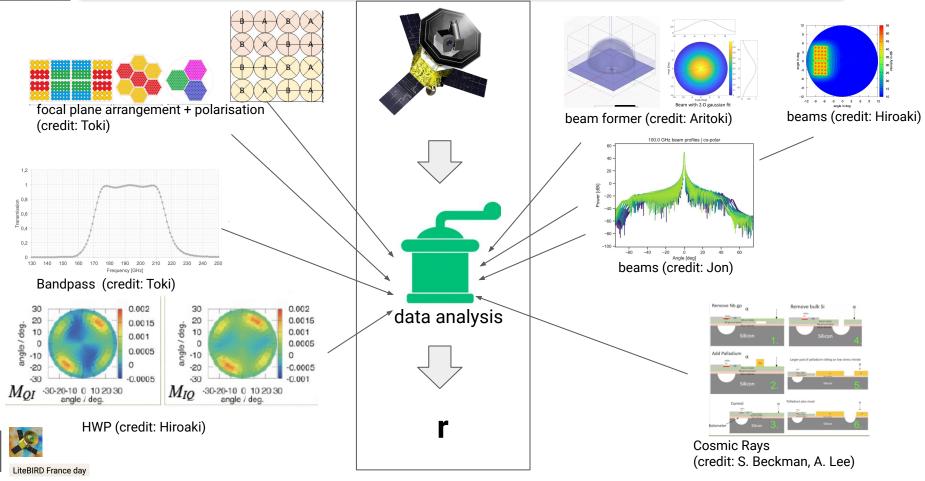
# LiteBIRD Day: Calibration

Sophie Henrot-Versillé on behalf of the LiteBIRD collaboration - July 2019

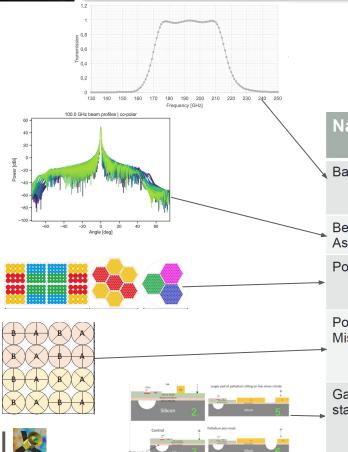


### To get to r we need to know our instruments





### Otherwise....



	Name	Origin	Description	Major mode of Leakage
	Bandpass Mismatch	Spectral Filters	Edges and shape of the spectral filters vary from detector to detector.	I -> P
-	Beam Mismatch and Asymmetry	Optical beams	Beam shape differs from an ideal Gaussian form.	l -> P E -> B
*	Pointing Uncertainty	Attitute control, pointing reconstruction	Detector pointing at location different from that given by reconstructed pointing data.	l -> P E -> B
*	Polarisation Misalignment	Detectors	Uncertainty in polarisation calibration. Polarisation axis misaligned with measured direction.	E -> B
*	Gain mismatch and stability	Detectors and Calibration	Gain calibration mismatch between detectors. These could also be variable over time	I -> P

LiteBIRD France day

#### From Ranajoy Banerji



We want to measure r with an accuracy of (68%CL):

 $\sigma_r = 0.001$ 

Assuming:

$$(\sigma_r = 0.001)^2 = \sigma_{\mathbf{syst}}^2 + \sigma_{\mathbf{fg}}^2 + \sigma_{\mathbf{margin}}^2$$

For each potential source of instrumental systematics:



We assign an error budget:

 $\sigma(r)_{svs} < 5.7 \text{ x } 10^{-6}$  as the budget (1% of total budget for systematic error)

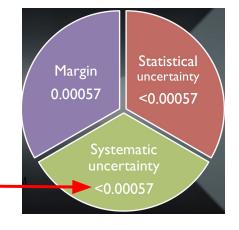


From this we derive a requirement on the knowledge of the underlying instrumental parameters. Calibration JSG !



3

Those requirements are used to best define the calibration method.





### A lot of studies have been performed

ID	Item	sub- ID	Source	w/o HWP	w/ HWP
6		6-1	Far side-lobes	√	V
		6-2	Near side-lobes	V	V
	Beam shape	6-3-	Main beam width	V	V
		1		÷	×
		6-3-	Main beam flattening	V	V
		2	Ghost		
		6-5	cross polarization w/		V
			HWP		
		6-6	Diff. Beam Pointing btw. det.	V	
		6-7	Diff. Beam ellipticity btw. det.	√	
		6-8	Diff. Beam width btw. det.	√	
		6-9	Diff. Cross-pol btw. det.	V	
		6-10	Diff. Side-lobes btw. det.	V	
7		7-1	HWP at 4f		V
	Instrumental	7-2	HWP at 4f side-band		V
	polarization	7-3	HWP at 2f leakage		V
		7-4	HWP at harmonics		V
		7-5	Optical system	√	
8	Polarization	8-1	HWP modulation effi-		V
	efficiency	8-2	ciency	V	1
		8-2	Detector polarization ef- ficiency	v	v
9	Relative	9-1	Variation in time (ran- dom)	~	V V
	Gain	9-2	Variation in time (1/f noise like)	V	V
		9-3	Inter frequency channels	√	V
		9-4	Diff. gain btw. det.(bias)	V	
		9-5	Diff. gain btw. det. (ran-	v	
			dom)	÷	
10	Absolute Gain	10-1		V	V
11		11-1	Offset	V	V
	Pointing	11-2	Time variation in ran- dom	V	V
		11-3	Time variation in time with 1/f	V	V
		11-4	Time variation with HWP rotation		V
12		12-1	Absolute Polarization angle	V	V
	Polarization angle	12-2	Relative Polarization an- gle	~	V
		12-3	Polarization leakage in- trinsic to HWP		V
		12-4	Polarization leakage due to HWP position error		V
		12-5	Variation in time (white like, 1/f like)	~	V
13		13-1	Individual Detector w/o HWP	V	
	1/f noise				

	Comment	]		
-	Beam knowledge: Leakage mainly from E to B,			
	T to B may contribute			
1	Beam knowledge	1		
1	Knowledge of the beam width	1		
-	Main beam ellipticity knowledge			
-	Effect happening inside the 5K shell			
1	Requirement to the knowledge of the cross pol	1		
	characteristics in beam			
1	Leakage from T to B	1		
1	Leakage from T to B			0
-	Leakage from T to B		14	Cost
	-			
	Leakage from E to B, similar to the pol. angle offset		15	
1	Leakage from T to B	1		
1	Knowledge of 4f signal	1		
	Direct leakage to the science band	1		Ban
1	Leakage from 2f to 4f due to finite observing	1		effe
	time and non-linearity			
	Lekakage from $3f$ , $5f$ and so on to $4f$			
	Differential effect in the optical system			
	Knowledge of the HWP modulation efficiency			
	Knowledge of the detector polarization effi-			
	ciency			
	Random variation per 600sec.			
-	Requirement in fince			
-	Related to FG subtraction, and Band pass effect ID=15			
-	Leakage from T to B			
-	Leakage from T to B			
	No E to B as Parity conserved. Related to the			
	Pol. efficiency in ID=8 Calibration with CMB			
	dipole. Absolute power of Cl, i.e., the absolute value of r			
1	E to B Expectation value from Vender's info.	1	16	
1	Disturbances in time uncorrelated way: Perhaps	1		Tran
	in a way that all the FC plane detector coher-			func
	ently			
	Disturbances in time correlated way:			
1	Wedge in transmissive HWP, tilt of the rotation			
-	axis of reflective HWP		17	
	Using CMB channels with $C_l^{EB}$ .			Nor
	Inter frequency channels, inter detectors			Non
	knowledge of $M_{QU}$ or $M_{UQ}$ in Mueller matrix			
1	Requirement to the knowledge to the HWP ro-			
-	tation position			
	Variance of pol. angle determination by STT			
1	Detector originated	1		

	13-2	Individual Detector after		V
		demodulation		
	13-3	Common mode	V	
	13-4	Inter channels	Ŵ	
	13-5	Noise modeling	Ú.	V
			1 × 1	
	13-6	HWP temperature varia-		V
		tion in time with $1/f$ like		· ·
		for monopole		I I
	13-7	HWP temperature vari-		1
	1.5-1	ation in time with $1/f$		N I
		noise for 2f		I I
		noise for 2j		
			L	
nic ray	14-1	Common mode	V	V
ies	14-2	Data acquisition (includ-	V	√
		ing data compression)		
	15-	Frequency shift of the	V	
	1-1	band w/o HWP in differ-		I I
		entiation.		
	15-	Frequency shift of the	1	V
	1-2		V	Y
l pass		band	1	
t	15-	Band shape w/o HWP	√	
	2-1			
	15-	Band shape	√	√
	2-2			1 1
	15-	Beam shape in band w/o	V	
	3-1	HWP		
	15-	Beam shape in band	V	V
	3-2	ovant snape in band	N I	V I
	3-2			
				1
	15-	Pol. angle wobble in	√	√
	4-1	band		
	15-5	Gain variation in band	√	V
	15-6	Instrumental Polariza-		V
		tion in band		11
	15-7	Polarization efficiency in		V
	1.5-7	band		Y
		Dand		
	15.0	0.1.1		1,
	15-8	Outer band	1	√
	16-1	Detector time constant	√	√
sfer		knowledge	100 A	1 ° 1
tion	16-2	Digital filter in readout	V	1
		system	1 ×	12
	16-3	Cross-talks	V	V
	16-3	Time constant variance	v	+ V
	10-4			V
		in time coupled to HWP		
		revolution		
	17-1	Detector response: pa-	V	√
		rameterized as g in a		
		model of $(1 + gd(t))d(t -$		
rity		$\tau d(t))$		
	17-2	Variation in time on g,	V	V
		white like or $1/f$ like		1 1
	17-3	HWP 2f synchronous:	-	V
	11-2	leakage from 2f to 4f		Y I
		icakage from 23 to 45		
	17-4	time constant $\tau$ [sec/uK]	V	V
		in the PB model (1 +		
		$gd(t)d(t - \tau d(t))$		1 1
	17-5		V	1
	17-5	Variation in time of $\tau$ in	~	1
	17-5		V	V

T .	in req. flow L3.08 1/10 of white noise at the
+ .	spin frequency 0.1rpm=1.6mHz Common mode in FP
+ -	With FG component separation
	Requirements to determine the noise stationar-
ļ .	ity; how long period the noise to be stable
	Loading from HWP changes the detector noise, the time correlated variation would cause the 1/f
	noise
+ -	Differential emissivity in the two axes will pro-
	duce 2f signal. The 1/f time variation of HWP
	temperature produces the fluctuation of the 2f
	which may be leaked to the 4f. Note that the multi-layer stacked AHWP may smear out this
	effect.
	Wafer base due to phonon propagation
	Additional noise due to down-sampling, Data
+ .	compression
	Band shift in a detector pair
	Knowledge of the band position
L .	
	Diff. of the band shape in a detector pair
+ -	Knowledge of the band shape
	· · ·
г ·	Diff. of frequency dependence of beam shape in
	band, caused by the spectrum difference. Cali-
+ -	bration using planets may cause difference Frequency dependence of beam shape in band,
	caused by the spectrum difference. Calibration
L .	using planets may cause difference
	Sinuous antenna wobble, may be canceled out
+ -	using combination of Q/U and two sides Gain calib. using CMB dipole may differ from
	that of FG due to spectrum diff.
† -	Frequency dependence of IP in HWP
ļ .	
	Related to the frequency dependence of the HWP retardance and/or sinuous antenna re-
	sponsivity
+ -	Contamination from the outside of frequency
L .	band.
	Detector time constant
+ -	Possible effect in time correlated way which
	cause the spatial correlation
	Cross-talks in frequency domain
	random 1/f type variation in time
+ -	Assuming maximal loading to the instrument in
	uK to set the working position
+ -	Non-stationarity of the non-linearity due to the
	change of the loading position
† -	May be related to ID=7, causing leakage to 4f,
	due to large 2f signal, To be related 2f emission
	in 18-1-2 Knowledge of the time response τ
	renowiedge of the time response r
Г <sup>-</sup>	Possible time dependence of the time constants
+ -	Provide affect in data commercian
L.	Possible effect in data compression process

a 13.00 1/10 c 1

hite noise at the z	18	Non-	18- 1-1	Transmissive HWP		V	Azimuthal angle dependence in oblique inci- dence of light
noise stationar-		uniformity in HWP	18-	Differential emissivity of transmissive HWP		V	Production of 2f signal, can be leaked to 4f with the position dependence.
o be stable e detector noise.			18-2	Reflective HWP		V	Azimuthal dependence in oblique incident an- gle. We will not consider this source.
wo axes will pro-			18-3	Position dependent HWP temperature fluc- tuation in white noise like		V	Increase the detector noise. We do not consider this source as this is related to the reflective HWP.
uation of the 2 <i>f</i> <i>f</i> . Note that the ty smear out this agation -sampling, Data	19	Uncertainties difficult to model and simulate	19-1	Multiple reflection be- tween HWP and FP		V	Requirement to HWP AR. Two ways: back-of- the envelope calculation to get first order req. In GRASP, the multiple reflection with HWP is difficult to simulate. One way is to measure the beam pattern w/ and w/o HWP using the real instruments.
			19-2	fknce	V		1/f noise f <sub>knee</sub> is unknown unless the real in- struments are tested, assigned for the case w/o HWP
n			19-3	Gain variation	V	V	Actual gain variation strongly depend on the in- strument environment, and difficult to model in a simulation
ector pair			19-4	FG spectrum and un- known components	V	V	Unknown features of the spectra and compo- nents in foregrounds

options with and without HWP. The column of  $\Delta r$  or  $\sigma_r$  shows the expected error of r. Details are given in each section. N.A. means "Not Available" for the sources that we have not yet studied and assign the 1% error budget of  $5.6 \times 10^{-6}$  as the requirement. The ID=13 (1/f noise) shows the  $\sigma_r$  values, while other sources show  $\Delta r$  values.

#### credit: Concept Design Report

The requirements are being and will be updated and further refined

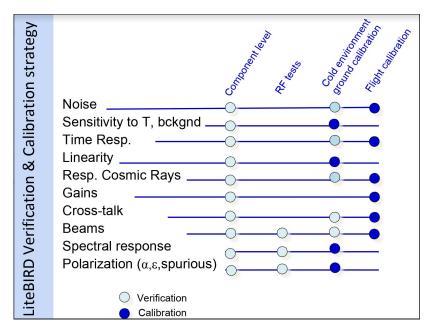




# How ? verification and calibration strategy

To reach the required accuracies the calibration strategy is setup in several steps. We will rely on measurements:

- on the ground and in-flight
- from component level to full integrated instruments

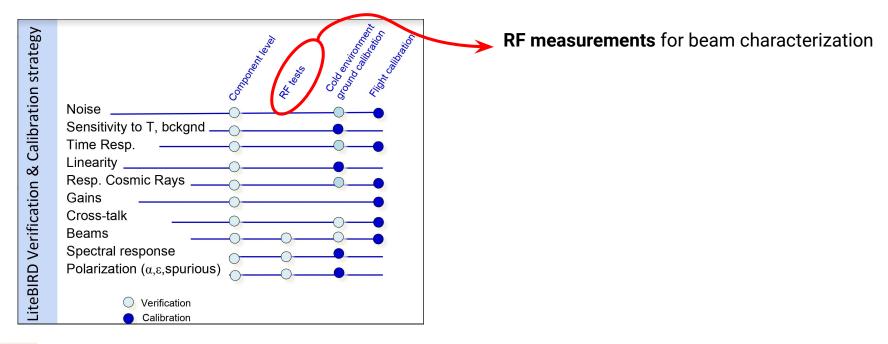




# LiteBIRD verification and calibration strategy

To reach the required accuracies the calibration strategy is setup in several steps. We will rely on measurements:

- on the ground and in-flight
- from component level to full integrated instruments



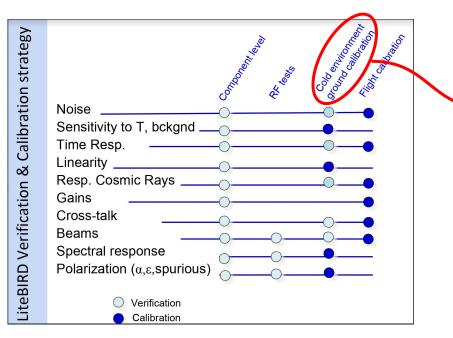
LiteBIRD France day



# LiteBIRD verification and calibration strategy

To reach the required accuracies the calibration strategy is setup in several steps. We will rely on measurements:

- on the ground and in-flight
- from component level to full integrated instruments



RF measurements for beam characterization

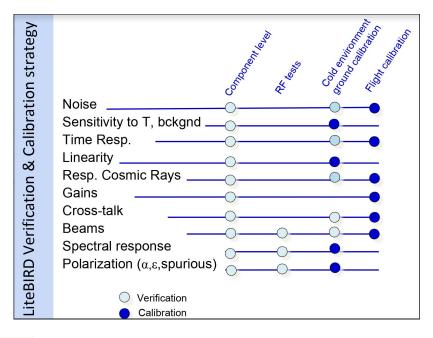
Cold environment "flight-like" loading
conditions on the instruments+calibration sources in a big cryogenic facility



# LiteBIRD verification and calibration strategy

To reach the required accuracies the calibration strategy is setup in several steps. We will rely on measurements:

- on the ground and in-flight
- from component level to full integrated instruments



#### RF measurements for beam characterization

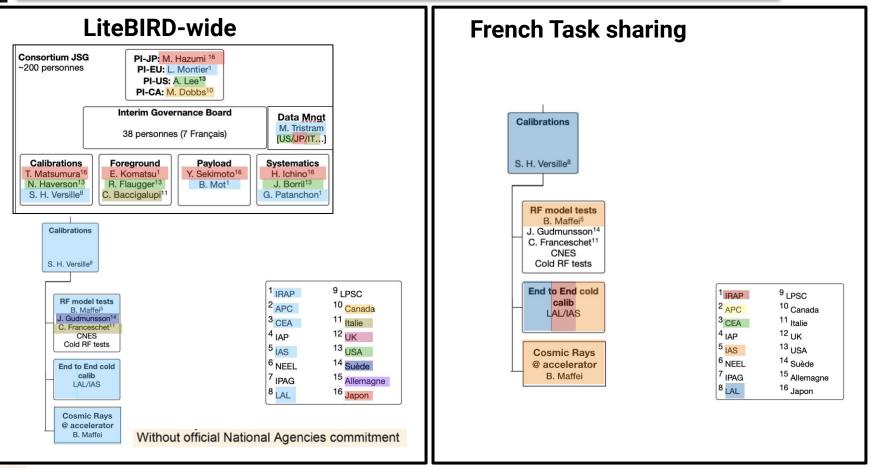
**Cold environment "flight-like"** loading conditions on the instruments+calibration sources in a big cryogenic facility

#### => In this talk I will focus on:

- Beams
- Spectro-polarimetry

(and will not address component level tests)

### French responsibilities in calibration activities



LiteBIRD France day



mid. 2021 : RF tests on DM beg. 2023 : EQM cold calibration end 2023 : EQM to JAXA beg. 2025 : FM cold calibration mid. 2025 : FM to JAXA

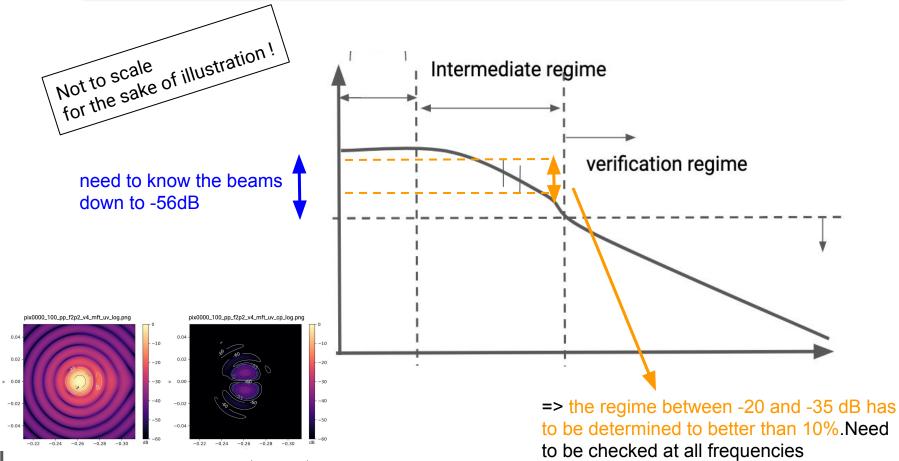
DM: Demonstration Model EQM: Engineering/Qualification Model FM: Flight Model





### Beams requirements (so far)

credit: Ryo, Davide, Tomo

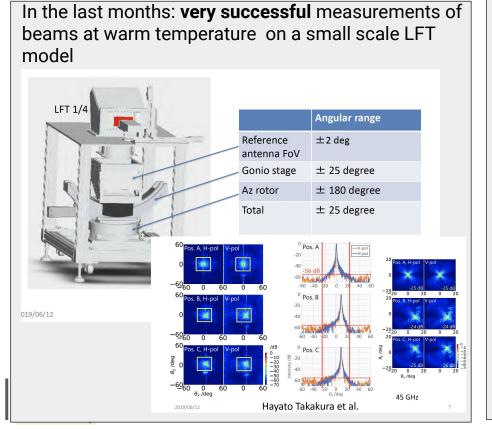


credit: the MHFT Optics working group (Jon et al.)



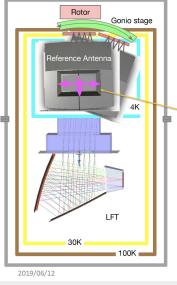
# RF ground measurements for LFT

The full strategy is being addressed and further refined with on-going measurements in Japan



=> Next steps: cold measurements

#### Reference antenna + Gonio + Az rotor



	Angular Range
Reference antenna FoV	$\pm 10 \deg x \pm 2 \deg$
Gonio stage	-1 ~ +15 degree
Az rotor	$\pm$ 180 degree
Total	$\pm$ 25 degree

credit: Yutaro



# Challenges of the RF measurements for MHFT

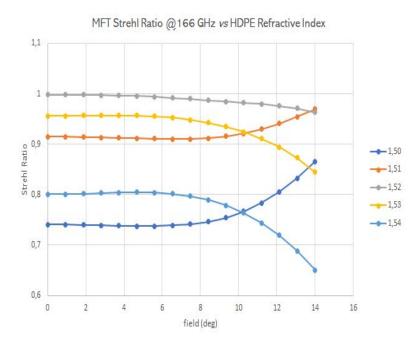
The properties of the lenses (indices of refraction) depends on the temperature

#### AND

the beam shape depends on the properties of the lenses

we need to cool down the instrument to measure the beams ! ...

Then the question is...far field cold measurement or near field cold measurement: how to define the best strategy ?



Eg: Strehl ratio for various refraction indices of lenses (typical of cold->warm variations)

credit: the MHFT Optics working group (Jon et al.)

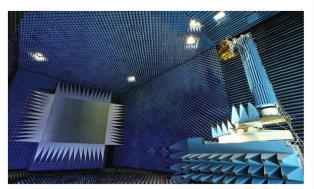
# RF ground measurements for MHFT

We are currently studying the best strategy, to build up a model fed with:

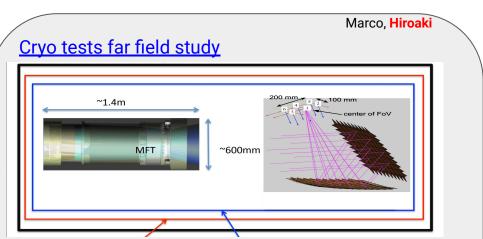
- sub-system, semi-integrated and integrated level measurements
- warm/cold measurements

#### On-going work at CNES/Toulouse:

Antenna models will be built on the basis of MHFT beam simulations (optics group) for 100 to 402 GHz => to be further characterized with the use of submm source in the CATR to perform a feasibility study in CNES facilities.



Modèle de vol de Saphir, instrument du satellite Megha-Tropiques, en essais en BCMA.



Far field measurements are what we need at the end !

=> near field @ cold ? (intensity and phase to translate to far field) => or directly measure the intensity in the far field ?

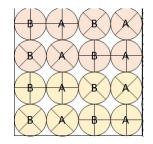
=> feasibility study on-going

credit: the MHFT RF working group (<u>Bruno, Jon, Cristian</u> + <mark>Hiroaki</mark>, Marco, Marco, Ludo, Baptiste, Sophie)

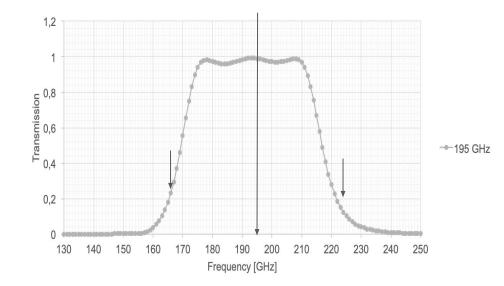
CNES CATR team



### Spectro-polarimetry requirements credit: Patricio & Enrique, Tommaso



=> The absolute polarization angle should be known with a resolution of the order of the arcmin (the requirements are driven by the 119 and 140GHz frequency bands)



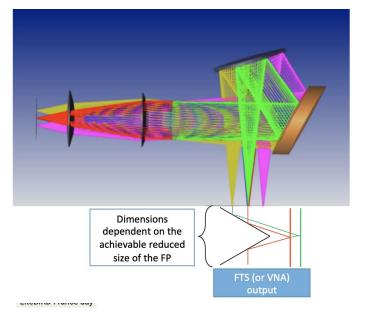
Worst case scenario (top hat function): => measurement resolution of the order of 0.5GHz (driven by the 337 and 402GHz channels).

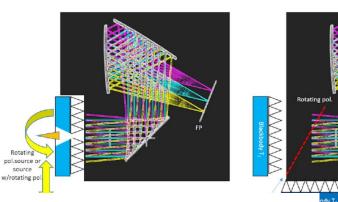


# Spectro-polarimetry ground measurements credit: Giorgio

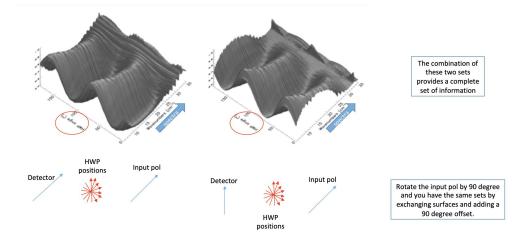
The presence of a polarization modulator couples the two tests:

- Spectral Response
- Polarimetric sensitivity
- => the instrument needs to be cold
- => within a cold "flight-like" environment





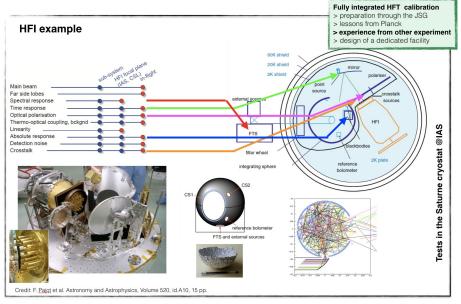
#### Expected output : the datacube





# Cold "flight-like" ground measurements

#### "a la Planck-HFI" strategy:



We are studying various possibilities for both LFT and MHFT





Jupiter @IAS/Orsav



LFT in Japan @ KEK or @ JAXA

credit: Masashi

#### MHFT in France...or in Europe...

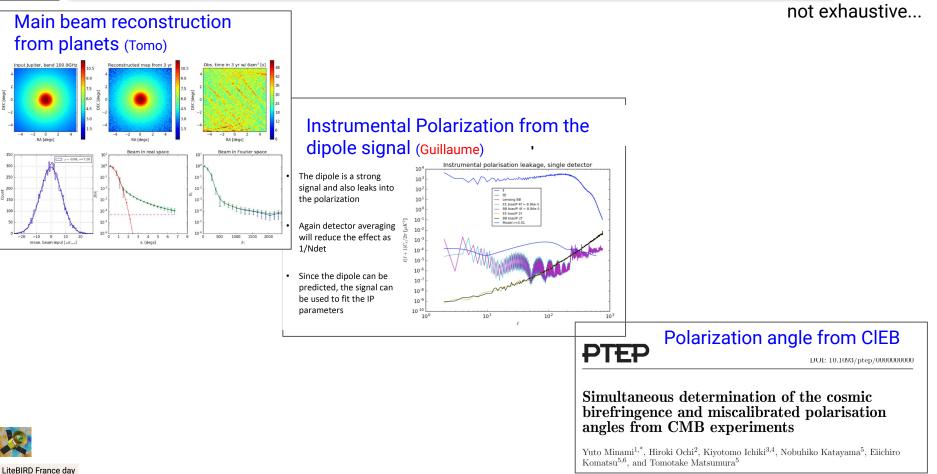


CSL/Liege or even ESA ...

-> on-going discussions & feasibility studies



### flight calibration





### ...Into the future

The LiteBIRD calibration operations are very challenging !

- The Systematics JSG teams are working hard to update the requirements for each frequency bands. Next step will be to <u>couple systematic effects</u> and further refine the analysis in collaboration with the foreground JSG, and perform <u>simulations</u>.
- The Calibration JSG teams are deeply involved in defining the best strategy to meet the requirements, as well as to prepare the calibration devices and the facilities, but also to make sure to get the longer possible time in the LiteBIRD schedule for the calibration operations (and with instruments as much integrated as possible).
- France is very well placed to have an important impact in LiteBIRD !

