

**IRSN**

INSTITUT  
DE RADIOPROTECTION  
ET DE SÛRETÉ NUCLÉAIRE

*Faire avancer la sûreté nucléaire*

# Multi-zone fuel irradiation model for ASTRID-like SFR with the CLASS code

3<sup>rd</sup> Technical Workshop  
on Fuel Cycle Simulation

July 9<sup>th</sup> - 11<sup>th</sup> 2018, Paris, France

**Neutronics and Criticality  
Safety Department**

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# Outline

Context & Objectives of the study

Multi-zone Fuel Irradiation Model

Multi-zone cross-sections Predictor

Impact of using a Power Predictor or a Flux Predictor on fuel composition estimation

Conclusion & Perspectives

# Context

- Uncertain placement of nuclear power in the future french energy mix
  - Energy Transition Act, political & scientific discussions
- Uncertain strategy of reactor fleet renewal
  - Extension of the PWR fleet
  - Deployment of new SFR-CFV (*low void effect*)  
(*Reference Strategy, CEA Report, 2015*)
- Uncertain Pu status: waste or valuable fuel for a future SFR fleet
  - *One waiting strategy*: stabilization of Pu inventory in cycle thanks to Pu multi-recycling
    - PWR (e.g. with MOXEUS fuel<sup>1</sup>, ...)
    - ASTRID-like reactors: breeder, isogenerator, burner

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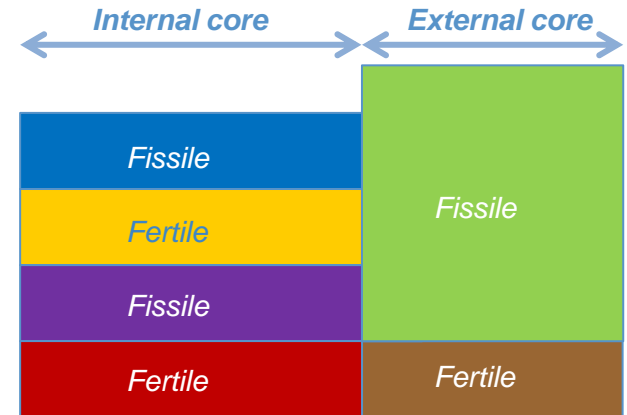
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## ➤ Possibilities for Pu in cycle dynamic management with SFR-CFV?

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# Objectives

- Pu isogenerator ASTRID-like SFR-CFV **heterogeneous core** design  
*(shape, fissile & fertile fuel zones)*
- For one Cycle time & one fresh fuel composition: each zone as a really **different behavior**
  - E.g. at EOC: the inner fertile zone acts like an inner fissile zone



*Sectional view of ASTRID-like reactor*

# Objectives

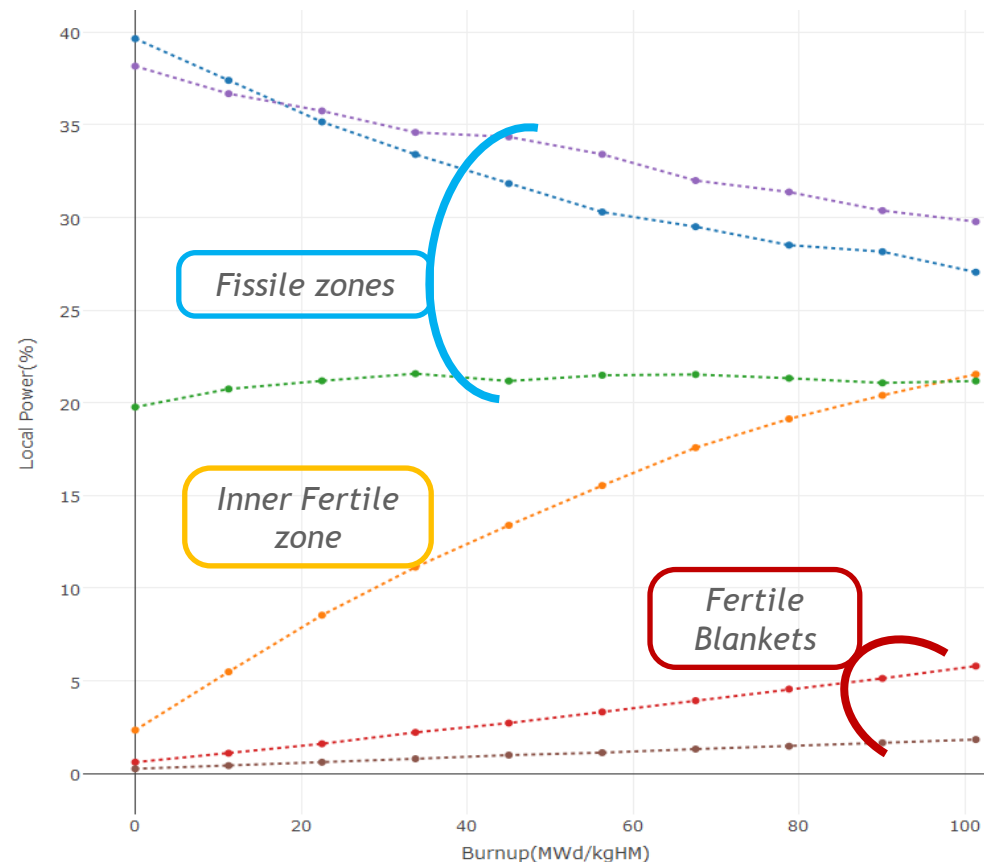
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Sectional view of ASTRID-like reactor



Evolution of Local Powers during irradiation

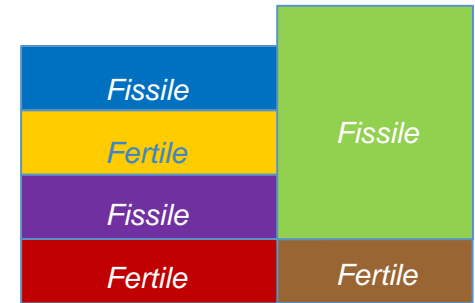


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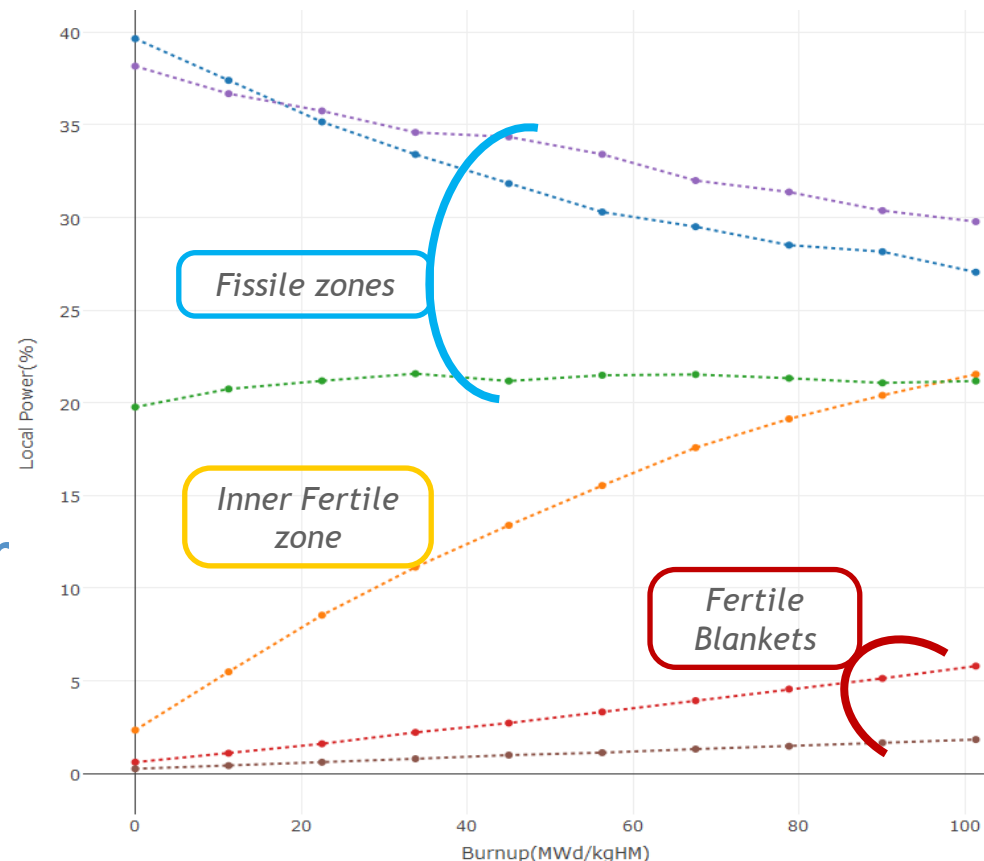
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- For one Cycle time & one fresh fuel composition: each zone as a really **different behavior**
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➔ How to maintain the reactor heterogeneity during the fuel irradiation while keeping interactions between the fuel zones?



Sectional view of ASTRID-like reactor



Evolution of Local Powers during irradiation

# Multi-zone Fuel Irradiation Model

- Cycle time, initial fuel composition of each evolutive zone  
→ *input data*
- Bateman equations resolution **for each zone**

$$\frac{dN_i}{dt} = \underbrace{-(\lambda_i + \sigma_i \varphi) N_i}_{\text{Loss}} + \underbrace{\sum_{j \neq i} (\lambda_{j \rightarrow i} + \sigma_{j \rightarrow i} \varphi) N_j}_{\text{Production}} \quad \begin{array}{l} i \text{ Isotope} \\ j \text{ Parent Isotope} \\ k \text{ zone} \end{array}$$

- Decay constants ( $\lambda$ )
- Local cross-sections ( $\sigma$ ) calculations → **a XS Model**
- Local flux ( $\varphi$ ): from a specific power calculation → **a Power Model**

- **With**  $P_{tot} = \sum_k P_k(t)$   $\varphi_k(t) = \sum_i \frac{P_k(t)}{\varepsilon_i^{fis} \times \sigma_{i,k}^{fis}(t) \times N_{i,k}(t)}$

# Multi-zone Fuel Irradiation Model

- Cycle time, initial fuel composition of each evolutive zone  
→ *input data*
- Bateman equations resolution **for each zone**

$$\frac{dN_i}{dt} = -(\lambda_i + \sigma_i \varphi) N_i + \sum_{j \neq i} (\lambda_{j \rightarrow i} + \sigma_{j \rightarrow i} \varphi) N_j$$

*i* Isotope  
*j* Parent Isotope  
*k* zone

- Local cross-sections calculations → **a XS Model**
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- Scenario simulation with the code CLASS
  - New dedicated model for fuel irradiation in multi-zone reactors
    - Generally: homogeneous fuel  $\sim$  approximation
    - 6 independant fresh fuel compositions: depletion over time and per zone
    - 2 predictive models based on Artificial Neural Networks (ANN)



Core Library for  
Advanced  
Scenario  
Simulation

# Multi-zone cross-sections predictor

- XS Model: training on **full core** depletion simulations
  - Zone number is an ANN new input parameter: **space discretization**
- Predictor accuracy verification

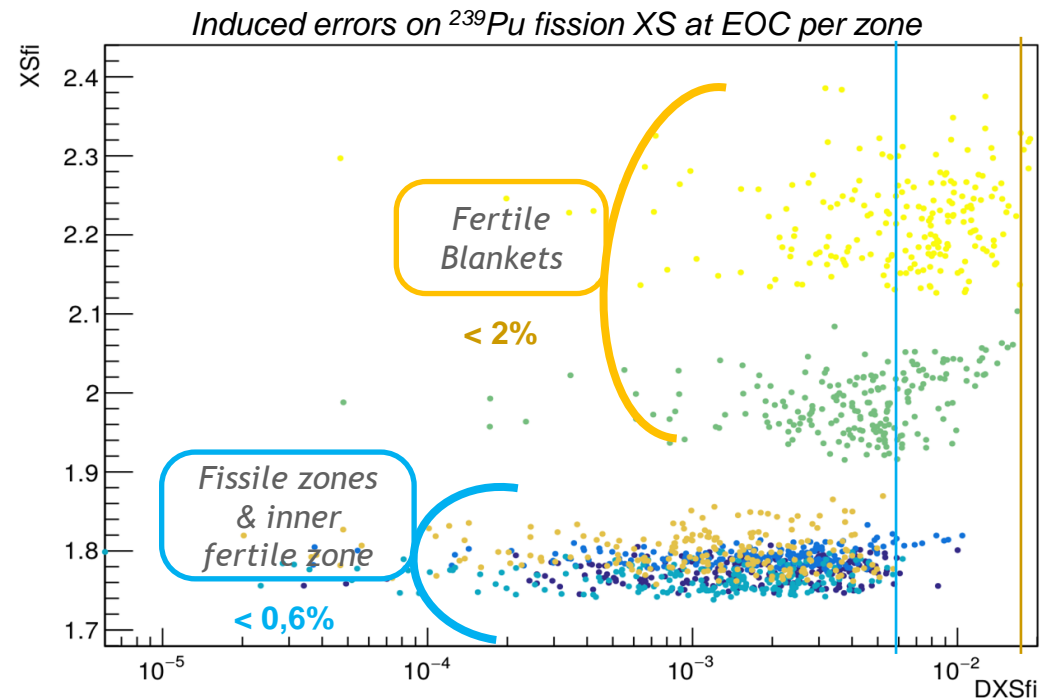
- Example of  $XS_{fission}$  (barn)  $^{239}\text{Pu}$  per zone

- $$DXS_{fi} = \left| \frac{XS_{fi}^{VESTA} - XS_{fi}^{CLASS}}{XS_{fi}^{VESTA}} \right|$$
at ~100 GWd/t

➔  $\text{Errors}_{\text{fertiles}} > \text{Errors}_{\text{fissiles}}$

➔ Induced errors by multi-zone  $XS_f$  predictors < 2%

➔ Direct impact of  $XS_f$  on flux calculation



# Local power predictor

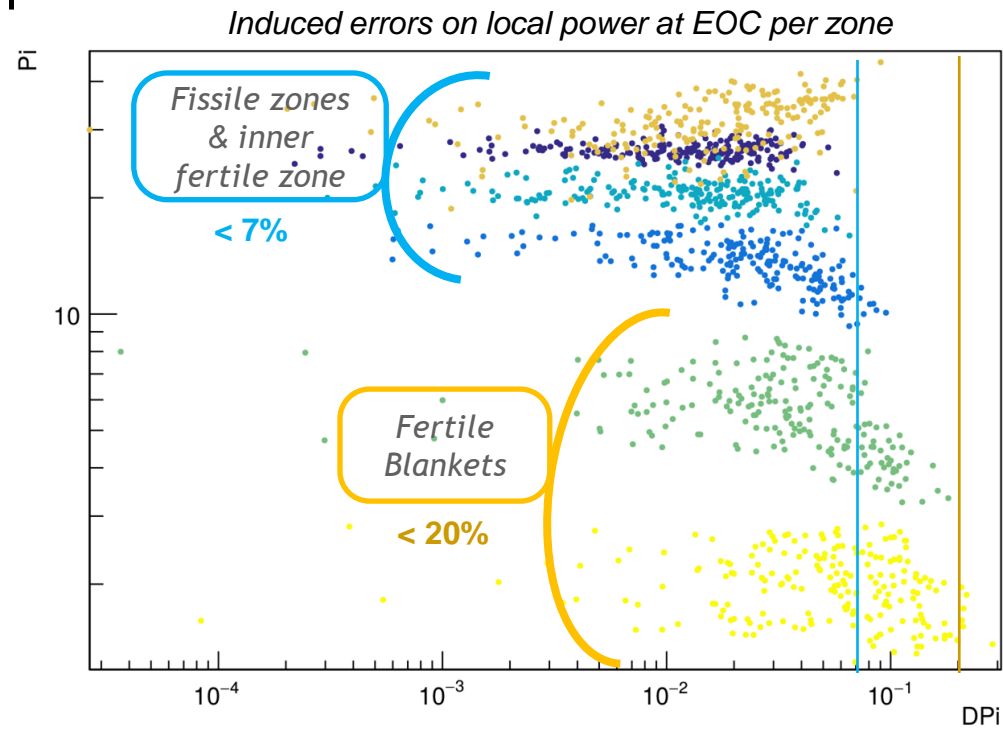
- Local power Model: training on **full core** depletion simulations
  - Zone number is an ANN new input parameter: **space discretization**
  - **Constraint on local power**:  $P_{tot} = \sum_k P_k(t)$

- **Predictor accuracy verification**

- $P_i$ : %power per zone

- $DP_i = \left| \frac{P_i^{VESTA} - P_i^{CLASS}}{P_i^{VESTA}} \right|$   
at ~100 GWd/t

- ➔ Induced error < 20%
- ➔ Direct impact on flux & composition per zone
- ➔ Important errors in fertile blankets but lower %power so lower impact on global inventories (<10% for  $Pu_i$ )



# Fuel composition estimation with a Power Model

- Example of  $^{239}\text{Pu}$  composition

## per zone

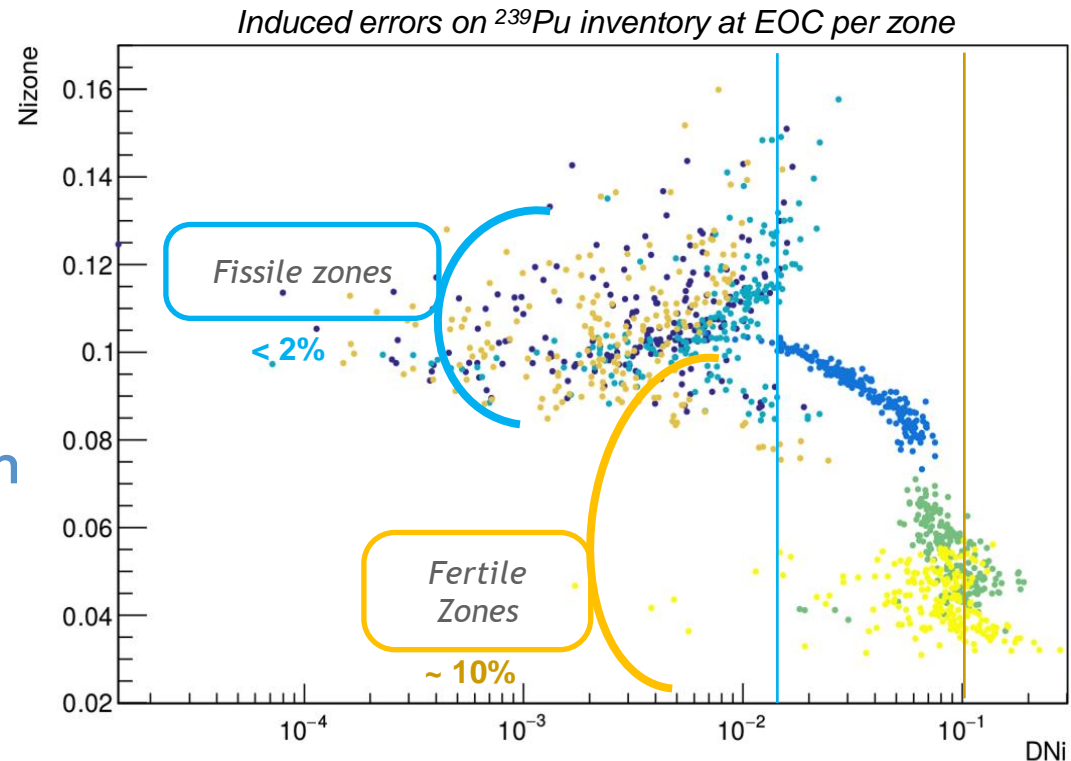
- $N_{i,\text{zone}}$ :  $^{239}\text{Pu}$  atomic proportion
- $DN_i = \left| \frac{N_i^{\text{VESTA}} - N_i^{\text{CLASS}}}{N_i^{\text{VESTA}}} \right|$   
at  $\sim 100 \text{ GWd/t}$

➔ Errors on  $^{239}\text{Pu}$  estimation in fertile zones  $\sim 10\%$

- Too many uncertainty ?

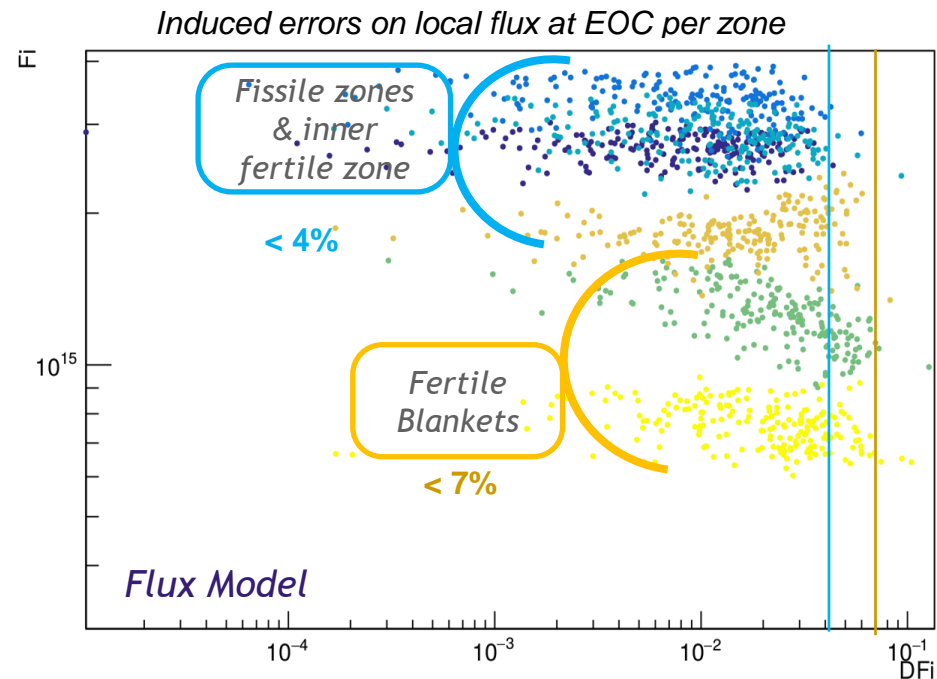
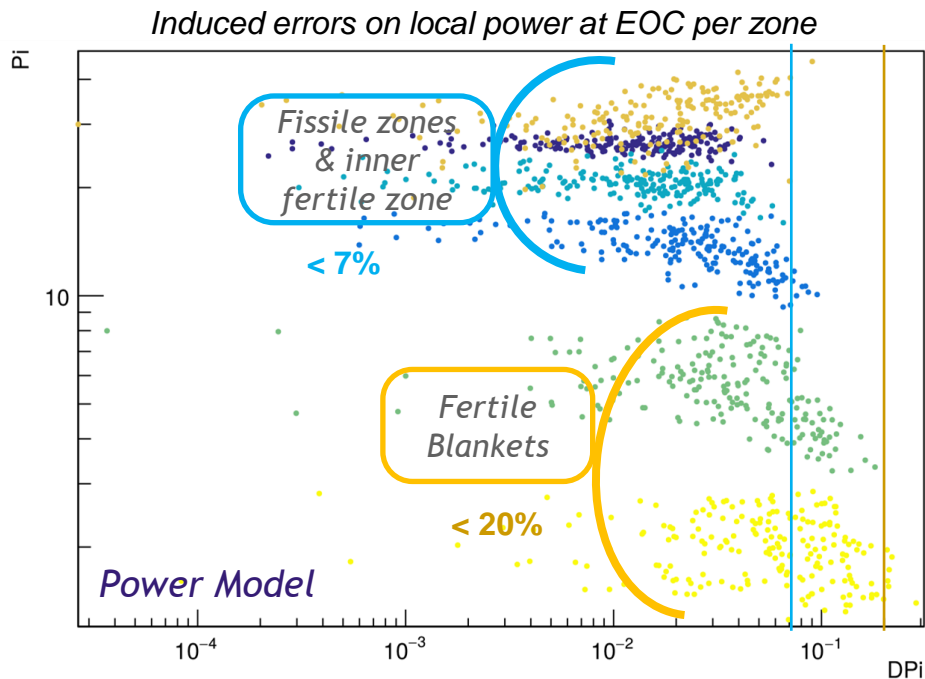
$$\varphi_k(t) = \sum_i \frac{P_k(t)}{\varepsilon_i^{\text{fis}} \times \sigma_{i,k}^{\text{fis}}(t) \times N_{i,k}(t)}$$

- Less constraint if direct prediction of local flux: **a Flux Model**
  - But size & reactor power modulations get more challenging



# Local power predictor or local flux predictor

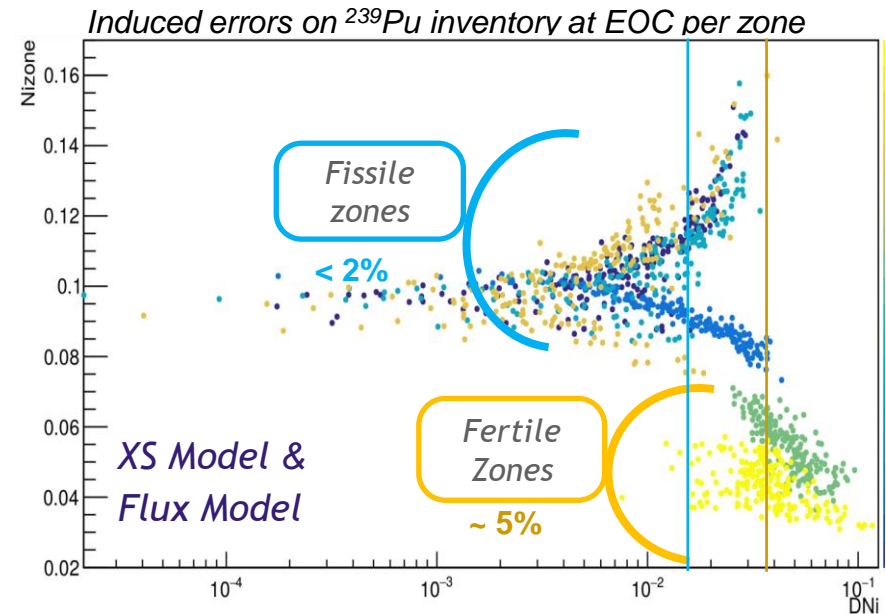
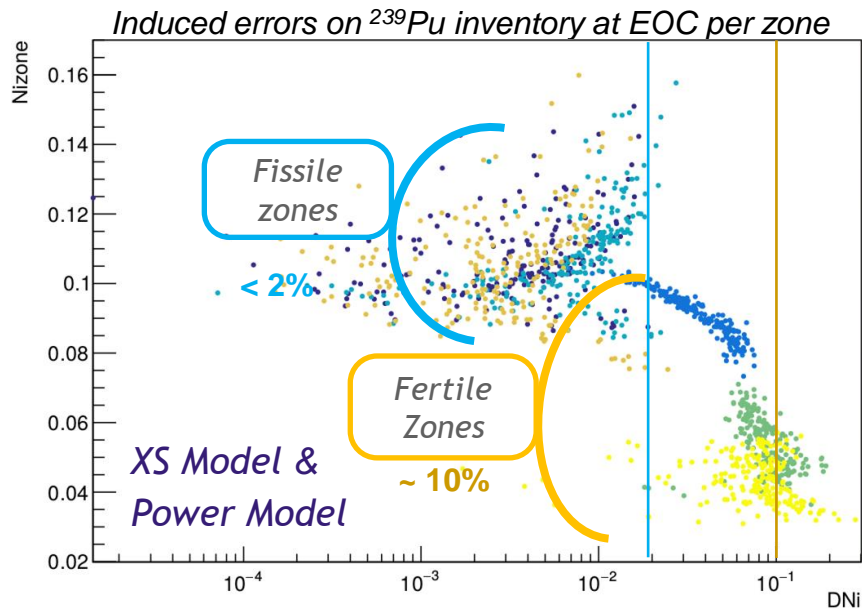
- Predictors accuracy verification: **Power Model VS Flux Model**
  - $P_i$ : %power per zone &  $F_i$ : local flux ( $1/\text{cm}^2/\text{s}$ )



- Induced errors by multi-zone local flux predictors < 7%
- Improvement by predicting directly local flux
- Still an impact on the CLASS compositions estimation per zone

# Impact of the model on fuel composition estimation

- Impact of both predictors on fuel composition estimation
- Example of  $^{239}\text{Pu}$  composition **per zone**
  - $N_{i\text{zone}}$ :  $^{239}\text{Pu}$  atomic proportion
  - $DN_i = \left| \frac{N_i^{\text{VESTA}} - N_i^{\text{CLASS}}}{N_i^{\text{VESTA}}} \right|$  at  $\sim 100$  GWd/t

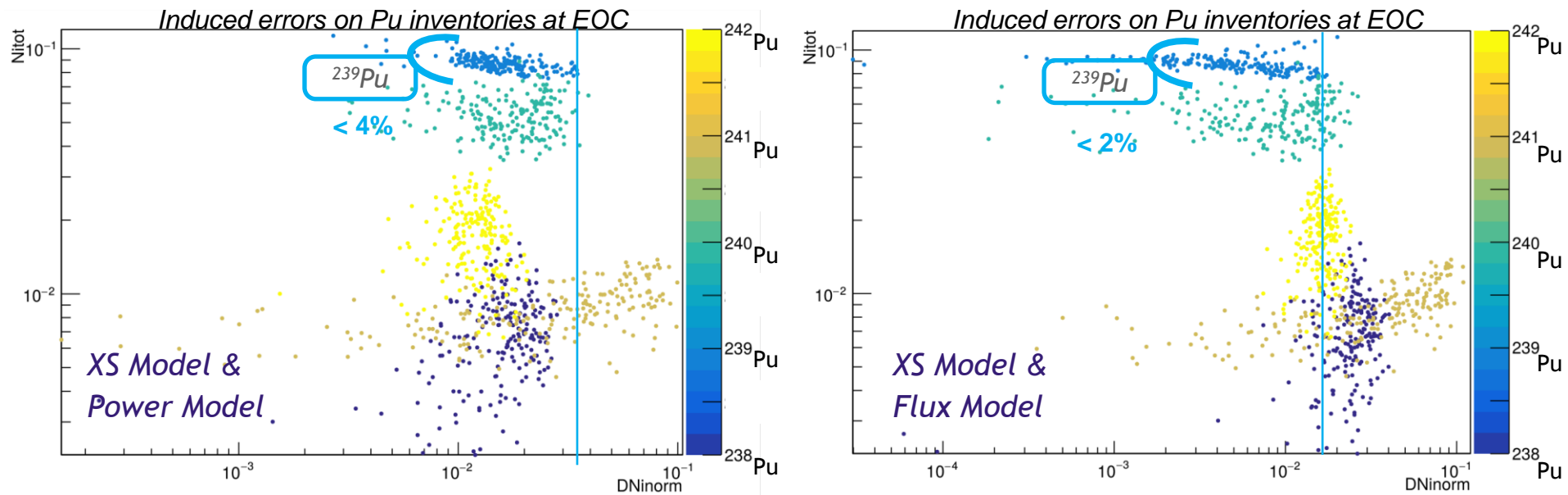


➔ Gain of a factor 2 on the  $^{239}\text{Pu}$  composition estimation



# Impact of the model on fuel composition estimation

- Impact of both predictors on fuel composition estimation
- Example of Pu composition → **global inventory: homogenization**
  - $N_{i\text{tot}}$ : total Pu atomic proportion
  - $DN_{inorm} = \left| \frac{N_i^{VESTA} - N_i^{CLASS}}{N_i^{VESTA}} \right|$  at  $\sim 100$  GWd/t



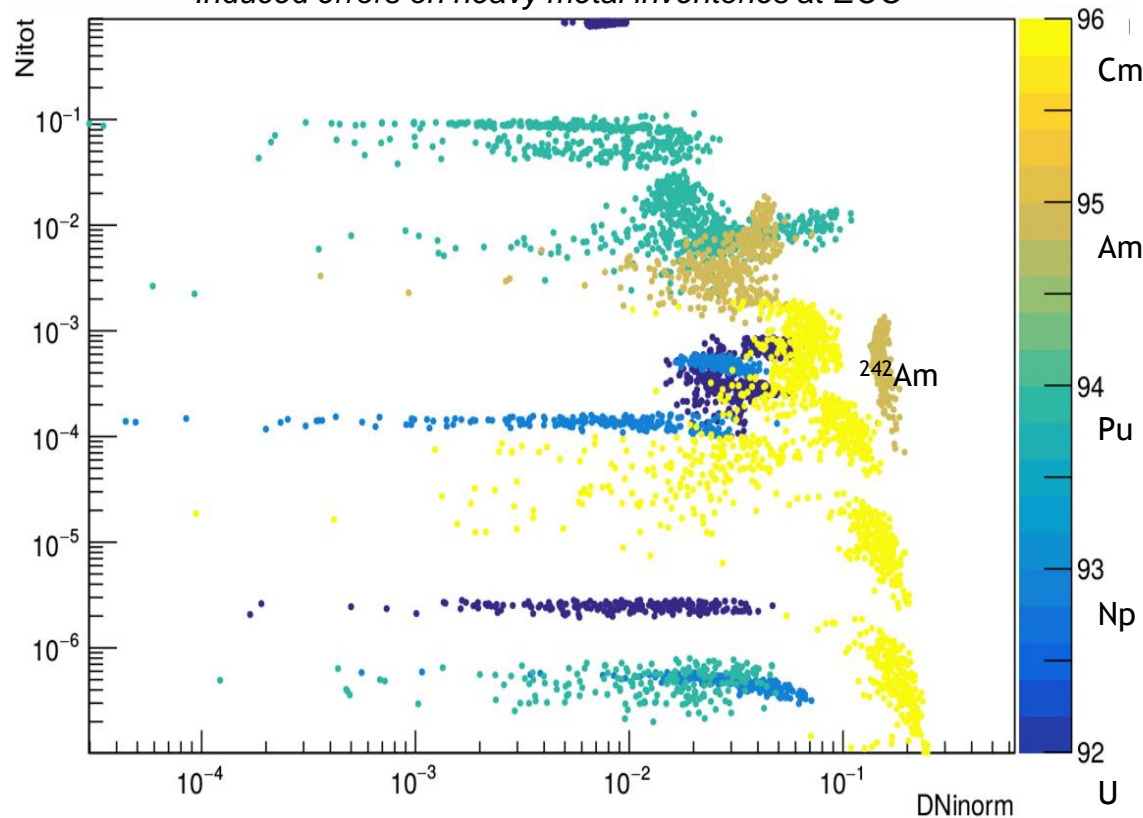
➤ Errors in fertile zones > Errors on a global reactor scale

➤ Fertile separation ?

# Fuel composition estimation with a Flux Model

- Isotopic composition → **global inventory: homogenization**
  - $N_{i_{tot}}$ : total Heavy Metal atomic proportion
  - $DN_{inorm} = \left| \frac{N_i^{VESTA} - N_i^{CLASS}}{N_i^{VESTA}} \right|$  at ~100 GWd/t

Induced errors on heavy metal inventories at EOC



➔ Good Pu estimation:  
new irradiation model  
appropriate for Pu  
stabilization in cycle

➔ Model not appropriate  
for MA recycling

# Conclusion & Perspectives

- To study the capability of ASTRID-like reactors to stabilize the Pu in cycle while keeping its heterogeneity
  - **A new multi-zone fuel irradiation model**
- Good multi-zone cross-sections predictions → errors induced < 2%
- Compromise between model accuracy & flexibility
  - Better prediction of local flux than local power → errors induced < 7%
    - better composition estimations
    - but no direct control of the reactor power
- Impact of multi-zone irradiation on the electronuclear fuel cycle
  - Irradiation model accuracy very related with the zone number
  - Uncertainty balanced on the reactor scale
    - no fissile & fertile separation management with the Power Model
- Impact of the multi-zone fuel irradiation model at a scenario scale ?
- Homogeneous irradiation model / Multi-zone fuel irradiation model ?
- Application with other type of reactor

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# Thank you for your attention !

*Special thanks to Marc Ernout, Xavier Doligez, Abdoul-Aziz Zakari-Issoufoub*



# Databank generation

## Learning and training database

- Draw of  $t_{pu}$  (2 cores), initial isotopic vector (5 isotopes) : 7 parameters
  - LHS method (*Latin HyperSquare*)
- Buffer  $^{239}\text{Pu}$
- U isotopic vector ( $^{238}\text{U}$  99.2% -  $^{235}\text{U}$  0.8%)
- 1000 initial fuel compositions

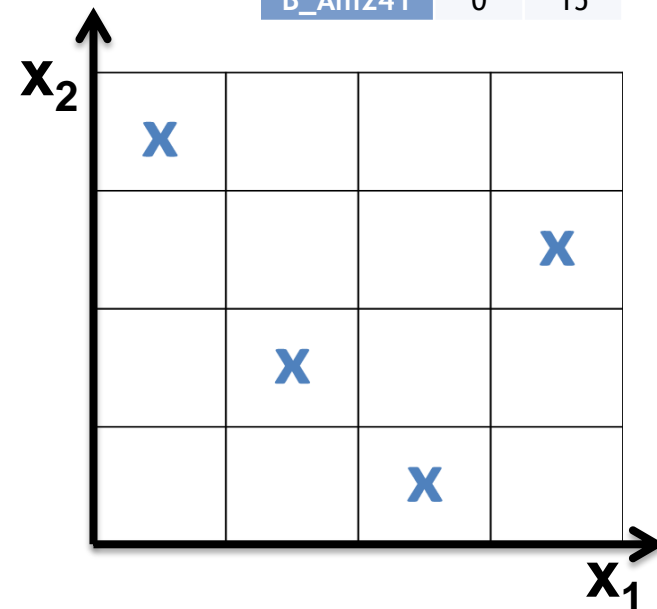
	Min	Max
T_Puint	15	40
T_Puext	15	40
B_Pu238	1	8
B_Pu240	20	40
B_Pu241	0	17
B_Pu242	5	17
B_Am241	0	15

➔ 1000 Monte-Carlo depletion calculations

## Testing database

- Same methodology
- 200 initial fuel compositions

➔ 200 Monte-Carlo depletion calculations



# Depletion calculations: 10 timesteps

➔ Relative error due to the random seed with one composition

## ■ Error EOC

Isotope	$^{239}\text{Pu}$ fission XS	Flux	$^{239}\text{Pu}$ Composition
Upper Fissile	0.13%	1.29%	0.12%
Lower Fissile	0.12 %	1.10%	0.09%
External Fissile	0.12%	2.92%	0.1%
Inner fertile	0.12%	0.64%	0.09%
Fertile Blanket internal	0.27%	1.37%	2.44%
Fertile Blanket external	0.75%	2.30%	1.15%