



# Mechanics studies at IN2P3

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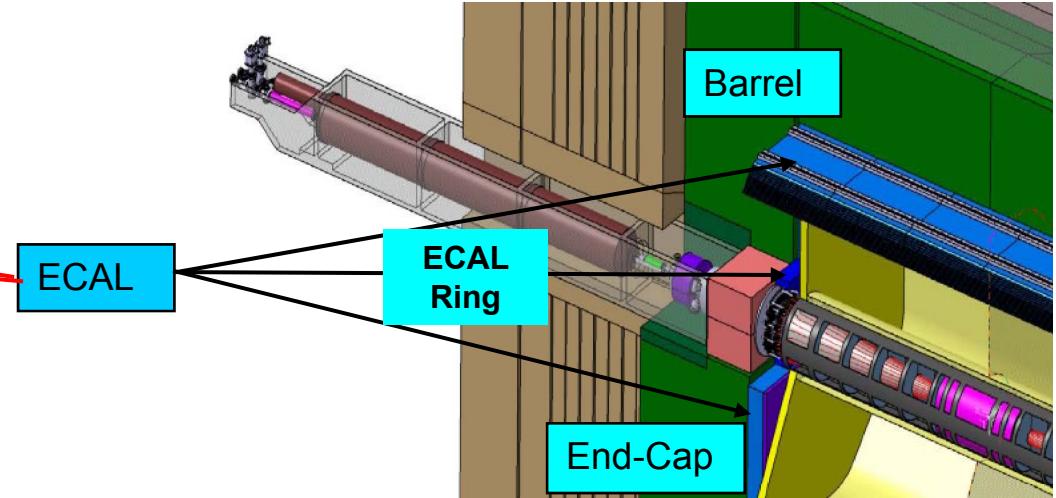
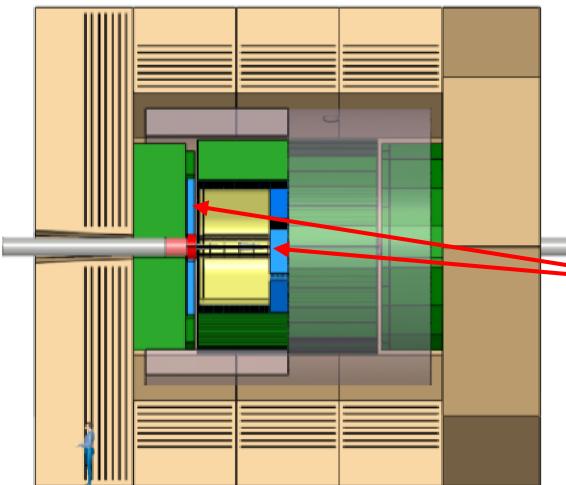
SOCLE 2008 @ LAPP



Denis Grondin / Marc Anduze – December 8 & 9<sup>th</sup>

# *Si-W ECAL: from ILD to R&D*

- Mechanical activities within IN2P3 on the ILD Electromagnetic Calorimeter



**ILD & CALICE** (20..)

**EUDET** (2009)

What we call “EUDET Module” is in fact the next SiW Ecal CALICE Prototype

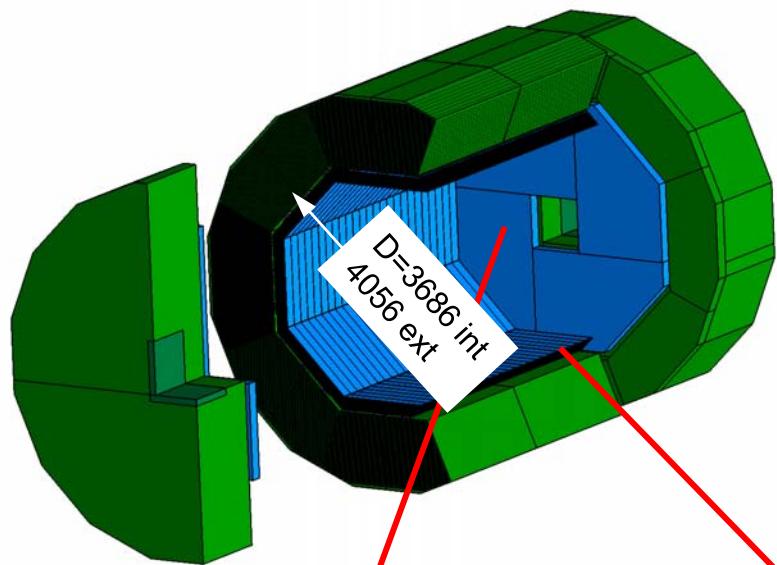


**Demonstrator** (2008-09)

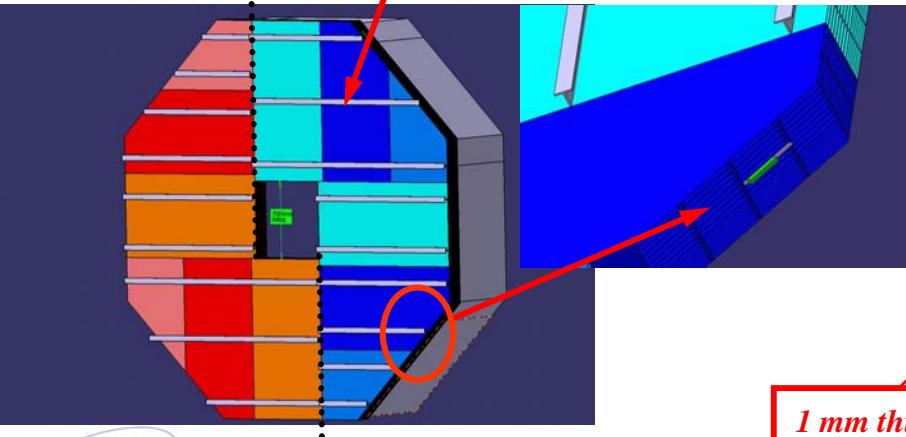


**Physical prototype** (2006)

# ECAL – Current baseline



Multi-module End-Cap

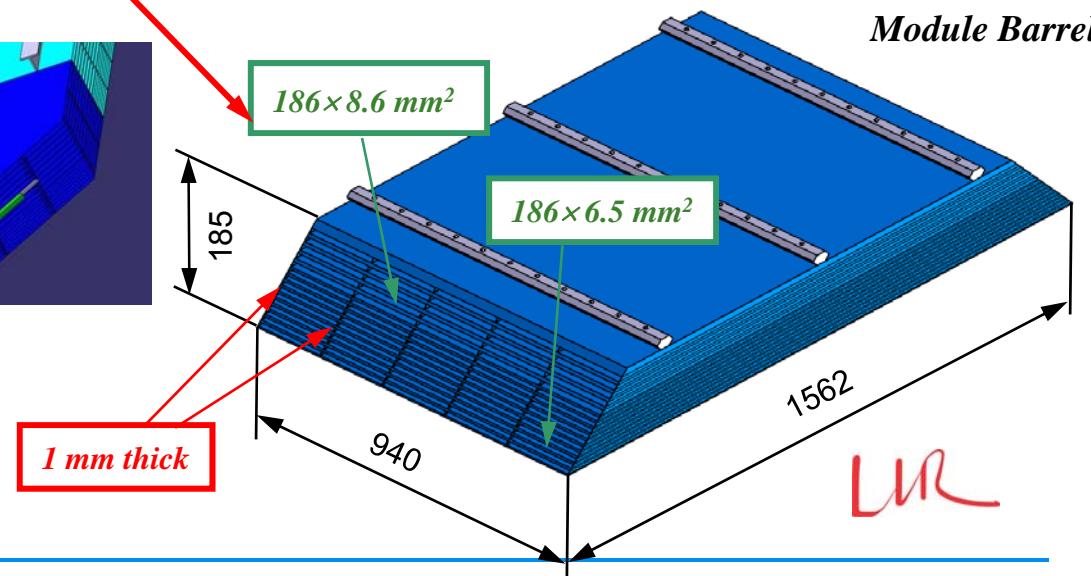


W/Si calorimeter (24  $X_0$  with 29 W layers)

Weight full ECAL:  $\sim 112$  T (80 barrel + 32 End-Cap)

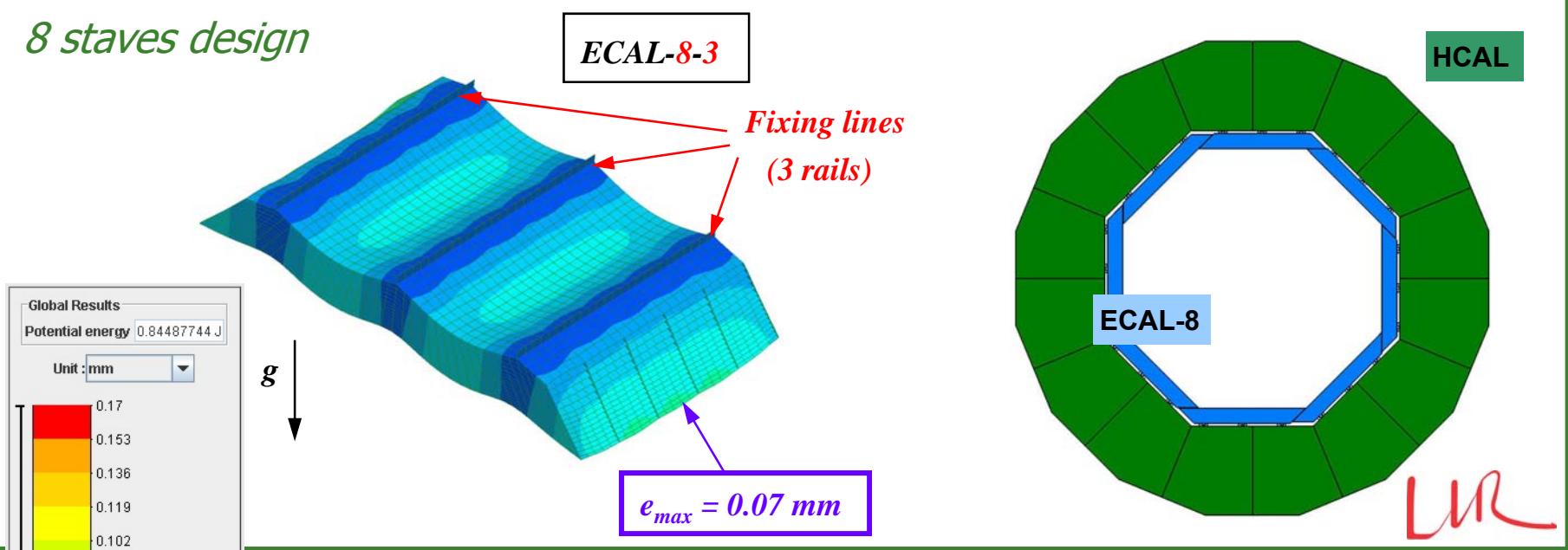
- Barrel : 40 identical trapezoidal modules
- End-Cap : constituted of 12 modules (3 types)
- ECAL module : alveolar structure - carbone fibers compound including half of W plates (fixed on HCAL End-Cap with rails)  
⇒ compactness and minimization of dead zones
- Detection elements (detector slab) in each alveolar case (Si+W), FE chips integrated, pad size : 5×5 mm<sup>2</sup>

Weight / module :  $\sim 2$  T

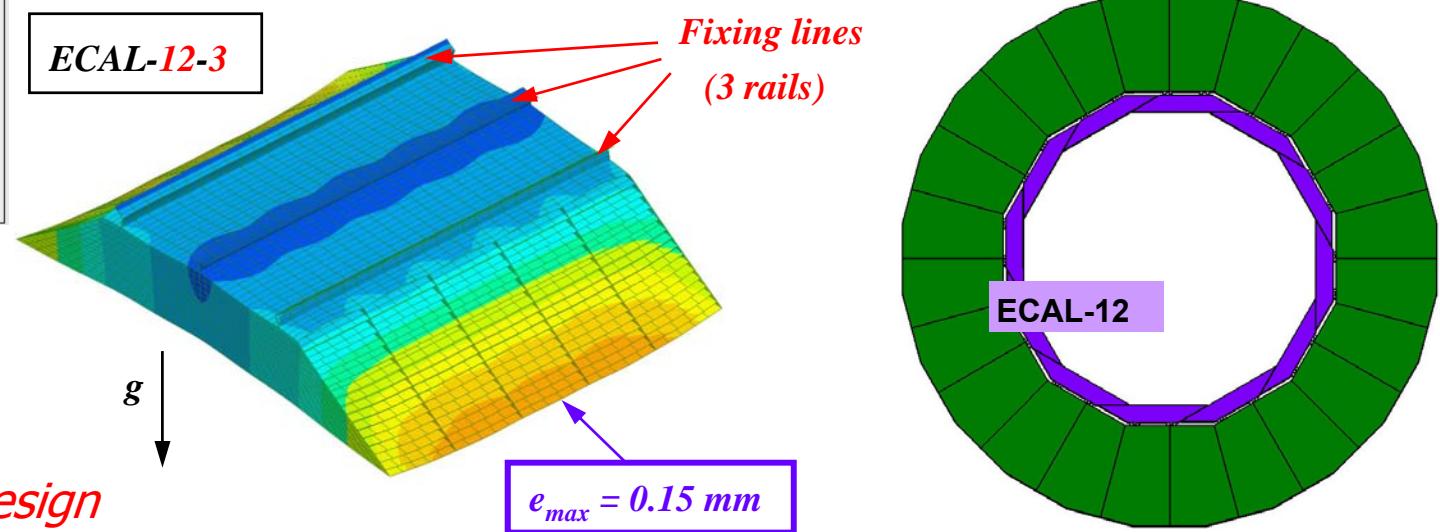


# ECAL - 8 vs 12 staves / HCAL

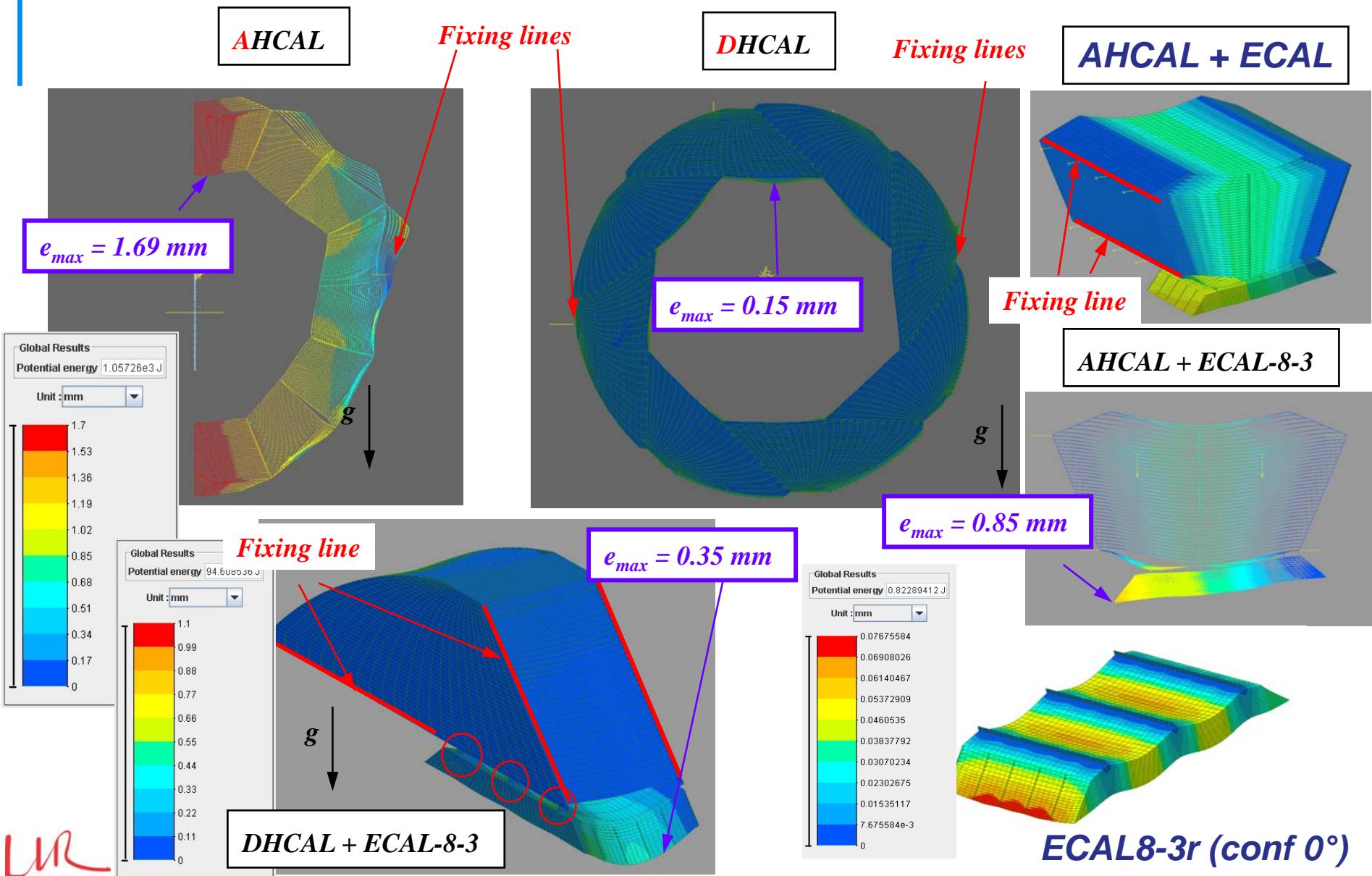
8 staves design



12 staves design



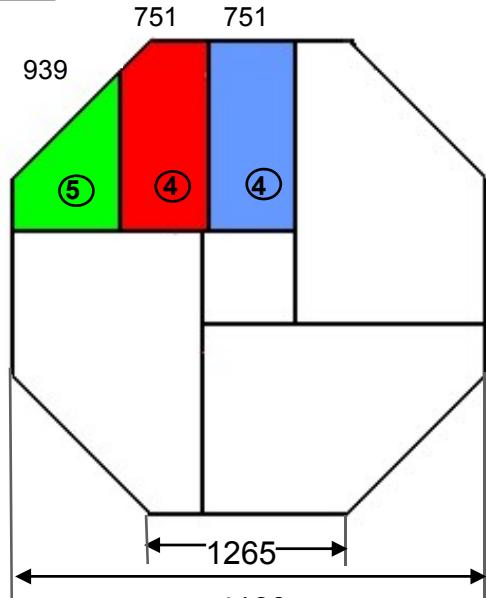
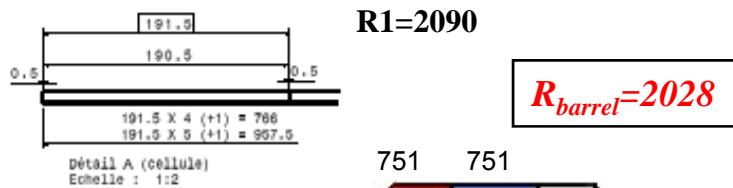
# AHCAL vs DHCAL structures



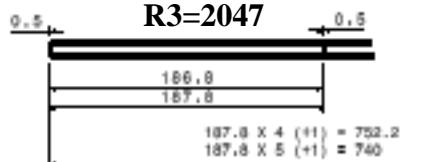
# ECAL - End-Caps design

- The same principle than barrel with an alveolar composite/tungsten structure, with different shapes and different sizes (width, end of slabs)
- 12 modules-3 distinct types (~780 cells & detectors slab)

## Design: 1

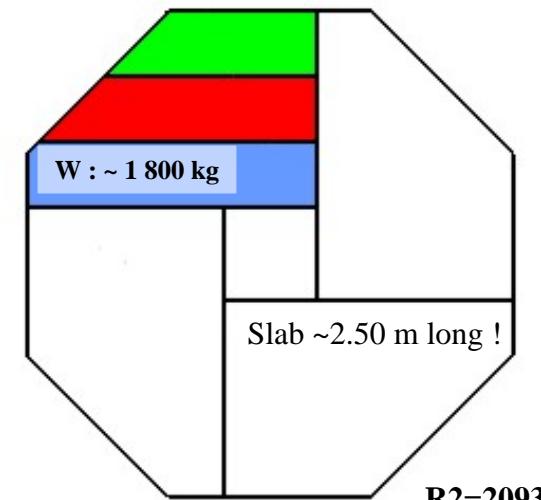
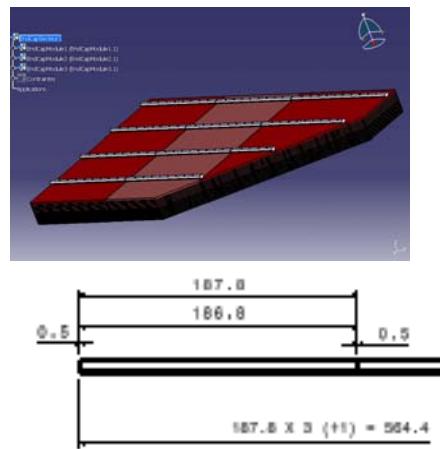


## Design: 3



## Design: 2

- Due to the possible crack in the geometry of design 1 the same general shape could be saved with different size and position of modules

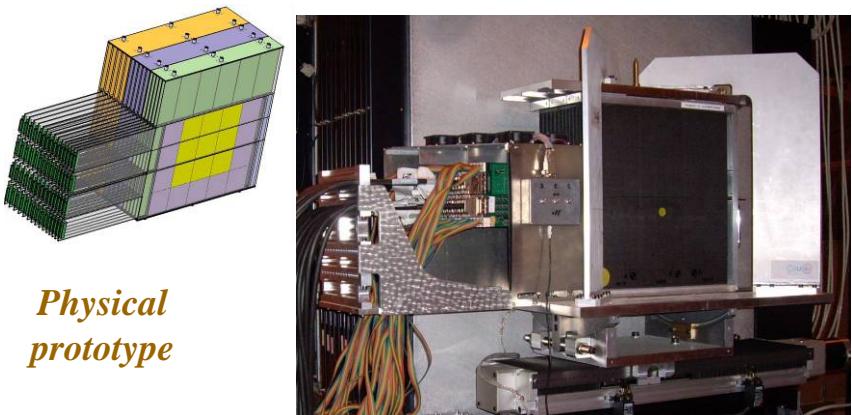


## Difficulties:

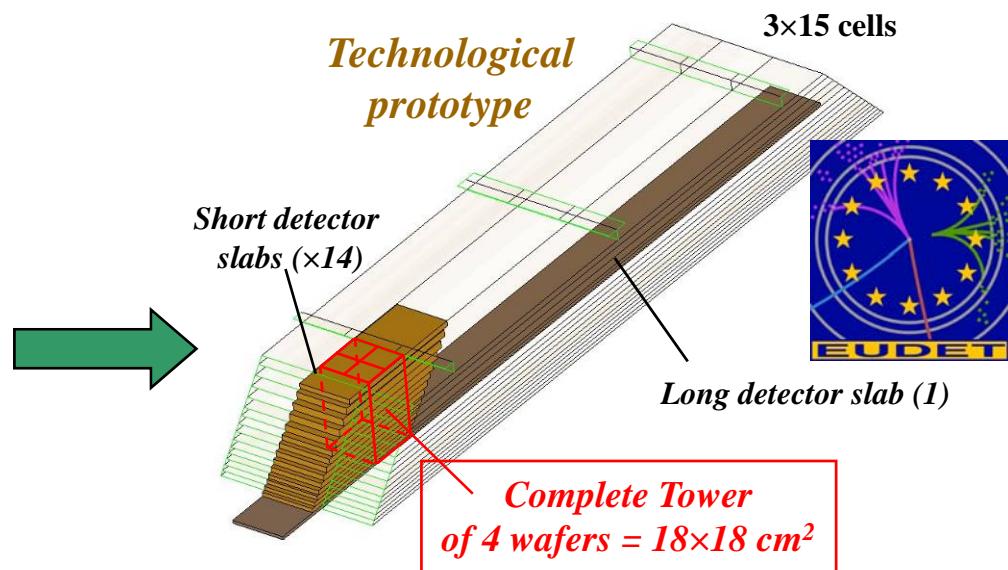
- Thermal (2.50m instead of 1.50m for longest):  $T^{\circ}$  dangerously rising in back-end of slabs
- Mechanical: >2.50m long thin alveoli maybe not feasible,
- Fastening system on HCAL /weight of module >3T ?
- Different shapes of long slabs: cost increasing

# Technological prototype : EUDET module

- Logical continuation to the physics prototype study which validated the main concepts : alveolar structure , slabs, gluing of wafers, integration
- Techno. Proto : study and validation of most of technological solutions which could be used for the final detector (moulding process, cooling system, sizes of structures,...)
- Taking into account industrialization aspect of process
- Finest cost estimation of one module



Physical prototype



**• 3 structures :  $24 X_0$   
( $10 \times 1.4\text{mm} + 10 \times 2.8\text{mm} + 10 \times 4.2\text{mm}$ )**  
**• sizes :  $380 \times 380 \times 200 \text{ mm}^3$**   
**• Thickness of slabs : 8.3 mm (W=1.4mm)**  
**• VFE outside detector**  
**• Number of channels : 9720 ( $10 \times 10 \text{ mm}^2$ )**  
**• Weight : ~ 200 Kg**

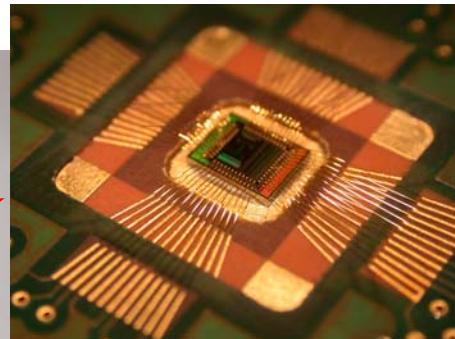
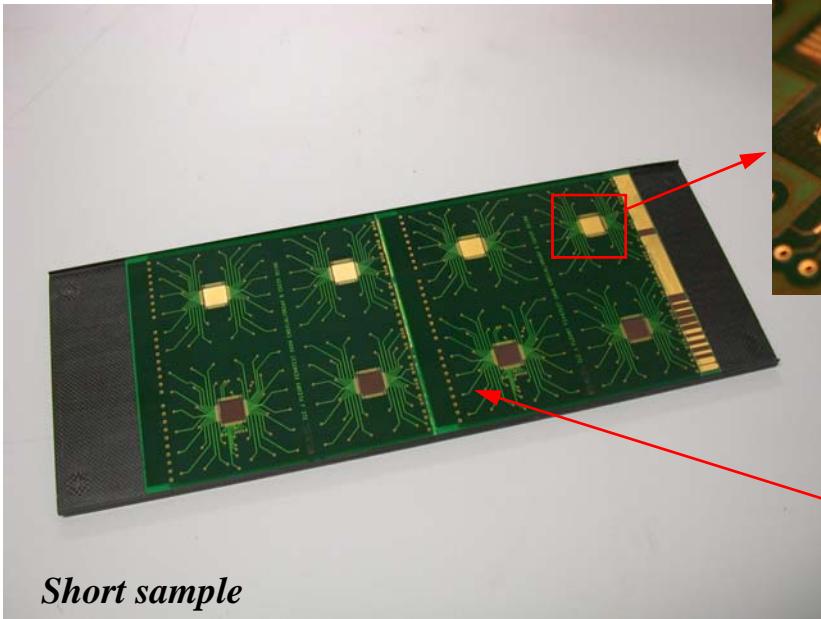
**• 1 structure :  $\sim 23 X_0$   
( $20 \times 2.1\text{mm} + 9 \times 4.2\text{mm}$ )**  
**• sizes :  $1560 \times 545 \times 186 \text{ mm}^3$**   
**• Thickness of slabs : 6.8 mm (W=2.1mm)**  
**• VFE inside detector**  
**• Number of chan. :  $\sim 37890$  ( $5.5 \times 5.5 \text{ mm}^2$ )**  
**• Weight : ~ 700 Kg**

# DéTECTEUR slab - principe

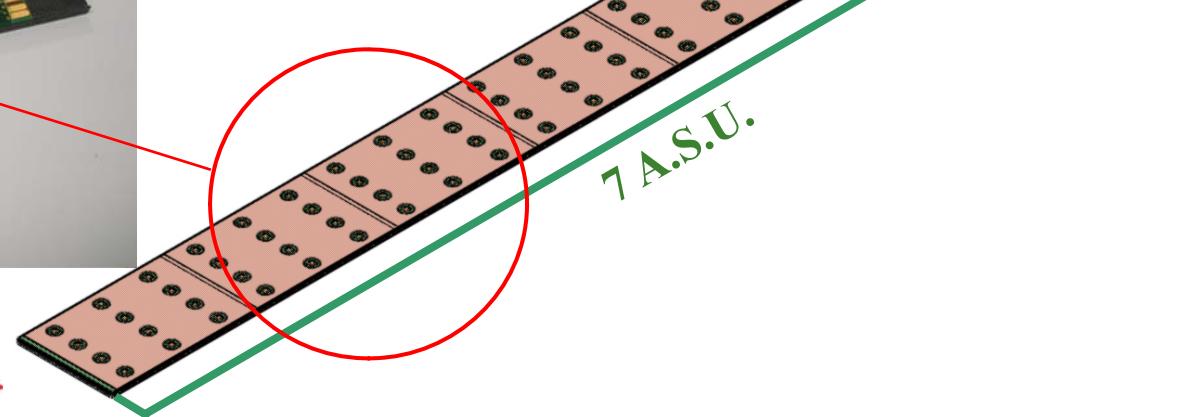
The slab is obtained with several short PCBs:

A.S.U. : Active Sensors Unit

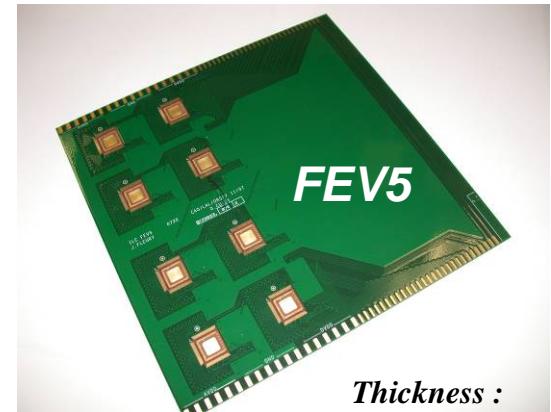
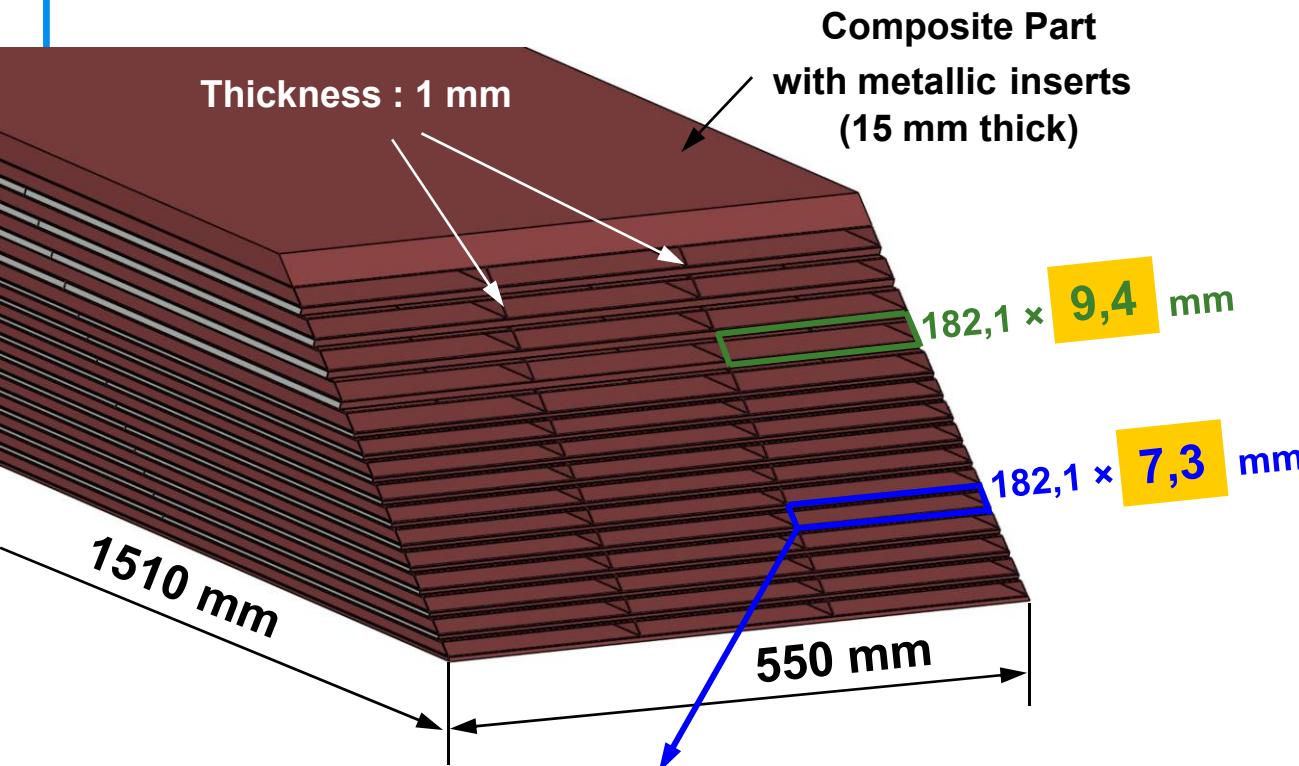
- Conception of **interconnexion** (gluing ?)
- Development easier : study, tests and integration of A.S.U **in parallel** of project
- The length of each slab is adjusted with one « end » PCB



*Chip embedded*



# EUDET - Current design (final)

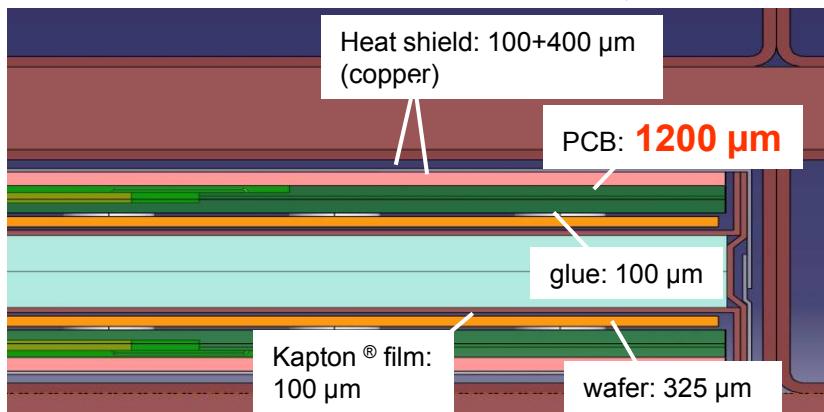


Thickness :

FEV5-1 : 1.17mm (+-0.04)

FEV5-2 : 1.19mm (+-0.04)

FEV5-3 : 1.20mm (+-0.02)

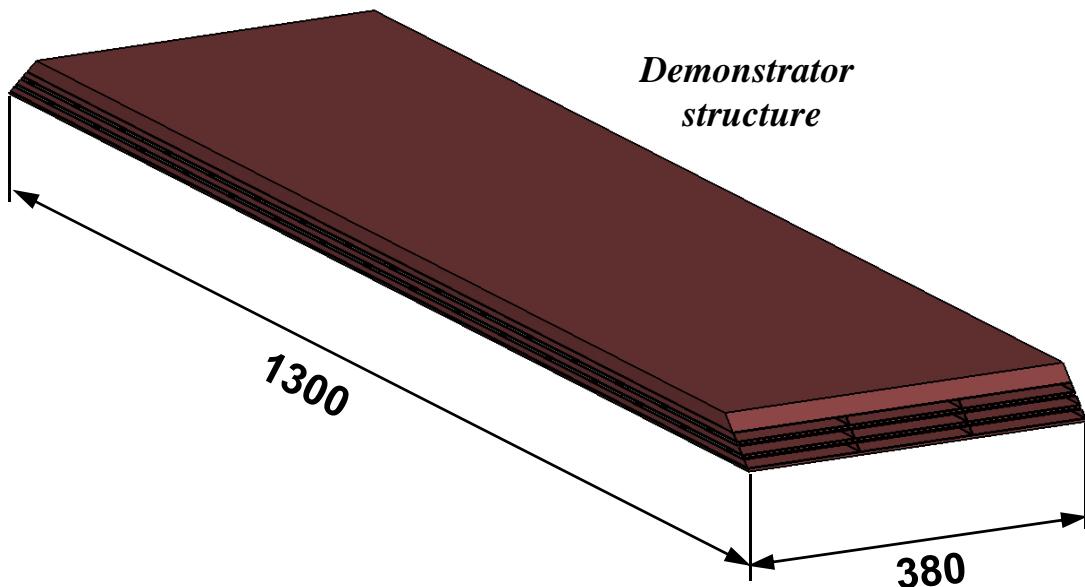


- ⇒ Gaps (slab integration) : 500  $\mu\text{m}$
- ⇒ Heat shield : 400  $\mu\text{m}$  ? Validation by the **demonstrator**
- ⇒ PCB : 800  $\mu\text{m}$  → 1200  $\mu\text{m}$
- ⇒ Thickness of glue : 100  $\mu\text{m}$
- ⇒ Thickness of wafer : 325  $\mu\text{m}$
- ⇒ Kapton® film HV : 100  $\mu\text{m}$  ? → Patrick's talk
- ⇒ Thickness of W : 2100/4200  $\mu\text{m}$  ( $\pm 80 \mu\text{m}$ ) **LM**

# Demonstrator design

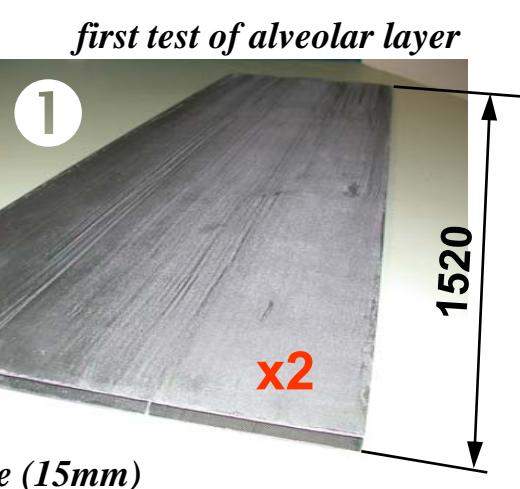
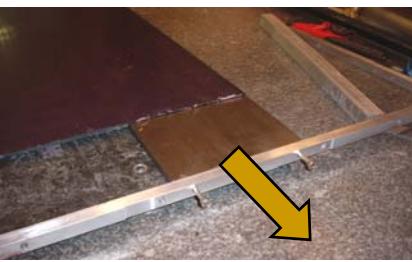
- We plan to build a first **small demonstrator** to validate all composite process before the EUDET module
- Width is based on physic prototype (124 mm)
- Used for **thermal studies** and analysis : design of a thermal PCB and cooling system.
- First test of **slab integration** (gluing, interconnection ...)

- **3 alveolar layers + 2 W layers**
- **3 columns of cells** : representative cells in the middle of the structure
- **Thermal studies support**
- **Width of cells** : **126 mm**
- **Identical global length** : **1.3m** and shape (trapezoidal)
- **Fastening system ECAL/HCAL**



# Demonstrator – Alveolar structure

Assembled structure : Each alveolar layer ① are done independently , cut to the right length and angle (②) and bonded alternatively with W plates in a second curing step. The assembling is closed by 2 composite plates ③ of 15 mm and 2 mm thick (from LPSC)



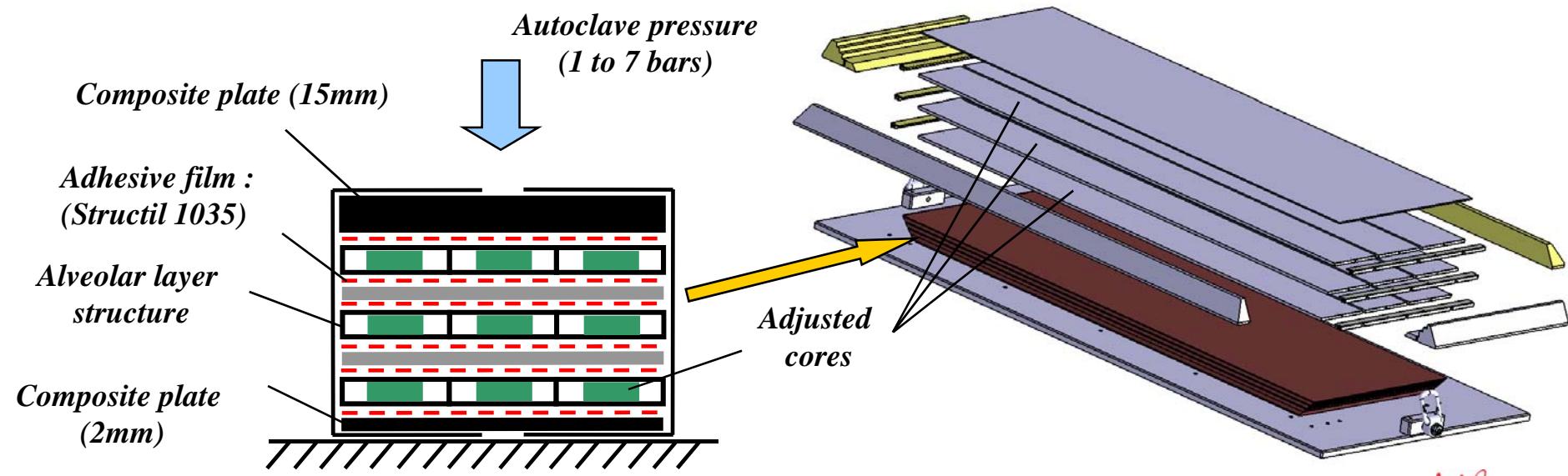
- ⇒ Global design : **OK**
- ⇒ 2/3 “Alveolar layer” structure ① : **OK**
- ⇒ Cutting test ② : **OK**
- ⇒ Composite plates (15mm and 2 mm) ③ : **OK**

# Demonstrator – Assembly mould

Several issues to be studied and validated yet:

- cores system for the assembly solution : use of **adjusted metallic cores** (in thickness) keeping each alveoli against W plates to obtain a correct assembly during the curing
- Curing parameters (thermal inertia)
- Reduce **costs** by changing the kind of carbon fibers
- Tests of deformation measurements by **sensors** embedded in the structure  
(optical fibers with bragg grating)

⇒ Design of mould : **OK**  
⇒ Ordered : **OK**  
⇒ W Needs : **OK**

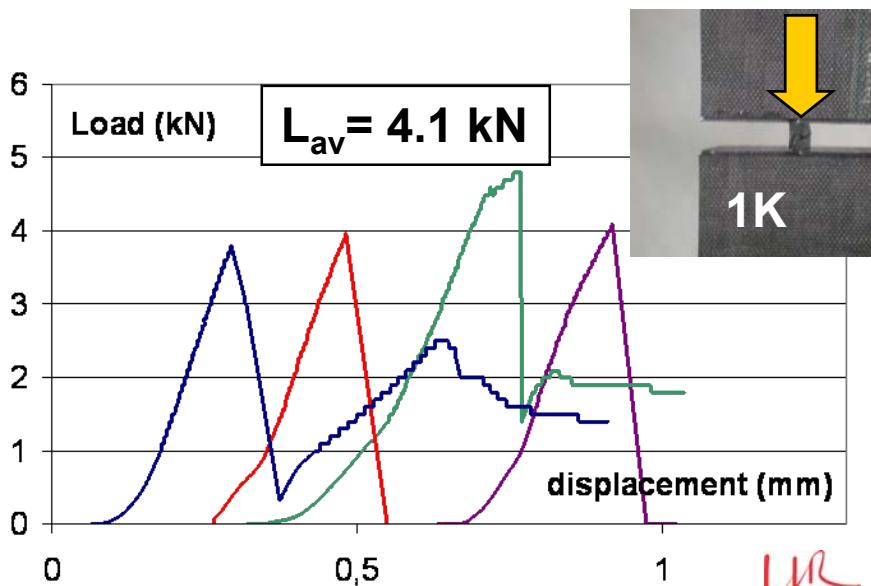
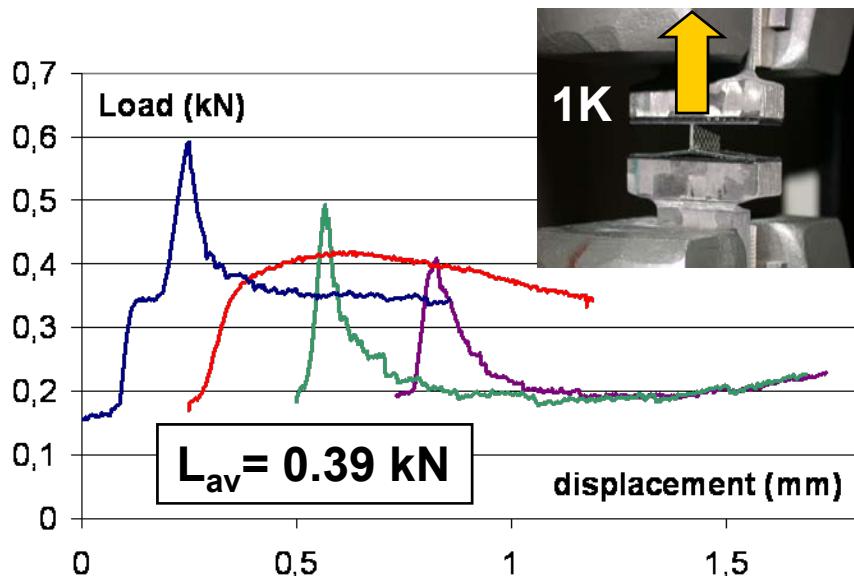
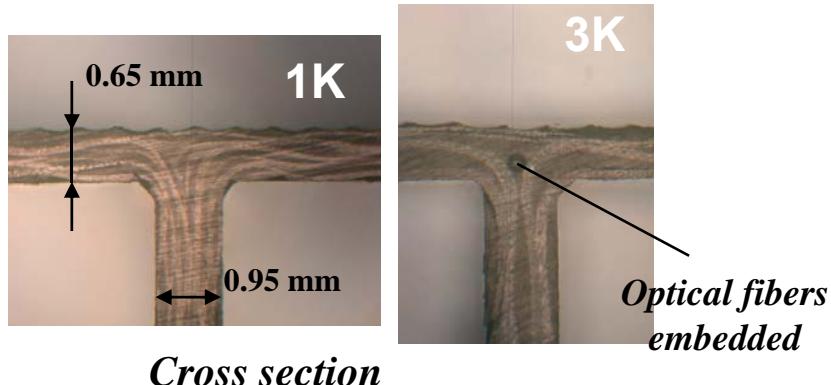


LUR

# Mechanical tests

- Destructive tests of inter alveolar walls until breaking of interface in order to evaluate loads and elongations under Tensile and compression loading cases
- 2 kinds of carbon fibers :
  - CC120 (1K) : 0.12 mm thick ; 130€/m<sup>2</sup>
  - CC202 (3K) : 0.25 mm thick ; 65€/m<sup>2</sup>

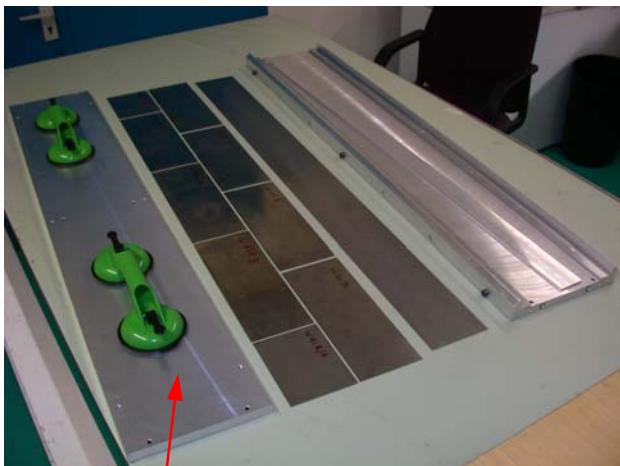
- ⇒ Destructive tests 1K: *OK*  
 ⇒ Destructive tests 3K: *ongoing*  
 ⇒ Measurements with optical fibers: *ongoing*



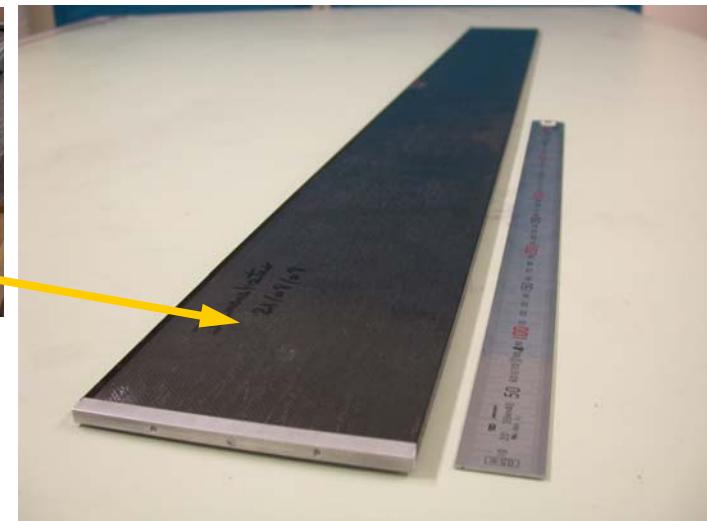
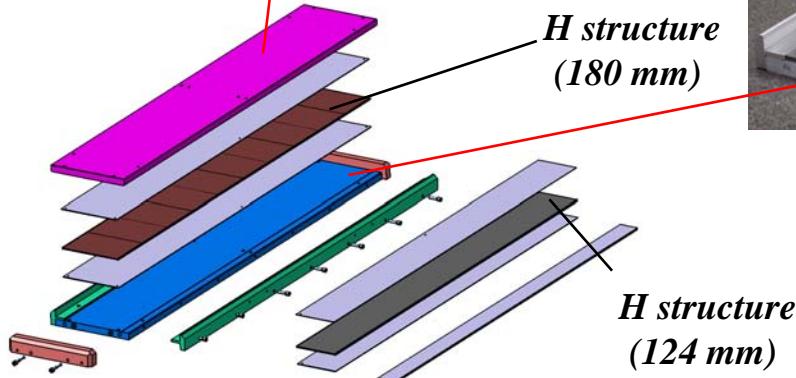
# Demonstrator - H structure

## Study of one mould for whole structures:

- Same principle than the mould used to do H physical prototype structures but using the autoclave)
- One long mould for both long and short H structures and 2 width (124 and 180 mm)



⇒ Design : **OK**  
⇒ Mould machining : **OK**  
⇒ H structure for demonstrator : **OK**



# Cooling: global circulation

## Power results :

2 FPGA per SLAB, power: 3 W each, then :  $3 \times 2 = 6$  W  
 SKIROC : 0.54 W / slab       $\rightarrow$  0.3 W soit :  $2 \times 0.3 = 0.6$  W

### Barrel :

Global Power : 19484 W       $\rightarrow$  3029 W

Power per module : 487 W       $\rightarrow$  75.7 W

Power per column : 97.4 W       $\rightarrow$  15.1 W

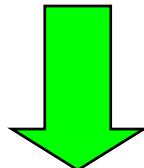
### End Cap :

Power per End Cap : 5060 W       $\rightarrow$  768 W

Average power per module :  $420 \text{ W } (390+390+480)/3$        $\rightarrow$  64 W

Average power moyenne per column : 97 W       $\rightarrow$  15 W

Global Power : 30 000 W       $\rightarrow$  4565 W !



## Rough estimate on fluid circulation:

Global flow rate : 150 l/min

Variation of fluid temperature :

in-out  $\Rightarrow 3^\circ\text{C}$

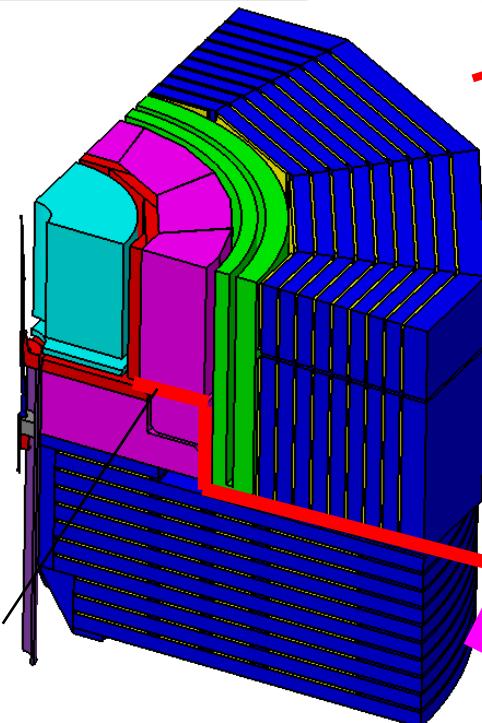
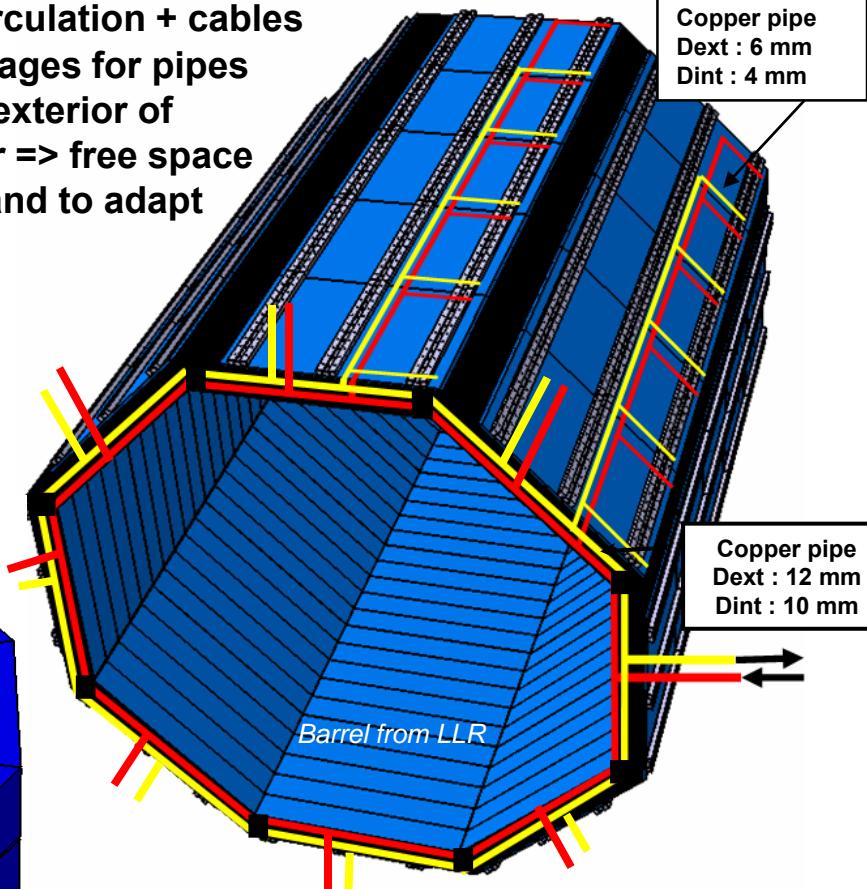
Fluid speed  $< 2$  m/s

Maximal pressure drop : 1.2 bar

1 feedind line for each group of 5 modules

## Fluid circulation + cables

=> passages for pipes toward exterior of detector => free space to find and to adapt

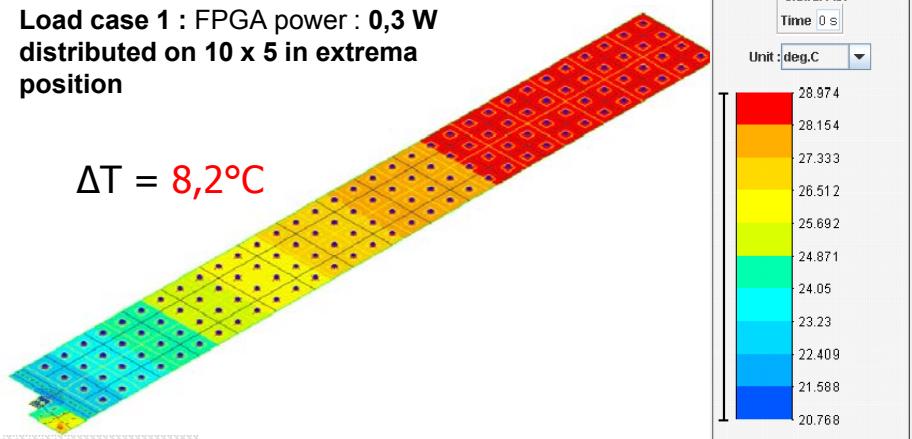


- Passage for pipes and cables under rails (machining on composite surface)
- Connection of pipes according mounting procedure for modules

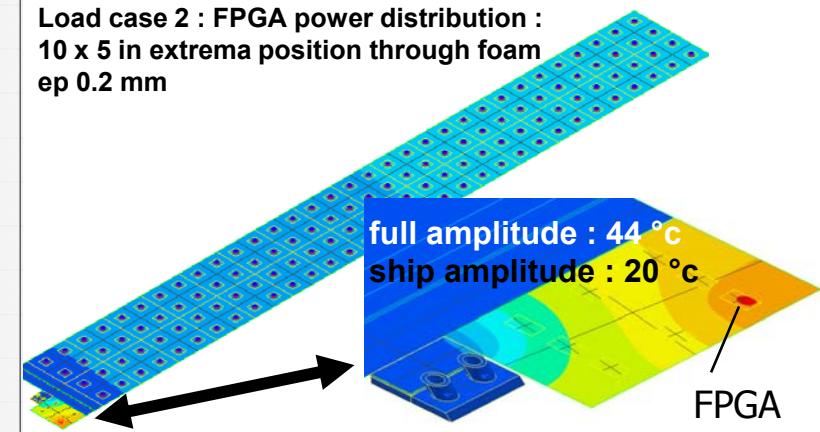
# Thermal analysis of slab

**Simulation** of heat conduction just by the heat copper shield : Influence of the **FPGA dissipation** (DIF) on current design of cooling system (Limit Condition of 20°C, with Main plate : 0.3 mm; Upper plate : 0.1 mm; L = 1,55 m; Copper layer :  $\lambda = 400 \text{ W/m/K}$  )

Load case 1 : FPGA power : 0,3 W distributed on 10 x 5 in extrema position

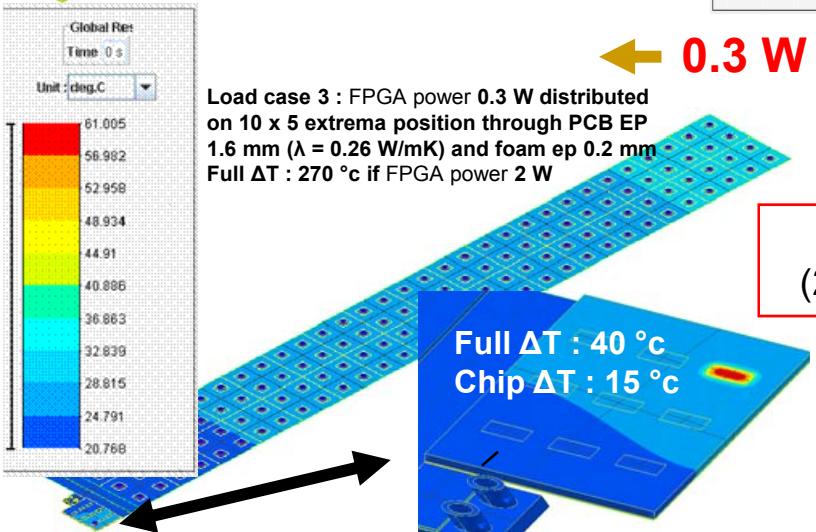


Load case 2 : FPGA power distribution : 10 x 5 in extrema position through foam ep 0.2 mm



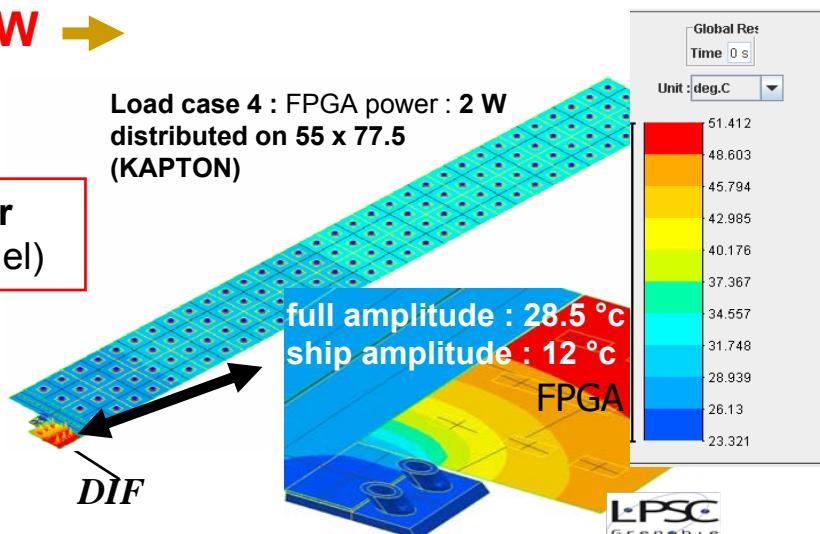
$$0.3 \text{ W} < \text{FPGA} < 2 \text{ W}$$

Load case 3 : FPGA power 0.3 W distributed on 10 x 5 extrema position through PCB EP 1.6 mm ( $\lambda = 0.26 \text{ W/mK}$ ) and foam ep 0.2 mm Full  $\Delta T$  : 270 °c if FPGA power 2 W



$$\Phi = 0,27 \text{ W/layer} \\ (25 \mu\text{W per channel})$$

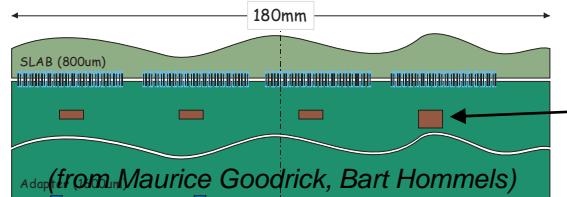
Load case 4 : FPGA power : 2 W distributed on 55 x 77.5 (KAPTON)



...better cooling if direct contact with FPGA !

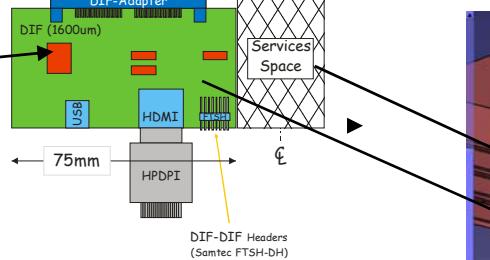
# SLAB COOLING – CONSTRAINTS

Mechanical constraints on ECAL electronics:  
Place available , heat sources power & situation

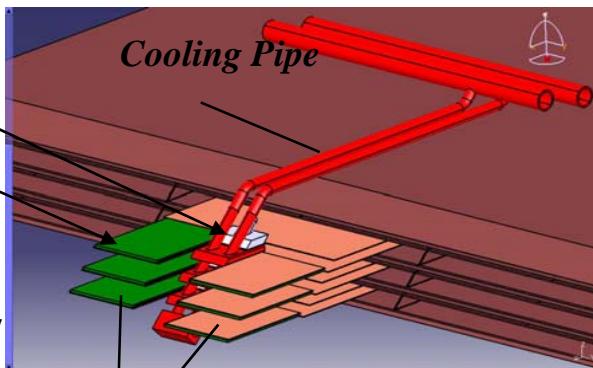


Hot points on  
interface card ?

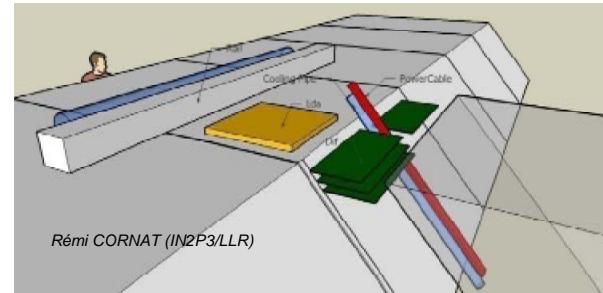
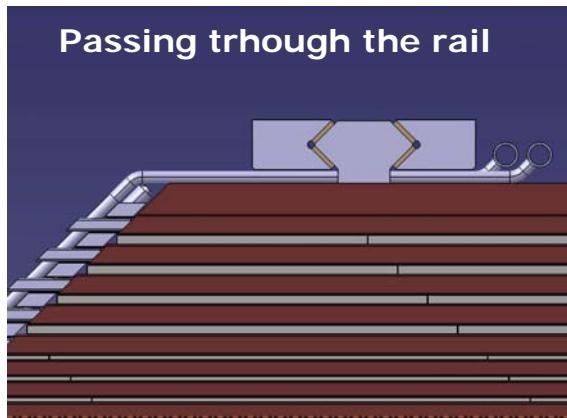
FPGA



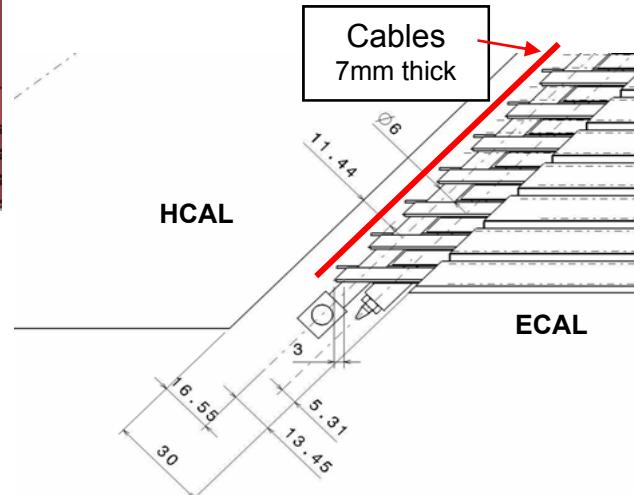
DIF is part of last ASU of the SLAB  
Minimum Space for cooling necessary



Demonstrator: cooling and  
copper drain extremities



Place for cabling : DAQ + HV  
+ GND  
Service space between cooling  
and HCAL >1cm



Space for HV and GND

# SLAB COOLING - EUDET

## Boundary condition:

Thermal foam :  $\lambda = 3 \text{ W/mK}$

Convective flux into pipe with fluid at 20°C ( $h = 3445 \text{ W/m}^2 \cdot \text{K}$ )

## Load (for 1 half slab = 1 side)

Channel heat flux : 25  $\mu\text{W}$

Number of channel / chip : 64 (Hardroc)

Number of chip / wafer : 4

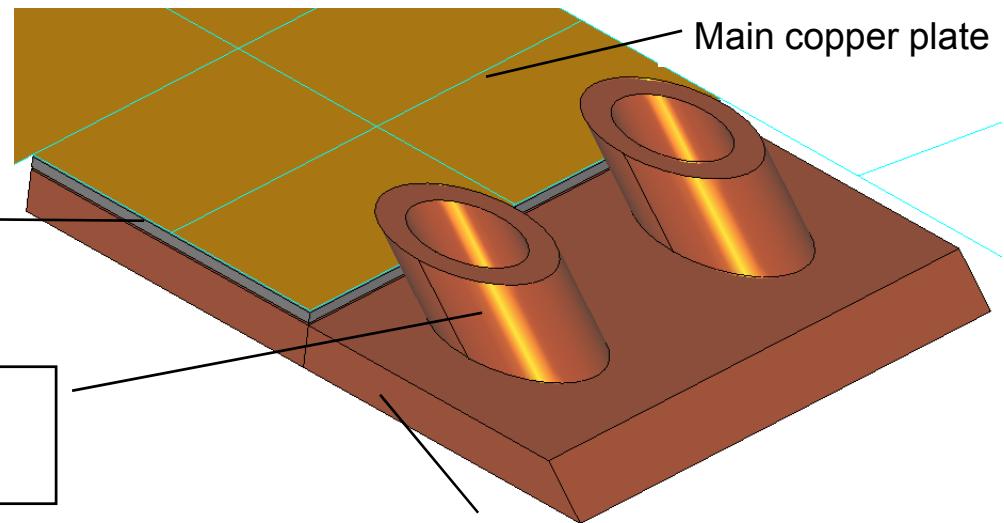
Number of wafer on  $\frac{1}{2}$  SLAB : 32

Total wafer power :

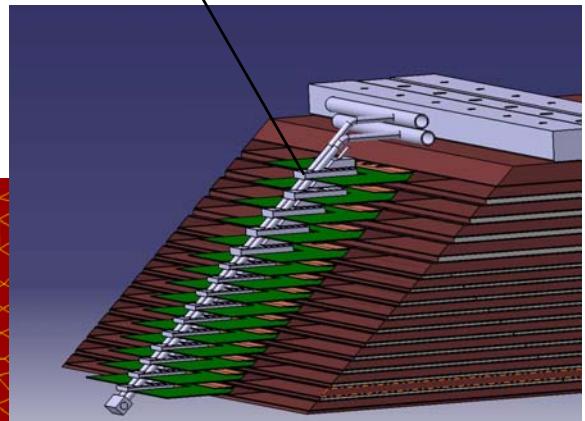
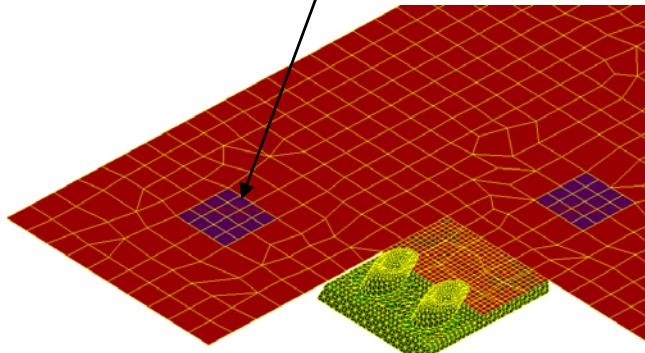
$$25 \times 10^{-6} \times 64 \times 4 \times 32 \\ = 0.205 \text{ W}$$

FPGA power : 0.3 W nominal

=> up to 2 W for test



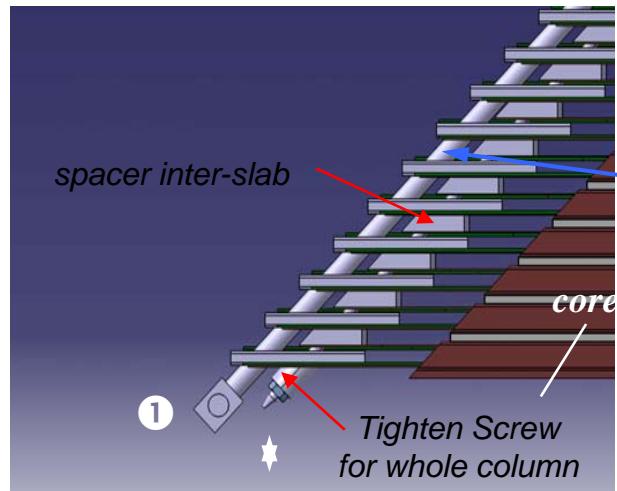
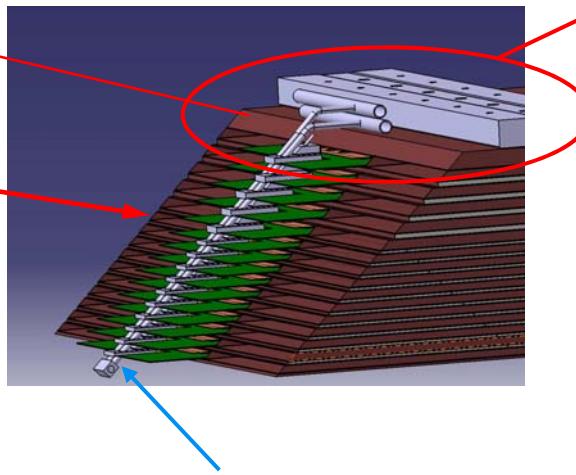
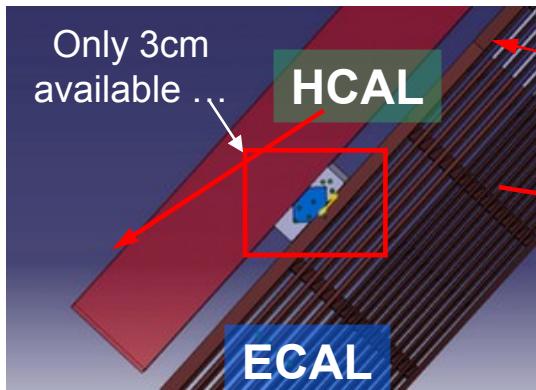
Heat surface and temperature point (FPGA location)  
0.2 to 2W...



# Fastening & cooling system

• Choice of **fasteners** : aluminum rails screwed through the medium of inserts. Non magnetic ( $B=4T$  !)

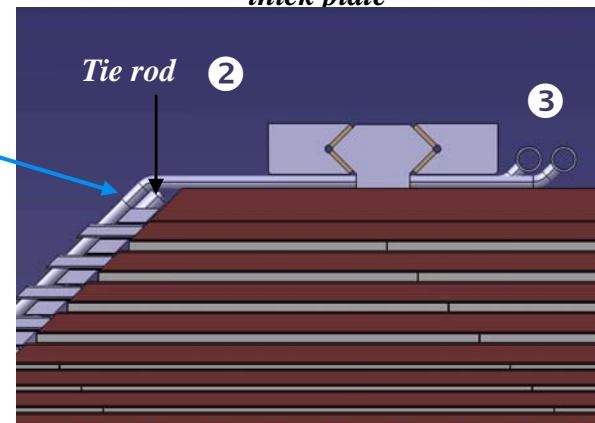
**Design** of connection system : each cooling system **①** is inserted and screwed to each column of slab with a thread rod and spacers **(②)** and connected to the cooling network in a second step **③**.



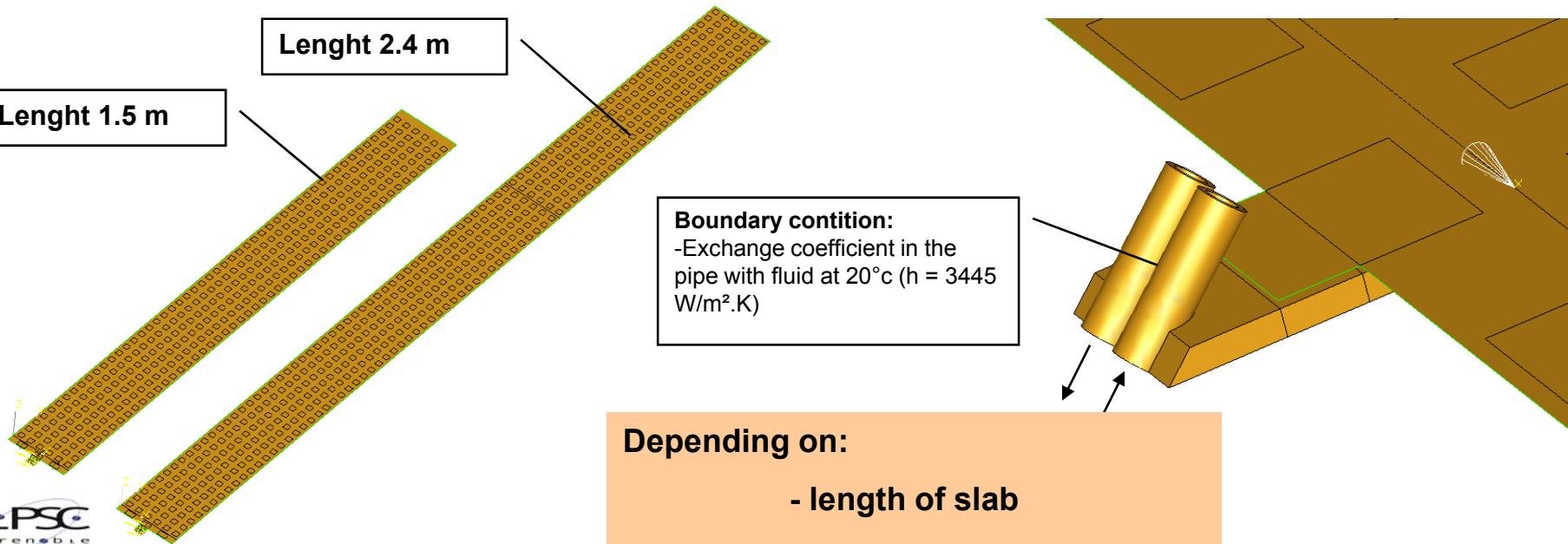
Cold copper bloc inserted between 2 copper plates of each slab



LPC  
Grenoble



# Cooling system: End-cap constraints



LPSC  
Grenoble

load : 1/2 SLAB		
FPGA power (one side of the SLAB)		0,3 W
SKIROC SLAB 1,5 m		0,27 W
SKIROC SLAB 2,4 m		0,42 W

copper thickness : 0.4 mm, FPGA power : 0.3 W

FPGA	SLAB : 1,5 m						SLAB : 2,4 m						Comments
	with			without			with			without			
Temperature (°C)	Tmin	Tmax	Difference	Tmin	Tmax	Difference	Tmin	Tmax	Difference	Tmin	Tmax	Difference	
Exchange coefficient inside pipe and fluid temperature of 20°C	20,2	29,1	8,9	20,1	28,1	7,9	20,3	40,0	19,7	20,2	38,8	18,6	Uniform copper thickness : 0,4 mm

load : 1/2 SLAB		
FPGA power (one side of the SLAB)		3 W

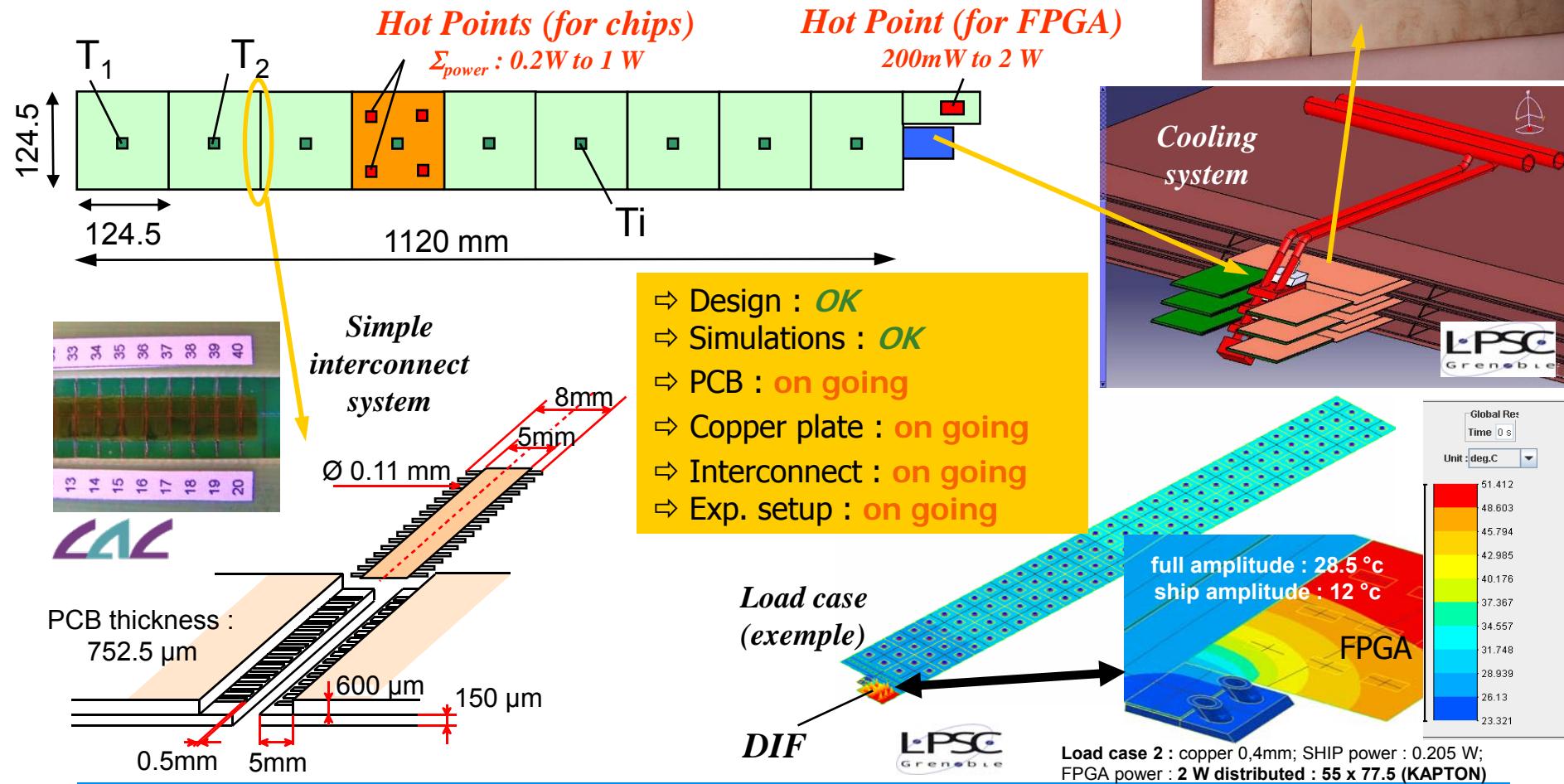
copper thickness : 0.4 mm, FPGA power : 3 W

FPGA	SLAB : 1,5 m						SLAB : 2,4 m						Comments
	with			without			with			without			
Temperature (°C)	Tmin	Tmax	Difference	Tmin	Tmax	Difference	Tmin	Tmax	Difference	Tmin	Tmax	Difference	
Exchange coefficient inside pipe and fluid temperature of 20°C	21,4	42,8	21,4	20,1	28,1	7,9	21,5	50,2	28,7	20,2	38,8	18,6	Uniform copper thickness : 0,4 mm

# Demonstrator – Thermal studies

## Slab cooling tests (1 Hot ASU + 8 thermal ASU):

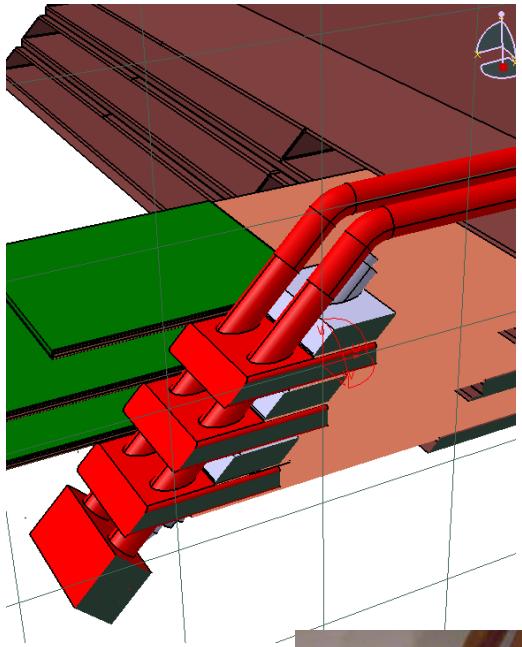
- Correlation with numerical **simulations** (transfer coefficients, contacts ...)
- Check a thermal dissipation behaviour close to **EUDET** design
- Validate **the cooling system** (400  $\mu\text{m}$  copper plate + pipes)



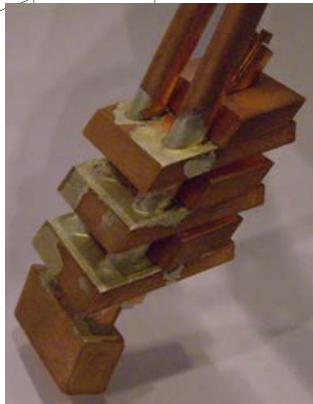
# SLAB COOLING - DEMONSTRATOR

## Cold plate : 3 Solutions

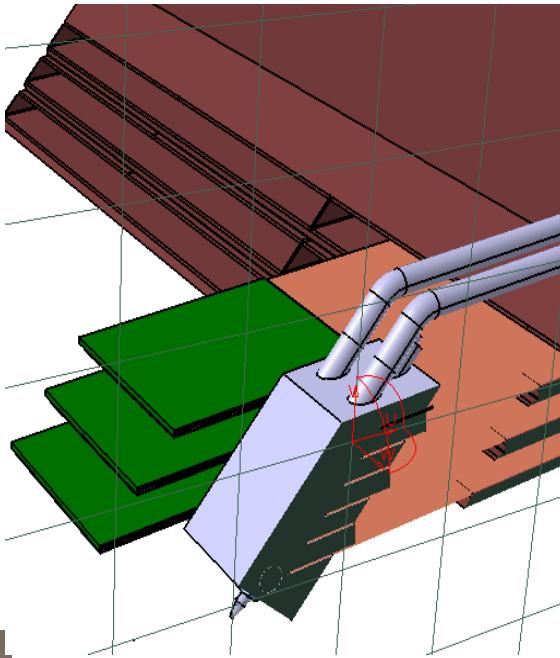
### ① Assembled solution



Water circulating  
into copper pipe  
(Internal  
diameter : 4 mm)

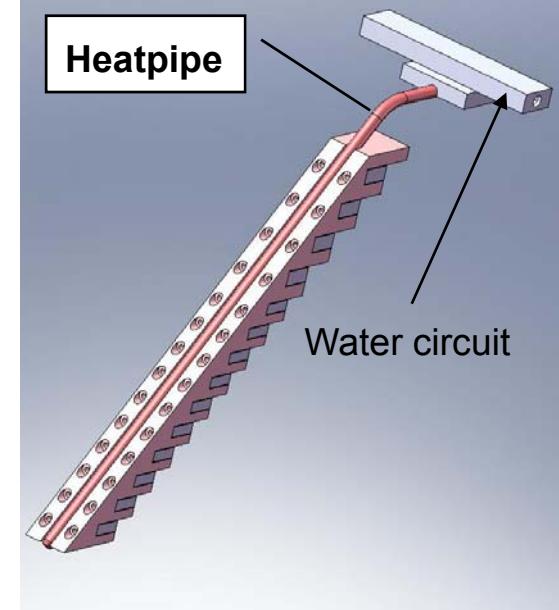


### ② Machining solution



- 1 block with water circulating into copper pipe (Internal diameter : 4 mm)
- Easier to build

### ③ Heatpipe



Heatpipe

Water circuit

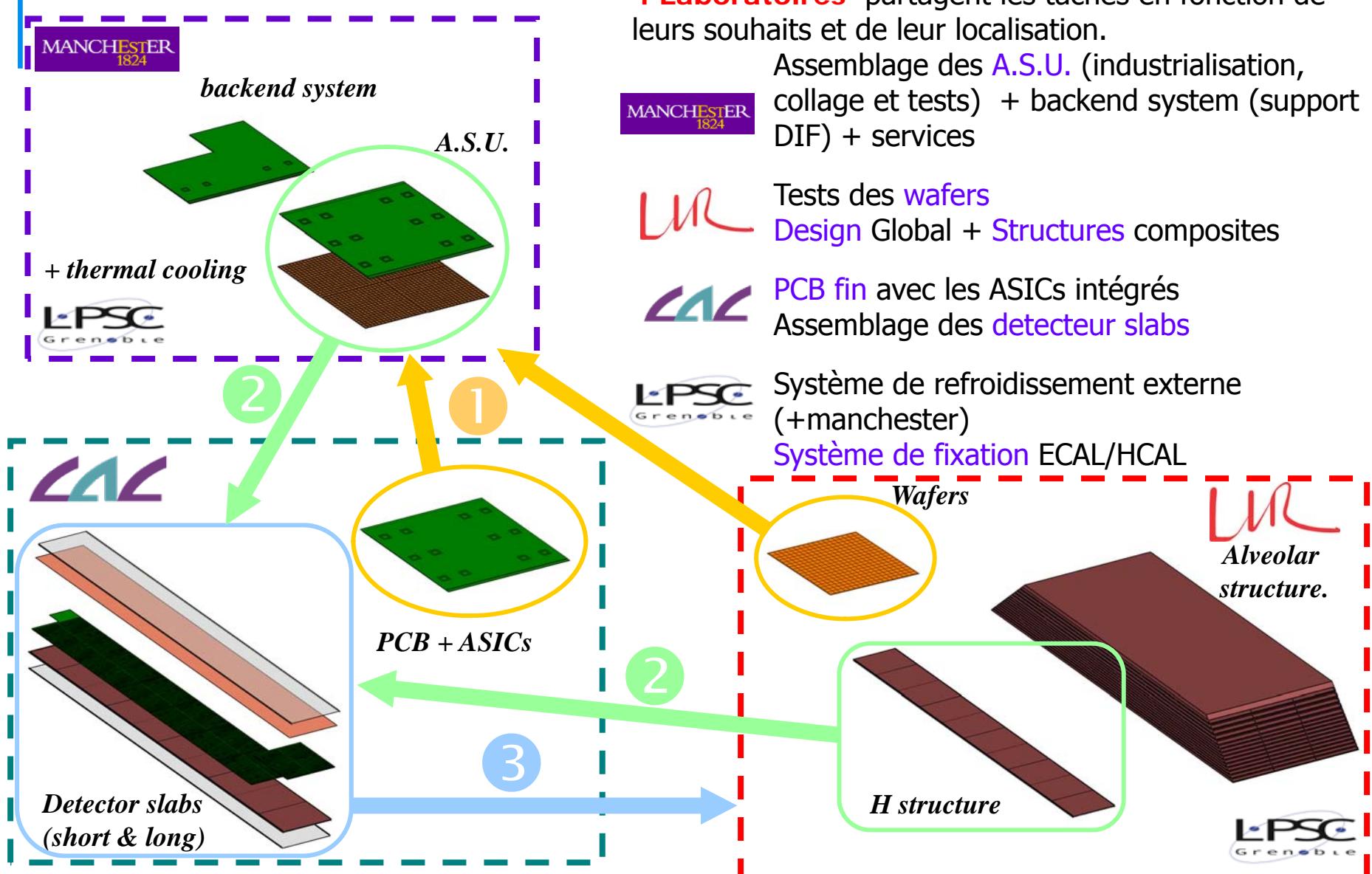
#### Main advantage :

Connection between Heat pipe and water circuit => contact, far from front-end.

Easy to assemble and reduces leak risk

~ Same geometry

# Organisation pour EUDET



# Conclusion : Schedule

## Demonstrator

■ H structure	Aug 08
■ 2/3 "alveolar layer" structures - Reception of the Cooling setup	Nov 08
■ Carbon fibers choice & destructive tests	Dec 08
■ Reception of the Assembly mould	Jan 09
■ Third alveolar layer with sensors embedded (& tests)	Jan 09
■ Slab cooling_tests & the 3 cooling systems	Jan 09
■ Demonstrator (3 layers) assembled - Optimization of cooling simulations	Fev 09

## EUDET

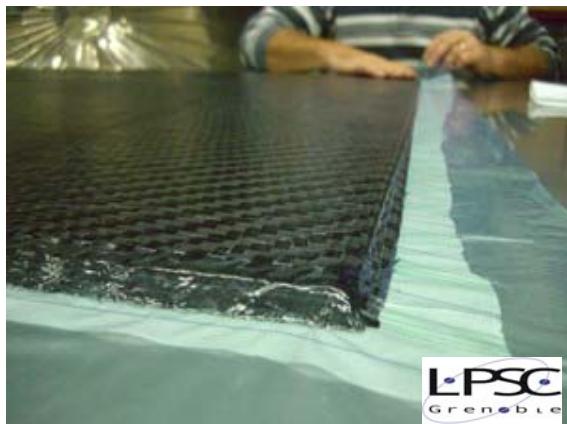
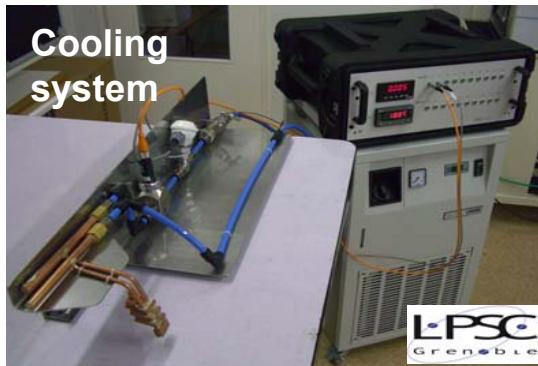
■ "Alveolar layer" mould ordered	Nov 08
■ Cooling system for EUDET & thick composite plates	Dec 08
■ "Assembly mould" design (with thermal curing studies)	Fev 09
■ Alveolar layers & H production	Mar 09
■ Eudet structure assembled	Jun 09

## ILD

*on going*

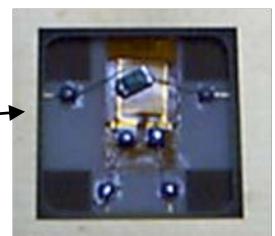
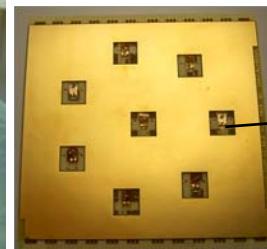
- Barrel + End-cap + ECAL Ring **design** & mechanical simulations
- Moulds for 1 layer of End-cap module n°2 and **optimization of composite elements**
- Design for the **whole** detector **cooling system**
- **Fastening system** ECAL/HCAL: alternative for thick composite plates and rails ...

## ILD - ECAL Mechanical R&D



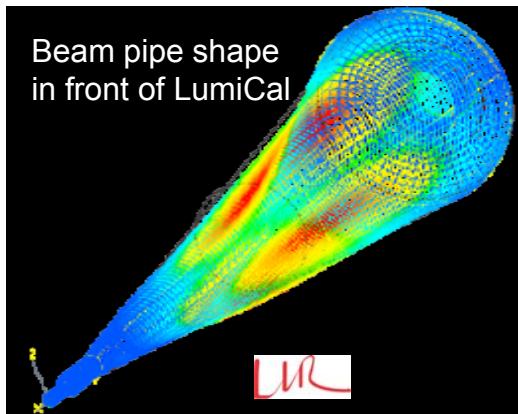
Fabrication and destructive tests of 15mm thick composite plate with inserts

**THERMAL PCB...**



**PCB FEV\_HEATERS**

**15mm thick plate with rails**



400 $\mu$ m thick & 180 mm larg copper heat shield

