdV TDS: VIR-0518A-20

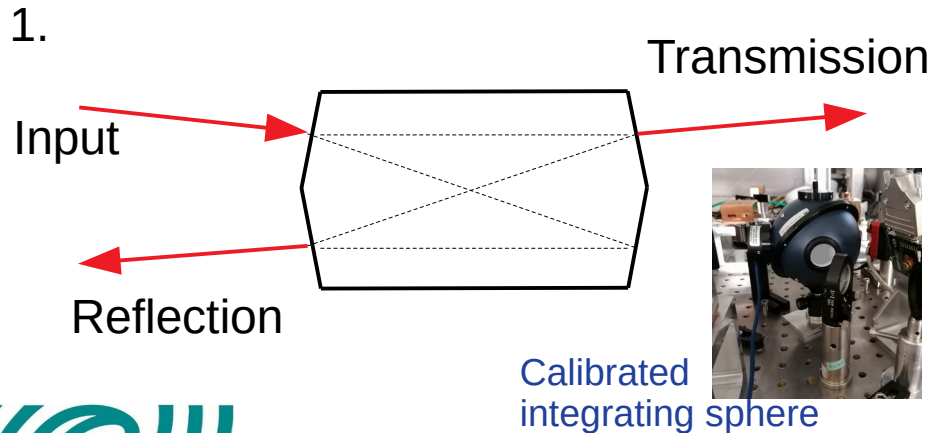
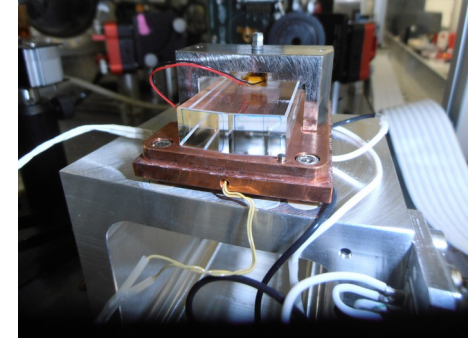


Characterized @ LAPP

Two Output Mode Cleaners (OMCs) will be replaced by 1 **High Finesse OMC** in Adv+

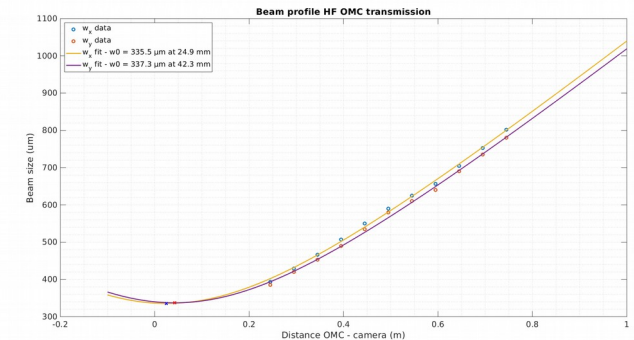
We are characterizing the OMC at LAPP:

1. **Losses = 3.5% ± 0.3 %** (during O3 Losses = 5%)  
 Losses = Input power – Transmitted power – Reflected power
2. Radius of Curvature ( $\rho$ ) of the spherical surface:  $\rho \sim 1700$  mm
3. High reflective coating residual transmission: few ppm



2.

$$w_0 = \sqrt{\frac{\lambda}{n\pi} \sqrt{2L_{geo}(\rho - 2L_{geo})}}$$

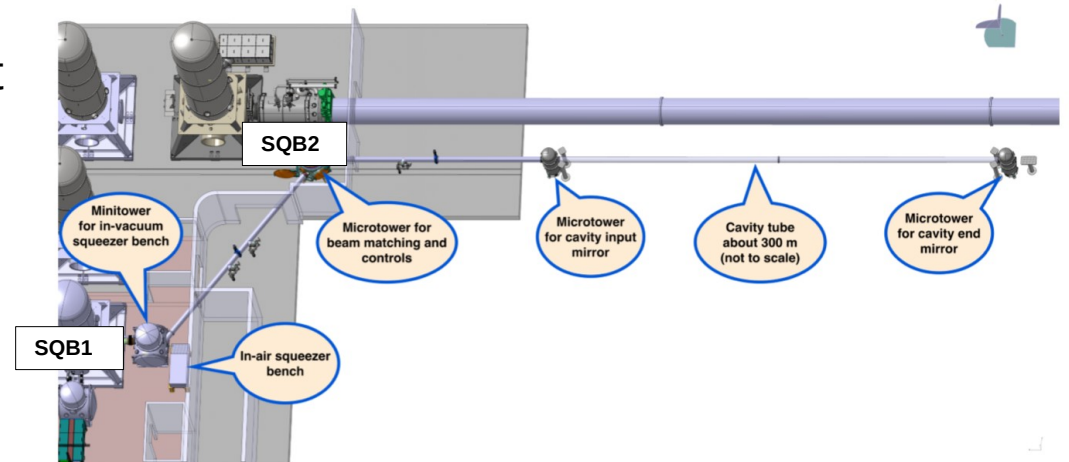


## Conclusions:

- ✓ Ghost beams study on Frequency Dependent Squeezing system
- ✓ Design of diaphragms and baffles
- ⚙ Construction of diaphragms and baffles
- ⚙ Mechanical installation of FDS system at Virgo
- ⚙ Characterization of OMC at LAPP

## Next steps:

- ✗ Pre-installation of SQB1 and SQB2 at LAPP (December 2020)
- ✗ Commissioning of the whole FDS system on site (beginning 2021)
- ✗ Commissioning of OMC on site (November 2020)
- ✗ Observing run O4 starts in 2022



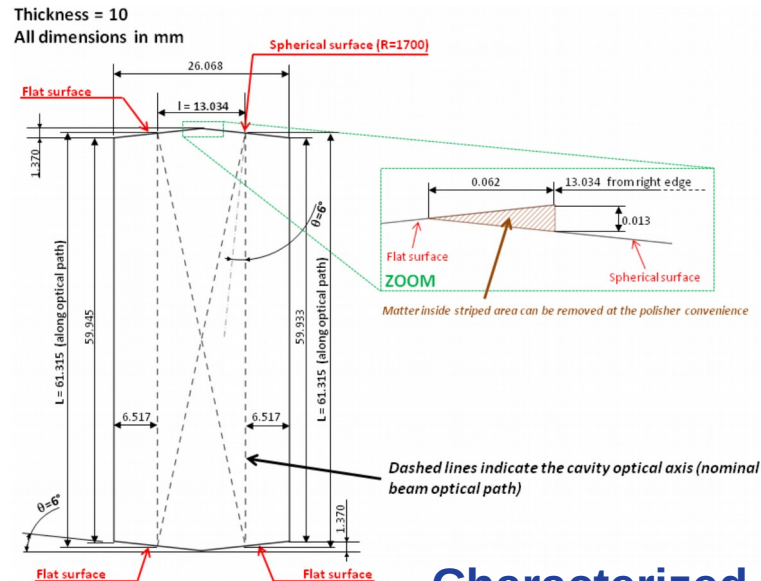
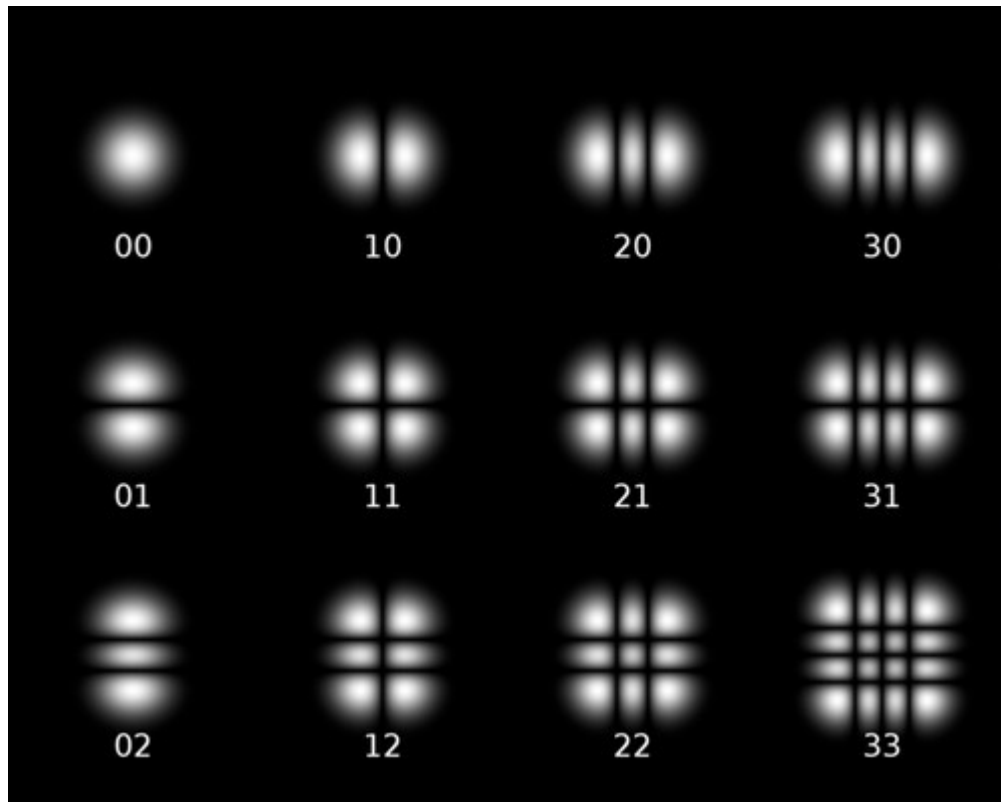




THANK YOU FOR THE ATTENTION

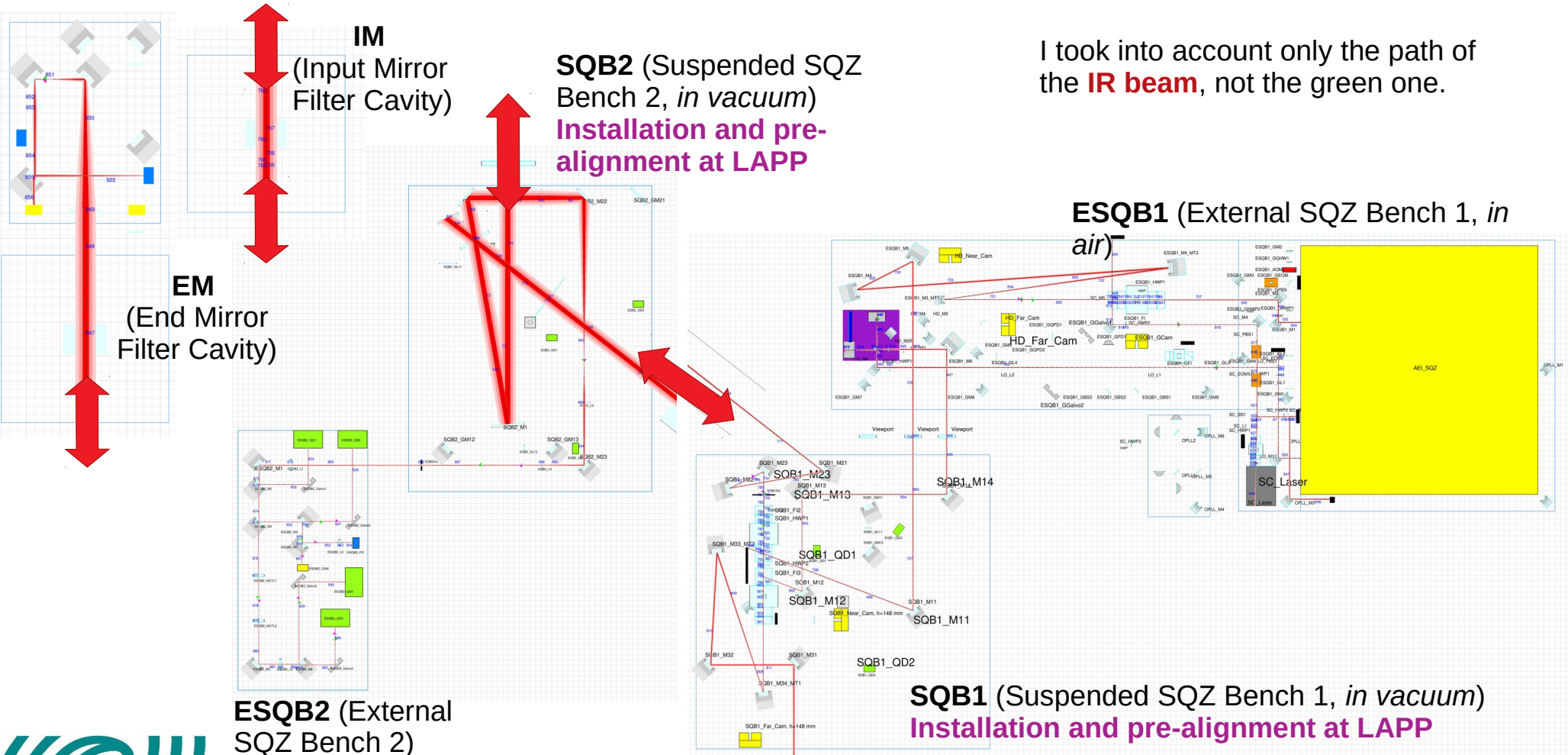


# EXTRA SLIDES



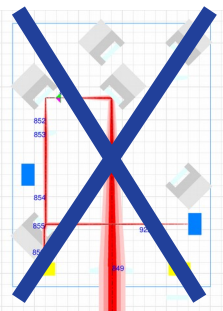
**Characterized @ LAPP**

Two Output Mode Cleaners (OMCs) will be replaced by 1 **High Finesse OMC** in AdV+

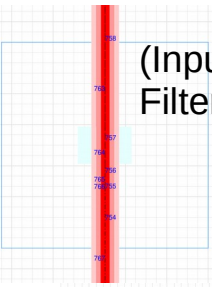


I took into account only the path of the **IR beam**, not the green one.

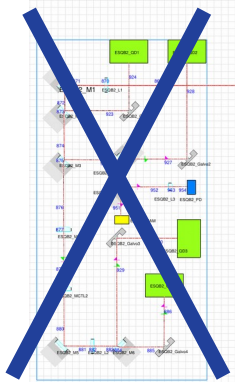




**IM**  
(Input Mirror Filter Cavity)

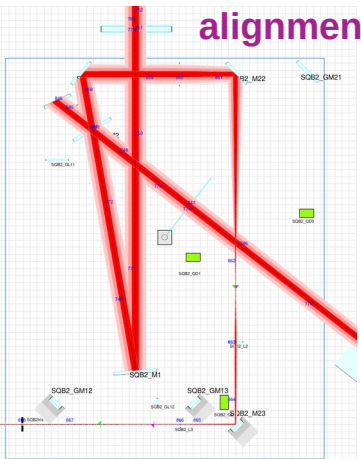


**EM**  
(End Mirror Filter Cavity)

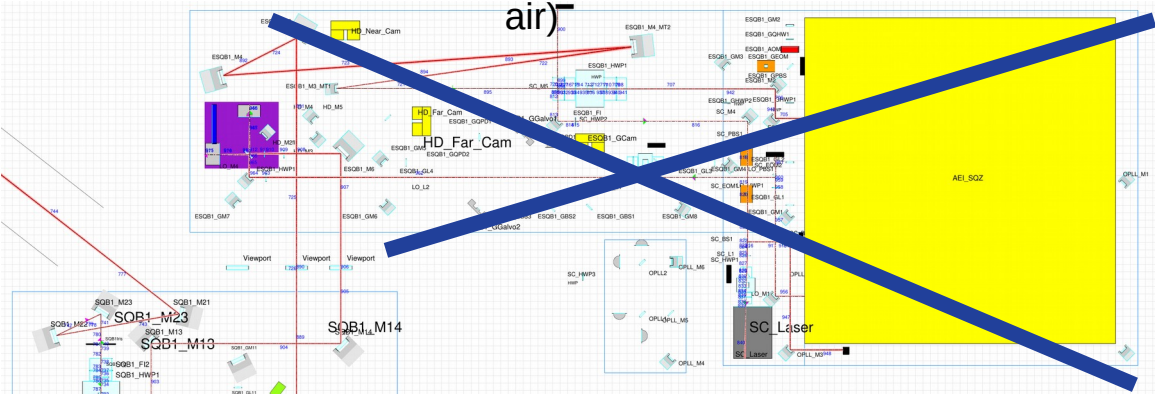


**ESQB2** (External SQZ Bench 2)

**SQB2** (Suspended SQZ Bench 2, *in vacuum*)  
Installation and pre-alignment at LAPP

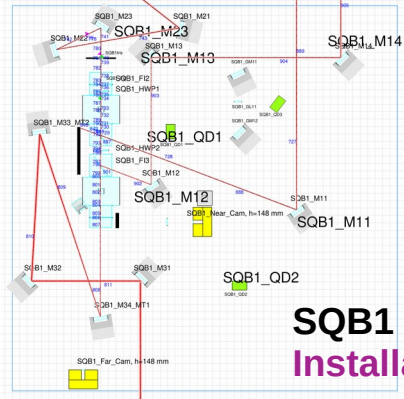


**ESQB1** (External SQZ Bench 1, *in air*)



Not studied yet.  
Less critical: **IN AIR**

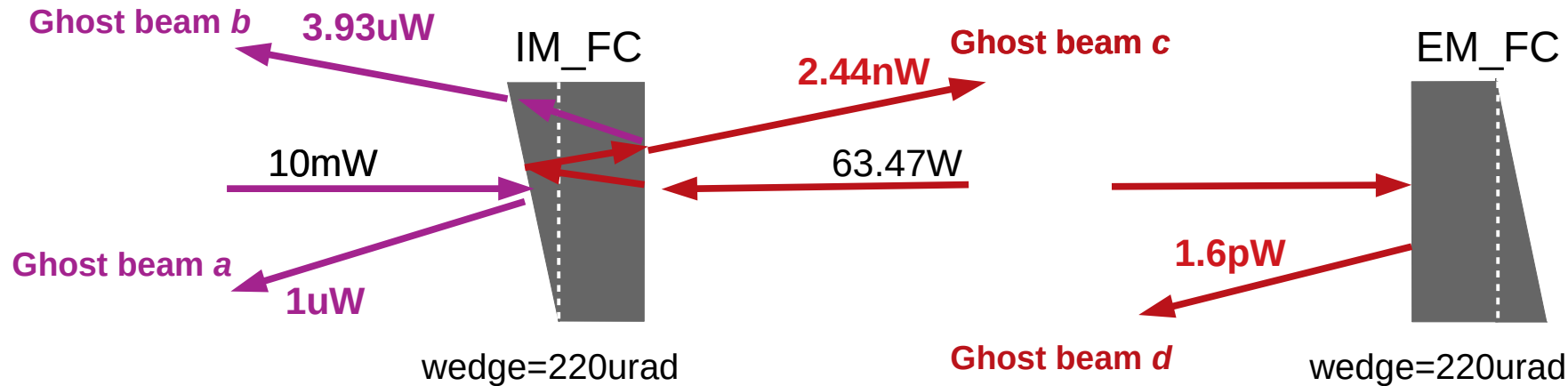
**SQB1** (Suspended SQZ Bench 1, *in vacuum*)  
Installation and pre-alignment at LAPP



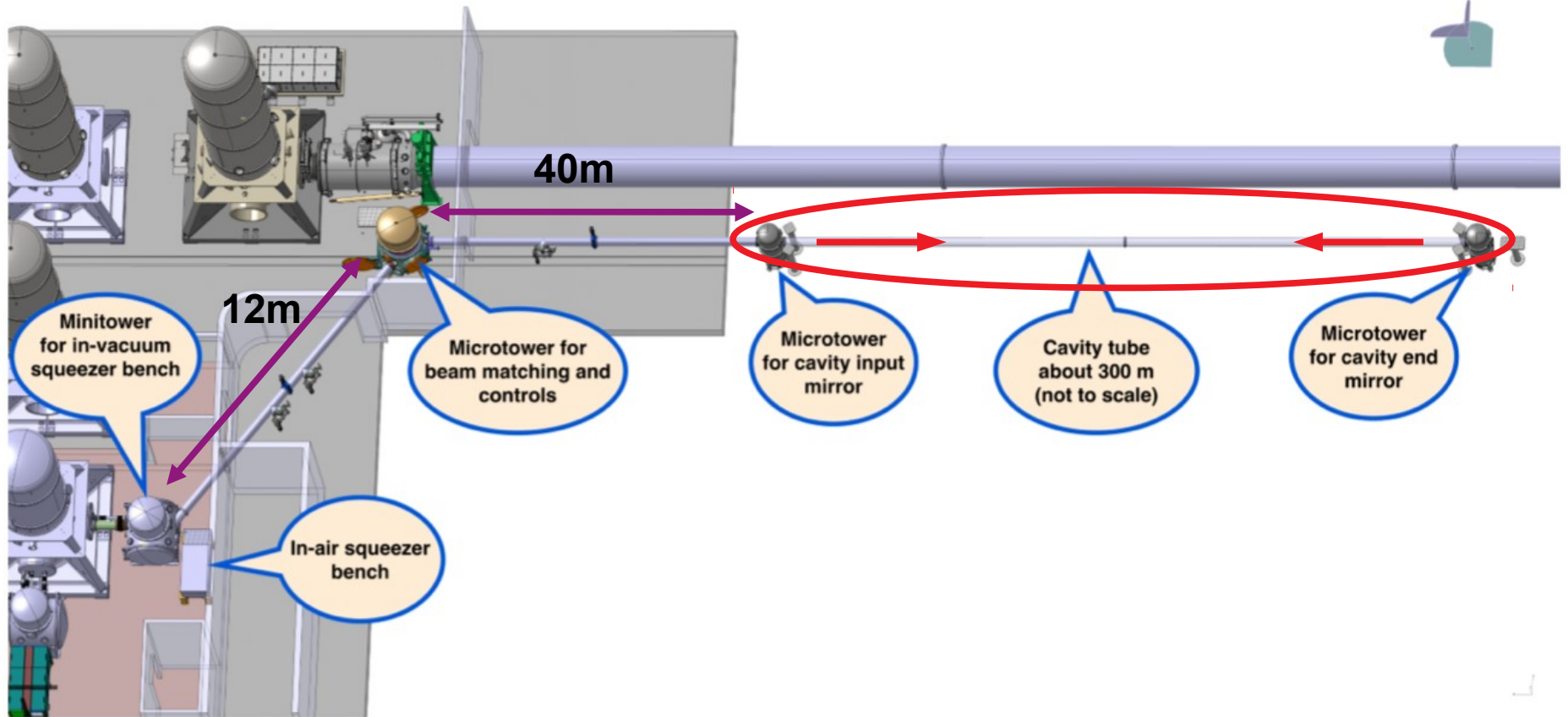
I studied the ghost beams propagation inside different tubes ([VIR-0585A-20](#)): **Filter Cavity** (both Input and End Mirrors), **Tube between SQB2 and FC**, **Tube between SQB2 and SQB1**. We are designing the **baffles** to install inside these three tubes.

## Filter Cavity ([VIR-0473A-20](#), [VIR-0584A-20](#)):

- These ghost beams are way **more powerful** than the others, so we need to dump them properly;
- *Ghost beams 'a' & 'b'* are dumped on **diaphragms on SQB1**;
- *Ghost beams 'c' & 'd'* are symmetrical and dumped on **baffles inside FC**.

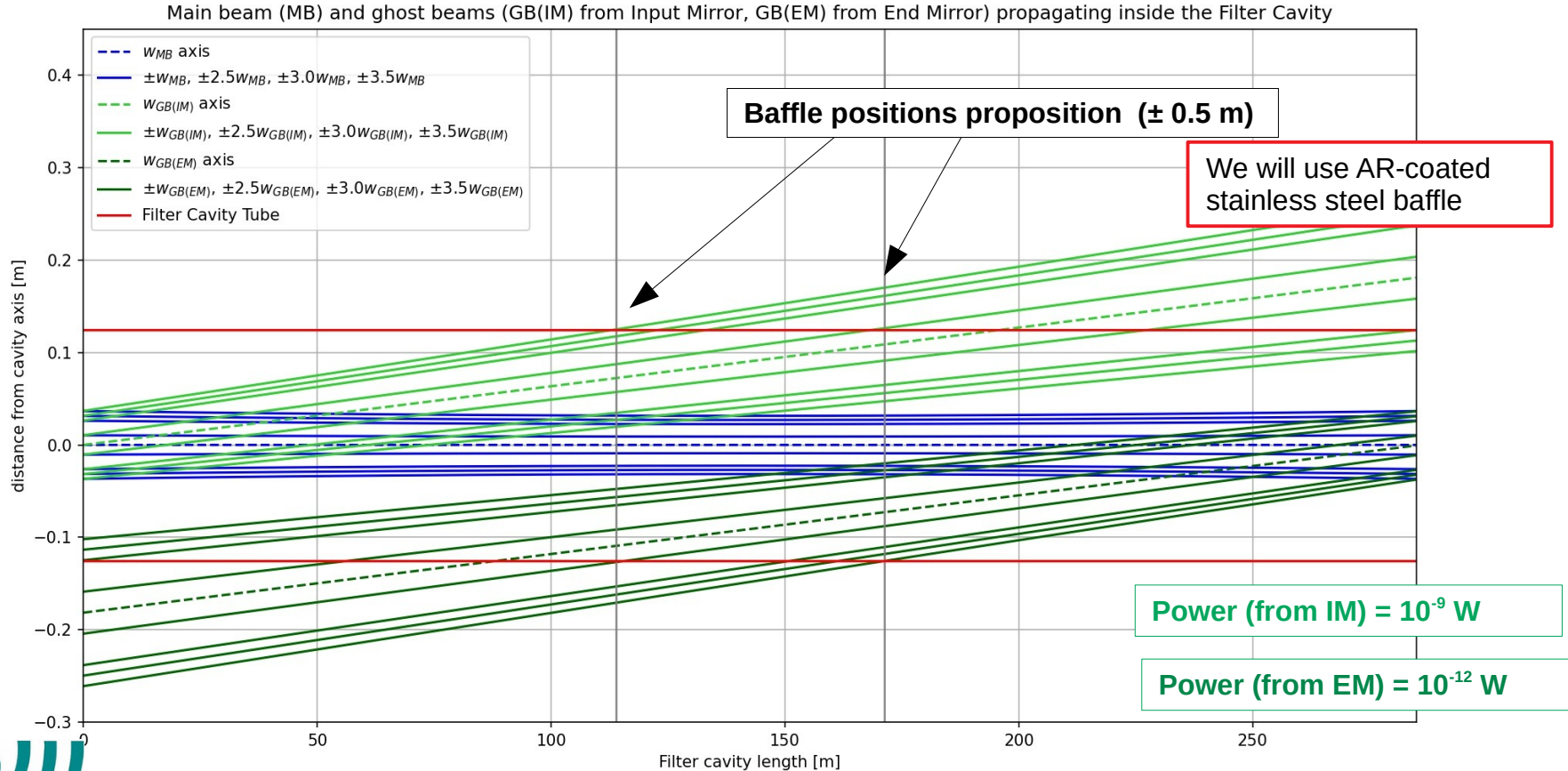


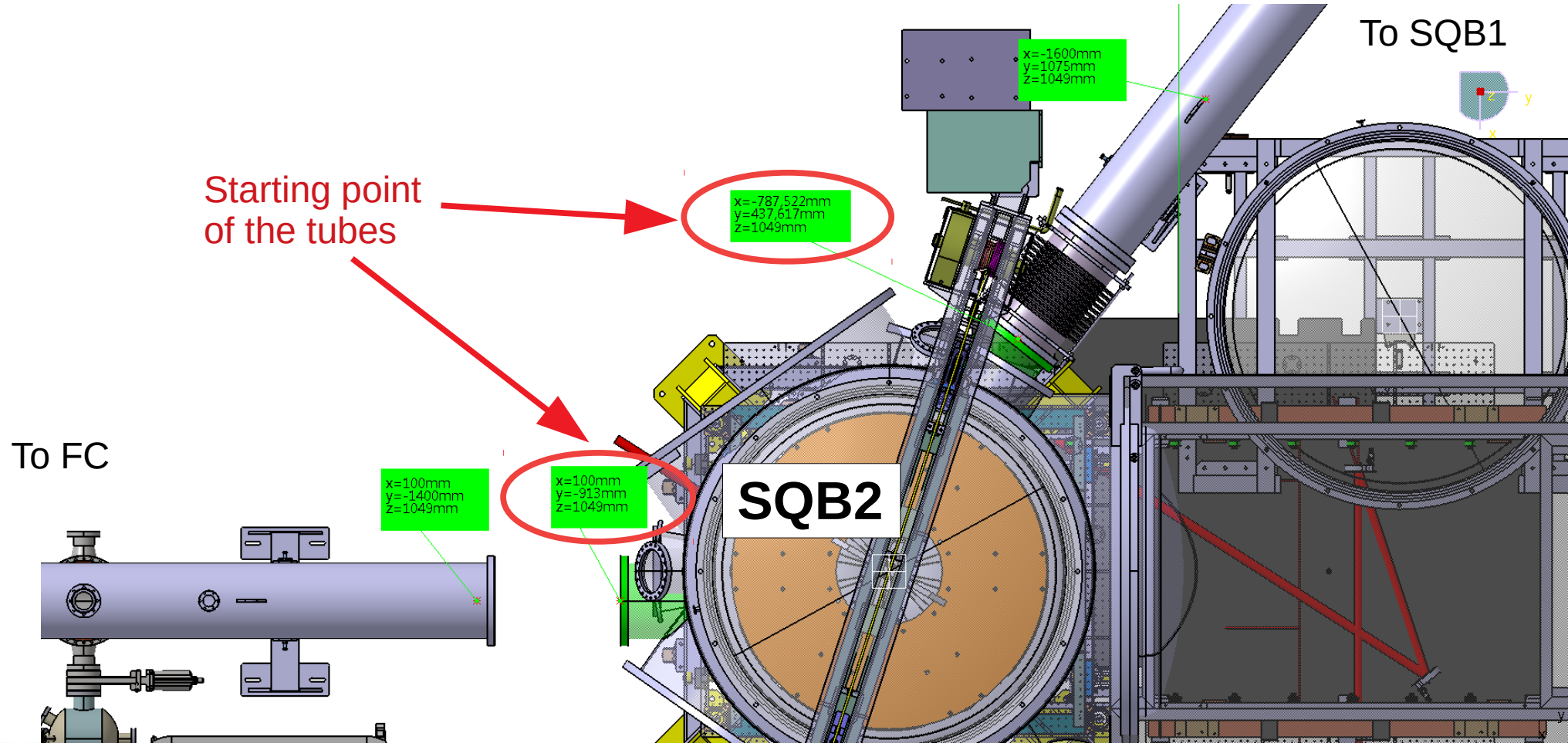




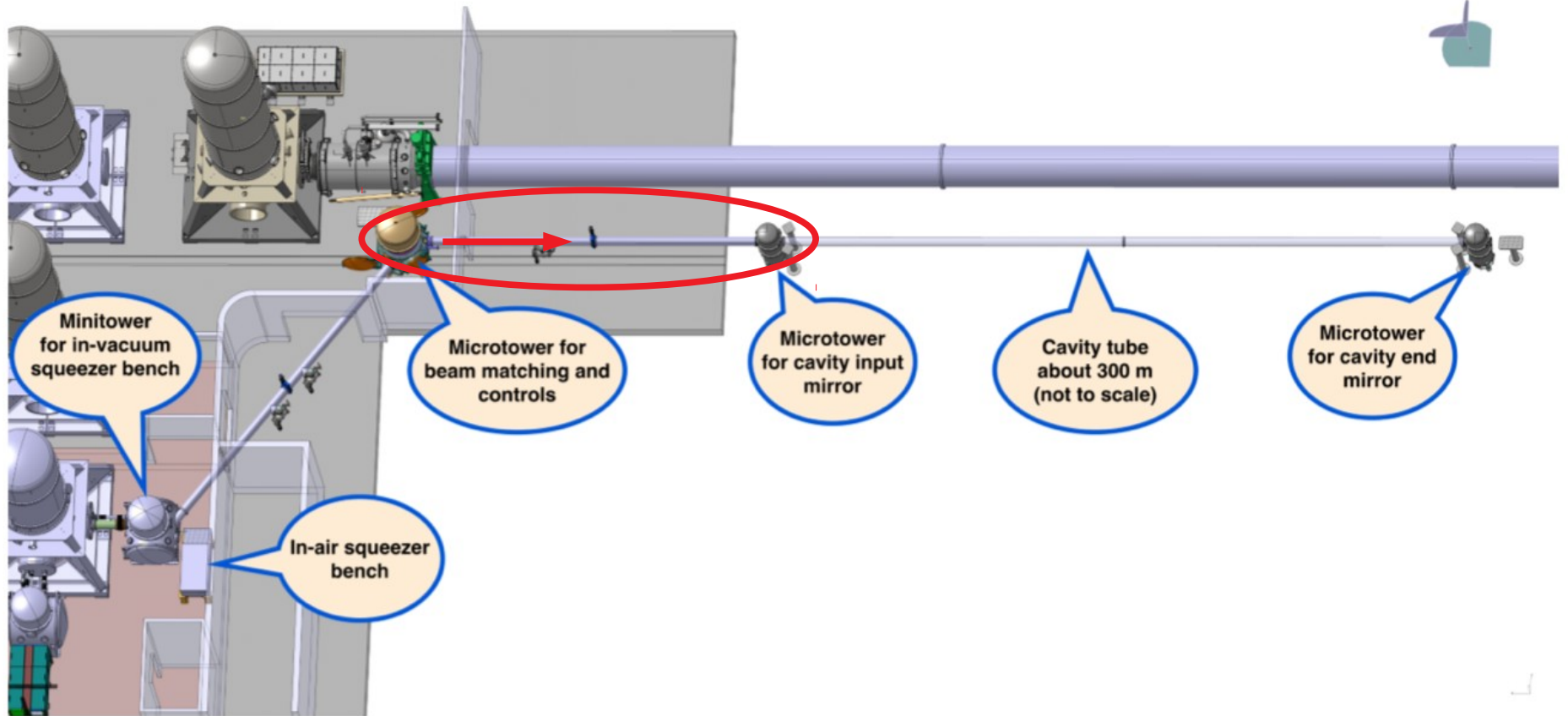
Discussion with FLT to install baffles at different locations inside the tube: **IN PROGRESS**.

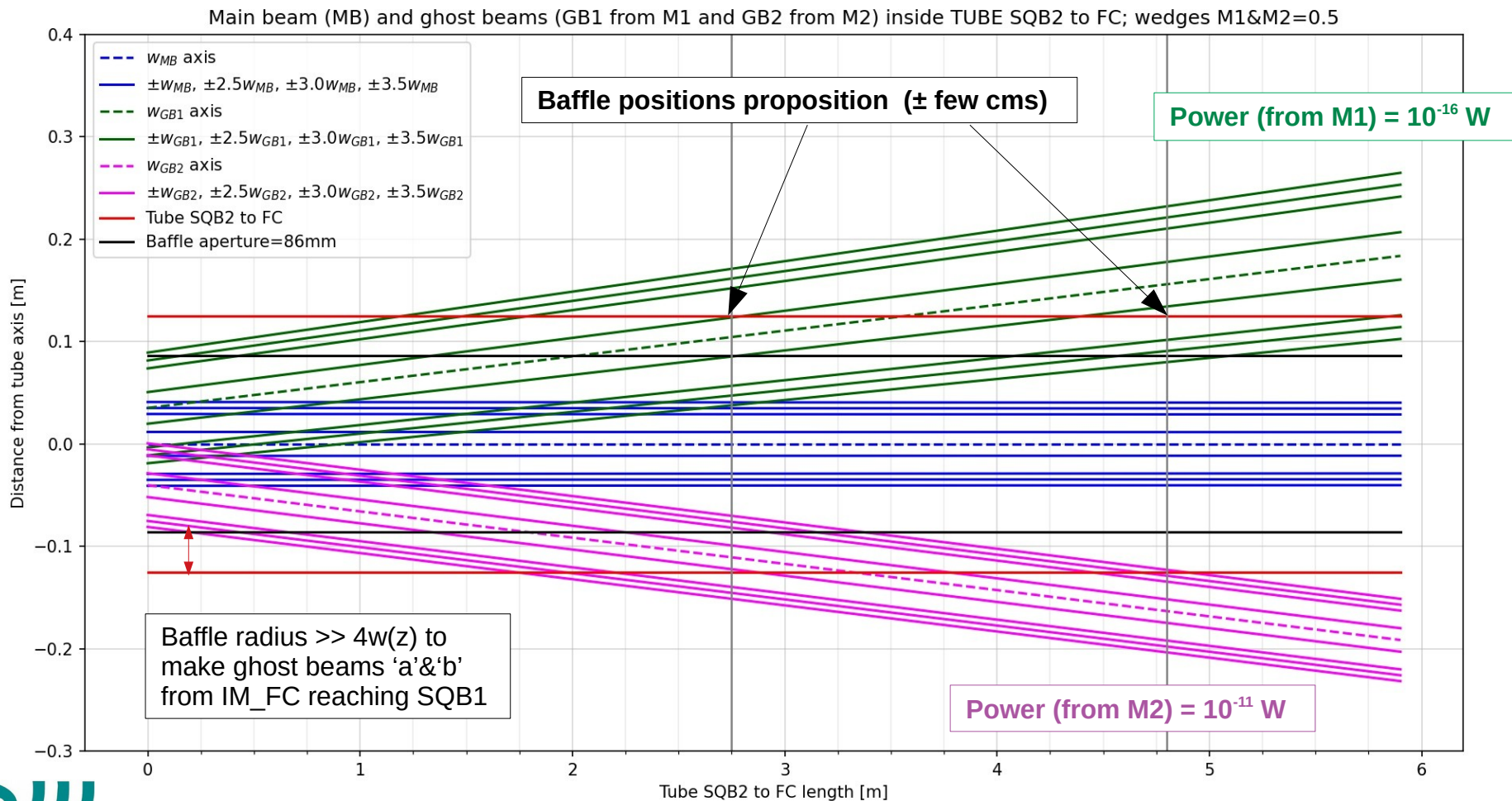
Constraints: available mechanical positions inside FC, do not cut the Ghost Beam in two with the baffle, minimize stray light etc.



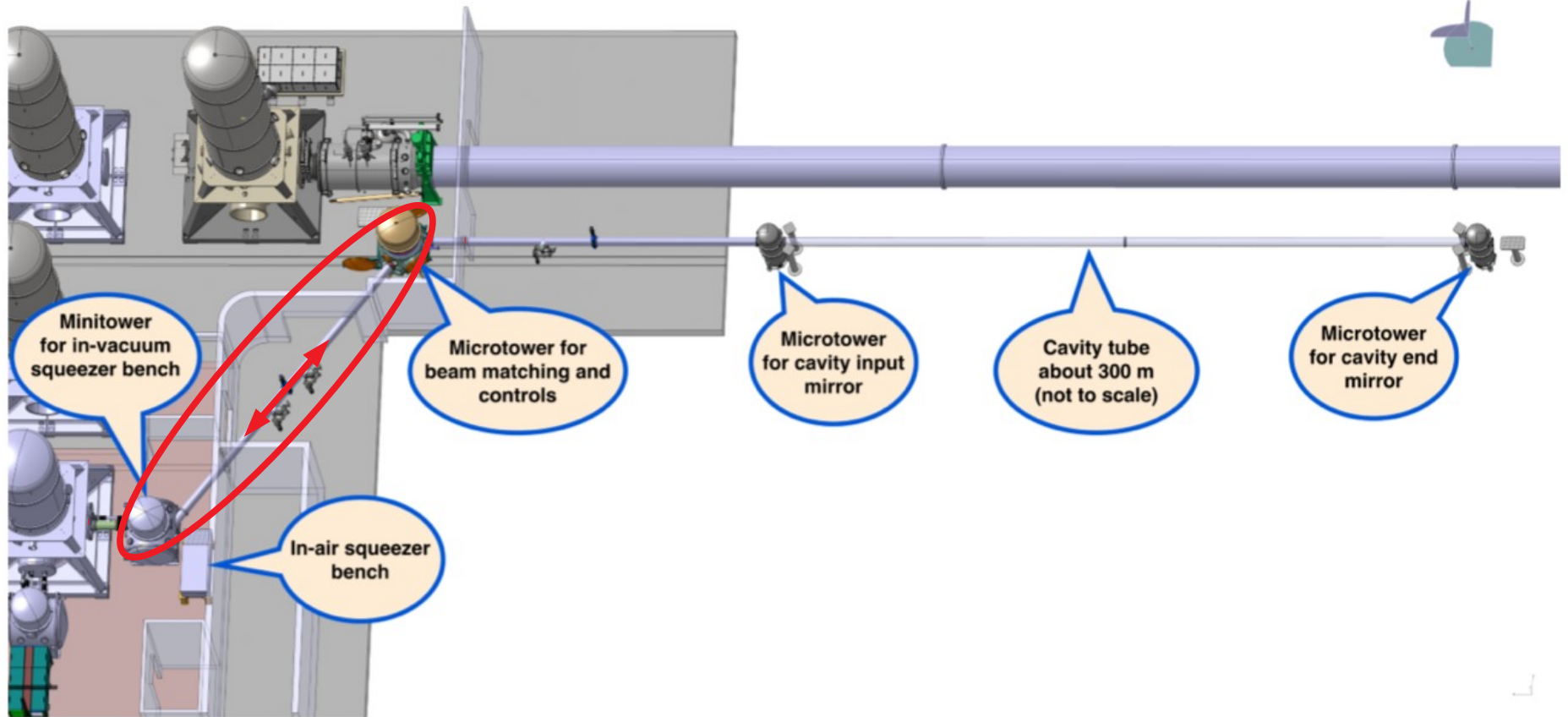


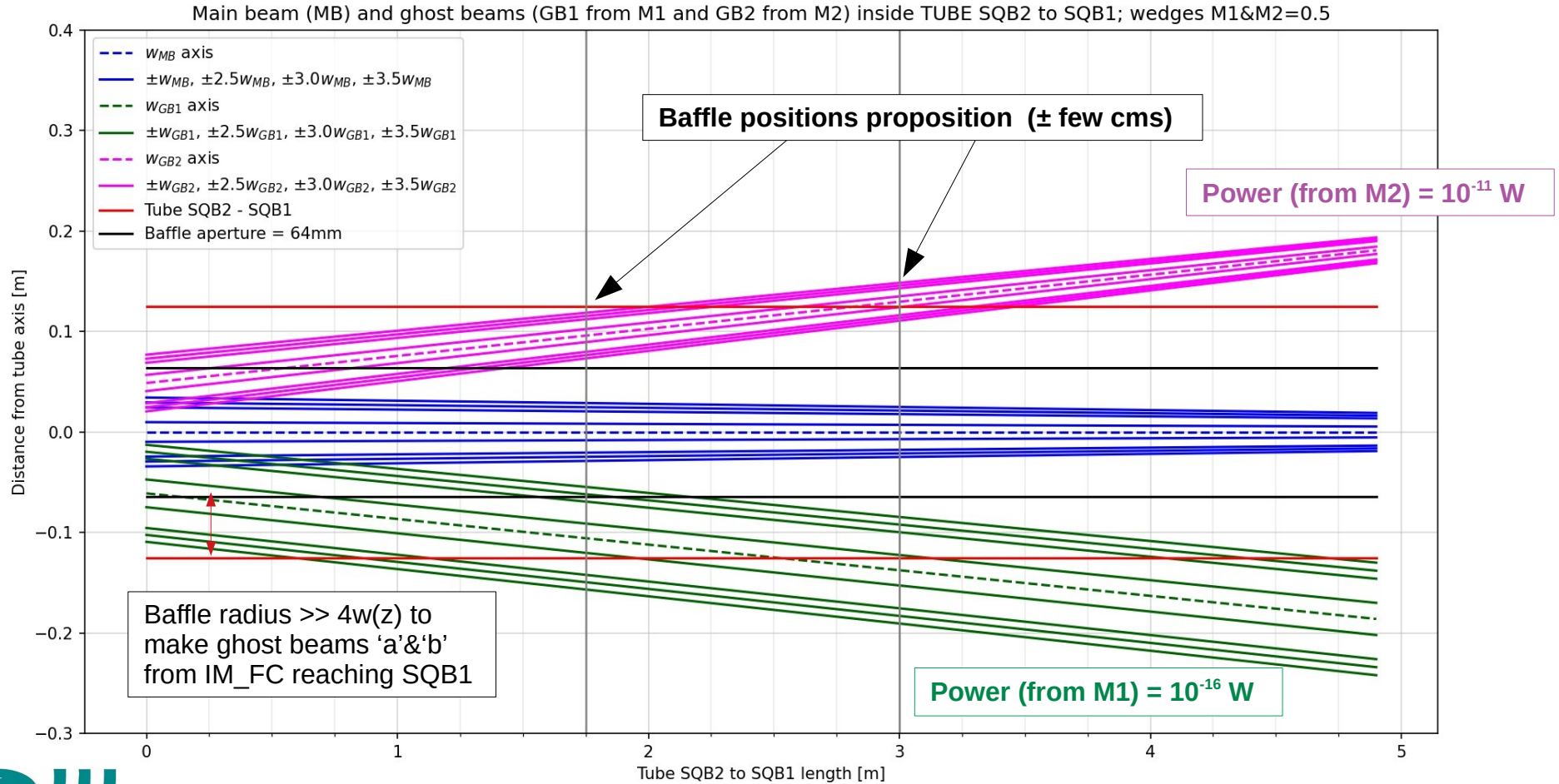


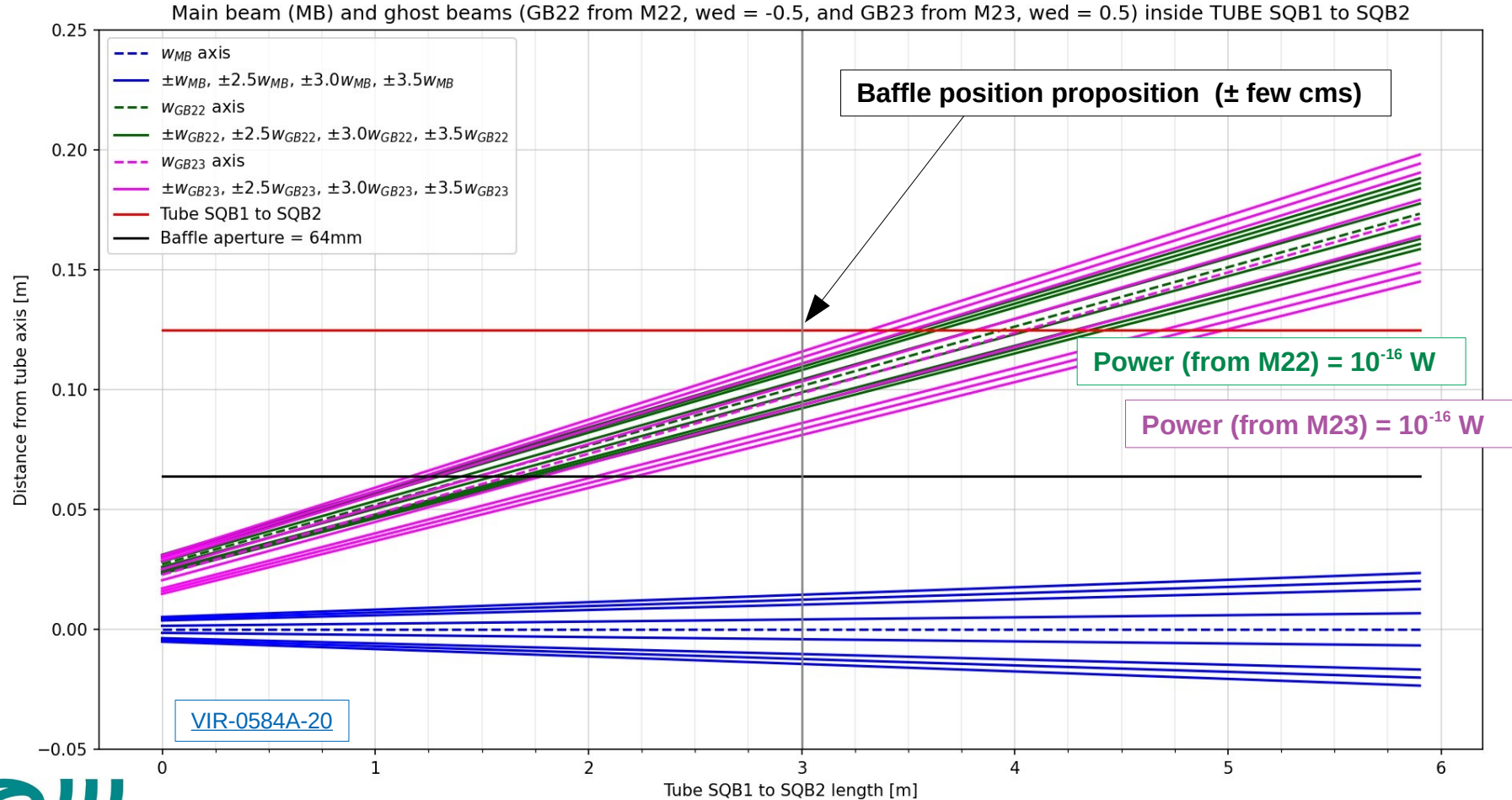








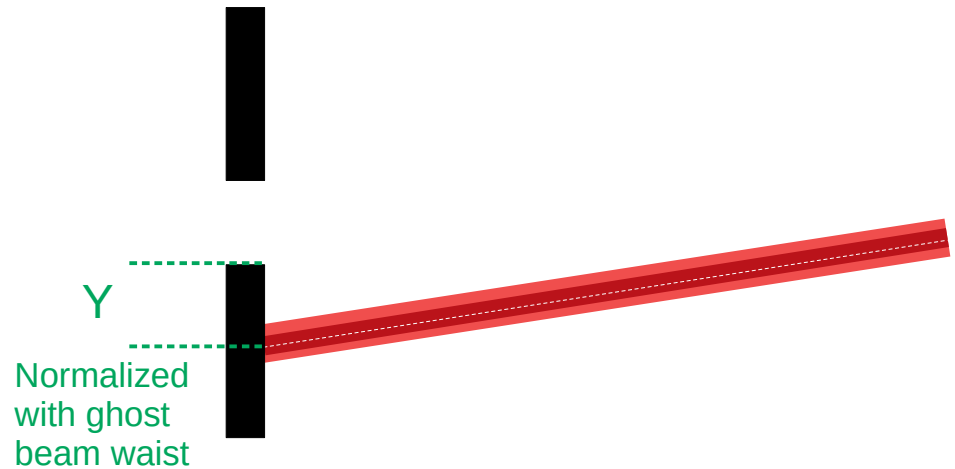
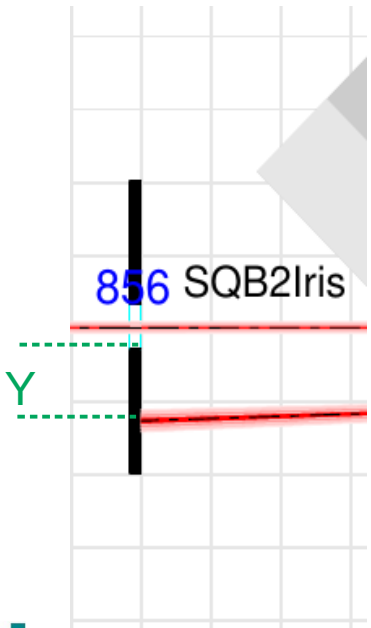




To understand if the ghost beams are stopped by diaphragms and baffles properly, we introduce a quantity  $Y$  defined as:

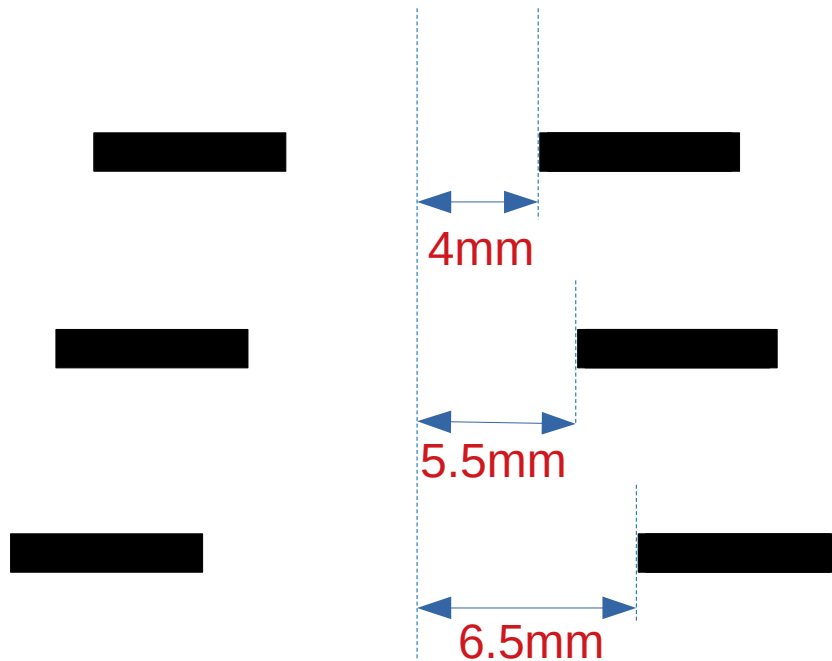
$$Y = (\text{distance ghost and main beams} - \text{aperture radius}) / \text{ghost beam radius}.$$

The fraction of ghost beam power passing through the aperture can be computed using the corrected error function  $\text{Erfc}(Y) = 1 - \text{Erf}(Y)$ .





I took 'standard apertures' in order to ease the production and installation processes.  
With  $a = 4, 5.5, 6.5$  mm we don't change the performances of diaphragms on benches.  
Concerning baffles, we need to consider stray light effect at the aperture edges.



We want  $a/w(z) = 3.5$  for diaphragms.  
I report this quantity using standard aperture radius.