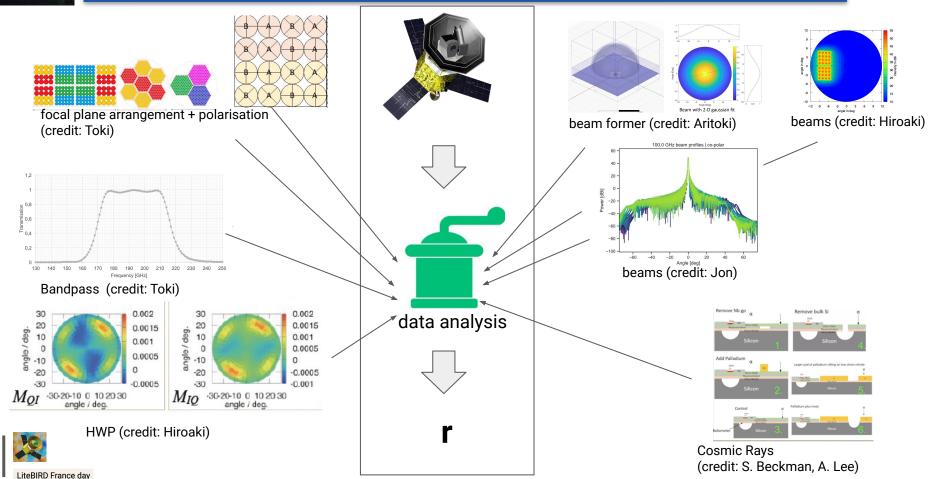
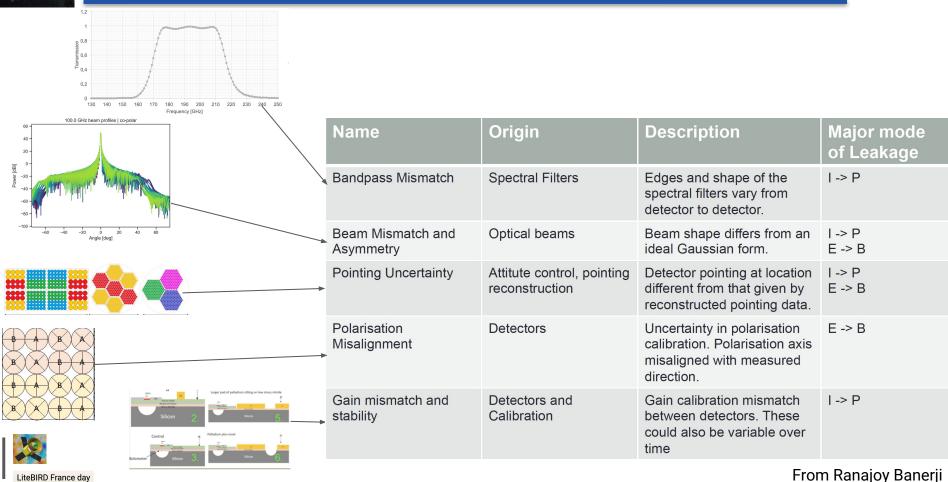




To get to r we need to know our instruments



Otherwise....



From Ranajoy Banerji



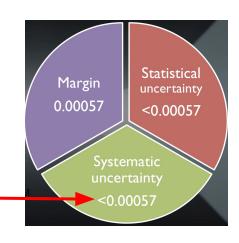
Up to which level?

We want to measure r with an accuracy of (68%CL):

$$\sigma_r = 0.001$$

Assuming:

$$(\sigma_r = 0.001)^2 = \sigma_{\text{syst}}^2 + \sigma_{\text{fg}}^2 + \sigma_{\text{margin}}^2$$



For each potential source of instrumental systematics:

- We assign an error budget: $\sigma(r)_{sys} < 5.7 \times 10^{-6}$ as the budget (1% of total budget for systematic error)
- From this we derive a requirement on the knowledge of the underlying instrumental parameters.



Those requirements are used to best define the calibration method.





A lot of studies have been performed

| ID | Item | sub- ID | Source | w/o HWP | w/ HWP | Comment |
|----|----------------------------|------------|---|------------|-----------|--|
| 6 | | 6-1 | Far side-lobes | V | √ | Beam knowledge: Leakage mainly from E to B, T to B may contribute |
| | | 6-2 | Near side-lobes | 1 | | Beam knowledge |
| | Beam shape | 6-3- | Main beam width | V, | V | Knowledge of the beam width |
| | | 1 | | V | v | |
| | | 6-3- | Main beam flattening | V | √ | Main beam ellipticity knowledge |
| | | 6-4 | Ghost | | 1 | Effect happening inside the 5K shell |
| | | 6-5 | cross polarization w/ | | V | Requirement to the knowledge of the cross po |
| | | 0.0 | HWP | | · | characteristics in beam |
| | | 6-6 | Diff. Beam Pointing btw. det. | √ | | Leakage from T to B |
| | | 6-7 | Diff. Beam ellipticity btw. det. | V | | Leakage from T to B |
| | | 6-8 | Diff. Beam width btw. | √ | | Leakage from T to B |
| | | 6-9 | det. Diff. Cross-pol btw. det. | V | | Leakage from E to B, similar to the pol. angle |
| | | 0.9 | Dill. Cross-por btw. det. | V | | offset |
| | | 6-10 | Diff. Side-lobes btw. det. | V | | Leakage from T to B |
| 7 | | 7-1 | HWP at 4f | | √ | Knowledge of 4f signal |
| | Instrumental | 7-2 | HWP at 4f side-band | | V | Direct leakage to the science band |
| | polarization | 7-3 | HWP at 2f leakage | | V | Leakage from $2f$ to $4f$ due to finite observing |
| | poiarization | | | | | time and non-linearity |
| | | 7-4 | HWP at harmonics | | V | Lekakage from 3f, 5f and so on to 4f |
| | | 7-5 | Optical system | V | | Differential effect in the optical system |
| 8 | Polarization efficiency | 8-1 | HWP modulation effi- ciency | | V | Knowledge of the HWP modulation efficiency |
| | emeiene, | 8-2 | Detector polarization ef- | V | V | Knowledge of the detector polarization effi- |
| | | | ficiency | | | ciency |
| 9 | Relative Gain | 9-1 | Variation in time (ran- dom) | V | √ | Random variation per 600sec. |
| | Gain | 9-2 | Variation in time (1/f noise like) | V | V | Requirement in fince |
| | | 9-3 | Inter frequency channels | V | √ | Related to FG subtraction, and Band pass effect ID=15 |
| | | 9-4 | Diff. gain btw. det.(bias) | V | | Leakage from T to B |
| | | 9-5 | Diff. gain btw. det. (ran- dom) | V | | Leakage from T to B |
| 10 | Absolute | 10-1 | dom) | V | V | No E to B as Parity conserved. Related to the |
| 10 | Gain | 10-1 | | v | v | Pol. efficiency in ID=8 Calibration with CMB dipole. Absolute power of Cl, i.e., the absolute value of r |
| 11 | | 11-1 | Offset | V | V | E to B Expectation value from Vender's info. |
| | Pointing | 11-2 | Time variation in ran- | V | V | Disturbances in time uncorrelated way: Perhaps in a way that all the FC plane detector coher- |
| | | | | | | ently |
| | | 11-3 | Time variation in time with 1/f | V | V | Disturbances in time correlated way: |
| | | 11-4 | Time variation with HWP rotation | | V | Wedge in transmissive HWP, tilt of the rotation axis of reflective HWP |
| 12 | | 12-1 | Absolute Polarization angle | V | √ | Using CMB channels with C_i^{EB} . |
| | Polarization angle | 12-2 | Relative Polarization an- gle | V | V | Inter frequency channels, inter detectors |
| | | 12-3 | Polarization leakage in- trinsic to HWP | | √ | knowledge of M_{QU} or M_{UQ} in Mueller matrix |
| | | 12-4 | Polarization leakage due to HWP position error | | V | Requirement to the knowledge to the HWP ro- tation position |
| | | 12-5 | Variation in time (white like, 1/f like) | √ | √ | Variance of pol. angle determination by STT |
| | | | | | | |
| 13 | | 13-1 | Individual Detector w/o | V | | Detector originated |
| 13 | | 13-1 | | √ | | Detector originated |

| | | 13-2 | Individual Detector after demodulation | | √ |
|----|------------------------|------------|--|-----|-----|
| | | 13-3 | Common mode | V | |
| | | 13-4 | Inter channels | V | |
| | | 13-5 | Noise modeling | V | √ |
| | | 13-6 | HWP temperature varia- | | √ |
| | | | tion in time with 1/f like for monopole | | |
| | | 13-7 | HWP temperature vari- | | √ |
| | | | ation in time with 1/f noise for 2f | | |
| | | | | ļ., | ١, |
| 14 | Cosmic ray glitches | 14-1 | Common mode Data acquisition (includ- | V | V |
| | ginenes | 0000000 | ing data compression) | | v |
| 15 | | 15- | Frequency shift of the | V | |
| | | 1-1 | band w/o HWP in differ- entiation. | | |
| | | 15- | Frequency shift of the | V | V |
| | Band pass | 1-2 | band | | 100 |
| | effect | 15- 2-1 | Band shape w/o HWP | V | |
| | | 15- | Band shape | V | √ |
| | | 2-2 | | | |
| | | 15- 3-1 | Beam shape in band w/o HWP | V | |
| | | 15- 3-2 | Beam shape in band | ٧ | V |
| | | 15- 4-1 | Pol. angle wobble in band | V | √ |
| | | 15-5 | Gain variation in band | V | √ |
| | | 15-6 | Instrumental Polariza- tion in band | | V |
| | | 15-7 | Polarization efficiency in band | | V |
| | | 15-8 | Outer band | V | V |
| 16 | Transfer | 16-1 | Detector time constant knowledge | V | V |
| | function | 16-2 | Digital filter in readout system | V | V |
| | | 16-3 | Cross-talks | V | V |
| | | 16-4 | Time constant variance in time coupled to HWP revolution | | V |
| 17 | | 17-1 | Detector response: pa- | V | V |
| | Non- | | rameterized as g in a | | |
| | | | model of $(1 + gd(t))d(t - \tau d(t))$ | | |
| | | | | | + - |
| | linearity | 17-2 | Variation in time on g, | V | V |
| | | 17-2 | white like or 1/f like HWP 2f synchronous: | ٧ | V |
| | | | Variation in time on g, white like or 1/f like HWP 2f synchronous: leakage from 2f to 4f | V | 1 |
| | | | white like or 1/f like HWP 2f synchronous: leakage from 2f to 4f time constant τ [sec/uK] | V | 1 |
| | | 17-3 | white like or 1/f like HWP 2f synchronous: leakage from 2f to 4f time constant τ [sec/uK] in the PB model (1 + | | V |
| | | 17-3 | white like or 1/f like HWP 2f synchronous: leakage from 2f to 4f time constant τ [sec/uK] | | V |

| T | in req. flow L3.08 1/10 of white noise at the |
|---|--|
| 1 | spin frequency 0.1rpm=1.6mHz |
| + | Common mode in FP With FG component separation |
| + | Requirements to determine the noise stationar- |
| | ity; how long period the noise to be stable |
| | Loading from HWP changes the detector noise, |
| | the time correlated variation would cause the 1/f |
| 1 | noise |
| | Differential emissivity in the two axes will pro- duce $2f$ signal. The $1/f$ time variation of HWP |
| | temperature produces the fluctuation of the 2f |
| | which may be leaked to the 4f. Note that the |
| | multi-layer stacked AHWP may smear out this |
| 1 | effect. |
| + | Wafer base due to phonon propagation |
| | Additional noise due to down-sampling, Data compression |
| + | Band shift in a detector pair |
| | pau |
| | |
| T | Knowledge of the band position |
| + | Port of the transfer of |
| | Diff. of the band shape in a detector pair |
| + | Knowledge of the band shape |
| | Knowledge of the band shape |
| + | Diff. of frequency dependence of beam shape in |
| | band, caused by the spectrum difference. Cali- |
| 1 | bration using planets may cause difference |
| | Frequency dependence of beam shape in band, |
| | caused by the spectrum difference. Calibration using planets may cause difference |
| + | Sinuous antenna wobble, may be canceled out |
| | using combination of Q/U and two sides |
| Ť | Gain calib. using CMB dipole may differ from |
| 1 | that of FG due to spectrum diff. |
| | Frequency dependence of IP in HWP |
| + | Related to the frequency dependence of the |
| | HWP retardance and/or sinuous antenna re- |
| | sponsivity |
| + | Contamination from the outside of frequency |
| 1 | band. |
| | Detector time constant |
| + | Possible effect in time correlated way which |
| | cause the spatial correlation |
| + | Cross-talks in frequency domain |
| + | random 1/f type variation in time |
| | |
| + | A |
| | Assuming maximal loading to the instrument in uK to set the working position |
| | are to set the working position |
| | |
| + | Non-stationarity of the non-linearity due to the |
| 1 | change of the loading position |
| | May be related to ID=7, causing leakage to 4f, |
| | due to large 2f signal, To be related 2f emission in 18-1-2 |
| + | Knowledge of the time response τ |
| | e or the inner response t |
| | |
| | |
| † | Possible time dependence of the time constants |
| 1 | Possible time dependence of the time constants Possible effect in data compression process |

| 18 | Non- uniformity in HWP | 18- 1-1 | Transmissive HWP | | V | Azimuthal angle dependence in oblique inci- dence of light |
|----|--|------------|---|---|---|--|
| | | 18- 1-2 | Differential emissivity of transmissive HWP | | V | Production of 2f signal, can be leaked to 4f with the position dependence. |
| | | 18-2 | Reflective HWP | | V | Azimuthal dependence in oblique incident an- gle. We will not consider this source. |
| | | 18-3 | Position dependent HWP temperature fluc- tuation in white noise like | | V | Increase the detector noise. We do not consider this source as this is related to the reflective HWP. |
| 19 | Uncertainties difficult to model and simulate | 19-1 | Multiple reflection be- tween HWP and FP | | V | Requirement to HWP AR. Two ways: back-of- the envelope calculation to get first order reg. In GRASP, the multiple reflection with HWP is difficult to simulate. One way is to measure the beam pattern w/ and w/o HWP using the real instruments. |
| | | 19-2 | fknee | ٧ | | 1/f noise f _{knee} is unknown unless the real in- struments are tested, assigned for the case w/o HWP |
| | | 19-3 | Gain variation | ٧ | V | Actual gain variation strongly depend on the in- strument environment, and difficult to model in a simulation |
| | | 19-4 | FG spectrum and un- | V | V | Unknown features of the spectra and compo- |

Table 4.1. List of sources of systematics identified so far. We add mark(s) to individual systematic sources relevant to the options with and without HWP. The column of Δr or σ , shows the expected error of r. Details are given in each section. N.A. means "Not Available" for the sources that we have not yet studied and assign the 1% error budget of 5.6×10^{-6} as the requirement. The ID=13 (1/f noise) shows the σ_r values, while other sources show Δr values.

credit: Concept Design Report

The requirements are being and will be updated and further refined

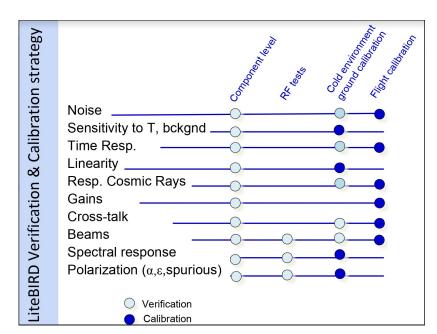




How? verification and calibration strategy

To reach the required accuracies the calibration strategy is setup in several steps. We will rely on measurements:

- on the ground and in-flight
- from component level to full integrated instruments





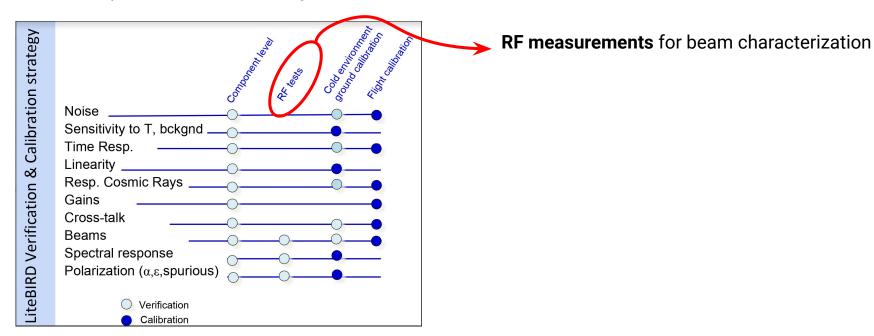
LiteBIRD France day



LiteBIRD verification and calibration strategy

To reach the required accuracies the calibration strategy is setup in several steps. We will rely on measurements:

- on the ground and in-flight
- from component level to full integrated instruments



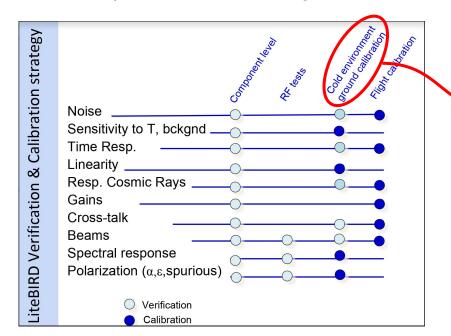




LiteBIRD verification and calibration strategy

To reach the required accuracies the calibration strategy is setup in several steps. We will rely on measurements:

- on the ground and in-flight
- from component level to full integrated instruments



RF measurements for beam characterization

Cold environment "flight-like" loading conditions on the instruments+calibration sources in a big cryogenic facility



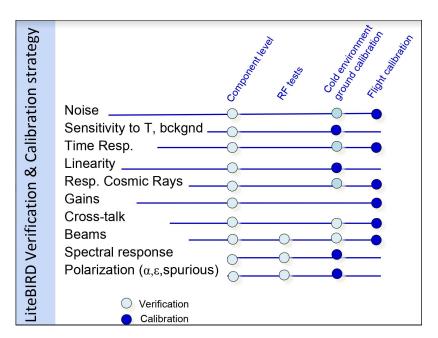
LiteBIRD France day



LiteBIRD verification and calibration strategy

To reach the required accuracies the calibration strategy is setup in several steps. We will rely on measurements:

- on the ground and in-flight
- from component level to full integrated instruments



RF measurements for beam characterization

Cold environment "flight-like" loading conditions on the instruments+calibration sources in a big cryogenic facility

=> In this talk I will focus on:

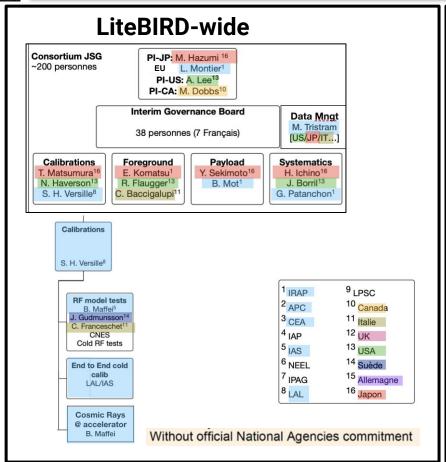
- Beams
- Spectro-polarimetry
 (and will not address component level tests)

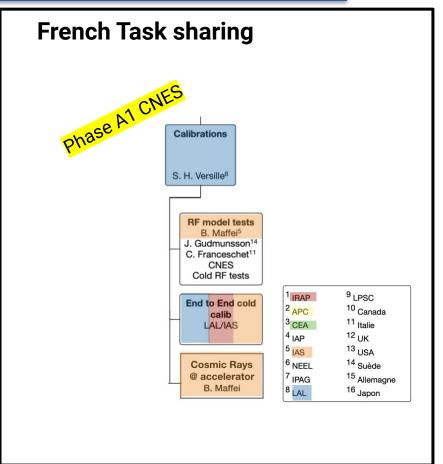






French responsibilities in calibration activities









Schedule for calibration operations

mid. 2021: RF tests on DM

beg. 2023: EQM cold calibration

end 2023: EQM to JAXA

beg. 2025: FM cold calibration

mid. 2025: FM to JAXA

DM: Demonstration Model

EQM: Engineering/Qualification Model

FM: Flight Model

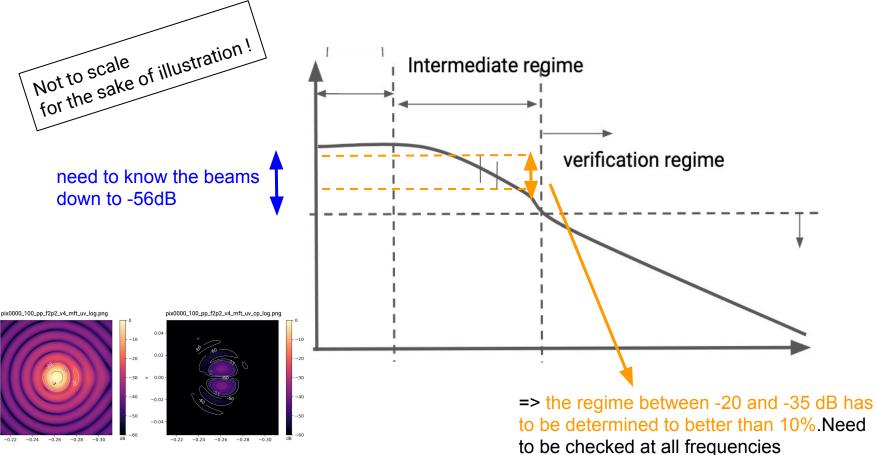




-0.02

credit: the MHFT Optics working group (Jon et al.)

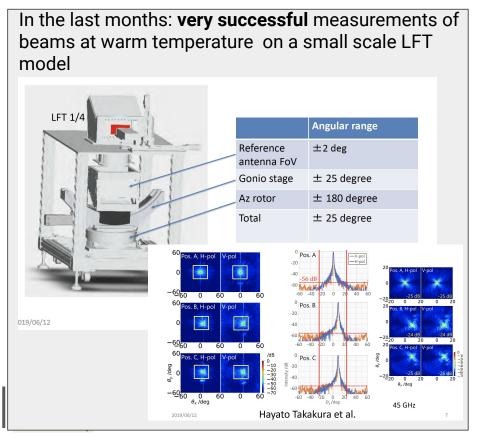
Beams requirements (so far)

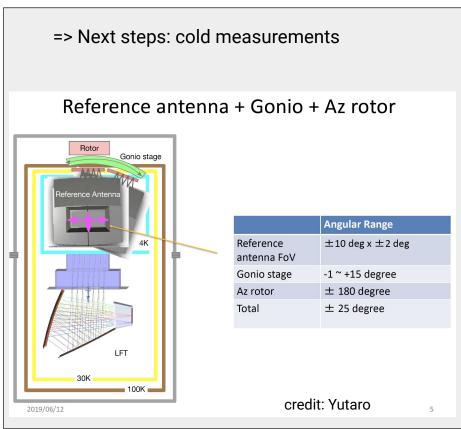




RF ground measurements for LFT

The full strategy is being addressed and further refined with on-going measurements in Japan







Challenges of the RF measurements for MHFT

The properties of the lenses (indices of refraction) depends on the temperature

AND

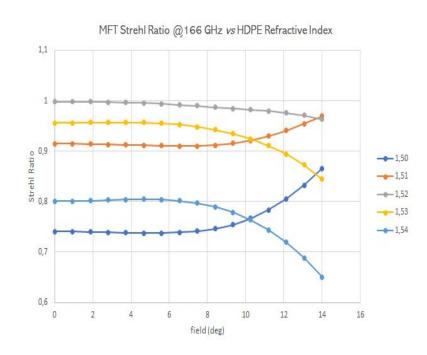
the beam shape depends on the properties of the lenses



we need to cool down the instrument to measure the beams!...



Then the question is...far field cold measurement or near field cold measurement: how to define the best strategy?



Eg: Strehl ratio for various refraction indices of lenses (typical of cold->warm variations)



RF ground measurements for MHFT

We are currently studying the best strategy, to build up a model fed with:

sub-system, semi-integrated and integrated level measurements

warm/cold measurements

credit: the MHFT RF working group (<u>Bruno</u>, <u>Jon</u>, <u>Cristian</u> + <u>Hiroaki</u>, Marco, Marco, <u>Ludo</u>, <u>Baptiste</u>, <u>Sophie</u>)

+ CNES CATR team

Marco, Hiroaki

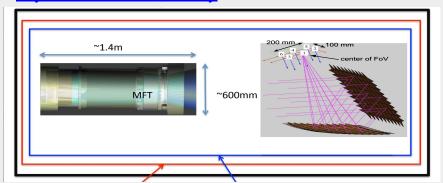
On-going work at CNES/Toulouse:

Antenna models will be built on the basis of MHFT beam simulations (optics group) for 100 to 402 GHz => to be further characterized with the use of submm source in the CATR to perform a feasibility study in CNES facilities.



Modèle de vol de Saphir, instrument du satellite Megha-Tropiques, en essais en BCMA

Cryo tests far field study



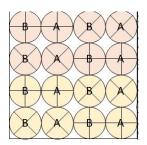
Far field measurements are what we need at the end!

- => near field @ cold? (intensity and phase to translate to far field)
- => or directly measure the intensity in the far field ?

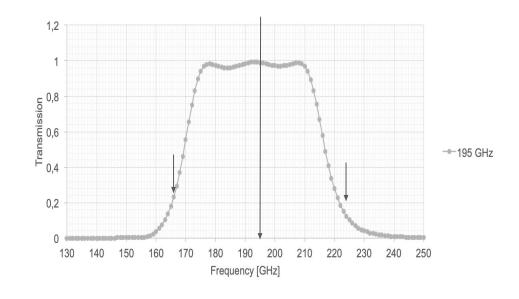
=> feasibility study on-going



Spectro-polarimetry requirements



=> The absolute polarization angle should be known with a resolution of the order of the arcmin (the requirements are driven by the 119 and 140GHz frequency bands)



Worst case scenario (top hat function): => measurement resolution of the order of 0.5GHz (driven by the 337 and 402GHz channels).



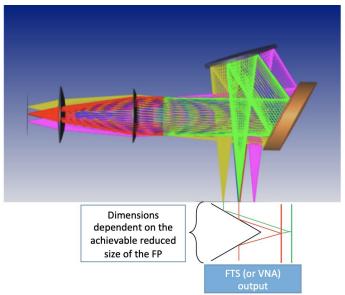


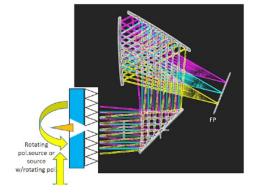
Spectro-polarimetry ground measurements

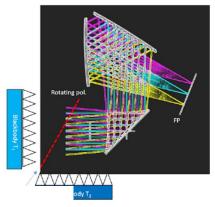
credit: Giorgio

The presence of a polarization modulator couples the two tests:

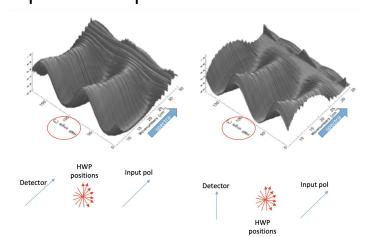
- Spectral Response
- Polarimetric sensitivity
- => the instrument needs to be cold
- => within a cold "flight-like" environment







Expected output: the datacube



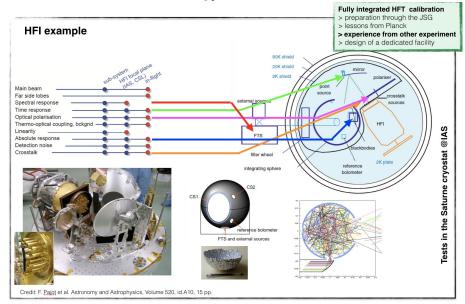
The combination of these two sets provides a complete set of information

Rotate the input pol by 90 degree and you have the same sets by exchanging surfaces and adding a 90 degree offset.



Cold "flight-like" ground measurements

"a la Planck-HFI" strategy:



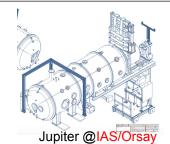
We are studying various possibilities for both LFT and MHFT





LFT in Japan @ KEK or @ JAXA

credit: Masashi





Erios @LAM/Marseille
NB: both need an upgrade

MHFT in France...or in Europe...



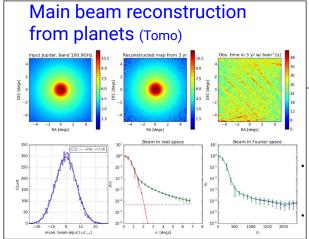
CSL/Liege or even ESA ...

-> on-going discussions & feasibility studies



flight calibration

not exhaustive...

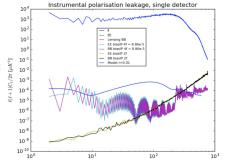


Instrumental Polarization from the dipole signal (Guillaume)

The dipole is a strong signal and also leaks into the polarization

Again detector averaging will reduce the effect as 1/Ndet

 Since the dipole can be predicted, the signal can be used to fit the IP parameters



PTEP

Polarization angle from CIEB

DOI: 10.1093/ptep/0000000000

Simultaneous determination of the cosmic birefringence and miscalibrated polarisation angles from CMB experiments

Yuto Minami^{1,*}, Hiroki Ochi², Kiyotomo Ichiki^{3,4}, Nobuhiko Katayama⁵, Eiichiro Komatsu^{5,6}, and Tomotake Matsumura⁵





...Into the future

The LiteBIRD calibration operations are very challenging!

- The Systematics JSG teams are working hard to update the requirements for each frequency bands. Next step will be to <u>couple systematic effects</u> and further refine the analysis in collaboration with the foreground JSG, and perform <u>simulations</u>.
- The Calibration JSG teams are deeply involved in defining the best strategy to meet the requirements, as well as to prepare the calibration devices and the facilities, but also to make sure to get the longer possible time in the LiteBIRD schedule for the calibration operations (and with instruments as much integrated as possible).
- France is very well placed to have an important impact in LiteBIRD!

