

New preamplifier  
in TSMC130nm  
for the ATLAS  
LArg Electromagnetic  
Calorimeter upgrade



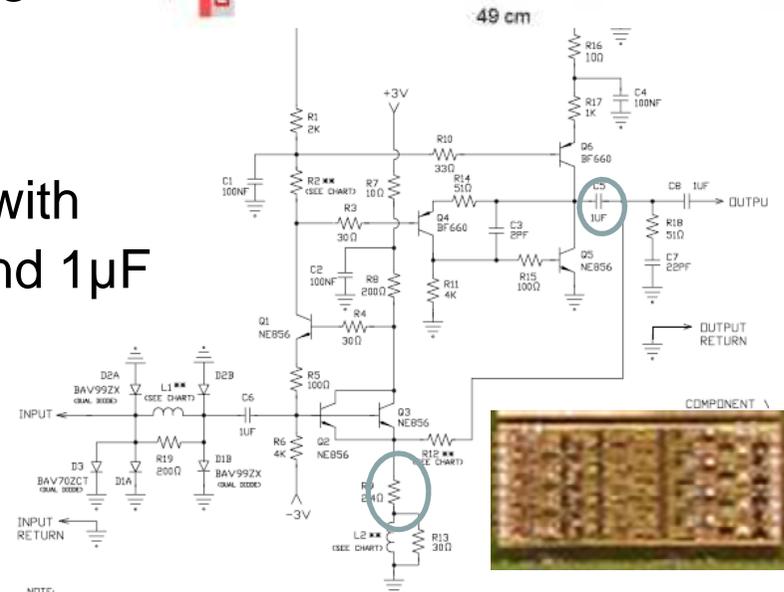
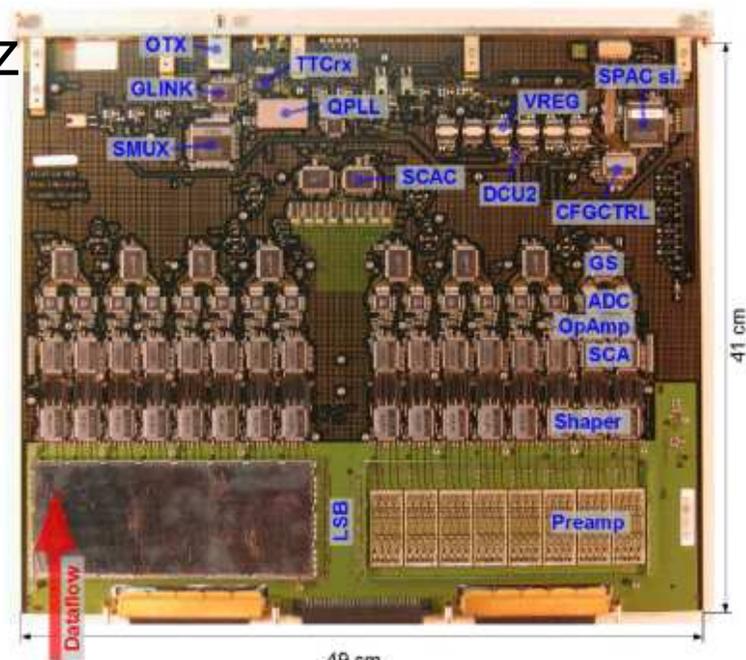
**Gisele Martin-Chassard**

# Upgrade motivations for front-end readout

- Speed up the digitization up to 40MHz
- Decrease power dissipation by 10  
→ Gather all blocks in an ASIC

**Cornerstone = Preamplifier :**  
“Universal” preamplifier with selectable dynamic range and input impedance (25/50 Ohm)

**Preamp : 0T configuration** with discrete components such as 2.4  $\Omega$  and 1  $\mu\text{F}$   
⇒ difficult to integrate in an ASIC  
⇒ New design



- Precise Input impedance  $Z_{in}$  50  $\Omega$  (Front) or 25  $\Omega$  (Middle/Back) to terminate the cables from the detector
- Low noise < 10  $\Omega$ , with  $C_d$  400 pF (Front) or 1 nF (Middle/Back) and  $t_p=50$  ns
- ENI as low as possible (large  $C_d$ , long duration signal) :  
0T50 400pF: ENI@50ns=55nA, 0T25 1.5nF: ENI@50ns=150 nA
- Dynamic range:
  - Input current 10  $\mu$ A up to 2 mA (Front)
  - Input current 10  $\mu$ A up to 10 mA (Middle/Back)
- Radiation resistance

# New line-terminating preamp

- New « negative noise figure preamp » (patent filed)

- Preamp Input impedance
  - Super Common Base: low input impedance
  - Amplifier = low noise voltage sensitive
  - Fine tuning of  $Z_{in}$  ( $\pm 5\%$ ) possible with  $C_2$

$$Z_{in}^{PA} = \frac{R_0 + Z_{in}(SCB)}{1 + |G|}$$

- Noise

- Electronically cooled resistor

$$\frac{4kTR_0}{(1 + |G|)^2}$$

- Preamp 50  $\Omega$ , 10 $\mu$ A to 2 mA max,  $C_d=400$ pF

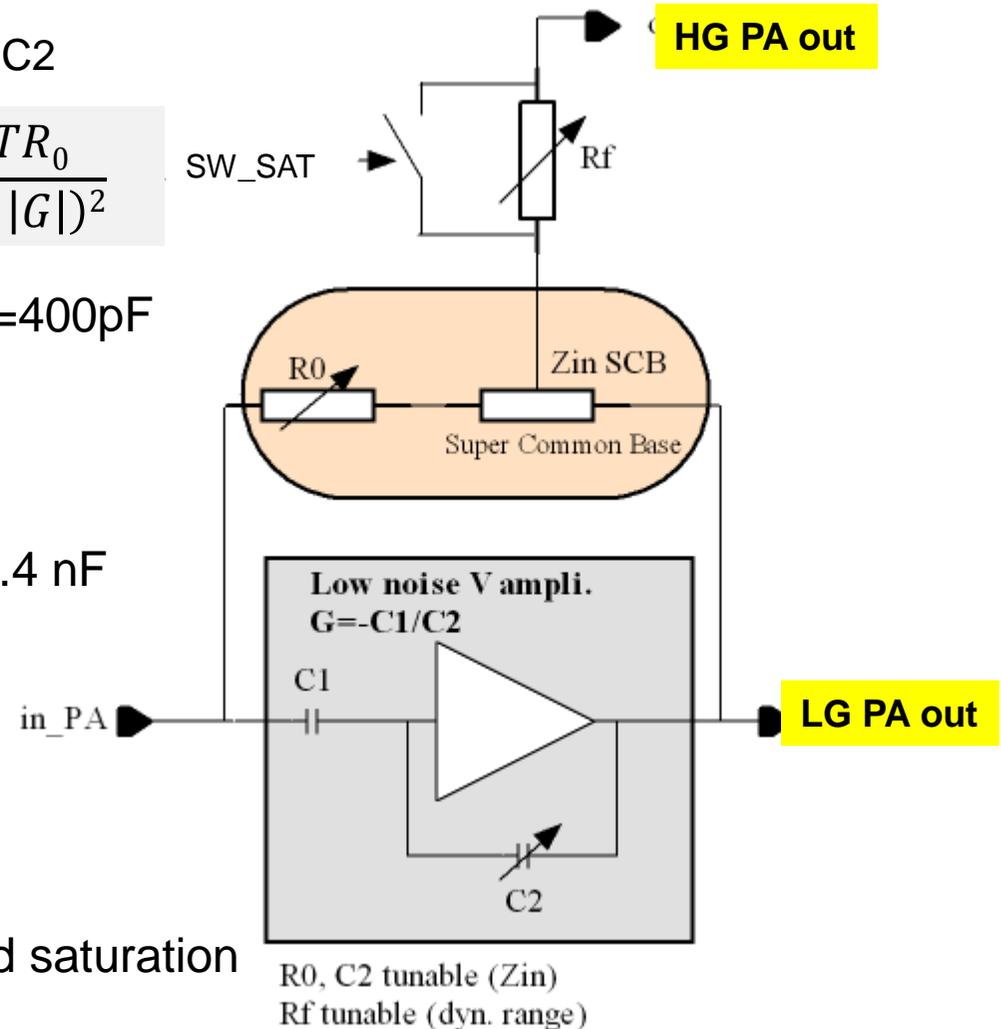
- $Z_{in}$  tuning:  $R_0= 500 \Omega$ ,  $G = -C_1/C_2=-9$
- Noise : 5  $\Omega$
- HG dynamic range:  $R_f=5$ K (or 10K)

- Preamp 25  $\Omega$ , up to 10 mA max,  $C_d=1.4$  nF

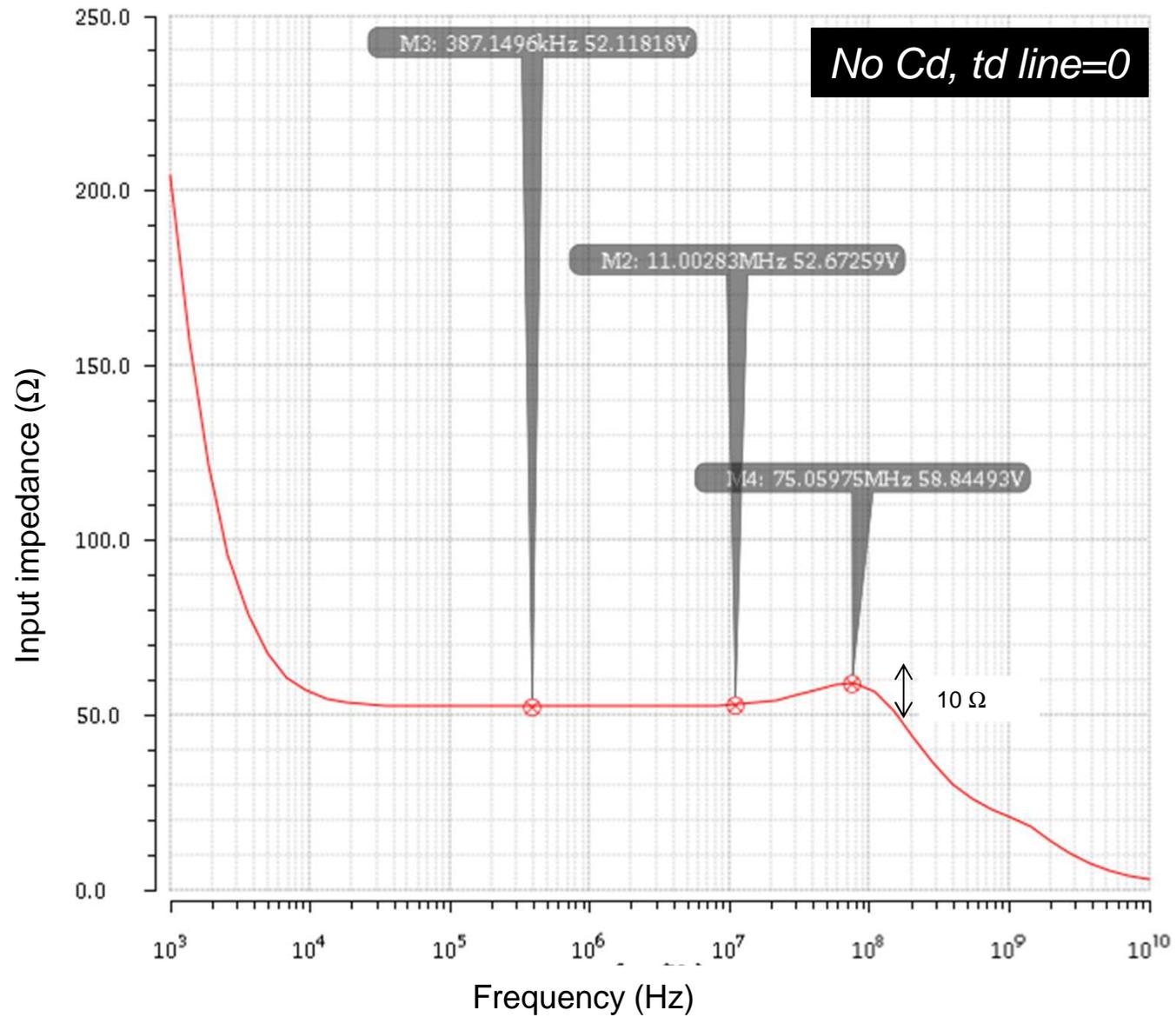
- $R_0= 100 \Omega$ ,  $G = -C_1/C_2= -3$
- Noise : 6  $\Omega$
- HG dynamic range:  $R_f=1$ K (or 2K)

- HG and LG outputs available :

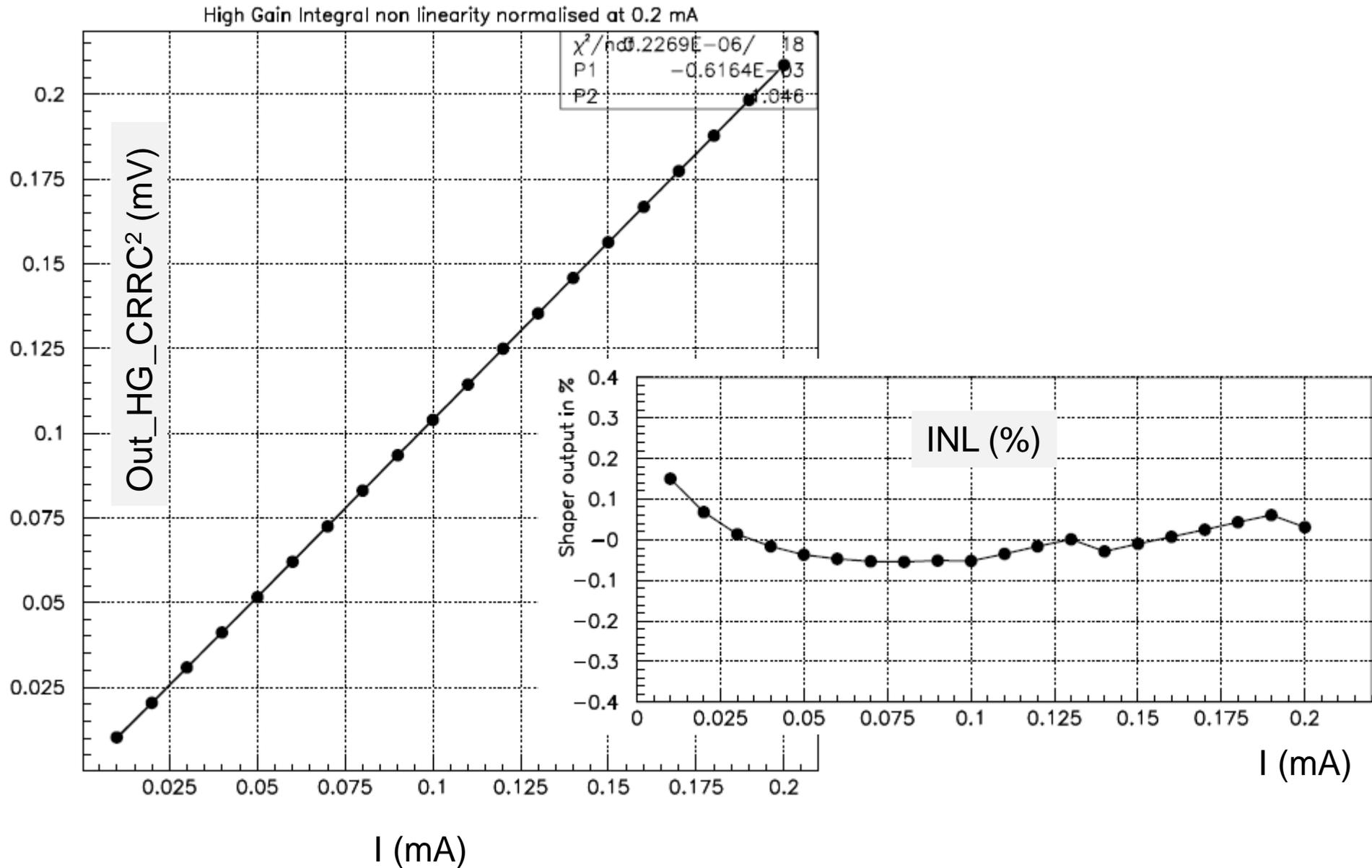
Switch (SW\_SAT) to short  $R_f$  and to avoid saturation



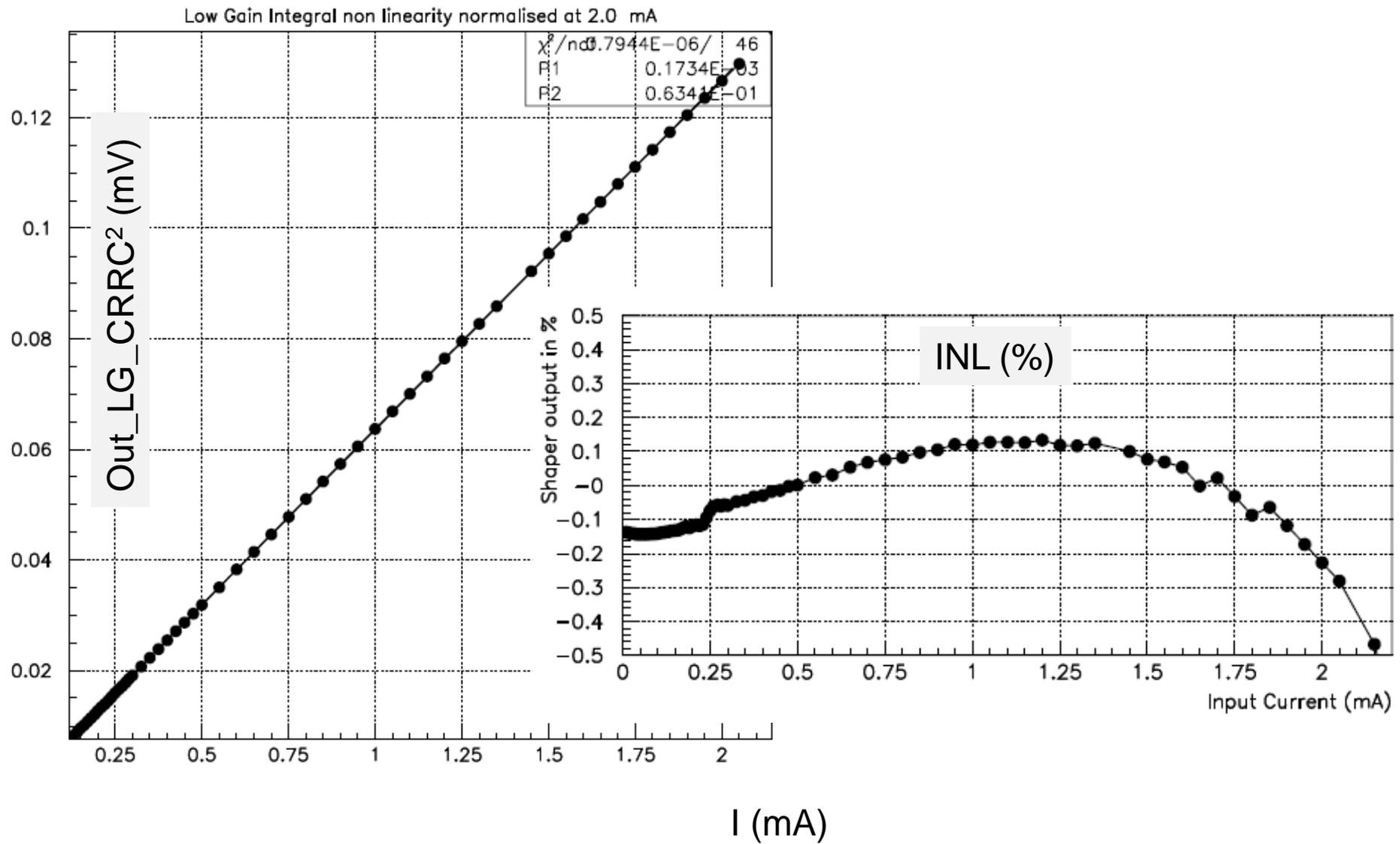
# Simulation results: Zin (50 PA) vs frequency



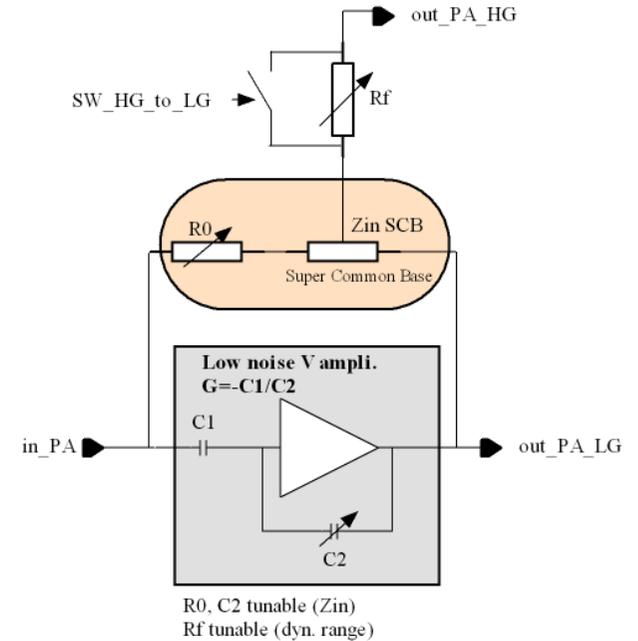
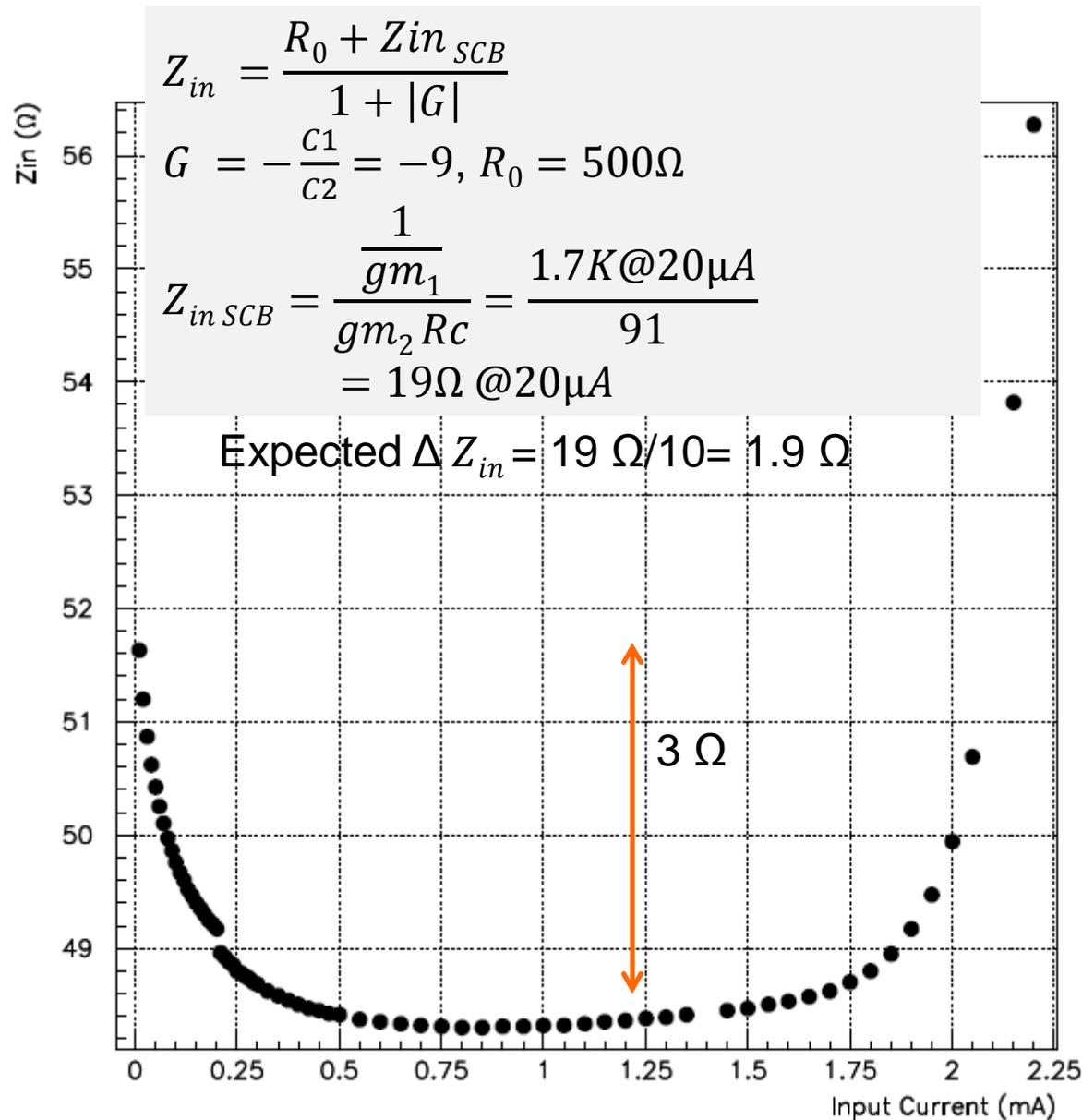
# Simulation results: 50 $\Omega$ HG CRRC<sup>2</sup> Linearity



# Simulation results: 50 $\Omega$ LG CRRC<sup>2</sup> Linearity

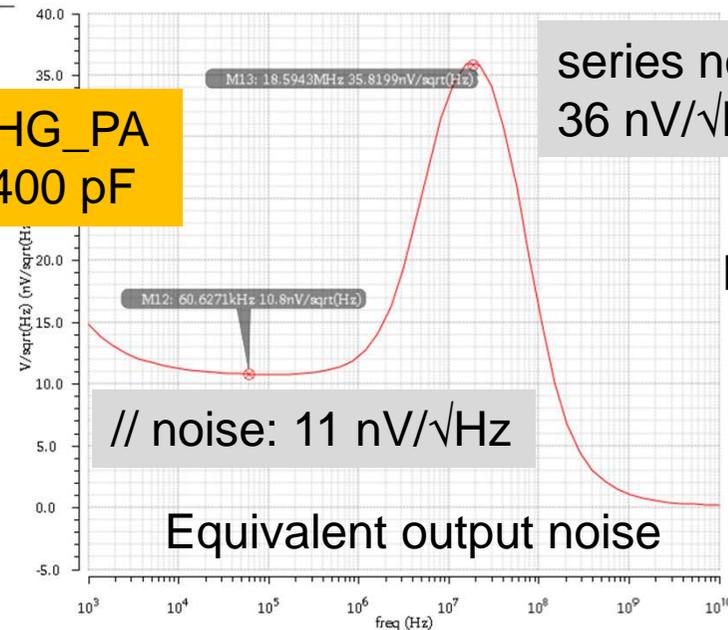


# Simulation results: $Z_{in}$ 50 $\Omega$ PA vs Input current



# Simulation results: HG 50Ω PA Noise

out\_HG\_PA  
Cd=400 pF



series noise  
36 nV/√Hz

$$\frac{4kTR_0}{(1+|G|)^2} \text{ with } G=-9$$

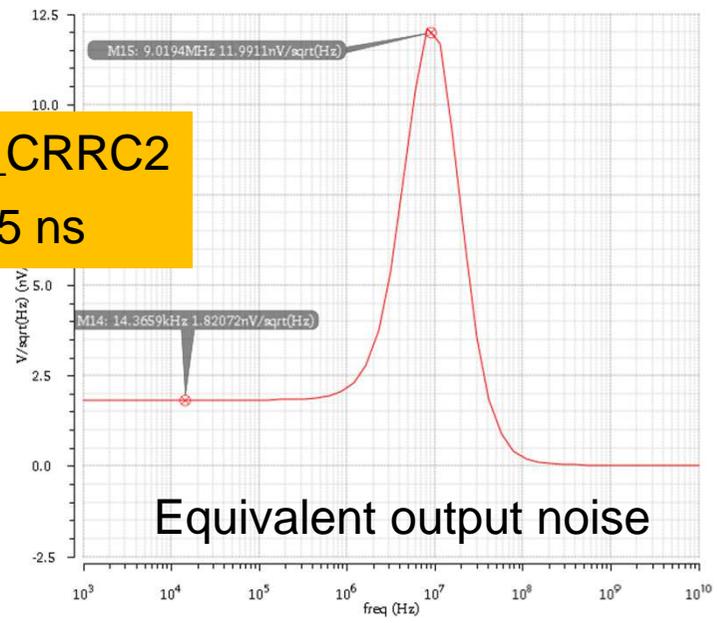
$R_0=500 \Omega \Rightarrow$  Equ. Noise: 0.28 nV/sqrt(Hz) or 5  $\Omega$

$\Rightarrow$  Voltage gain @ output of the preamp  $R_f / Z_{in}$   
 $=5K/50=100$

$\Rightarrow$  Input Noise: 36 nV/100=0.36 nV/√Hz or 8  $\Omega$

$\Rightarrow$  < 10  $\Omega$  requirement

out\_CRRC2  
 $\tau=15$  ns



rms noise= 46  $\mu$ V

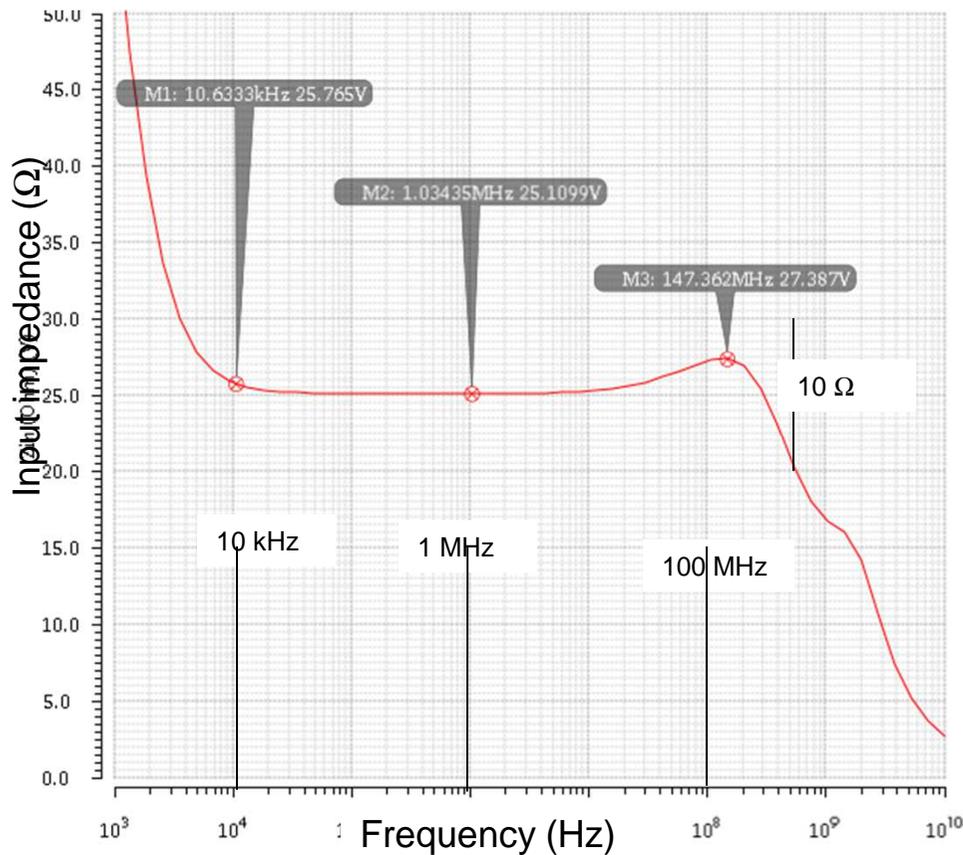
$I_{det}=100 \mu$ A gives 100 mV  
at the output of the HG CRRC2

$\Rightarrow$  ENI=46 nA

ENI similar to the ENI measured with the current 0T

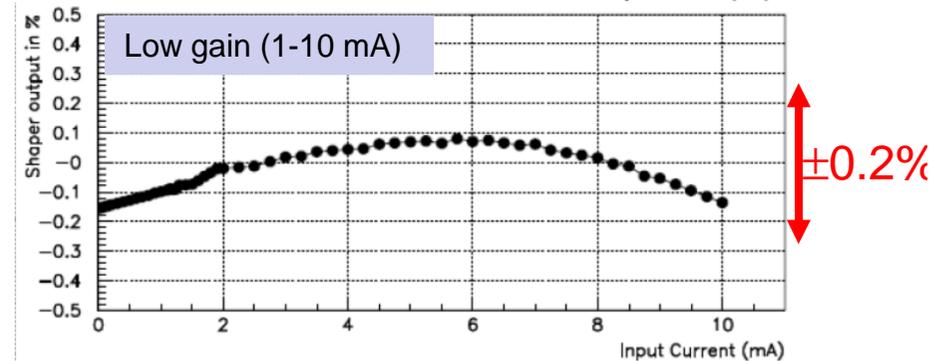
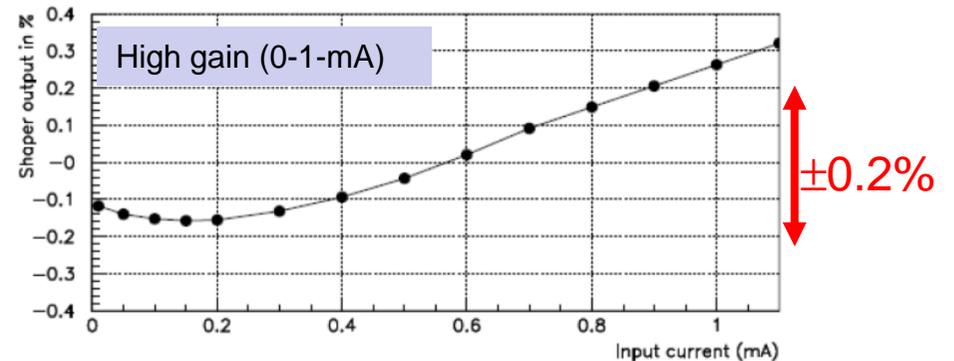
0T50 400pF: ENI@50ns=55nA,  
0T25 1.5nF: ENI@50ns=150 nA

# Simulation performance results (25 $\Omega$ /10 mA)



Impedance flat from 10 kHz to 100 MHz  
 $< 1 \Omega$  variation versus current due to Super Common base  $Z_{in}$  variation

Integral non linearity (/linear fit) with CR-RC2 (40 ns peaking time)



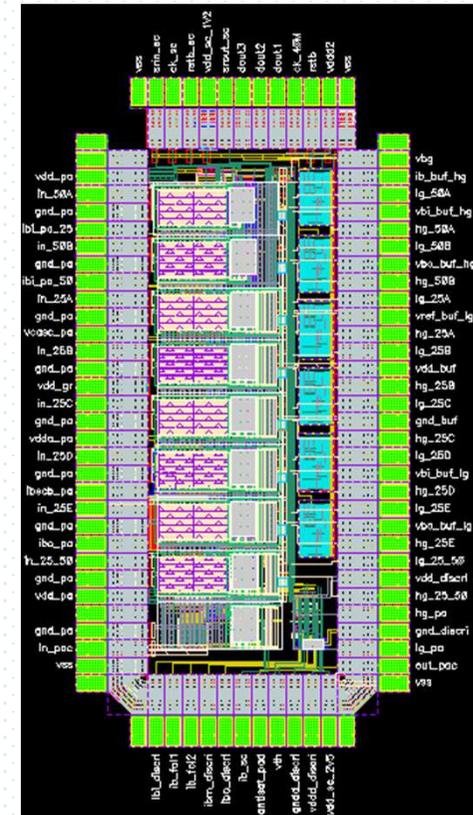
Noise dominated by R0 and NMOS ampli : 150 nA with 1.5 nF

# Chip submitted



8 channels with various preamps :

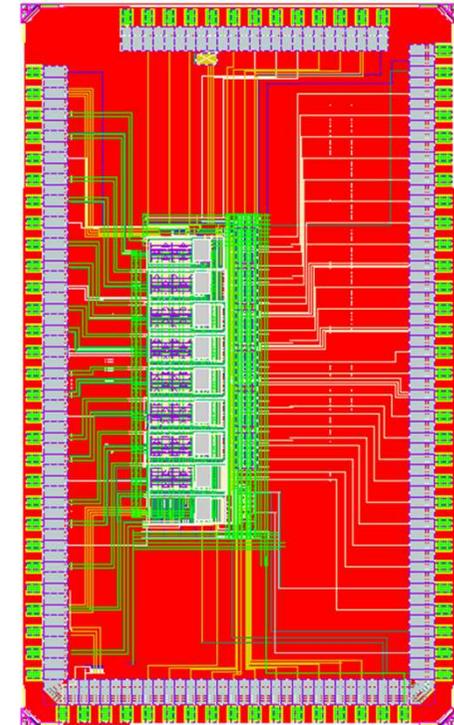
	Zin	Gain&Dyn range	Others
<b>PA 50A</b>	Fixed Zin (fixed R0 and C2)	Fixed Rf	
<b>PA 50B</b>	Adjustable Zin (with C2)	Adjustable Rf	
<b>PA 25A</b>	Adjustable Zin (with C2)	Adjustable Rf	Input trans area = Nominal size
<b>PA 25B</b>	Adjustable Zin (with C2)	Adjustable Rf	Input trans area = Nominal size/2
<b>PA 25C</b>	Adjustable Zin (with C2)	Adjustable Rf	Input trans area = 2xNominal size
<b>PA 25D</b>	Adjustable Zin (with C2)	Adjustable Rf	protection diodes
<b>PA 25E</b>	Fixed Zin (with C2)	Fixed Rf	
<b>PA 25-50</b>	Switches to choose 25 or 50 $\Omega$ Adjustable Zin (with C2 and R0)	Adjustable Rf	



Slow Control parameters and switches to change  $R_0$  and  $C_2$  (Zin) and  $R_f$  (dyn. Range)  
 Each PA can be switched OFF when not used. Outputs (HG and LG) go to pads thru buffer and LG go to discri  
 Discri provides antisat signal (1 architecture with 3 various grounding to characterize techno).  
 24-bit counter triple voting @ 100MHz to test the digital kit and to simulate digital activity in chip.

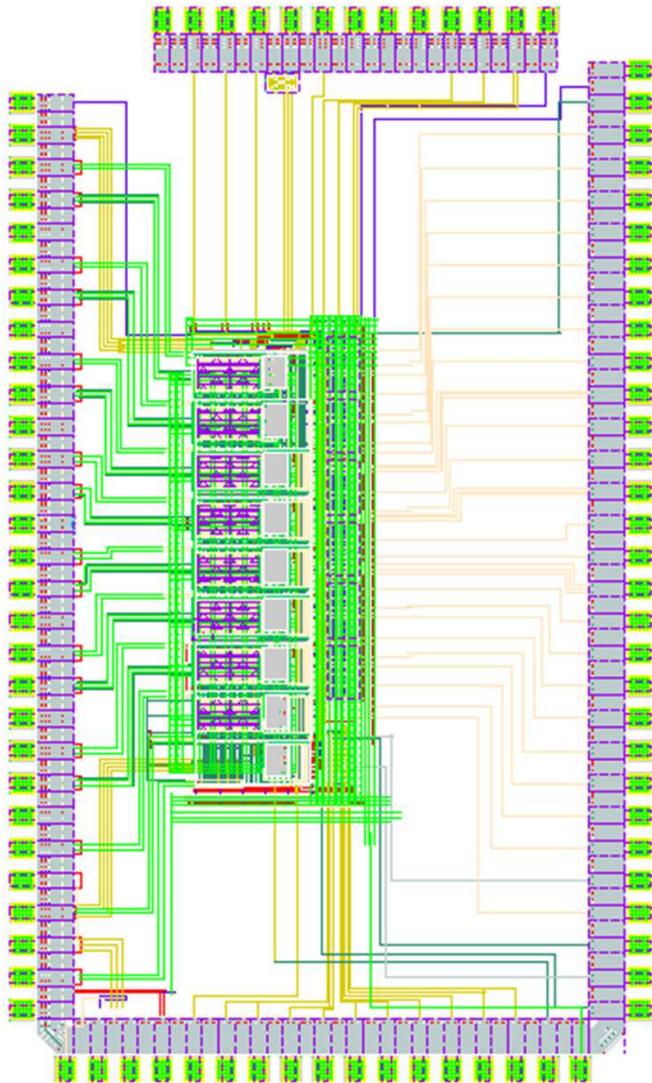
Use of 130 nm layout kit has shown to be a bit difficult but chip was submitted on May 15<sup>th</sup> through CERN/IMEC .

- Collaboration: LAL, OMEGA (+BNL)
  - LAL: N. Morange, L. Serin, S. Simion
  - OMEGA: P. Dinaucourt, C. de La Taille, G. Martin-Chassard, N. Seguin-Moreau
- Integrated preamp
  - 3 designs: OMEGA+LAL (130nm CMOS), BNL (65 nm CMOS) and Penn University (130nm SiGe)
  - Collaborative effort with BNL to converge toward common architecture
- Testbench designed by LAL + BNL
  - Preamps characterization
  - Irradiation tests









- Sealring :
- scribeline
  - corners
- Filling :
- diffusion
  - metalx
  - slots

