

# Fifth IDPASC School

LPNHE - APC

Paris, France

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<https://indico.in2p3.fr/event/10777/>

# CMB detectors

Michel Piat

[piat@apc.univ-paris7.fr](mailto:piat@apc.univ-paris7.fr)

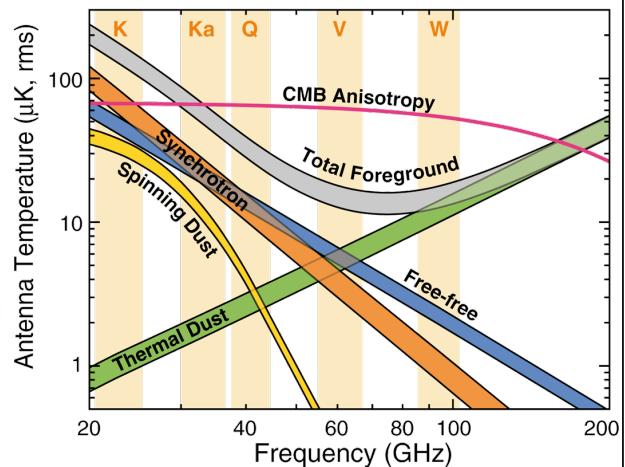


# Outline

1. CMB photons and CMB instruments
2. Bolometers principle
3. System aspects
4. Development of bolometer arrays

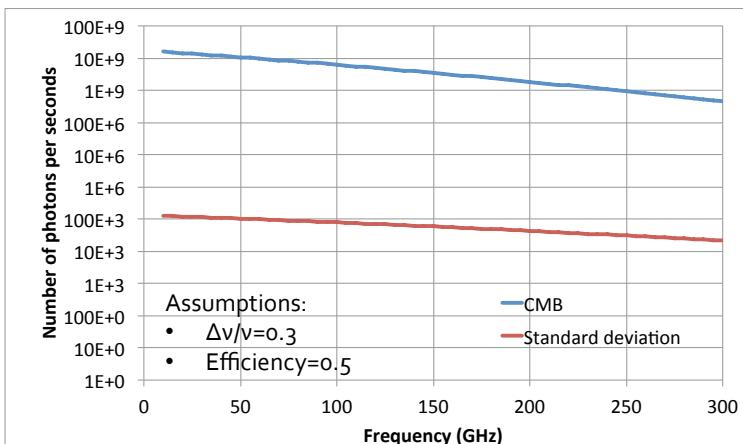
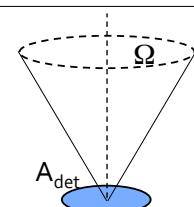
# 1. CMB photons

- $T_{CMB} = 2.725\text{K}$  (COBE)
  - Max emission at  $\nu \sim 150\text{GHz}$ ,  $\lambda \sim 2\text{mm}$
  - Photon energy: fraction of meV
- Monopole dominant between  $\sim 500\text{MHz}$  to  $\sim 800\text{GHz}$
- Anisotropies dominant between  $\sim 40\text{GHz}$  to  $\sim 200\text{GHz}$



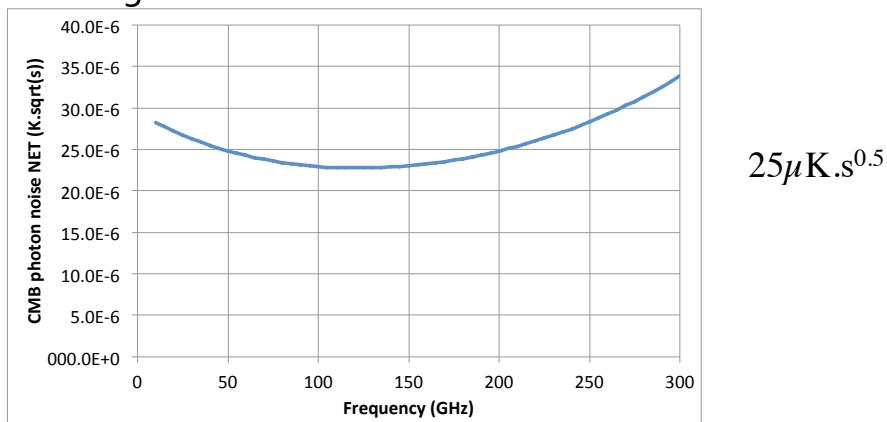
## CMB photon flux

- Photon flux:  $P \approx B_\nu(T_{CMB}) A_{\text{det}} \Omega \Delta\nu$ 
  - Diffraction limited:  $A_{\text{det}} \Omega = \lambda^2$
  - Number of photons per seconds:  $N = P/(h\nu)$
- Photon noise
  - Photon flux  $\approx$  Poisson flux
  - Standard deviation:  $\sigma = \sqrt{N}$



# CMB photon noise

- Noise Equivalent Temperature (NET)
  - Noise expressed as a CMB temperature fluctuation in 1 second of integration time:

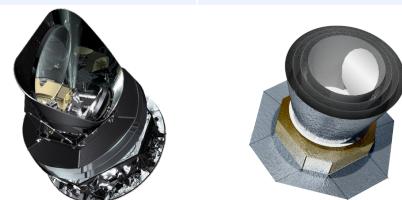


- For N detectors, scale as  $N^{-0.5}$

# CMB instruments

- Assuming perfect detectors, limited by the CMB photon noise:

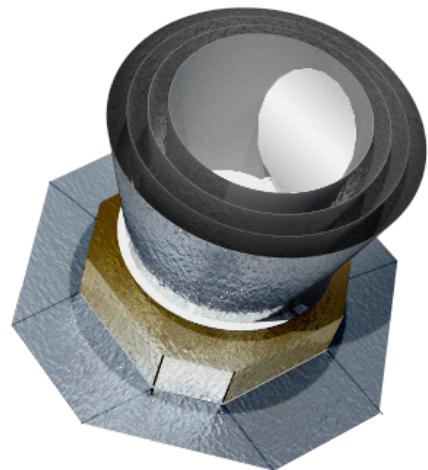
	T anisotropies	B-modes
Required sensitivity	$6\mu\text{K}$	$100\text{nK}$
Angular resolution	5 arcmin	30 arcmin
Integration time per angular resolution for a 1 year mission	5s	190s
Required NET	$13\mu\text{K} \cdot \text{s}^{0.5}$	$1.4\mu\text{K} \cdot \text{s}^{0.5}$
Number of detection chain needed	~4	~320
Missions	Planck	CORe+



# COrE+

## The Cosmic Origins Explorer

- Proposal for ESA's M4 space mission (2026)
- Ultimate mission for CMB polarisation anisotropies
- Concept:
  - 15-20 frequency bands between 60GHz and 600GHz
  - Very high sensitivity ( $6\text{onK}_{\text{CMB}}$  on 30 arcmin)
    - ✓ Cryogenic detectors (100mK)
  - 1.5m telescope
  - L2 orbit

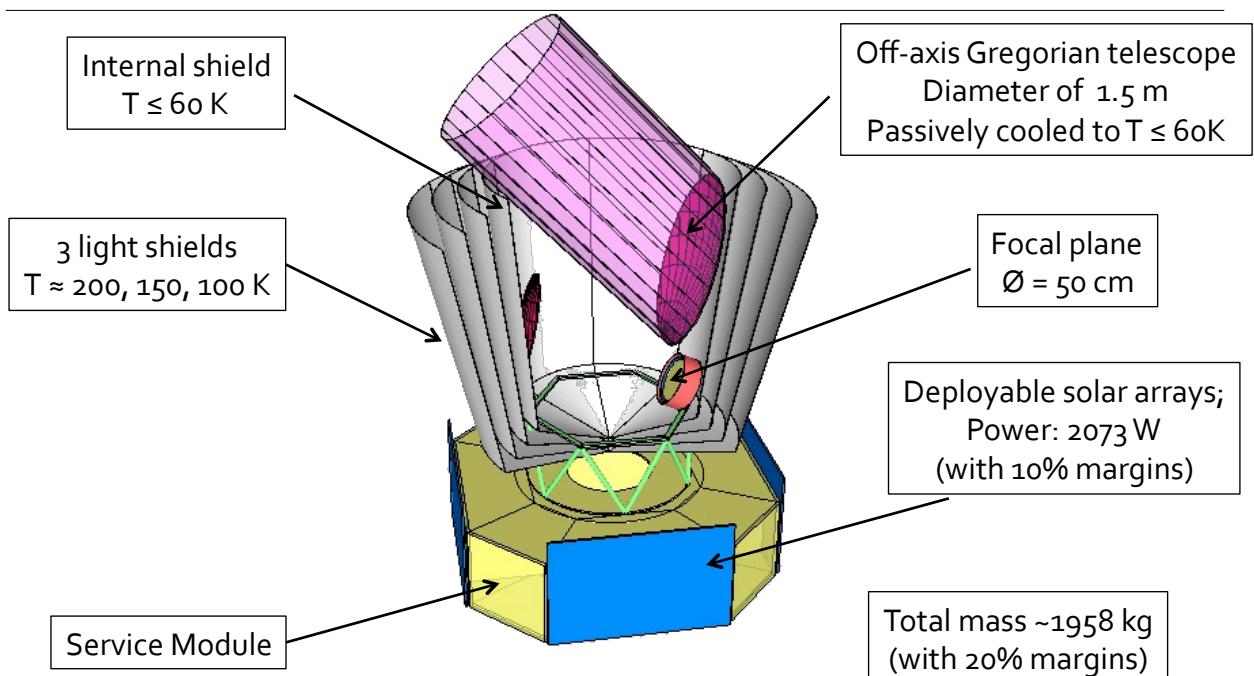


**Proposal leader:**

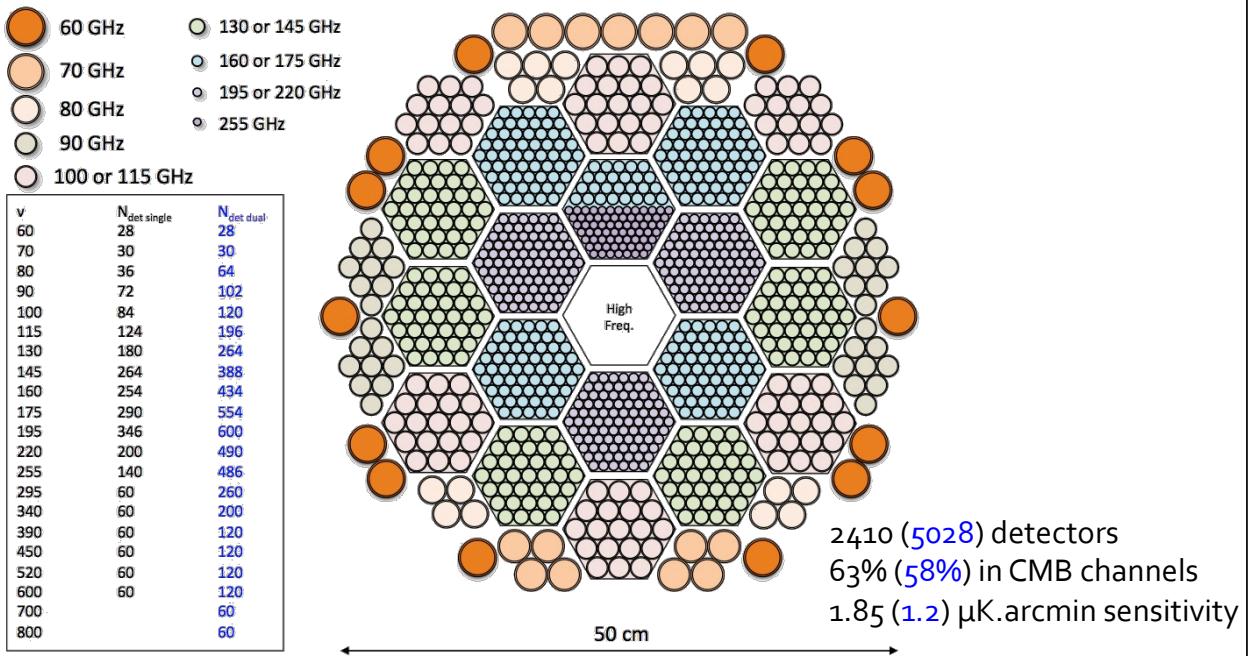
*Paolo de Bernardis;*

**Co-leaders:** *François Bouchet & Jacques Delabrouille*

## COrE+ satellite



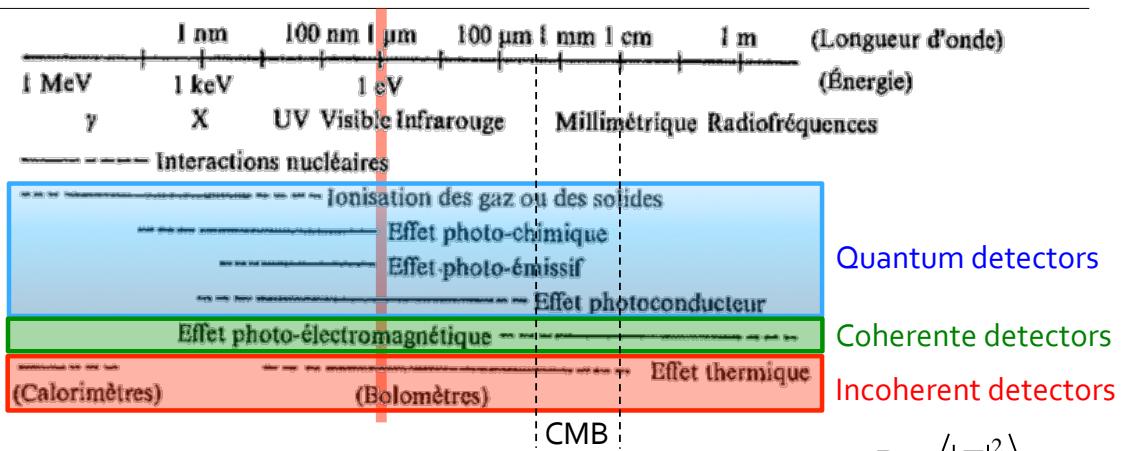
# COrE+ focal plane



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9

## CMB detectors?



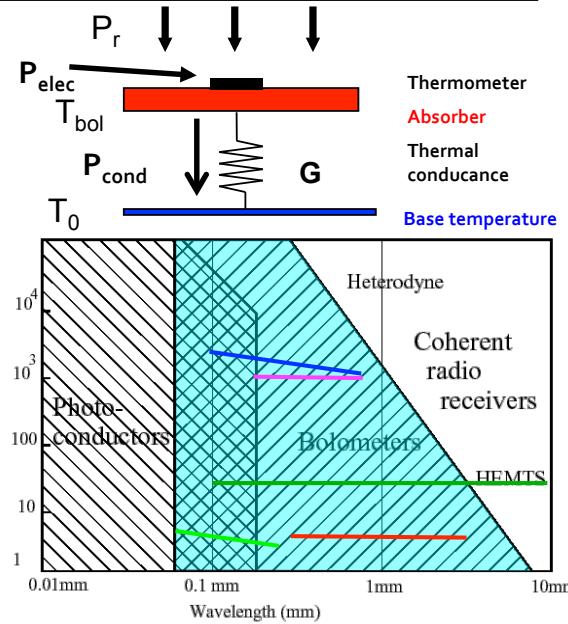
- Incoherent detectors: sensitive to the average EM power  $P \propto \langle |E|^2 \rangle$ 
  - Bolometer, Kinetic Inductance Detectors
- Coherent detectors: sensitive to E field
  - Amplitude and phase
  - Intrinsically limited in sensitivity

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10

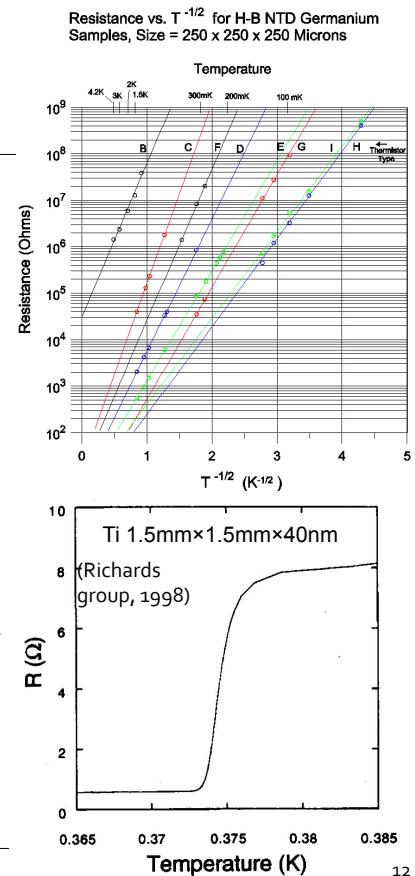
## 2. Bolometer principles

- Thermal detector
  - Macroscopic system
  - Measure of the heating from the absorption of radiation
  - Thermometer = resistor  $R(T)$
  - Readout:  $R=U/I$
- The best detectors for large bandwidth detection in the wavelength range  $100\mu\text{m} \rightarrow 3\text{mm}$ 
  - Cooled to low  $T < 300\text{mK}$
  - Sensitivity limited by photon noise



## Thermometer

- Parameter:  $\alpha = \frac{T}{R} \frac{dR}{dT}$
- Semi-conductor:  $\alpha \# -5 \rightarrow -10$ 
  - Implanted Si
  - Ge NTD (Haller-Beeman)
  - NbSi thin film (CSNSM Orsay)
- Superconductor:  $\alpha \# 100 \rightarrow 1000$  (*Transition Edge Sensor TES*)
  - Ti:  $T_c \approx 400\text{mK}$
  - Mo/Cu, Mo/Au...:  $T_c$  tuning by proximity effect
  - NbSi thin film (CSNSM):  $T_c$  depends on composition Nb (>12%) vs Si



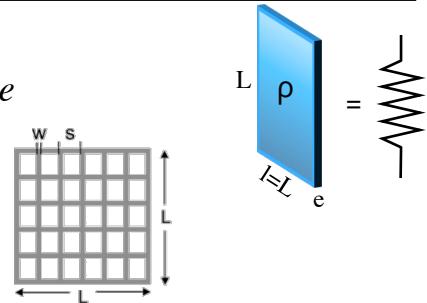
# Absorber

- **Absorber = metal film**

➤ Square resistance of a uniform film:  $R_c = \rho/e$

➤ Metal grid:  $R_c = \rho/e \times s/w$

✓ Equivalent to a uniform film  
if  $\lambda \gg s$  and  $w$

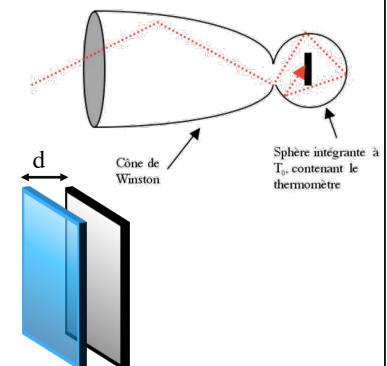


- In vacuum:

➤ Vacuum impedance:  $Z_0 = \sqrt{\mu_0/\epsilon_0} = 377\Omega$

➤ Max absorption = 50% for  $R_c = Z_0/2$

➤ Integrating sphere to increase absorption



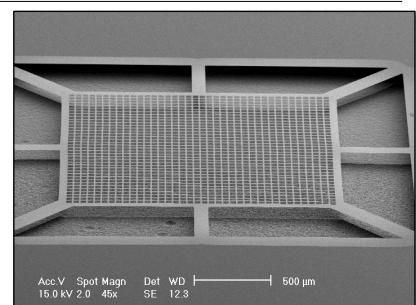
- With a reflective layer at  $d=\lambda/4$  (modulo  $\lambda/2$ )

➤ Max absorption = 100% for  $R_c = Z_0$

# Thermal conductance

- Micro-technologies

➤ Membranes in silicon nitride (SiN) or in silicon (Si)



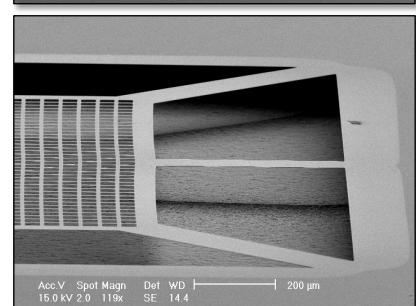
- Thermal conduction in Si or SiN

➤ Diffusive phonons transport

➤ At very low temperature: diffusion on edges

✓ Mean free path > sample size

✓ Radiative transport



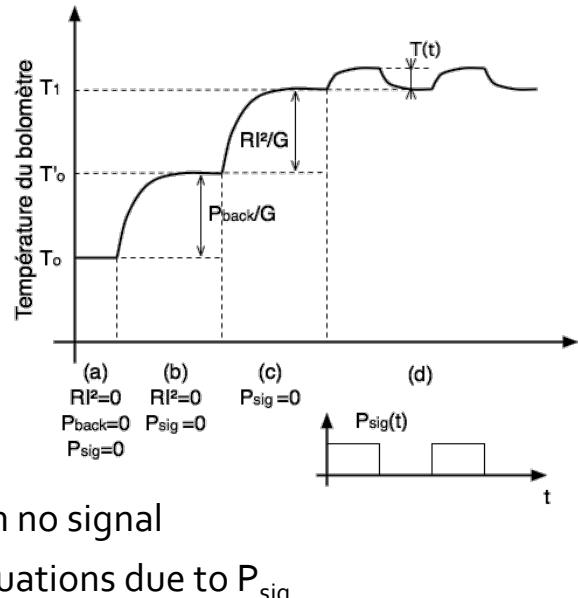
- Classical modelisation :

$$(diffusive) \quad P = K(T_1^{\beta+1} - T_0^{\beta+1}) \quad \text{with } \Delta T = T_1 - T_0$$

$$G_d = \left( \frac{dP}{dT_1} \right)_{T_0=cste} = (\beta+1)K T_1^\beta$$

# Bolometer in operation

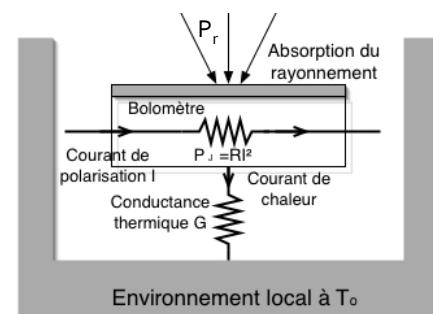
- $P_r = P_{\text{back}} + P_{\text{sig}}(t)$   
with  $P_{\text{sig}}/P_{\text{back}} \ll 1$ 
  - $P_{\text{back}}$ : average power, *background power*
  - $P_{\text{sig}}$ : radiative power to be measured
- $T_{\text{bol}} = T_1 + T(t)$  avec  $T/T_1 \ll 1$ 
  - $T_1$ : bolometer temperature with no signal
  - $T$ : bolometer temperature fluctuations due to  $P_{\text{sig}}$



## Bolometer response in harmonic regime

- In temperature:

$$\begin{cases} \frac{\tilde{T}}{\tilde{P}_{\text{sig}}} = \frac{1}{G_{\text{eff}}(1 + j\omega\tau_{\text{eff}})} \\ \tau_{\text{eff}} = \frac{C}{G_{\text{eff}}} \end{cases}$$



C: bolometer heat capacity [J/K]  
 $G_{\text{eff}}$ : bolometer effective thermal conductance [W/K]

- 1. Trade-off between time constant and response  
 2. Low C require  $\Rightarrow$  low temperatures

# Electro Thermal Feedback (ETF)

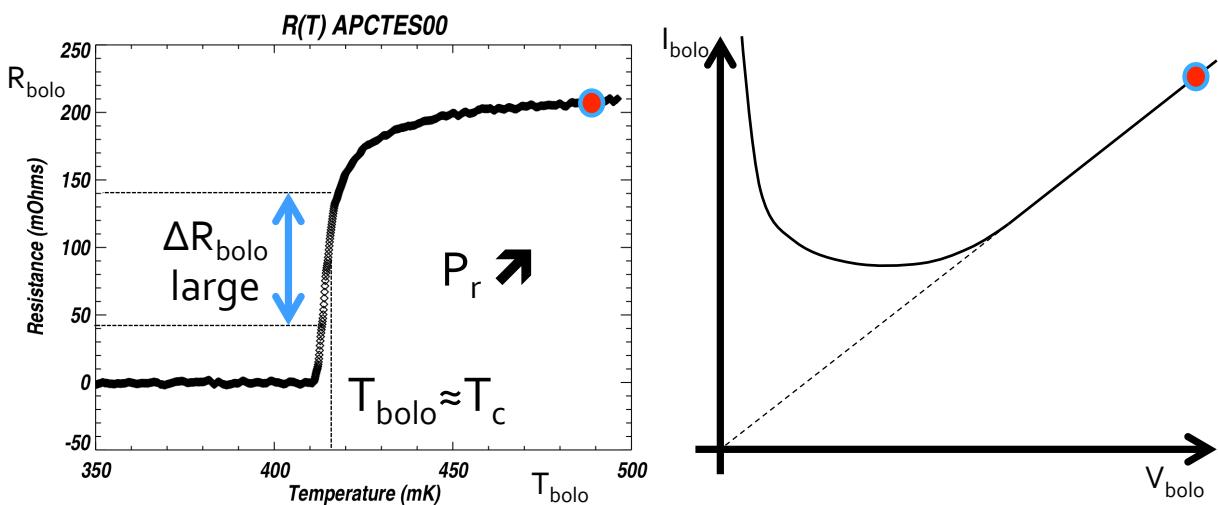
- Case  $\alpha < 0$ : semi-conducting bolometer
  - Current biasing:  $T \uparrow \Rightarrow R \downarrow \Rightarrow P_{elec} = RI_{bias}^2 \downarrow \Rightarrow T \downarrow$
- Case  $\alpha > 0$ : superconducting bolometer
  - Voltage biasing:  $T \uparrow \Rightarrow R \uparrow \Rightarrow P_{elec} = V_{bias}^2/R \uparrow \Rightarrow T \uparrow$
- Feedback system:
 

$P_r \rightarrow$  +  $\rightarrow$  Thermal circuit  $\rightarrow T_{bol}$

$P_{elec}$   $\uparrow$   $\rightarrow$  Thermistor  $\rightarrow$  Thermal circuit
- Interesting effect if  $|\alpha|$  is large: **superconducting bolometers**

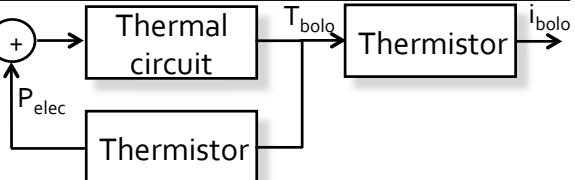
## ETF in TES

- In quasi-static:  $P_r + P_{elec} = P_{cond}$



# ETF effect on TES

- Feedback system:
  - 1<sup>st</sup> order thermal circuit:  $\tau = C/G$



- Bolometer response:

$$S_I(\omega) = -\frac{1}{V} \cdot \frac{L}{1+L} \cdot \frac{1}{1+i \cdot \omega \tau_{eff}}$$

$$\text{Time constant: } \tau_{eff} = \frac{\tau}{1+L}$$

$$\text{Open loop gain: } L = \frac{|\alpha| \cdot P_{elec}}{T_1 G_d} \text{ with } \alpha = \frac{T}{R} \frac{dR}{dT}$$

- If  $L \gg 1$ : (strong ETF)

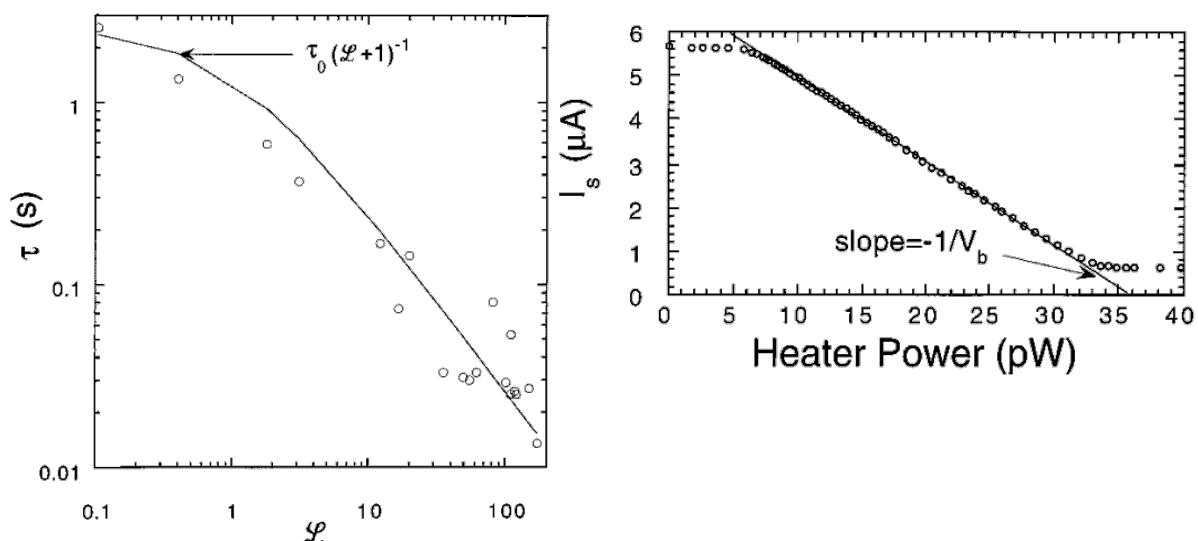
Superconducting bolometers

$\alpha=100-1000$

$L=10-100$

## Strong ETF in TESs

- A. Lee, P. Richards et al. 1998



# Noise Equivalent Power (NEP)

- Power Spectral Density (PSD) of a noise
  - Characterise its spectral content
- Noise expressed in photon flux input power (W):
 
$$\text{NEP} = \sqrt{\text{PSD}}$$
 [W.Hz<sup>-0.5</sup>]
- White noise: PSD = constant
  - NEP = standard deviation of the noise, expressed in photon flux input power, for 1Hz of bandwidth (or ½ second of integration time)
$$\sigma = \frac{\text{NEP}}{\sqrt{2 \times t_{obs}}}$$
- Noises are generally Gaussian (central limit theorem)

## TES intrinsic noise sources

- Johnson noise:
  - Electrical resistor R at temperature T
 
$$\text{PSD}_J = \frac{4kT}{R} \quad [\text{A}^2.\text{Hz}^{-1}]$$
- Phonon noise:
  - Conductance G<sub>d</sub> at uniform temperature T
 
$$\text{NEP}_{Ph}^2 = 4kT^2G_d \quad [\text{W}^2\text{Hz}^{-1}]$$
  - Bolometer: not at thermal equilibrium
    - ✓ Overestimation of NEP<sub>ph</sub> by about 30% [Mather]
- Bolometer total intrinsic noise:
 
$$\text{NEP}_{bol}^2 = \text{NEP}_J^2 + \text{NEP}_{Ph}^2$$

# TES optimisation

- Requirements:

- No saturation:  $P_{cond} = [3 - 6] \times P_{back}$

- Strong ETF:  $L = \frac{|\alpha| \cdot P_{elec}}{T_1 G_d} \gg 1$  (Reminder:  $P_{elec} = P_{cond} - P_{back}$ )  
✓ Phonon noise dominant

- Reasonable bolometer temperature:  $T_1 - T_0 = [0.3 - 1] \times T_0$

- In this case:

- With reasonable assumptions :  $G_d = \frac{dP_{cond}}{dT} \approx [3 - 20] \frac{P_{back}}{T_0}$

- NEP:

$$NEP_{bol}^2 \approx [3 - 20] \times 4kT_0 P_{back}$$

## Bolometer limited by photon noise (BLIP)

- NEP of photons noise:

- With a radiative input power  $P_{back}$  in  $\nu \pm \Delta\nu/2$ :

$$NEP_{hv}^2 \approx 2h\nu P_{back}$$

- Background limited performances (BLIP):

$$NEP_{bol}^2 \leq NEP_{hv}^2$$

- With an optimised bolometer:

$$T_0 \leq 350mK \times \frac{1mm}{\lambda}$$

**Very low T needed**

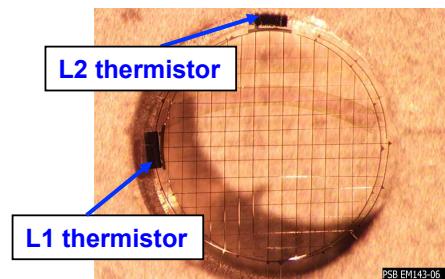
# Planck bolometers

## Spider web bolometers (Caltech-JPL)

- Absorber:  $\text{Si}_3\text{N}_4$ 
  - $e \sim 1\mu\text{m}$ ,  $l \sim 5\mu\text{m}$ , cell  $\sim 100\mu\text{m}$
  - Metallization Au
- Ge NTD thermometer
- Polarisation Sensitive Bolometer (PSB)
  - 2 bolometers in 1 module
  - Metallization in one direction

**Detectors of**

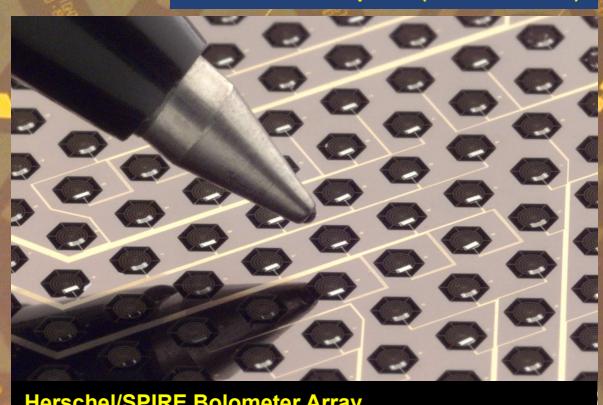
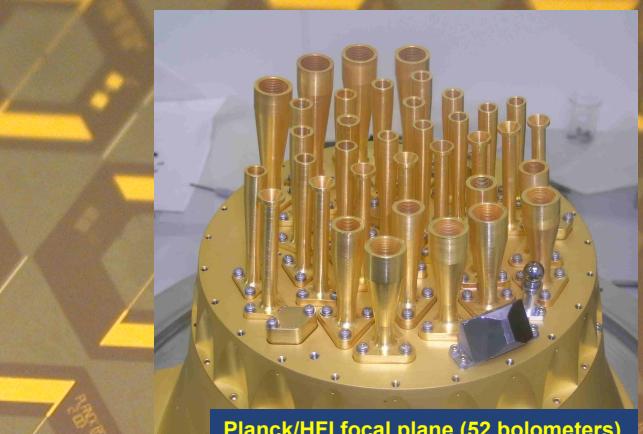
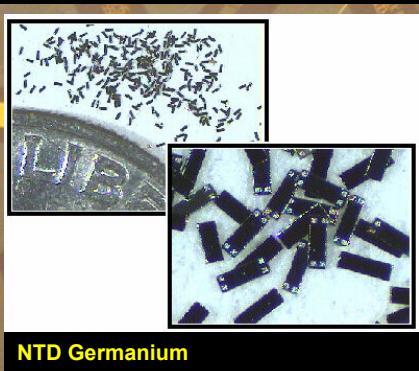
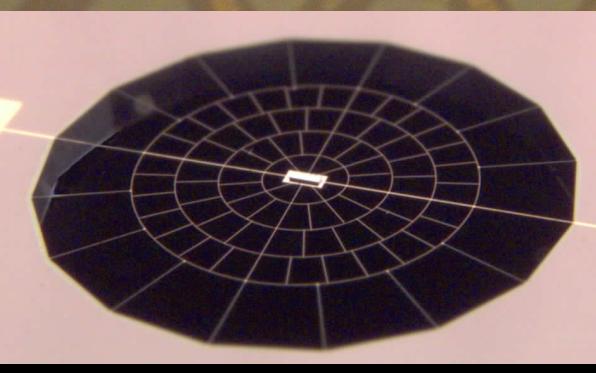
  - Boomerang
  - QUAD
  - BICEP1
  - Planck-HFI



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25

### NTD Bolometers for Planck & Herschel

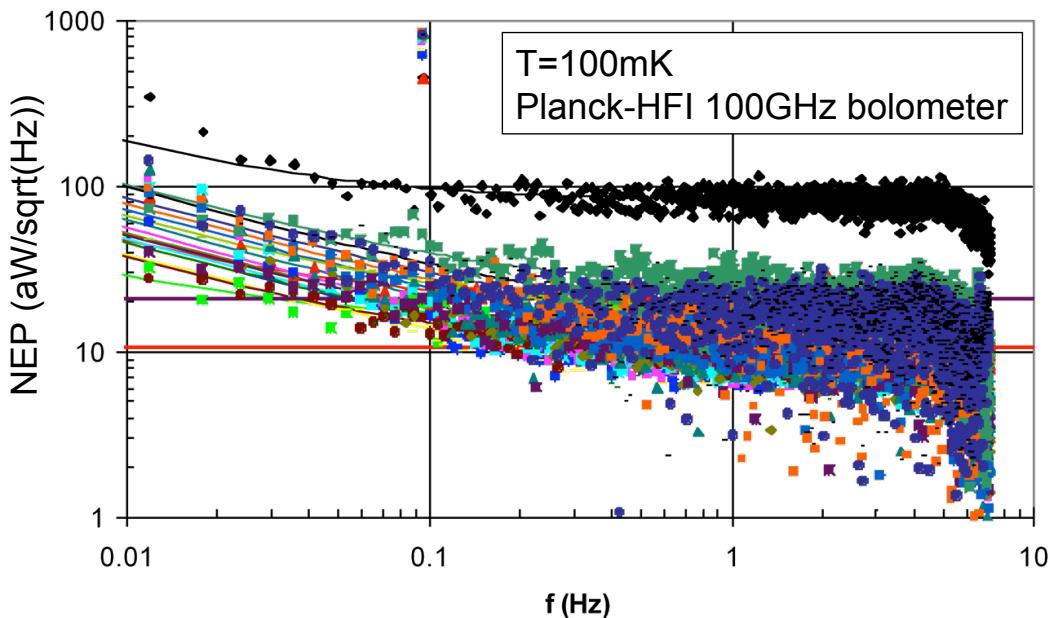


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(From J. Bock, JPL)

# Planck bolometers NEP

PSB100-34J45

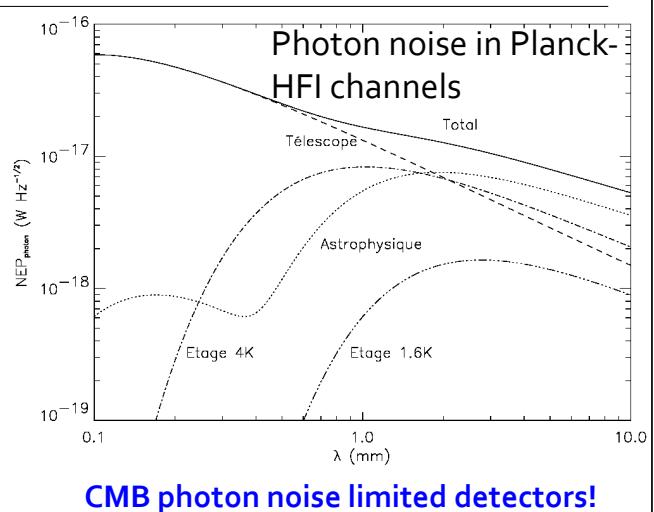


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27

## Spider web bolometer performances

- at 300mK
  - $\text{NEP} = 1,5 \cdot 10^{-17} \text{ W}/\text{Hz}^{1/2}$
  - $\tau = 11 \text{ ms}$
  - $C = 1 \text{ pJ/K}$
- at 100mK:
  - $\text{NEP} = 1,5 \cdot 10^{-18} \text{ W}/\text{Hz}^{1/2}$
  - $\tau = 1,5 \text{ ms}$
  - $C = 0,4 \text{ pJ/K}$



Sensitivity improvement  $\Rightarrow$  increase of bolometer number

**Bolometers array**

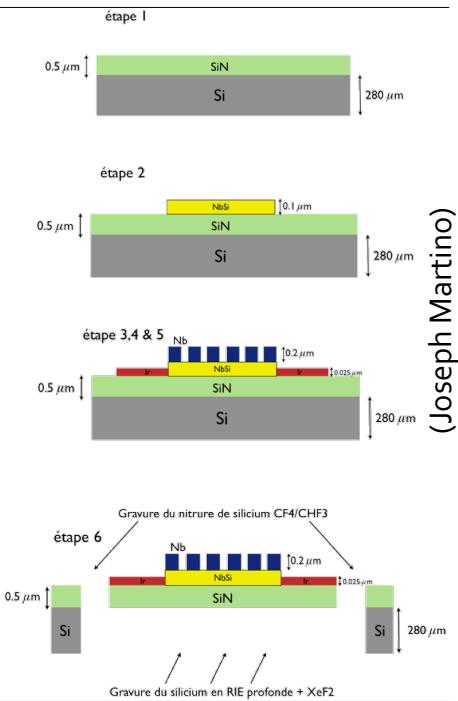
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28

# Bolometer production

- Based on microtechnologies
- Absorber: photolithography
- Metallisation
- Thermal sensor:
  - Planck bolo: NTD Ge by hand
  - Deposited during the process

**Micro fabrication facility required**



## 3. System aspects

- Bolometer sensitivity  $\sim 10^{-17}\text{W}$  to  $10^{-18}\text{W}$
- Instrumental design
  - Risk of sensitivity degradation
- The whole system has to be designed carefully!
  - System approach
  - Bolometer to be tested with their subsystems

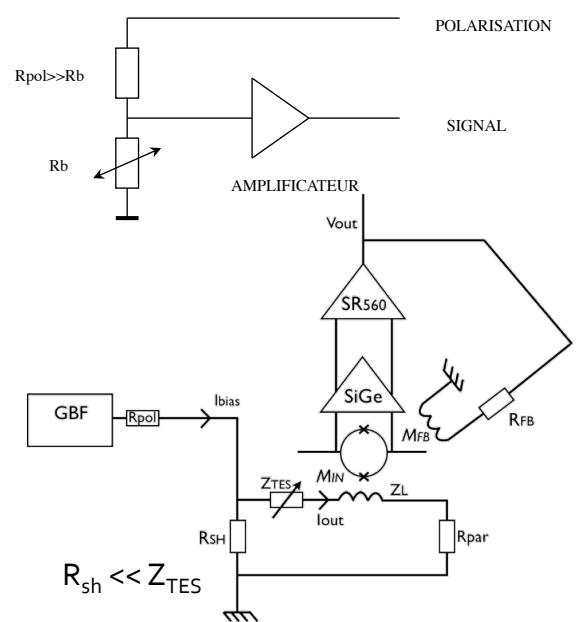


# Extra noise sources

- Readout electronics noise
- $1/f$  noise
- Straylight
- Temperature fluctuations
- Microphonics
- Cross-talk
- Electro-magnetic interferences
- Cosmic rays effects
- ...

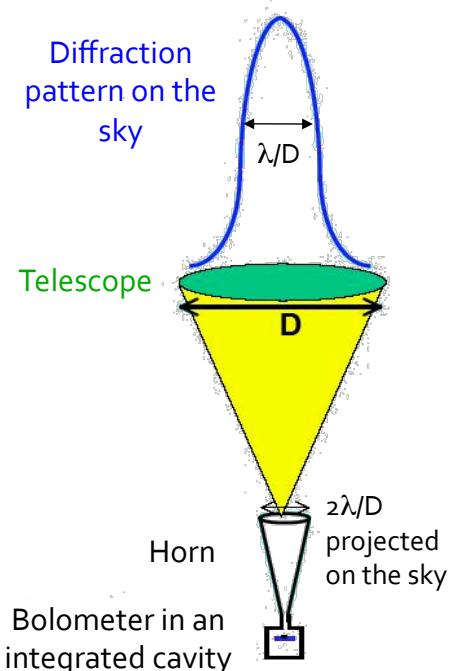
# Readout electronics

- Semi-conducting bolometers:
  - $R_b \# M\Omega$
  - Impedance matching : JFET at  $\sim 120K$  as a follower
- Superconducting bolometers:
  - $R_b \# 100m\Omega$
  - SQUID: *Superconducting QUantum Interference Device*
    - ✓ Current readout
    - ✓ Multiplexing possible



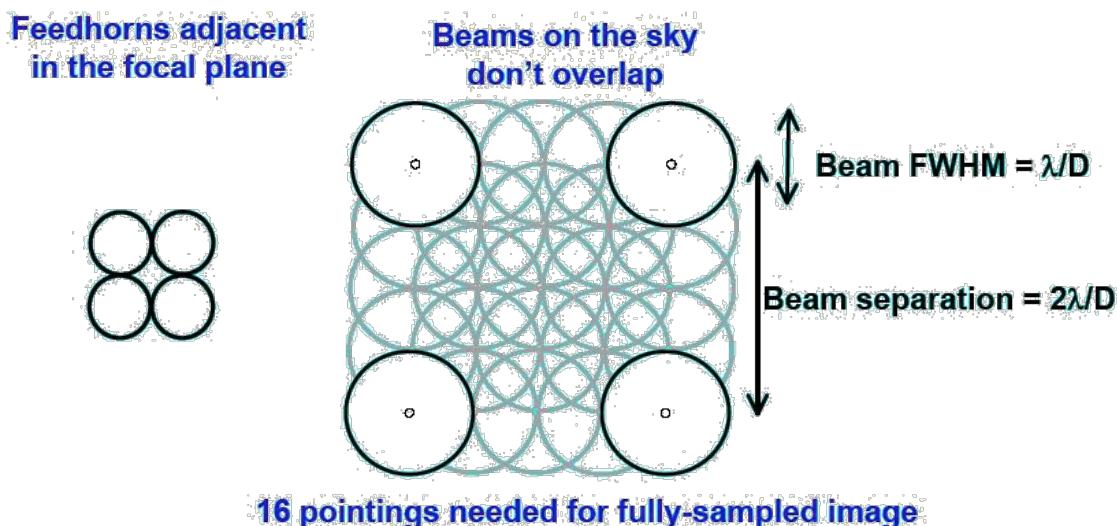
# Bolometer optical coupling: horns

- Define the beam pattern
- Singlemode ( $A\Omega = \lambda^2$ ) or multimode ( $A\Omega = N_{\text{modes}} \times \lambda^2$ )
- Singlemode:
  - Quasi-gaussian beam pattern
  - Maximum efficiency for a horn diameter of  $2\lambda/D$  (on the sky)
  - Beam pattern given by diffraction limit  $\lambda/D$

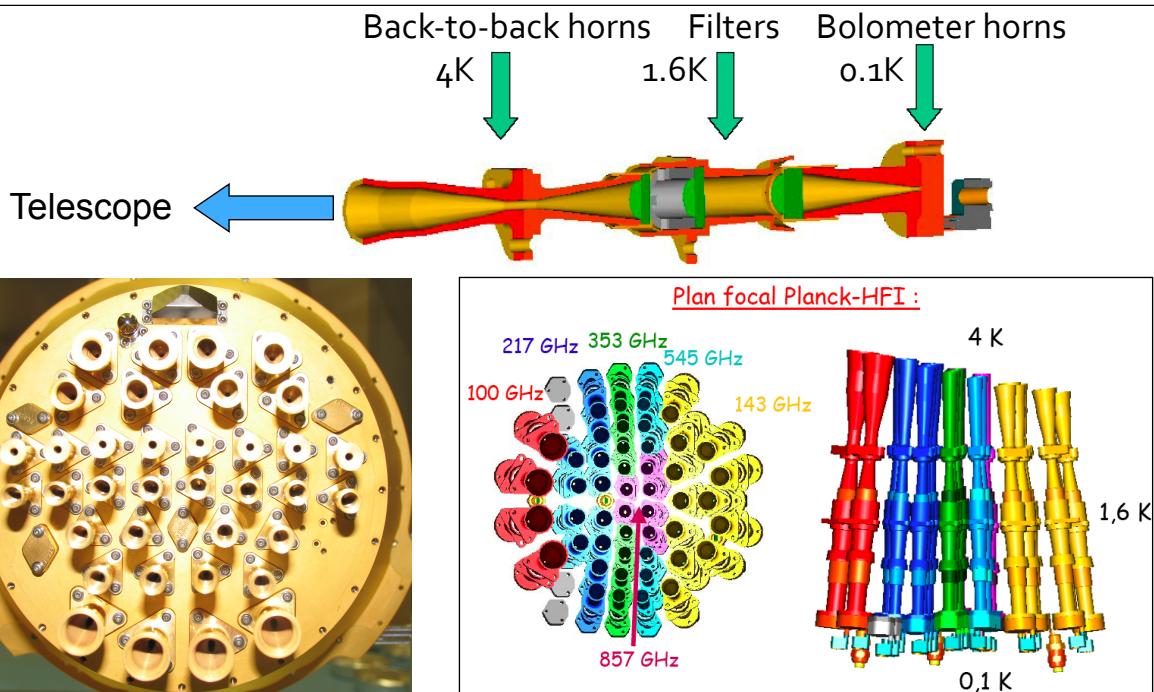


## Mapping with horns

- Beam patterns do not overlap in the sky
- Requires pointing change to sample the sky (Nyquist criteria)



# Example: Planck-HFI

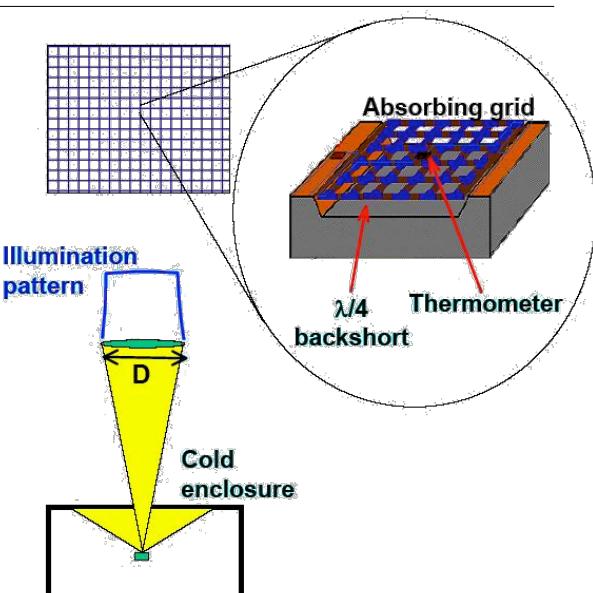


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35

## Bolometer optical coupling: filled array

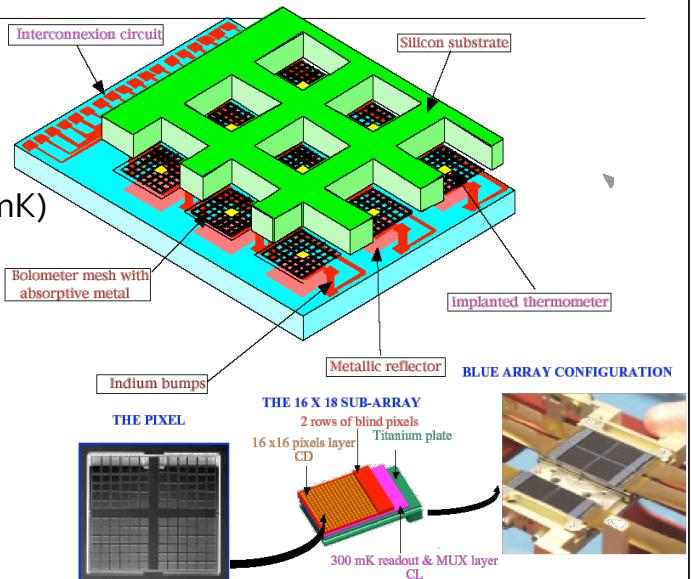
- CCD-like
- Pixel size on the sky=  $0.5 \times \lambda / D$ 
  - Correct sampling of the sky
- The bolometer sees about  $\pi$  sr!
  - Requires a cold enclosure
  - Background power: has to be estimated from all sources in the bolometer solid angle



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# Example: CEA/LETI bolometers for Herschel/PACS

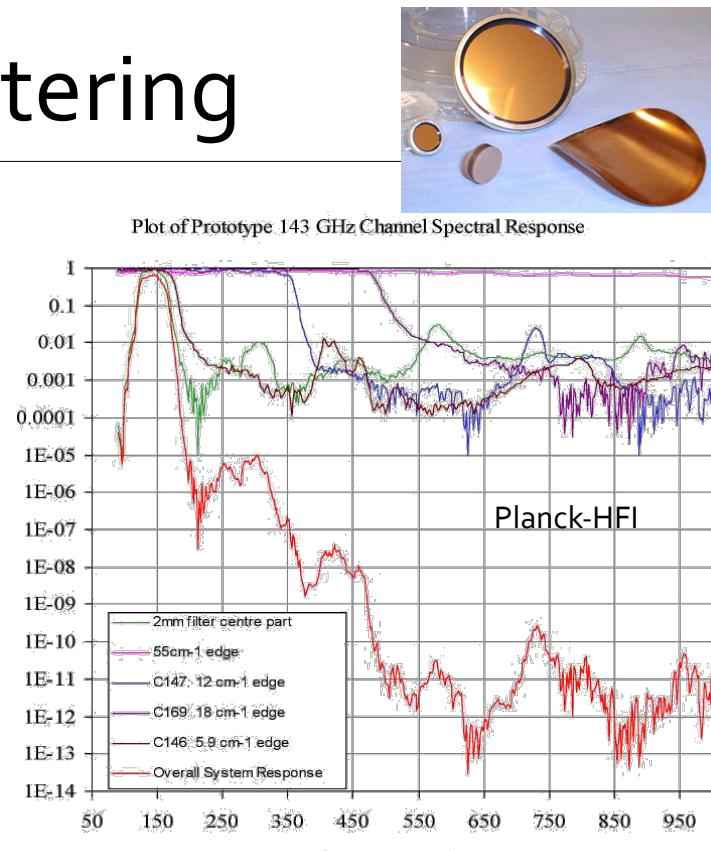
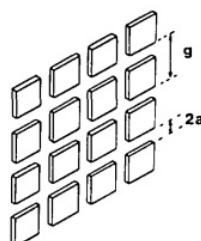
- 2 Si wafers
  - Bolometers and readout
  - Connected by indium bumps
- Thermometer: implanted Si (300mK)
- Photon absorption
  - Metallisation
  - $\lambda/4$  cavity
- Impedance matching in CMOS technology on the second wafer
  - Operate at 300mK
  - Very close to the detector
  - TDM with 8 detectors
  - High readout voltage noise ➔ thermometer  $R \sim 10G\Omega$



Herschel/PACS array:  
 $32 \times 64 = 2048$  detectors at 300mK  
 Channels: 100 $\mu$ m and 170 $\mu$ m,  $NEP < 10^{-16} W.Hz^{-0.5}$

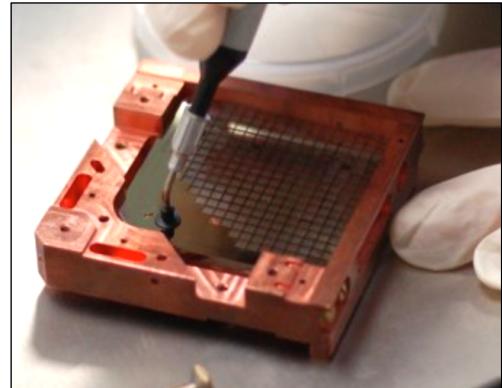
# Filtering

- High IR rejection needed
  - Cold optics, telescope
- Use of capacitive grid filters:
  - Low pass
- Waveguide cut-off
  - High pass



# 4. Development of bolometer arrays

- Motivations:
  - Increase of the mapping speed
  - Increase of the sensitivity
- Requirements:
  - Sensitivity (limited by photon noise)
  - Time constant
  - Array size (from  $10^2$  to  $10^4$  pixels)
  - Filling factor
  - Optical coupling
- Constraints
  - Cryogenics: limited cooling power, multiplexing required
  - Readout electronics: close to the detectors

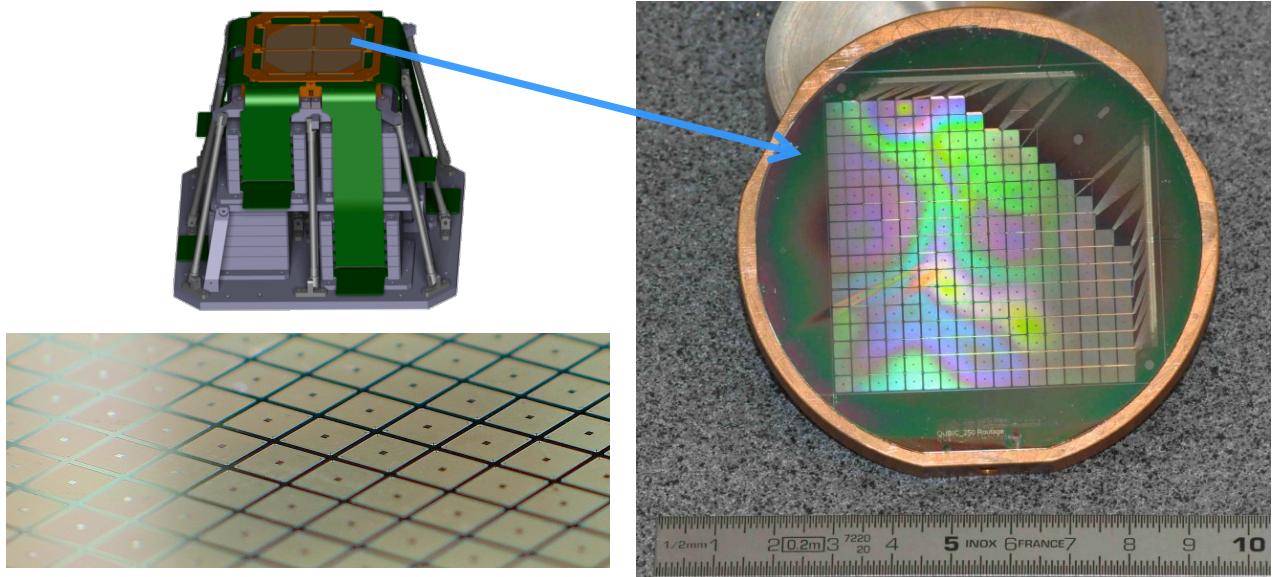


## Multiplexing?

- Readout of N detectors with a single amplifier
- Time Domain Multiplexing (TDM)
  - Successive readout of each detector
  - Required an amplifier noise level lower by a factor  $\sim N^{0.5}$
- Frequency Domain Multiplexing (FDM)
  - Readout of all detector at all time
  - Each detector is modulated at a given frequency
  - Multiple lock-in detection to recover the signal
  - Require an amplifier dynamic higher by a factor  $\sim N^{0.5}$

# Example: 248 TES QUBIC (France)

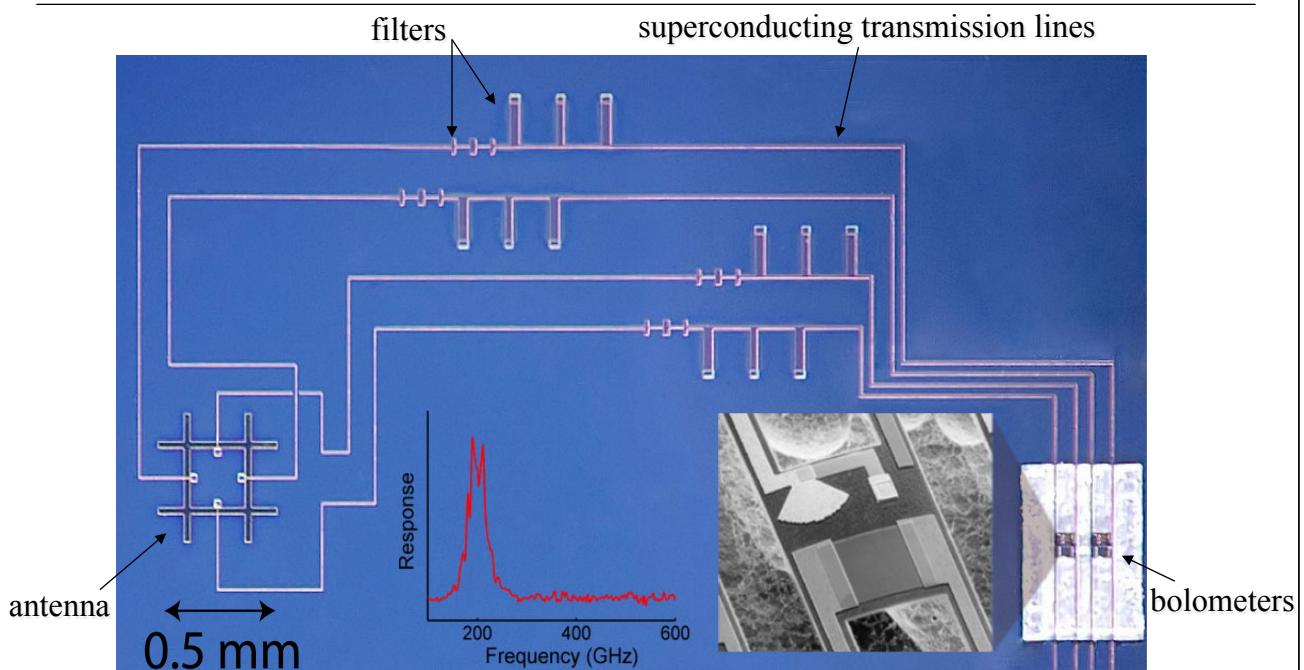
- Superconducting NbSi (CSNSM, IEF, APC)



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41

## Antenna coupled bolometers (Polarbear, UCB/LBNL)

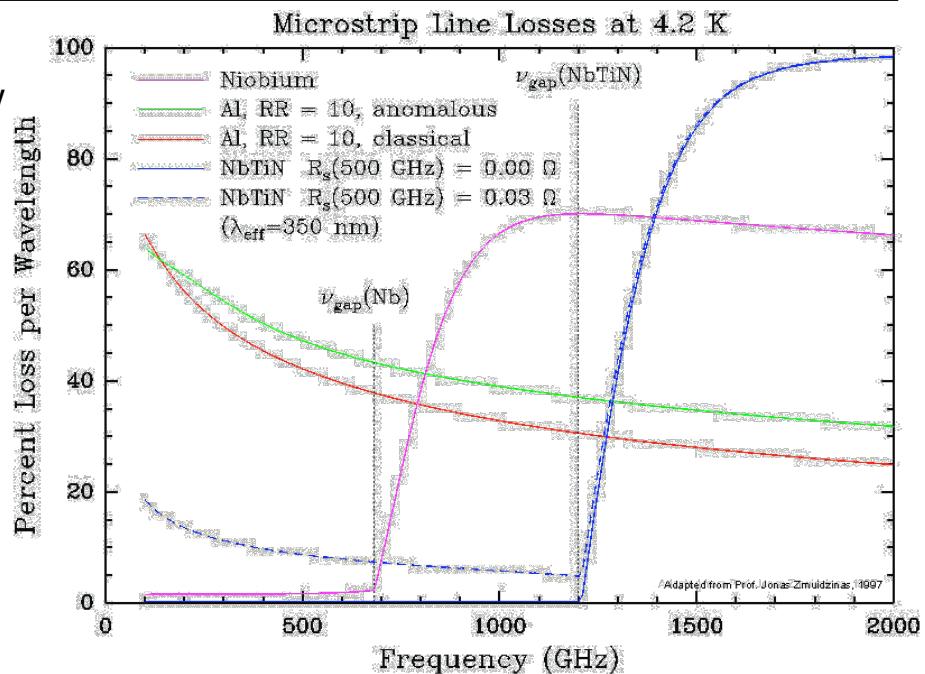


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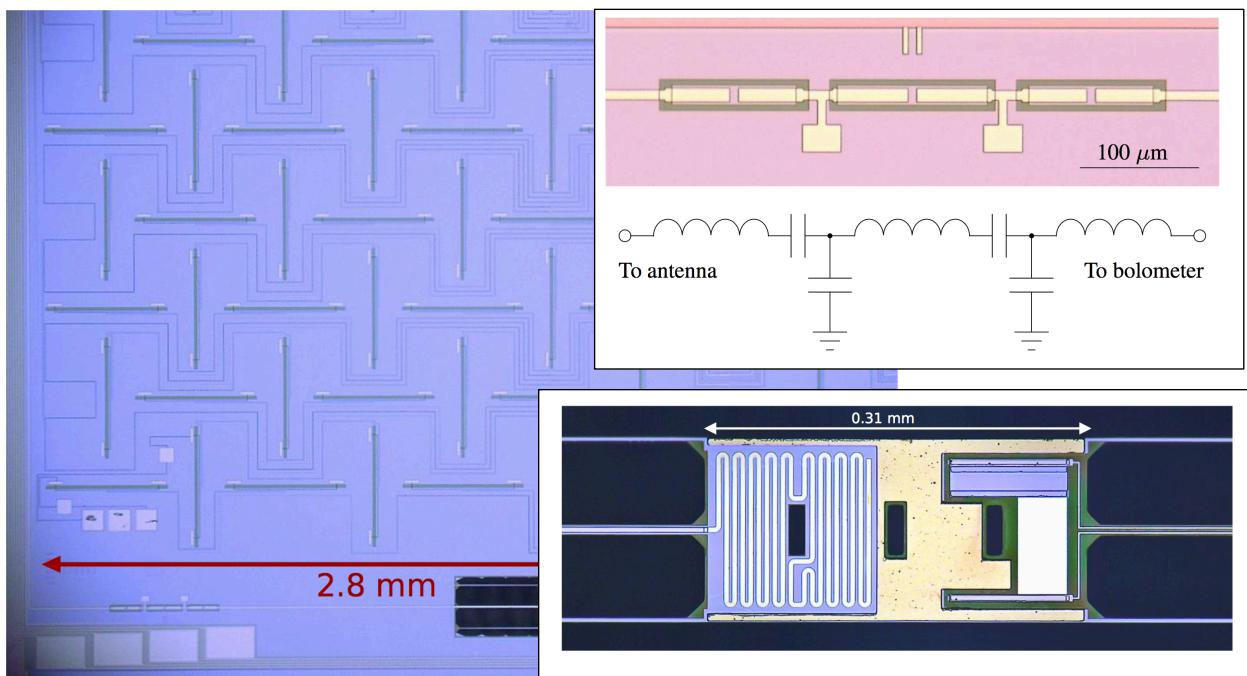
42

# Superconducting microstrip line

- Supercond.  
Niobium: low  
losses up to  
700GHz
- Nb:  $T_c = 9.2\text{ K}$

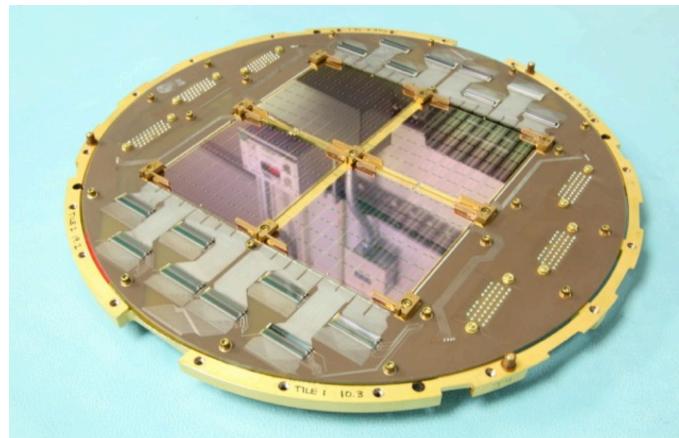


# BICEP2 detectors



# BICEP2 detectors

- 1 pixel:
  - 2 orthogonal  
12x12 slot  
antenna phased  
array
  - Bandpass filter  
on stripline
  - 2 small TESs (Ti and Al)
- 8x8 pixels per tiles, 4 tiles
- Total of 256 pixels and 512 TESs
  - Time Domain Multiplexing
  - MUX factor = 33



# Conclusions

- Requirements for next generation CMB space mission:
  - Thousands detectors
  - NEP #  $10^{-17}$  à  $10^{-18} \text{W.Hz}^{-0.5}$  per pixel
  - $\tau$  # ms
- Complex technology
  - Heavy cryogenics
  - Importance of system aspects
  - Solid state physics, thermal physics, micro-technology, low noise electronics, cryogenics...
- TESs are a mature technology for a space mission

